



BASS, NIXON & KENNEDY, INC., CONSULTING ENGINEERS
6310 CHAPEL HILL ROAD, SUITE 250, RALEIGH, NC 27607
919/851-4422 ■ FAX 919/851-8968 BNK@BNKinc.com

STORMWATER CALCULATIONS

**COBBLESTONE VILLAGE
SOUTH MAIN STREET
ROLESVILLE, NORTH CAROLINA
TOWN OF ROLESVILLE PROJECT # 19157**



**PREPARED BY
BASS, NIXON & KENNEDY, INC.
FEBRUARY 2021**

COBBLESTONE VILLAGE
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**Cobblestone Village
Rolesville, North Carolina
Stormwater Control Calculations
February, 2021**

The site for the Cobblestone Village project is located on the west side of Main Street (US 401) at the intersection of East Young Street (SR 1945) in Rolesville, North Carolina. The current property consists of 10 individual properties that will be recombined into one lot. The new lot will be 10.96 acres to be used for Residential, Mixed Use development. The existing properties have some old buildings with gravel drives. The property is mostly undeveloped. The site drains to the northwest and eventually to Sanford Creek, then the Neuse River.

Stormwater management is required for this site. An SCM is designed for the Cobblestone Village project. The total drainage area to the SCM is 9.33 ac with 1.63 acres bypassing the SCM. Note the SCM (Wet Pond) will be located on the west side of the property.

There is one point of interest (POI) used for the pre-development hydrologic analysis of the site. POI # 1 is the exit point at the west side of the site. Most of the site drains in that direction. For the post-development hydrologic analysis POI #1 is the portion of the site that discharges to the west side of the site. This area is routed through the SCM. We have a Post Development Detained that is a portion of the site routed through the SCM at the west side of the site. Post Development Not Detained is a portion of the site that is not captured in the SCM and this drainage drains to the west side of the site and is not captured in the SCM.

The wet pond outlet control structure is designed to control the peak stormwater run-off for the 1-year 24-hour storm to be less than the pre-existing conditions. The SCM will meet the 85% total suspended solids (TSS) requirement.

Stormwater routing was evaluated using a 10-year storm for pipe capacity sizing.

DETENTION CALCULATIONS

**STORMWATER RUNOFF SUMMARY
PRE VS. POST DESIGN PARAMETERS
SCM 1 CALCULATIONS
1 AND 100 – YEAR ROUTING CALCULATIONS**

Water Quality Retention Calculations

Project Name: **Cobblestone Village**

Determine Surface Area Required for Permanent Pool:

Drainage Area: 9.33 ac
Impervious Area: 7.01 ac
Percent Impervious: 75.1%
Permanent Pool Elevation: 424.50 (¹/₂ way up vegetated shelf)
Volume: 28431.50 cf
Surface Area: 12926.00 sf
Hydraulic Depth: 3.34 ft (Option 2 Calculation BMP Manual)
SA/DA Required: 2.95%
SA/DA Provided: 3.18% **OK**

Forebay Volume Check:

Forebay Volume at Crest of Berm: 5459.50 cf
Permanent Pool Volume: 28431.50 cf
Forebay Volume % of Perm. Volume: 19.20% **OK - Approximately 20% of total perm. volume**

Calculate the Volume Required to Treat the First Flush:

Rainfall to Treat: 1 in
Runoff Coefficient (R_v) = $0.05 + 0.009 * (\% \text{ Impervious})$
Runoff Coefficient (R_v): 0.73 in/in
Runoff Volume (V) = Rainfall * (R_v) * (Drainage Area)
Runoff Volume (V): 24,588 cf

Calculate the Depth Required for the Temporary Pool:

Temporary Pool Volume (Required): 24,588 cf
Total Volume (Perm. + Temp.): 53,019 cf
Temporary Pool Elevation between: 426.00 and 427.00
Temporary Pool Elevation: 426.15
Temporary Pool Depth: 1.65 measured from Permanent Pool Elevation

Determine the Orifice Size for 2-5 Day Drawdown of Temporary Pool:

Orifice Invert Elevation: 424.50
Temporary Pool Elevation: 426.15
Orifice Diameter: 2.50 in

Use the orifice equation to determine flow and drawdown time:

Orifice Equation: $Q = CA(2gh)^{0.5}$
Volume to Draw Down: 24,588 cf
Flow for 2-Day Drawdown: 0.14 cfs
Flow for 5-Day Drawdown: 0.06 cfs
C: 0.60
g: 32.20 ft/s²
A: 0.03 sf
Number of Increments for Orifice Flow: 10 Increments
Depth of Temp. Pool from Top of Orifice: 1.44 ft

Incremental Orifice Flow Drawdown Calculations

For Temp Pool above top of orifice (Equations III-13, Malcom):

Index:	Avg Driving Head (ft)	Q (from Orifice Eq)	Drawdown Time (s)	Drawdown Time (Days)
0	1.4019	0.1943	11,054.75	0.1279
1	1.2577	0.1841	11,671.26	0.1351
2	1.1135	0.1732	12,403.93	0.1436
3	0.9693	0.1616	13,294.54	0.1539
4	0.8251	0.1491	14,409.42	0.1668
5	0.6809	0.1354	15,861.86	0.1836
6	0.5368	0.1203	17,865.86	0.2068
7	0.3926	0.1028	20,891.01	0.2418
8	0.2484	0.0818	26,264.45	0.3040
9	0.1042	0.0530	40,555.12	0.4694
Total				2.1328

For Temp Pool below top of orifice (Equations III-13, Malcom):

Index:	Avg Driving Head (ft)	Q (Malcom III-13)	Drawdown Time (s)	Drawdown Time (Days)
0	0.2083	0.0531	29249.56	0.3385
1	0.1042	0.0188	82730.25	0.9575
Total				1.2961

Drawdown Time:**3.43 days (OK - Drawdown is between 2 and 5 days)**

Stormwater Attenuation Requirements Using Rational Methodology

The following calculations summarize the pre-development and post development discharge calculations for the 1-year and 100-year 24-hr storm events using the Rational Method. The Q1 and Q100 pre-developed discharge was calculated based on the actual site pre-developed conditions. Hydraflow computer software was used for performing the analysis. Calculations were done in accordance to the Town of Knightdale standards and specifications. All hydrographs and supporting calculations are provided in the Detention Calculations section of this report. Supporting drainage area maps and rainfall data are provided in the Appendix. The following summarizes the findings of the analysis:

Description	Rational Method Storm Event (cfs)			
	Q1			Q100
Pre-Development Discharge	20.69			43.65
Post-Development Discharge	37.34			78.78
Attenuation Required	16.65			N/A
Discharge into SCM	34.37			72.50
Discharge out of SCM	0.14			0.20
Combined Discharge (including bypass)	3.77			7.90
Attenuation Provided	33.57			70.88
<p>The proposed attenuation provided by the Wet Pond provides enough stormwater attenuation so that the Q1 and Q100 post-developed discharge does not exceed the pre-development discharge.</p>				

Pre/Post Design Parameters										
POI #1	Drainage Area	Land Use Areas (ac)				Design Storm Flows (cfs)				
	ac	Impervious	Managed Pervious	Wooded Area	Off-Site 70% Imp	1"	Q1		Q100	
PR to SCM	9.33	7.01	2.32	0.00	0.00	---	33.94		71.59	
PR to Bypass SCM	1.63	0.47	1.16	0.00	0.00	---	3.68		7.76	
SCM Outfall	0.00	---	---	---	---	---	0.14		0.20	
PR Final	10.96	7.48	3.48	0.00	0.00	---	3.77		7.90	
EX	10.96	1.83	9.13	0.00	0.00	---	20.69		43.65	
Surface Area at SCM		Design Storm Surface Elevations (ft)					426.15	425.29		426.09
12,926		Freeboard (ft)					1.35	2.21		1.41

Average Depth Calculation

Project Name: Cobblestone Village

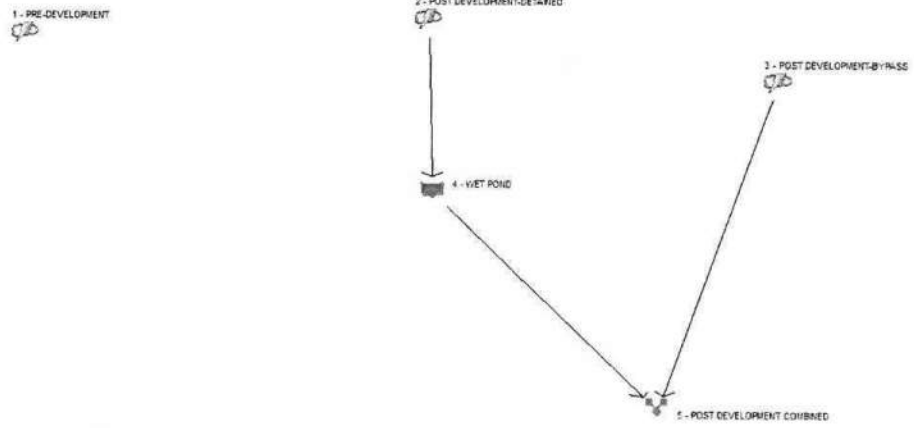
Permanent Pool Elevation:	424.50 ($\frac{1}{2}$ way up vegetated shelf)
Surface Area at Perm. Pool:	12926.00 sf
Elevation of Bottom of Shelf:	424.00
Surface Area at Bottom Shelf:	8026.00
Area at Bottom of Pond:	3739.00
Depth (from bottom of shelf to pond bottom):	4.00
Hydraulic Depth:	3.34 ft (Option 2 Calculation BMP Manual)

Hydraflow Table of Contents

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Watershed Model Schematic

Hydraflow Hydrographs by Intelisolve v9.01



Legend

<u>Hyd. Origin</u>	<u>Description</u>
1	Rational PRE-DEVELOPMENT
2	Rational POST DEVELOPMENT-DETAINED
3	Rational POST DEVELOPMENT-BYPASS
4	Reservoir WET POND
5	Combine POST DEVELOPMENT COMBINED

Hydrograph Return Period Recap

Hydraflow Hydrographs by Intelisolve v9.01

Hyd. No.	Hydrograph type (origin)	Inflow Hyd(s)	Peak Outflow (cfs)								Hydrograph description	
			1-Yr	2-Yr	3-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr		
1	Rational	-----	20.69	-----	-----	-----	-----	-----	-----	-----	43.65	PRE-DEVELOPMENT
2	Rational	-----	34.37	-----	-----	-----	-----	-----	-----	-----	72.50	POST DEVELOPMENT-DETAINED
3	Rational	-----	3.677	-----	-----	-----	-----	-----	-----	-----	7.758	POST DEVELOPMENT-BYPASS
4	Reservoir	2	0.137	-----	-----	-----	-----	-----	-----	-----	0.201	WET POND
5	Combine	3, 4	3.768	-----	-----	-----	-----	-----	-----	-----	7.899	POST DEVELOPMENT COMBINE

Hydrograph Summary Report

Hydraflow Hydrographs by Intelisolve v9.01

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph description
1	Rational	20.69	1	5	6,207	---	-----	-----	PRE-DEVELOPMENT
2	Rational	34.37	1	5	10,310	---	-----	-----	POST DEVELOPMENT-DETAINED
3	Rational	3.677	1	5	1,103	---	-----	-----	POST DEVELOPMENT-BYPASS
4	Reservoir	0.137	1	10	9,280	2	425.30	10,266	WET POND
5	Combine	3.768	1	5	10,383	3, 4	-----	-----	POST DEVELOPMENT COMBINE
02.05.21 Cobblestone Village.gpw					Return Period: 1 Year			Friday, Feb 5, 2021	

Hydrograph Report

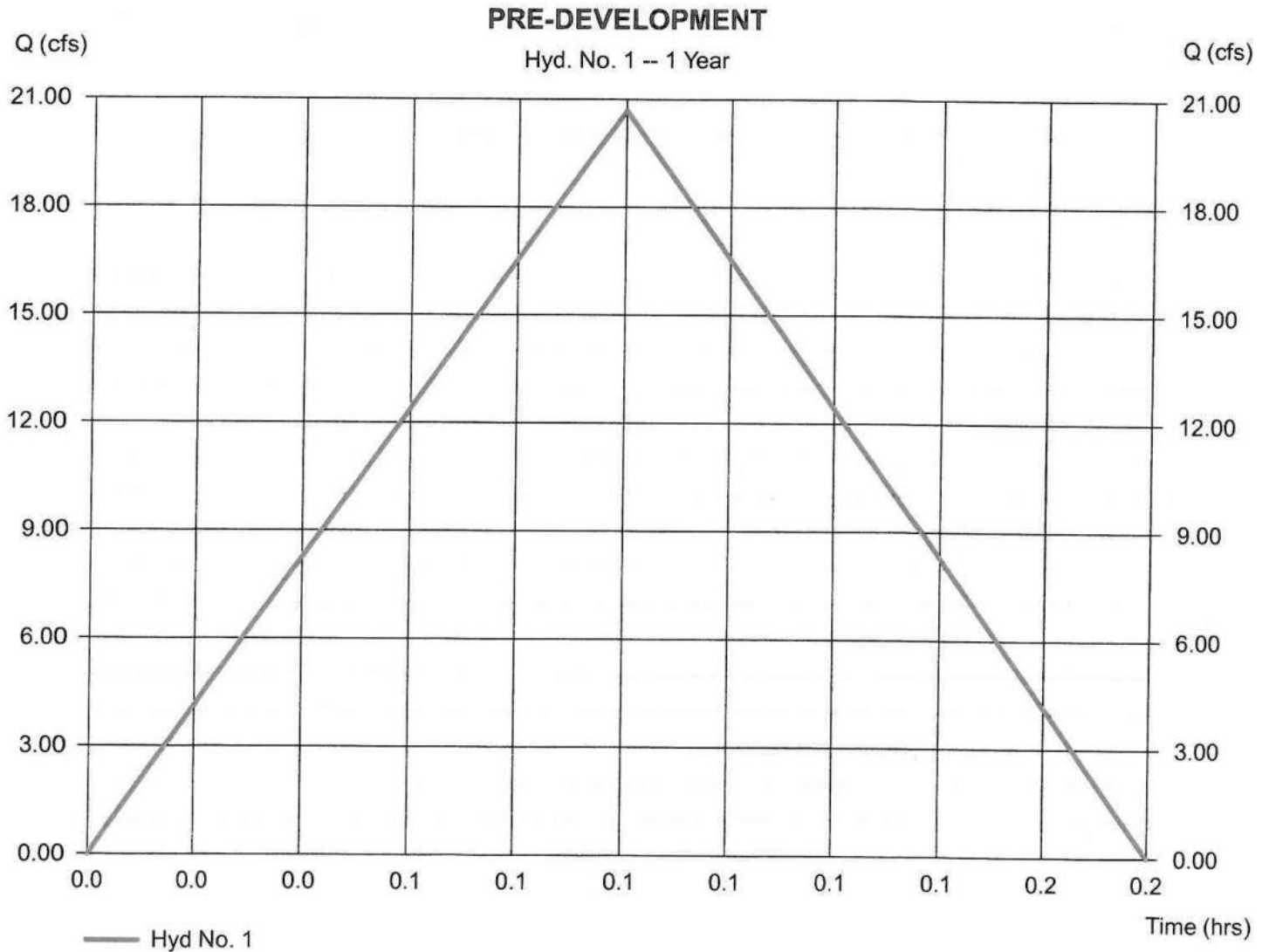
Hyd. No. 1

PRE-DEVELOPMENT

Hydrograph type = Rational
Storm frequency = 1 yrs
Time interval = 1 min
Drainage area = 10.960 ac
Intensity = 4.604 in/hr
IDF Curve = WakeCounty.IDF

Peak discharge = 20.69 cfs
Time to peak = 0.08 hrs
Hyd. volume = 6,207 cuft
Runoff coeff. = 0.41*
Tc by User = 5.00 min
Asc/Rec limb fact = 1/1

* Composite (Area/C) = $[(1.830 \times 0.95) + (9.130 \times 0.30)] / 10.960$



Hydrograph Report

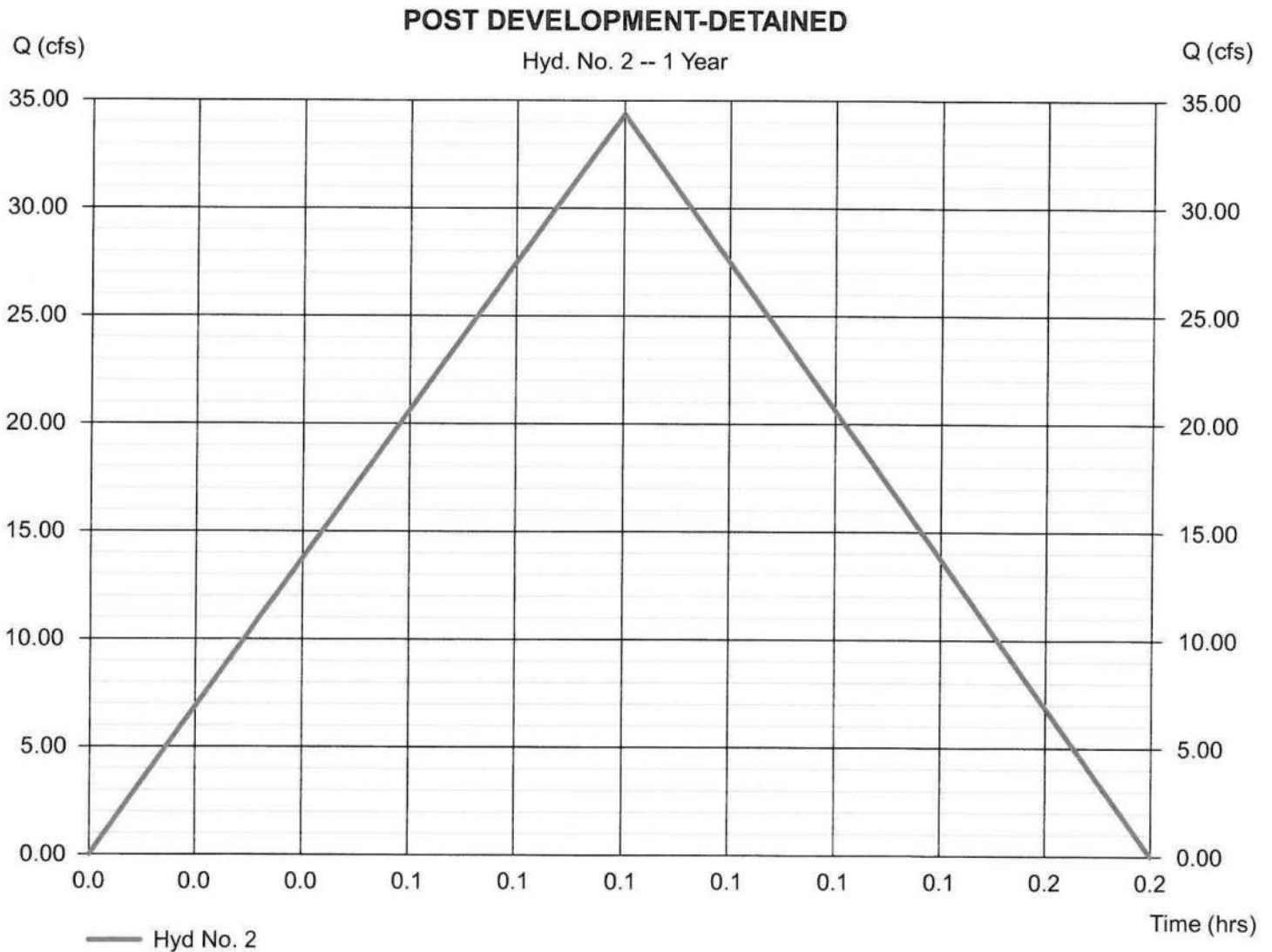
Hyd. No. 2

POST DEVELOPMENT-DETAINED

Hydrograph type = Rational
Storm frequency = 1 yrs
Time interval = 1 min
Drainage area = 9.330 ac
Intensity = 4.604 in/hr
IDF Curve = WakeCounty.IDF

Peak discharge = 34.37 cfs
Time to peak = 0.08 hrs
Hyd. volume = 10,310 cuft
Runoff coeff. = 0.8*
Tc by User = 5.00 min
Asc/Rec limb fact = 1/1

* Composite (Area/C) = [(2.320 x 0.30) + (7.010 x 0.95)] / 9.330



Hydrograph Report

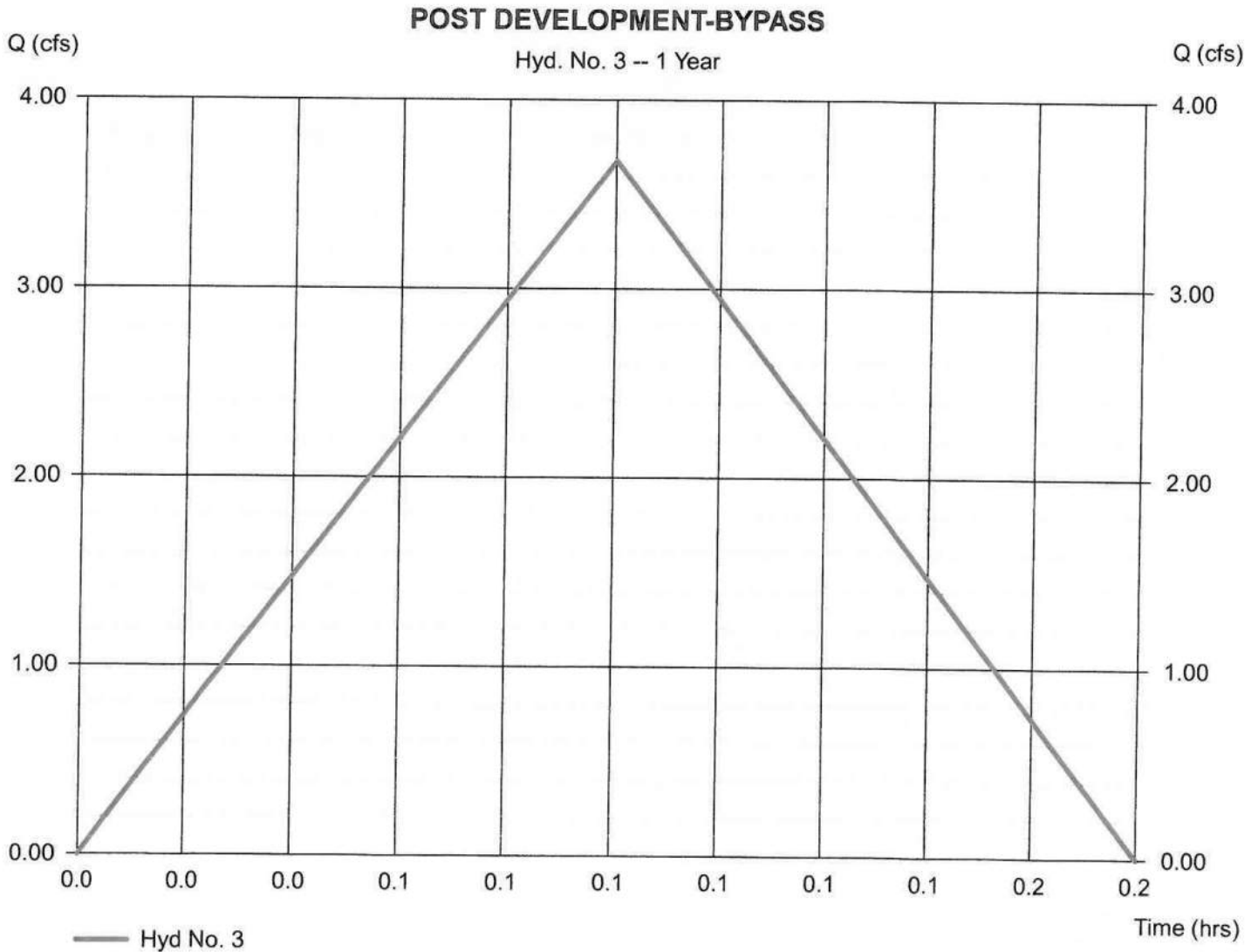
Hyd. No. 3

POST DEVELOPMENT-BYPASS

Hydrograph type = Rational
Storm frequency = 1 yrs
Time interval = 1 min
Drainage area = 1.630 ac
Intensity = 4.604 in/hr
IDF Curve = WakeCounty.IDF

Peak discharge = 3.677 cfs
Time to peak = 0.08 hrs
Hyd. volume = 1,103 cuft
Runoff coeff. = 0.49*
Tc by User = 5.00 min
Asc/Rec limb fact = 1/1

* Composite (Area/C) = $[(1.160 \times 0.30) + (0.470 \times 0.95)] / 1.630$



Hydrograph Report

Hydraflow Hydrographs by Intelisolve v9.01

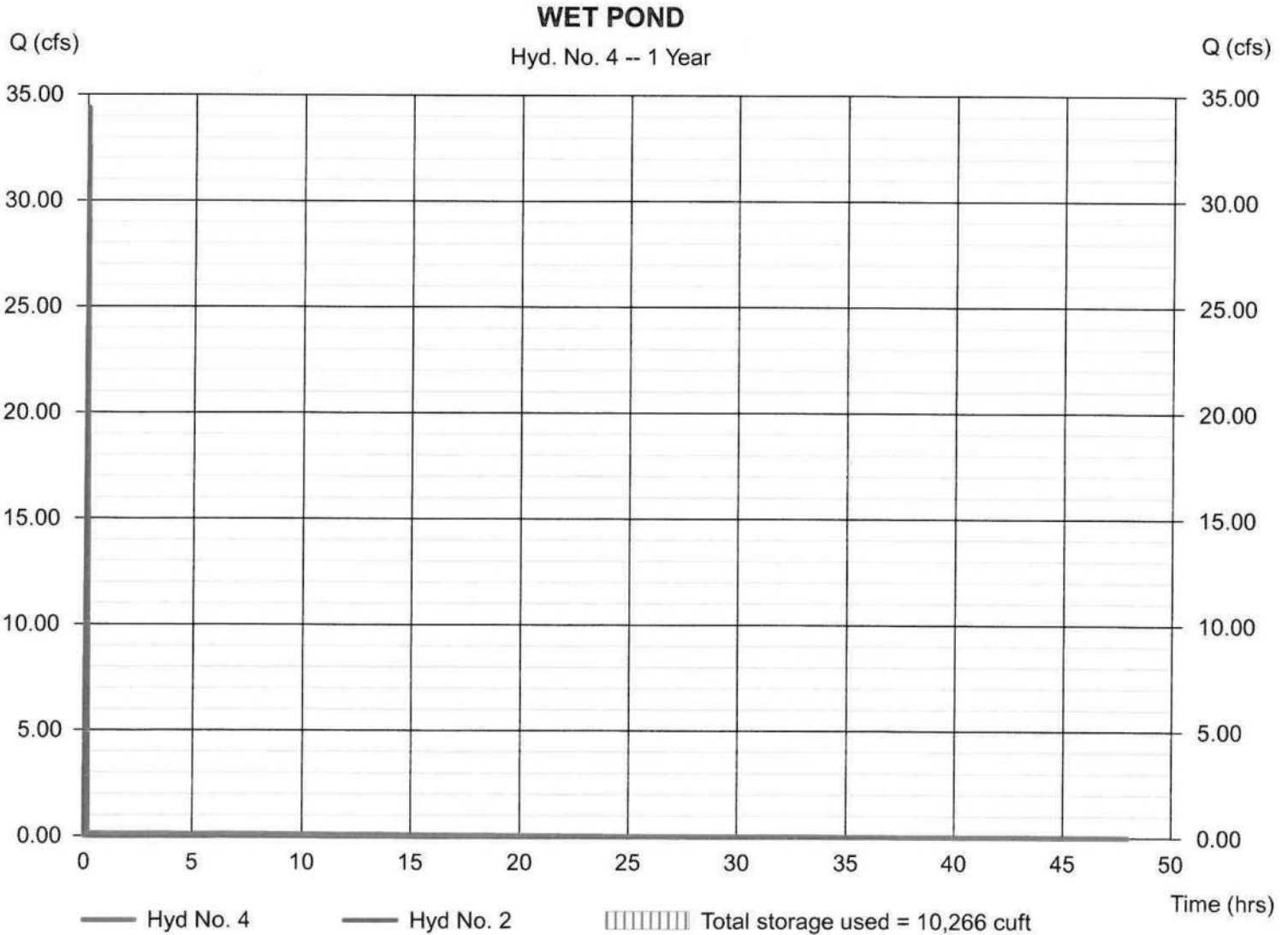
Friday, Feb 5, 2021

Hyd. No. 4

WET POND

Hydrograph type	= Reservoir	Peak discharge	= 0.137 cfs
Storm frequency	= 1 yrs	Time to peak	= 0.17 hrs
Time interval	= 1 min	Hyd. volume	= 9,280 cuft
Inflow hyd. No.	= 2 - POST DEVELOPMENT-DETAINED	Max. Elevation	= 425.30 ft
Reservoir name	= WET POND	Max. Storage	= 10,266 cuft

Storage Indication method used.



Pond Report

Hydraflow Hydrographs by Intelisolve v9.01

Friday, Feb 5, 2021

Pond No. 1 - WET POND

Pond Data

Trapezoid - Bottom L x W = 200.0 x 61.0 ft, Side slope = 3.0:1, Bottom elev. = 424.50 ft, Depth = 3.00 ft

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	424.50	12,200	0	0
0.30	424.80	12,673	3,731	3,731
0.60	425.10	13,153	3,874	7,604
0.90	425.40	13,639	4,019	11,623
1.20	425.70	14,131	4,165	15,788
1.50	426.00	14,630	4,314	20,102
1.80	426.30	15,135	4,465	24,567
2.10	426.60	15,647	4,617	29,184
2.40	426.90	16,166	4,772	33,956
2.70	427.20	16,691	4,928	38,884
3.00	427.50	17,222	5,087	43,971

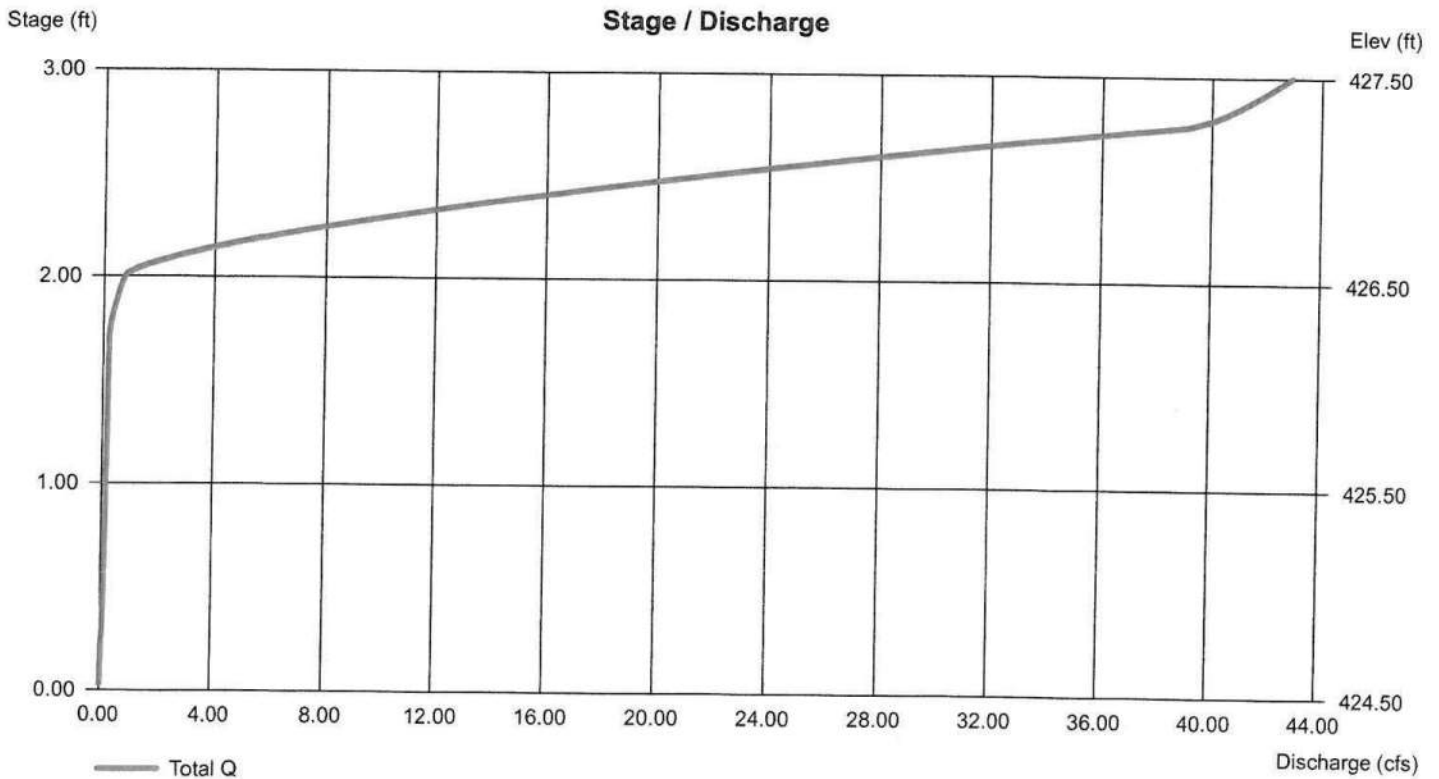
Culvert / Orifice Structures

	[A]	[B]	[C]	[PrfRsr]
Rise (in)	= 24.00	2.50	0.00	0.00
Span (in)	= 24.00	2.50	0.00	0.00
No. Barrels	= 1	1	0	0
Invert El. (ft)	= 420.00	424.50	0.00	0.00
Length (ft)	= 1.00	2.00	0.00	0.00
Slope (%)	= 1.00	1.00	0.00	n/a
N-Value	= .013	.013	.013	n/a
Orifice Coeff.	= 0.60	0.60	0.60	0.60
Multi-Stage	= n/a	No	No	No

Weir Structures

	[A]	[B]	[C]	[D]
Crest Len (ft)	= 16.00	1.00	0.00	0.00
Crest El. (ft)	= 426.50	426.20	0.00	0.00
Weir Coeff.	= 3.33	3.33	3.33	3.33
Weir Type	= Riser	Rect	---	---
Multi-Stage	= Yes	No	No	No
Exfil.(in/hr)	= 0.000 (by Contour)			
TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet and outlet control. Weir risers are checked for orifice conditions.



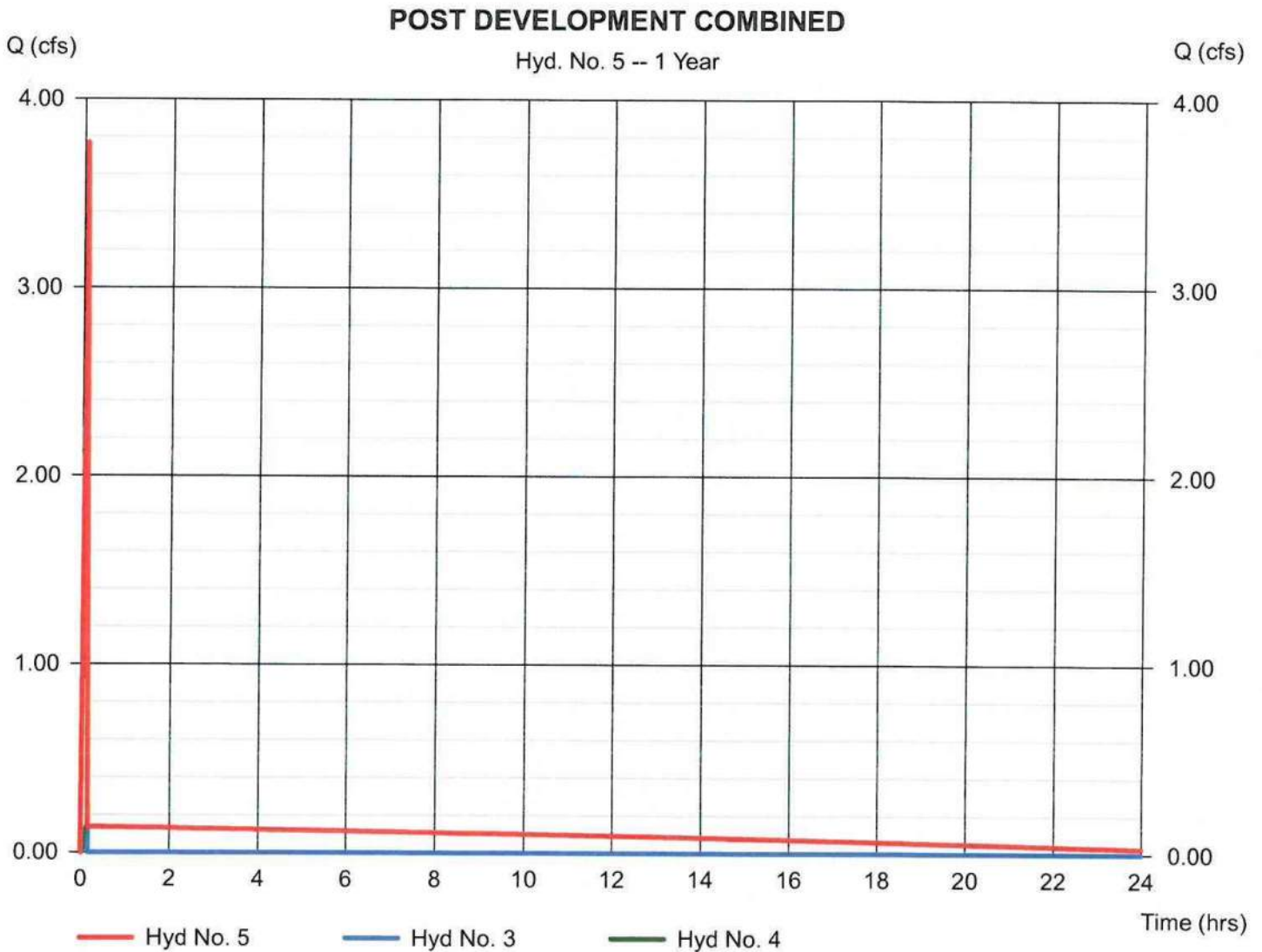
Hydrograph Report

Hyd. No. 5

POST DEVELOPMENT COMBINED

Hydrograph type = Combine
Storm frequency = 1 yrs
Time interval = 1 min
Inflow hyds. = 3, 4

Peak discharge = 3.768 cfs
Time to peak = 0.08 hrs
Hyd. volume = 10,383 cuft
Contrib. drain. area = 1.630 ac



Hydrograph Summary Report

Hydraflow Hydrographs by Intelisolve v9.01

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph description
1	Rational	43.65	1	5	13,094	----	-----	-----	PRE-DEVELOPMENT
2	Rational	72.50	1	5	21,749	----	-----	-----	POST DEVELOPMENT-DETAINED
3	Rational	7.758	1	5	2,327	----	-----	-----	POST DEVELOPMENT-BYPASS
4	Reservoir	0.201	1	10	19,606	2	426.11	21,678	WET POND
5	Combine	7.899	1	5	21,933	3, 4	-----	-----	POST DEVELOPMENT COMBINE
02.05.21 Cobblestone Village.gpw					Return Period: 100 Year			Friday, Feb 5, 2021	

Hydrograph Report

Hydraflow Hydrographs by Intelisolve v9.01

Friday, Feb 5, 2021

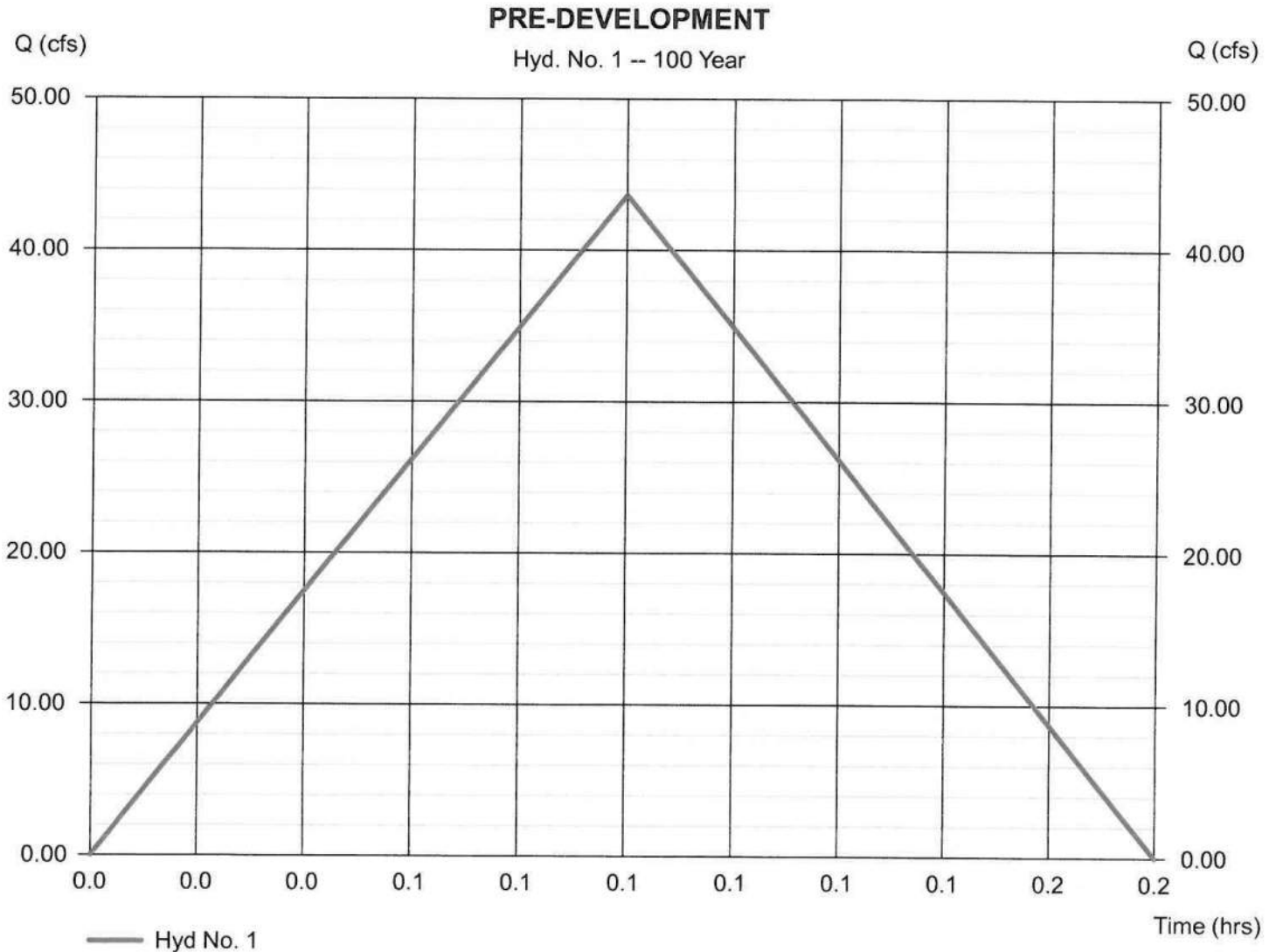
Hyd. No. 1

PRE-DEVELOPMENT

Hydrograph type = Rational
Storm frequency = 100 yrs
Time interval = 1 min
Drainage area = 10.960 ac
Intensity = 9.713 in/hr
IDF Curve = WakeCounty.IDF

Peak discharge = 43.65 cfs
Time to peak = 0.08 hrs
Hyd. volume = 13,094 cuft
Runoff coeff. = 0.41*
Tc by User = 5.00 min
Asc/Rec limb fact = 1/1

* Composite (Area/C) = [(1.830 x 0.95) + (9.130 x 0.30)] / 10.960



Hydrograph Report

Hydraflow Hydrographs by Intelisolve v9.01

Friday, Feb 5, 2021

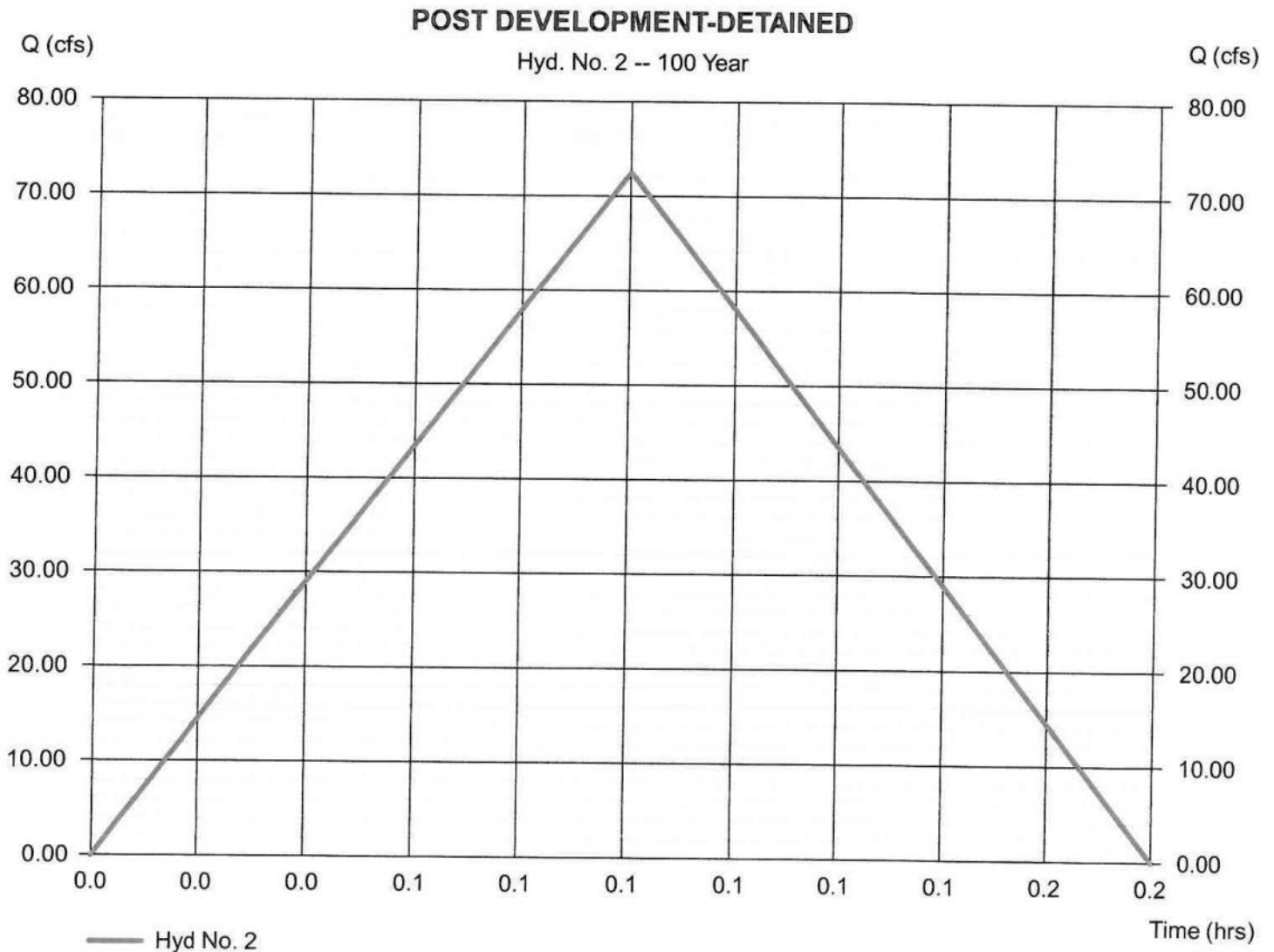
Hyd. No. 2

POST DEVELOPMENT-DETAINED

Hydrograph type = Rational
Storm frequency = 100 yrs
Time interval = 1 min
Drainage area = 9.330 ac
Intensity = 9.713 in/hr
IDF Curve = WakeCounty.IDF

Peak discharge = 72.50 cfs
Time to peak = 0.08 hrs
Hyd. volume = 21,749 cuft
Runoff coeff. = 0.8*
Tc by User = 5.00 min
Asc/Rec limb fact = 1/1

* Composite (Area/C) = [(2.320 x 0.30) + (7.010 x 0.95)] / 9.330



Hydrograph Report

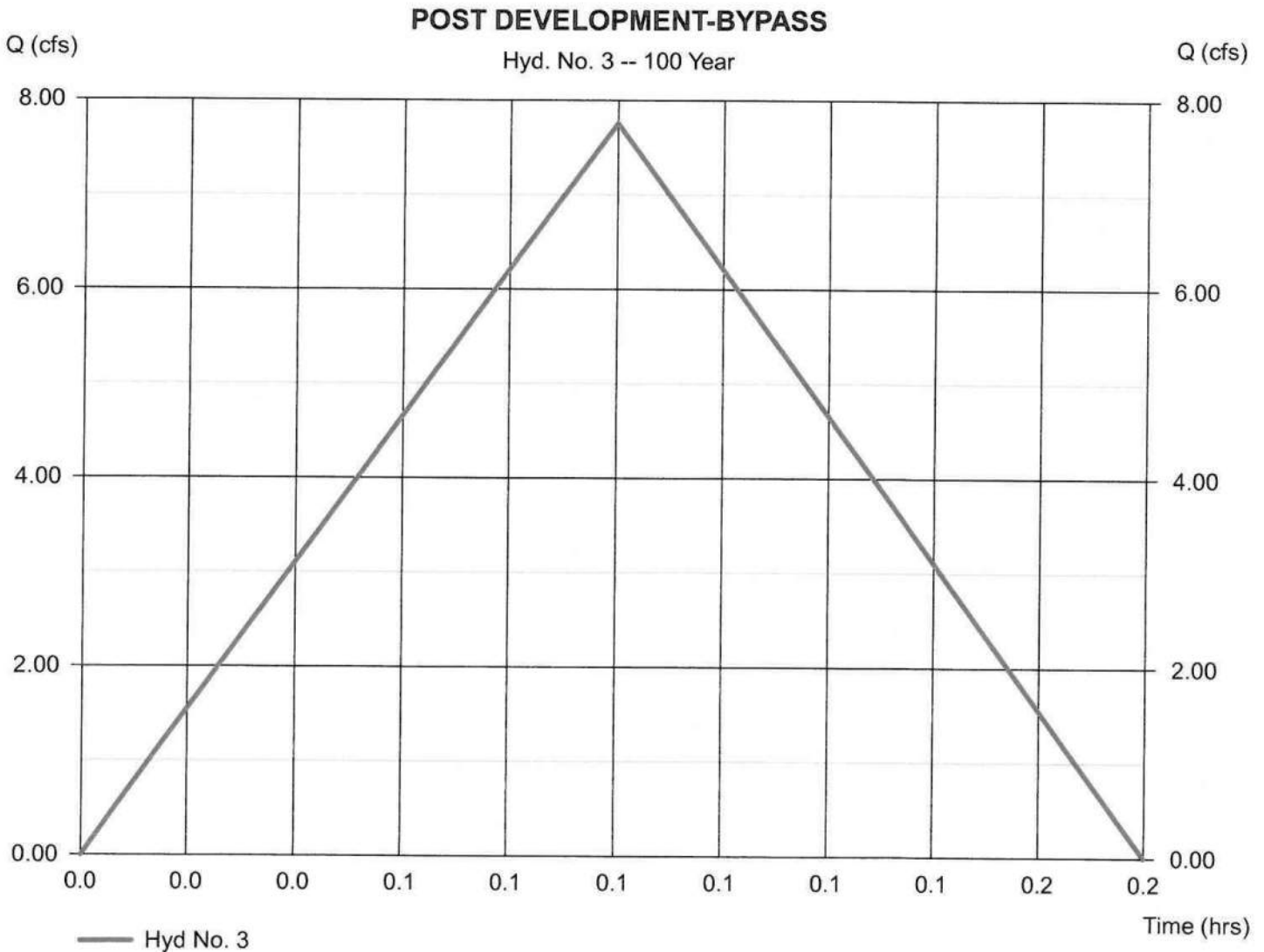
Hyd. No. 3

POST DEVELOPMENT-BYPASS

Hydrograph type = Rational
Storm frequency = 100 yrs
Time interval = 1 min
Drainage area = 1.630 ac
Intensity = 9.713 in/hr
IDF Curve = WakeCounty.IDF

Peak discharge = 7.758 cfs
Time to peak = 0.08 hrs
Hyd. volume = 2,327 cuft
Runoff coeff. = 0.49*
Tc by User = 5.00 min
Asc/Rec limb fact = 1/1

* Composite (Area/C) = [(1.160 x 0.30) + (0.470 x 0.95)] / 1.630



Hydrograph Report

Hydraflow Hydrographs by Intelisolve v9.01

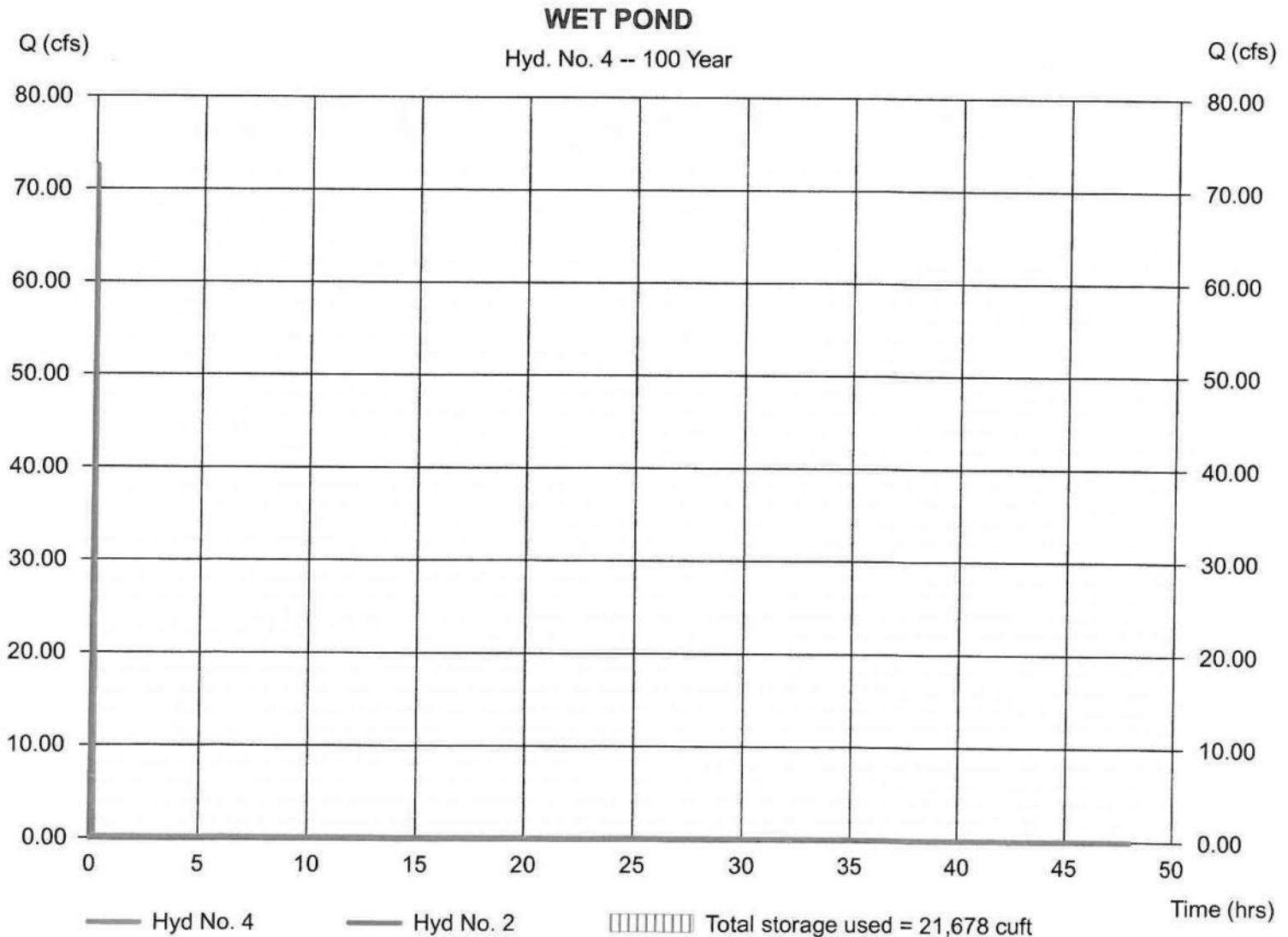
Friday, Feb 5, 2021

Hyd. No. 4

WET POND

Hydrograph type	= Reservoir	Peak discharge	= 0.201 cfs
Storm frequency	= 100 yrs	Time to peak	= 0.17 hrs
Time interval	= 1 min	Hyd. volume	= 19,606 cuft
Inflow hyd. No.	= 2 - POST DEVELOPMENT-DETAINED	Max. Elevation	= 426.11 ft
Reservoir name	= WET POND	Max. Storage	= 21,678 cuft

Storage Indication method used.



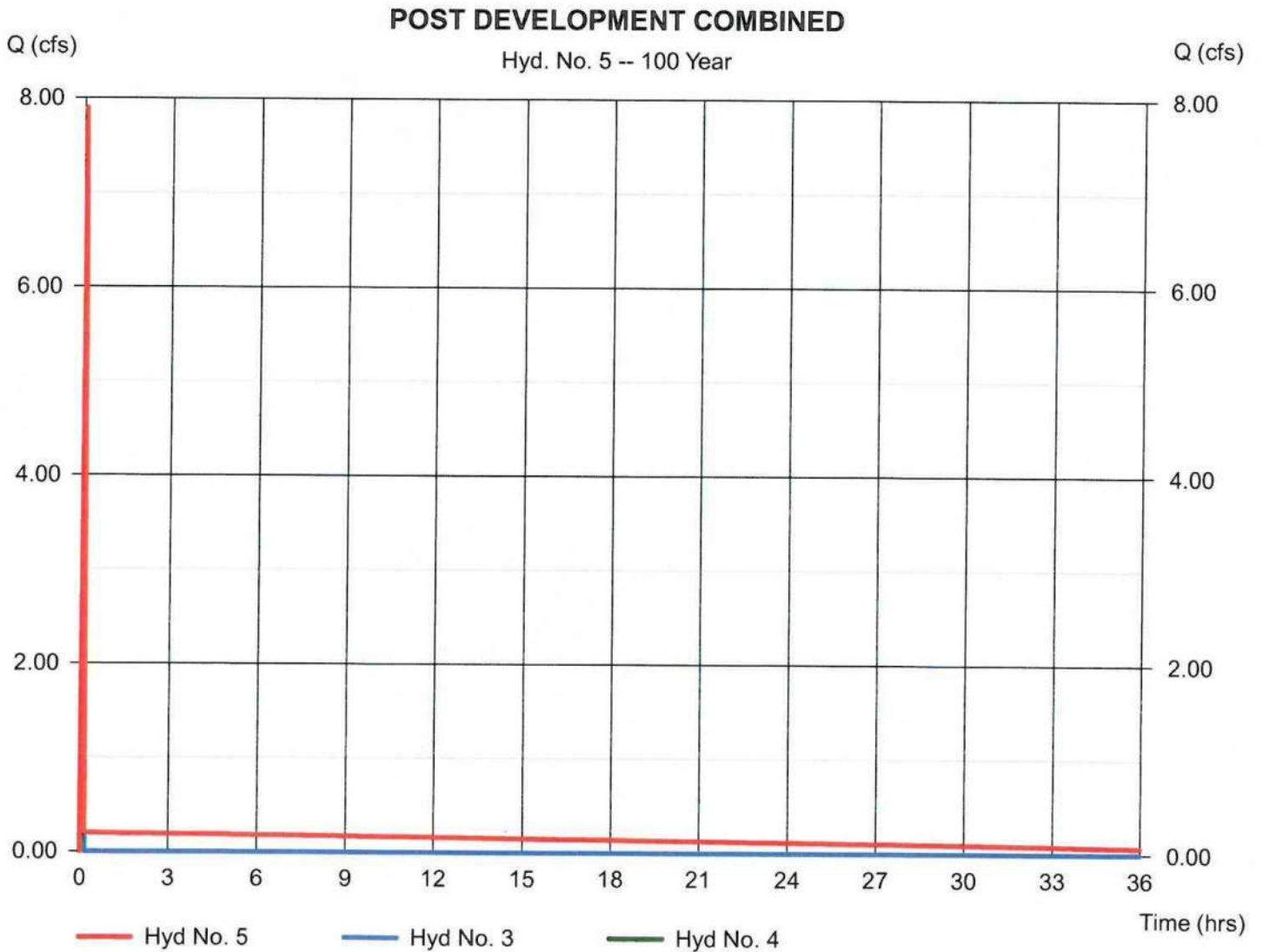
Hydrograph Report

Hyd. No. 5

POST DEVELOPMENT COMBINED

Hydrograph type = Combine
Storm frequency = 100 yrs
Time interval = 1 min
Inflow hyds. = 3, 4

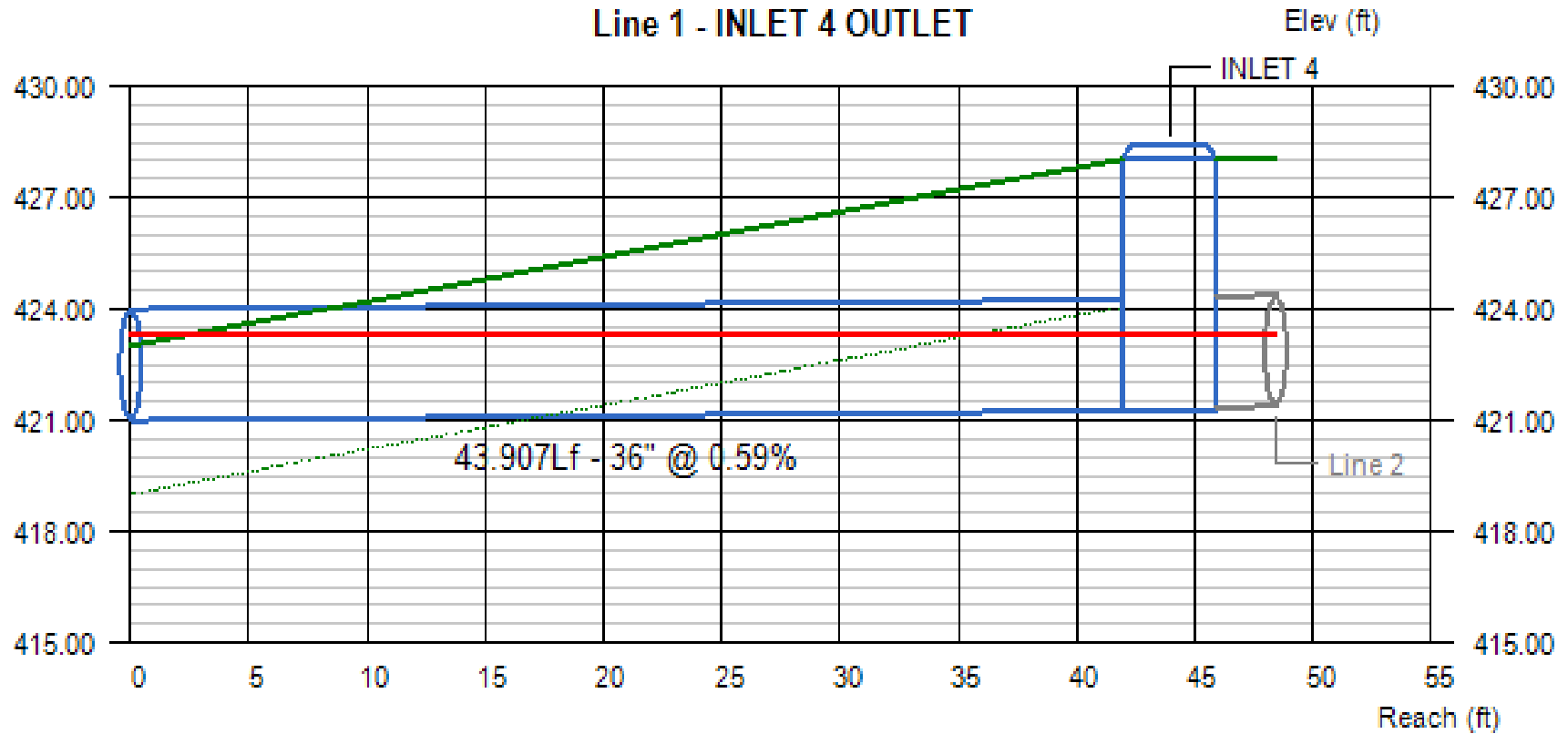
Peak discharge = 7.899 cfs
Time to peak = 0.08 hrs
Hyd. volume = 21,933 cuft
Contrib. drain. area= 1.630 ac



STORMWATER RUNOFF

**10-YEAR PIPE SIZING
10-YEAR HYDRAULIC GRADE LINES**

COBBLESTONE VILLAGE
FEBRUARY 2021



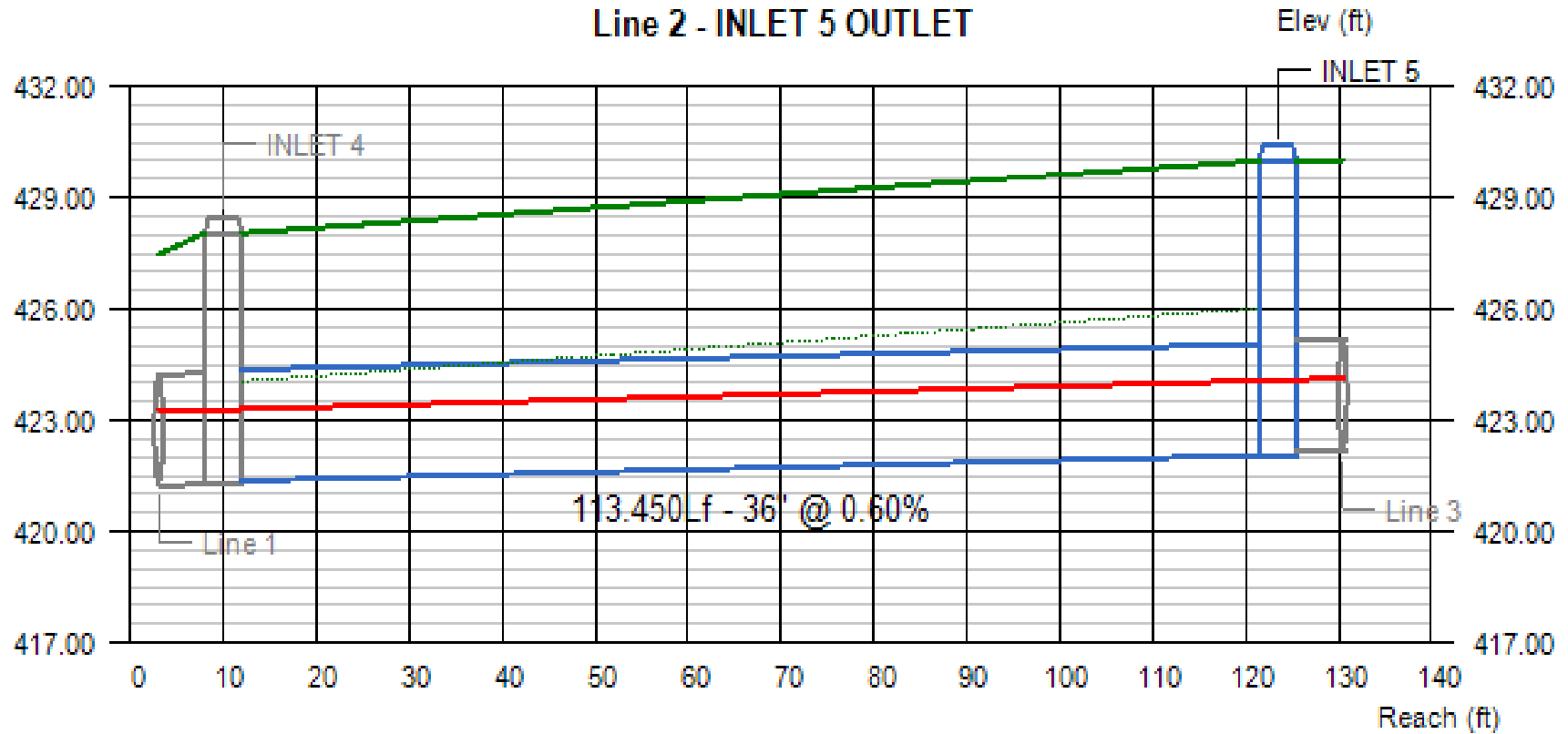
Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
1	38.53	421.00	421.26	2.33	2.02	2.02	423.33	423.28	423.28	6.54	7.62	-1.00	3.78

Project File:

No. Lines: 30

Run Date: 2/12/2021

Line Profile (Line 2) - INLET 5 OUTLET

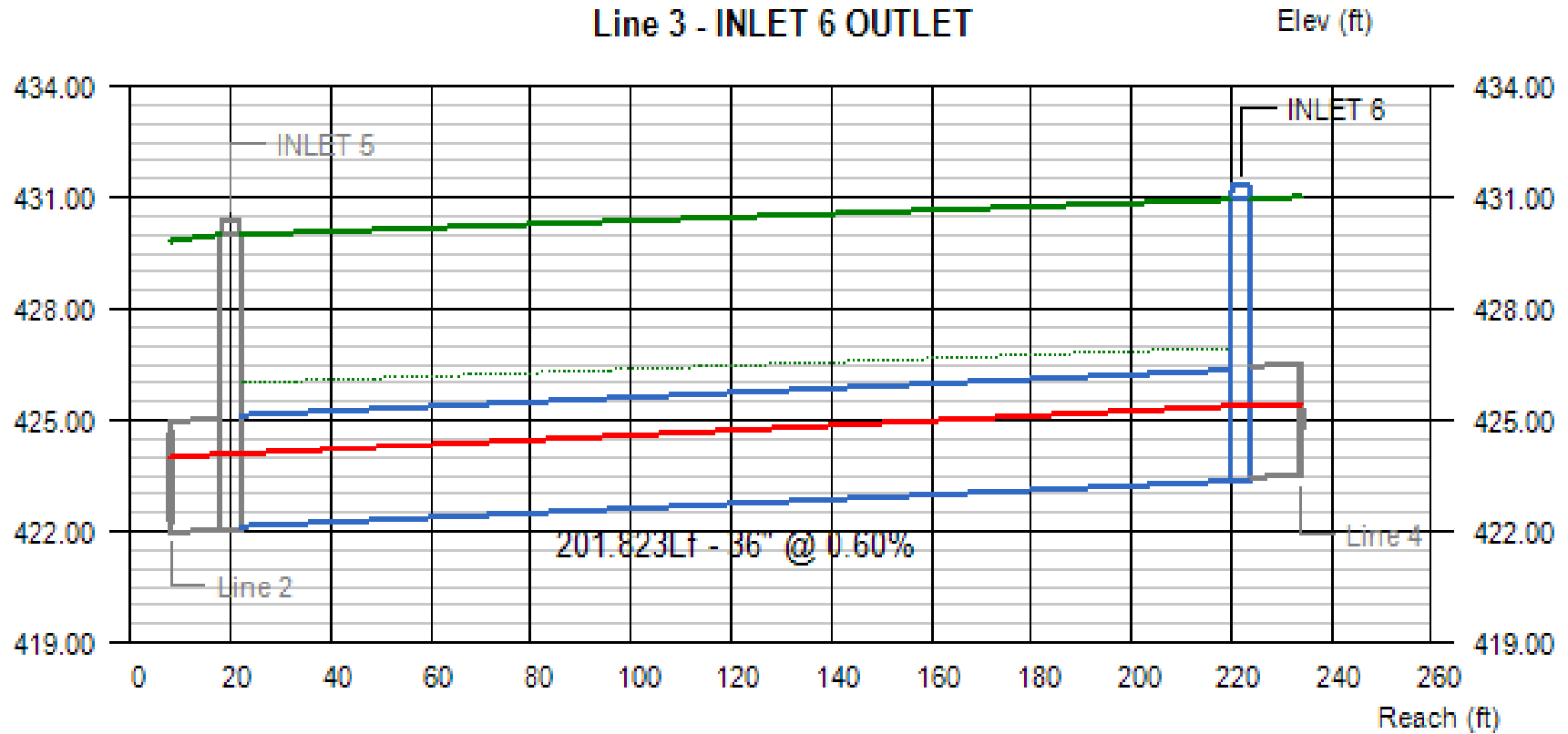


Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
2	38.82	421.36	422.04	1.94	2.03	2.03	423.30	424.07	424.07	8.02	7.64	3.68	4.96

Project File:

No. Lines: 30

Run Date: 2/12/2021



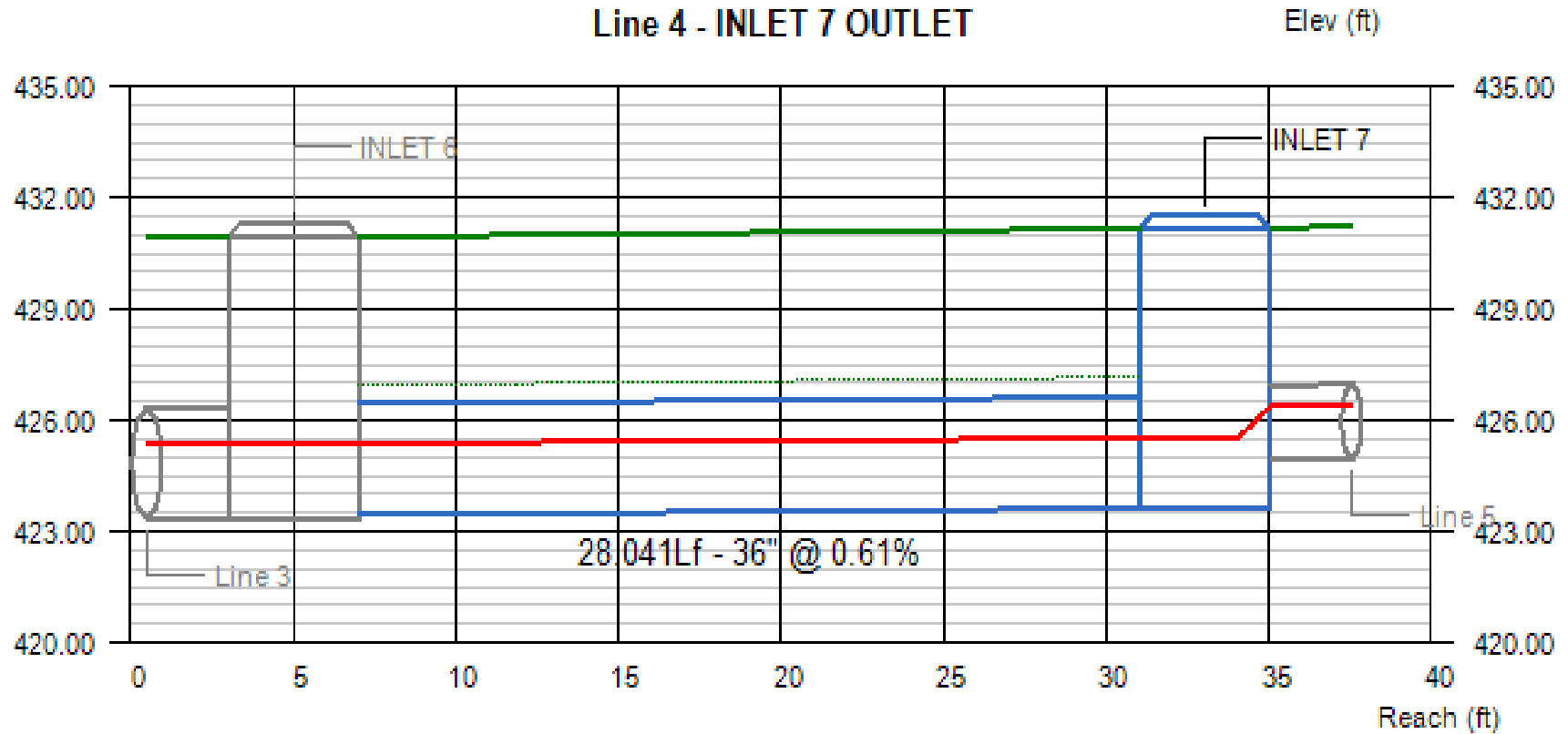
Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
3	39.16	422.14	423.35	1.95	2.03	2.03	424.09	425.38	425.38	8.03	7.67	4.86	4.59

Project File:

No. Lines: 30

Run Date: 2/12/2021

Line Profile (Line 4) - INLET 7 OUTLET

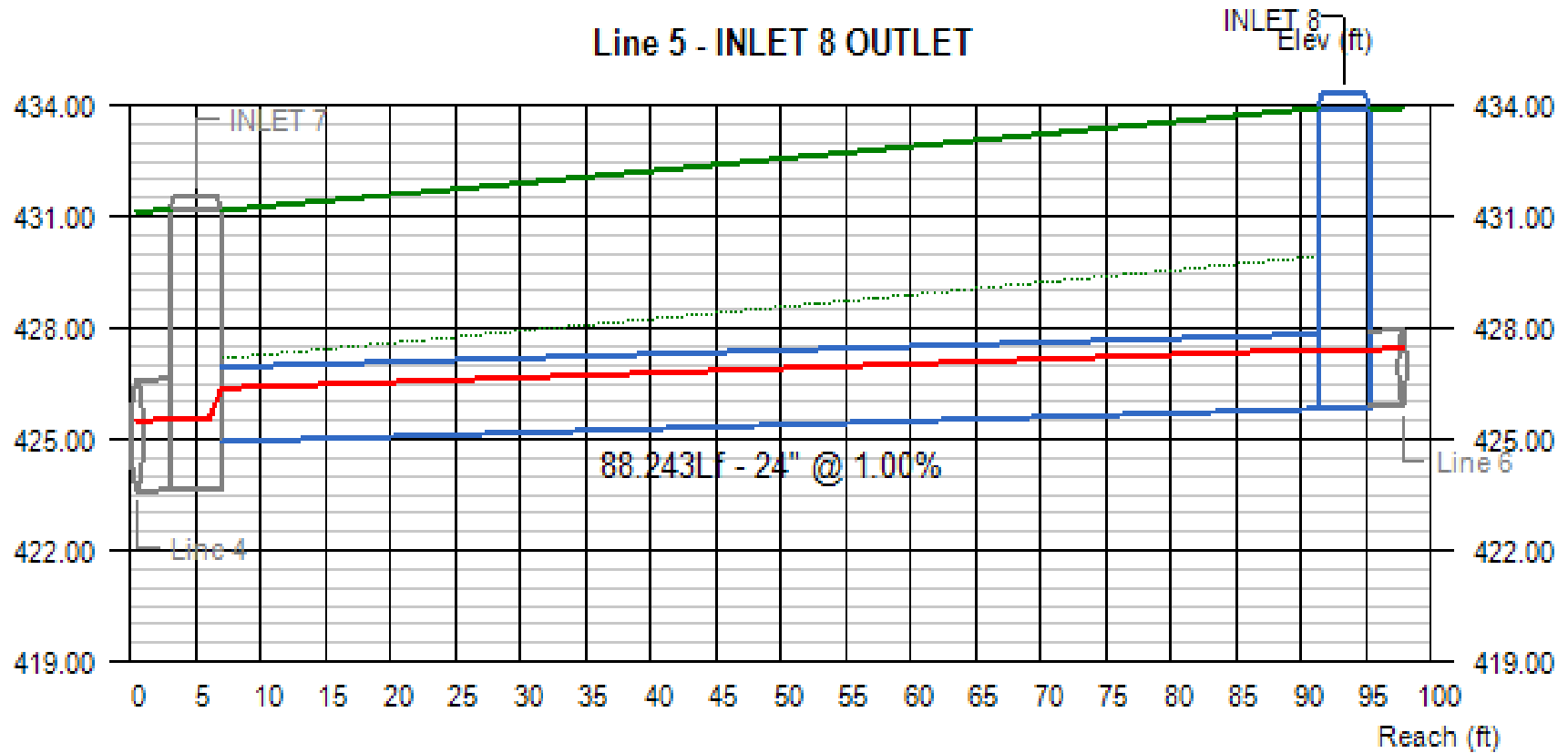


Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
4	34.35	423.45	423.62	1.93	1.90	1.90	425.38	425.52	425.52	7.13	7.27	4.49	4.54

Project File:

No. Lines: 30

Run Date: 2/12/2021



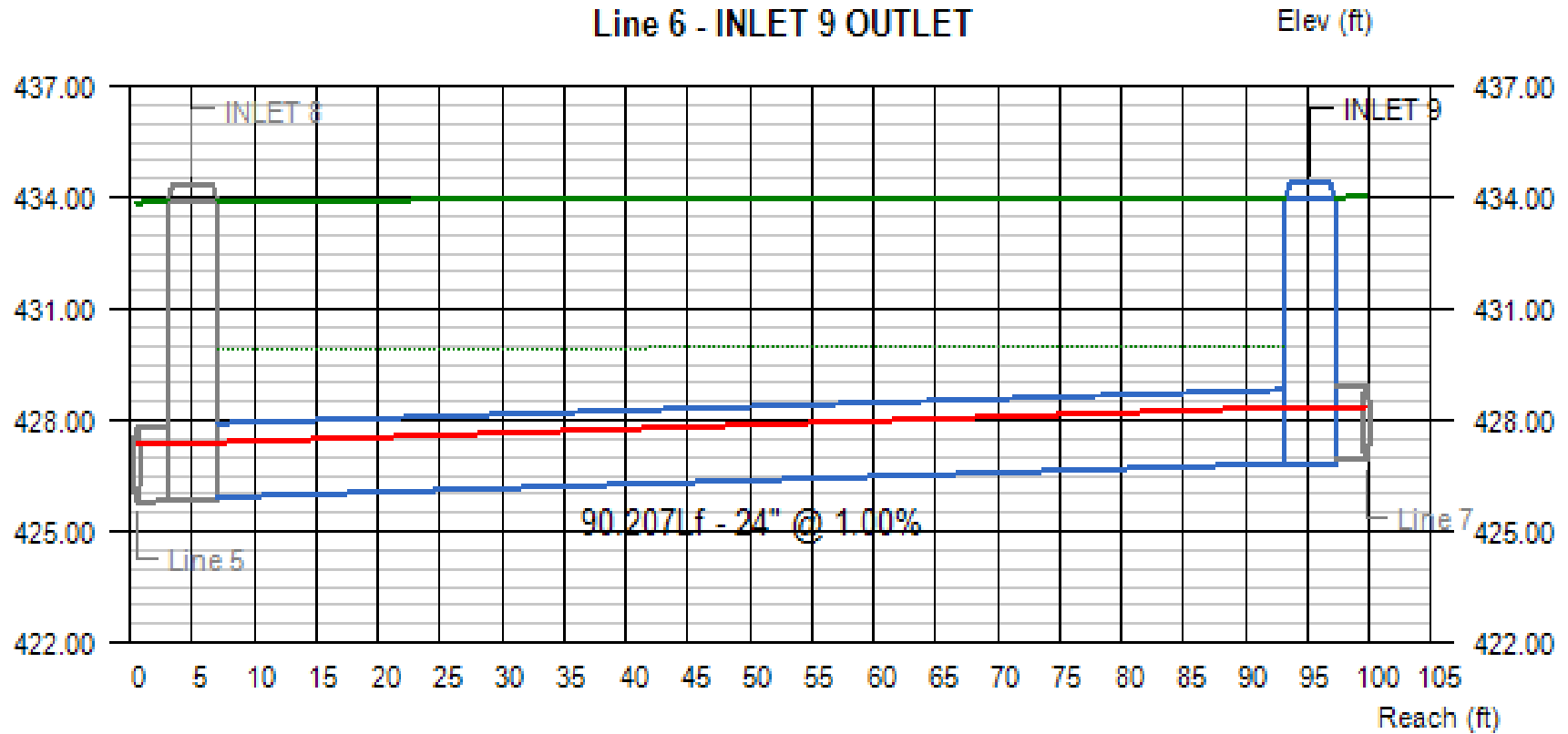
Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
5	19.53	424.94	425.82	1.44	1.59	1.59	426.38	427.41	427.41	8.09	7.30	4.22	6.10

Project File:

No. Lines: 30

Run Date: 2/12/2021

Line Profile (Line 6) - INLET 9 OUTLET



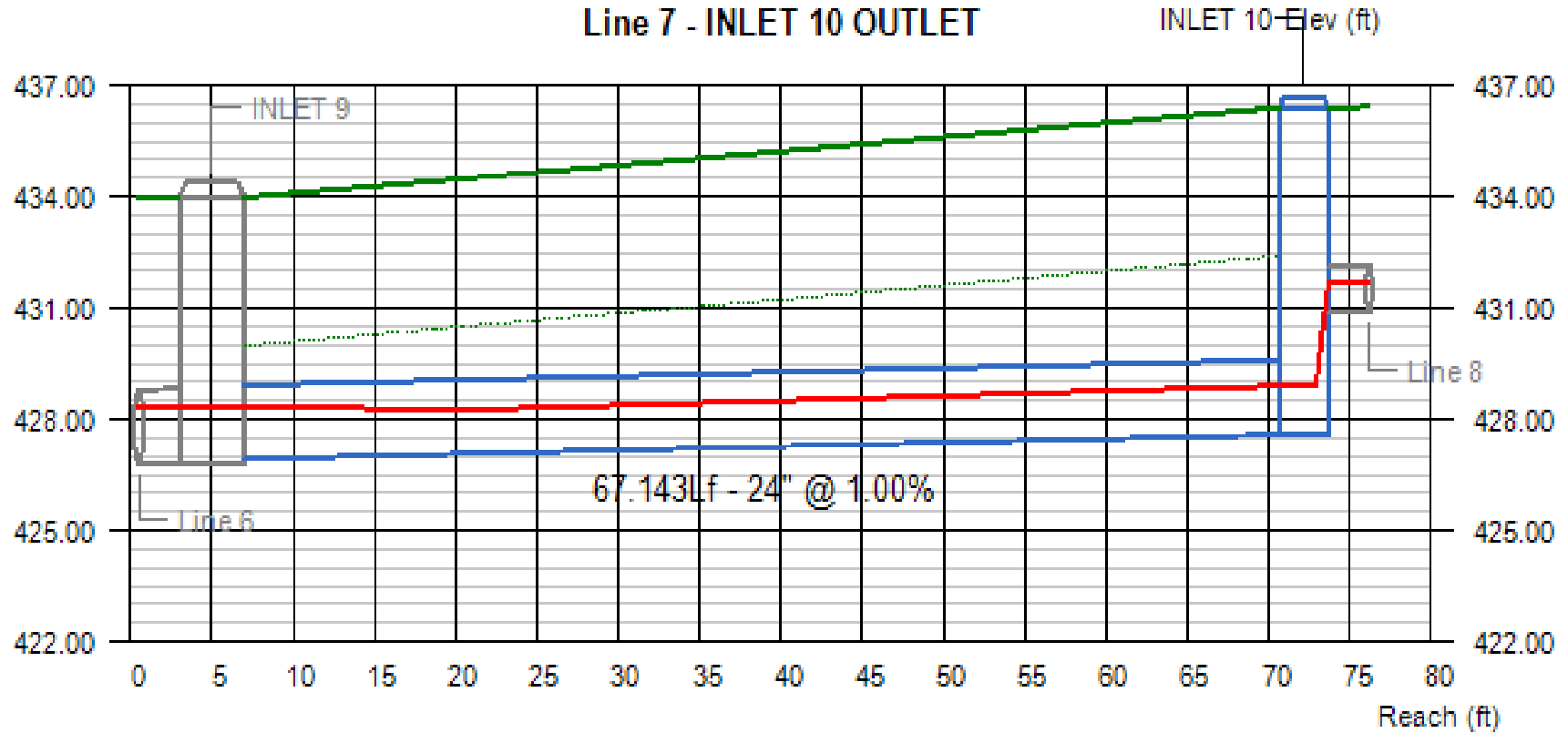
Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
6	18.07	425.92	426.82	1.49	1.53	1.53	427.41	428.35	428.35	7.21	7.01	6.00	5.15

Project File:

No. Lines: 30

Run Date: 2/12/2021

Line 7 - INLET 10 OUTLET

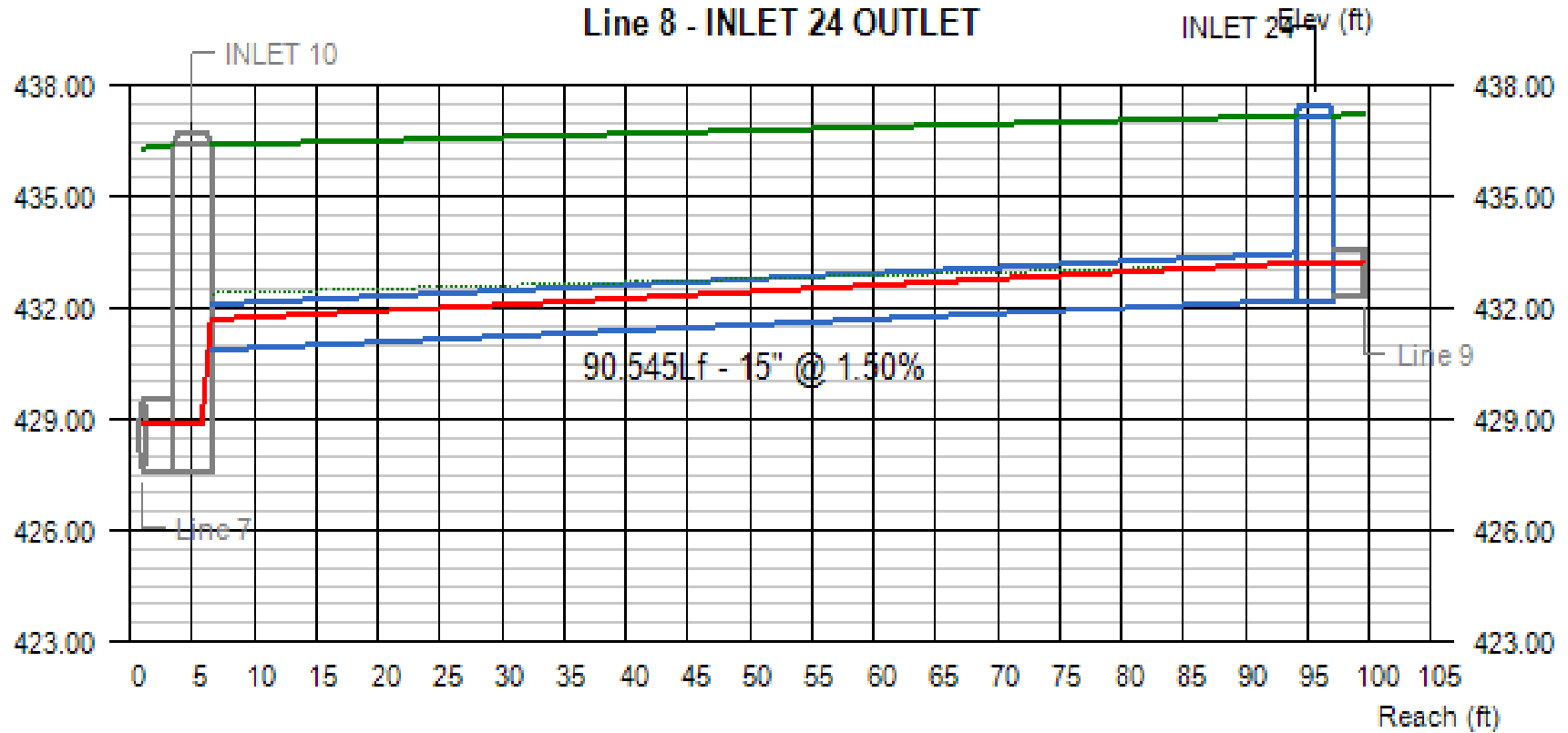


Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
7	13.29	426.92	427.59	1.43	1.31	1.31	428.35	428.90 j	428.90	5.53	6.09	5.05	6.81

Project File:

No. Lines: 30

Run Date: 2/12/2021



Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
8	6.05	430.86	432.22	0.82	0.99	0.99	431.68	433.21	433.21	7.10	5.78	4.29	3.71

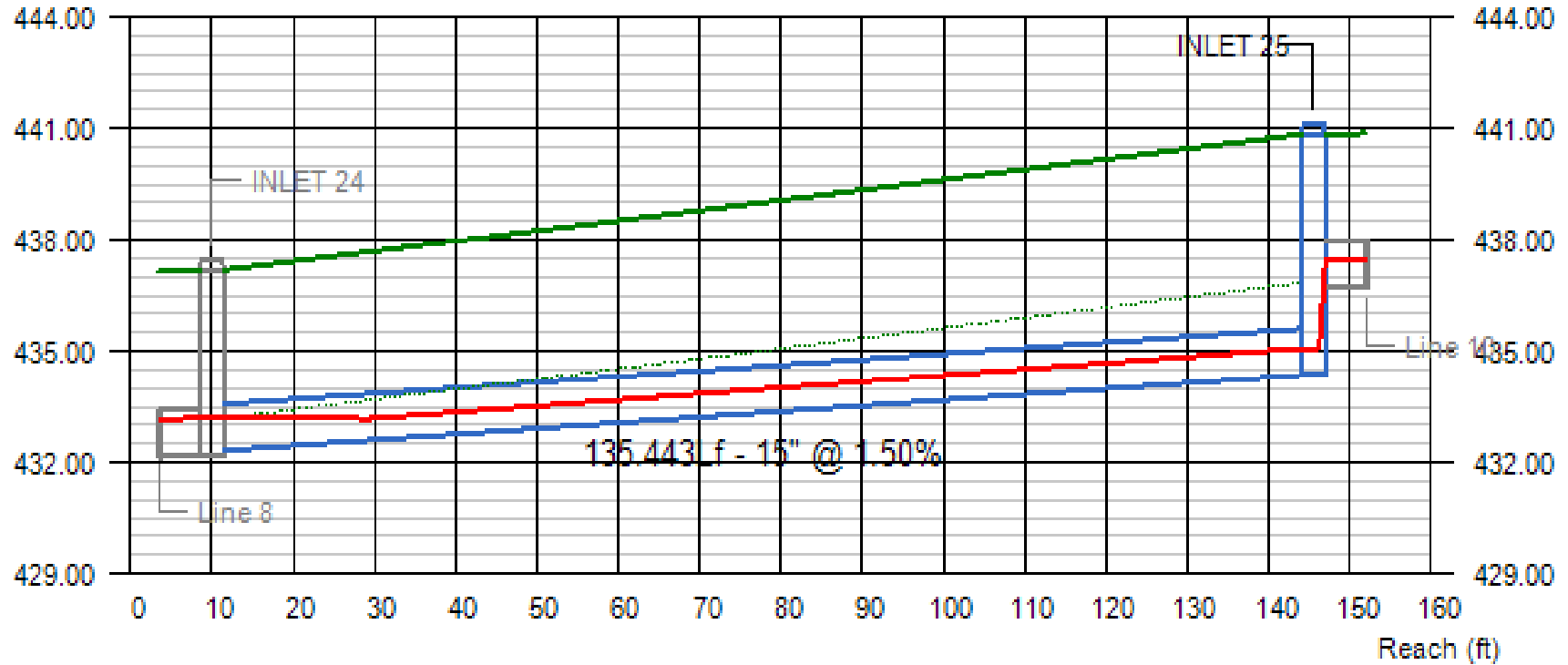
Project File:

No. Lines: 30

Run Date: 2/12/2021

Line 9 - INLET 25 OUTLET

Elev (ft)



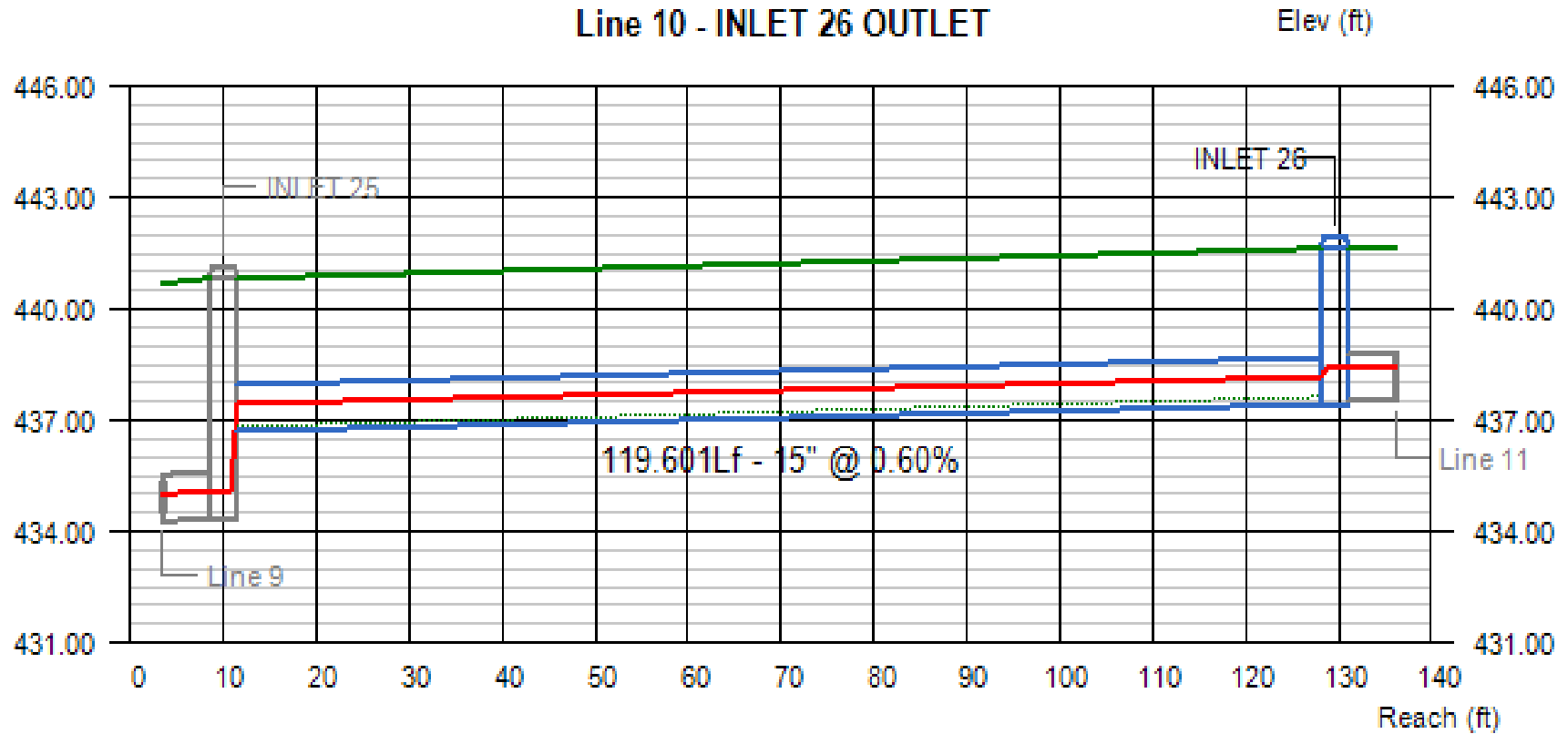
Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
9	3.23	432.32	434.35	0.89	0.72	0.72	433.21	435.07 j	435.07	3.44	4.39	3.61	5.23

Project File:

No. Lines: 30

Run Date: 2/12/2021

Line Profile (Line 10) - INLET 26 OUTLET

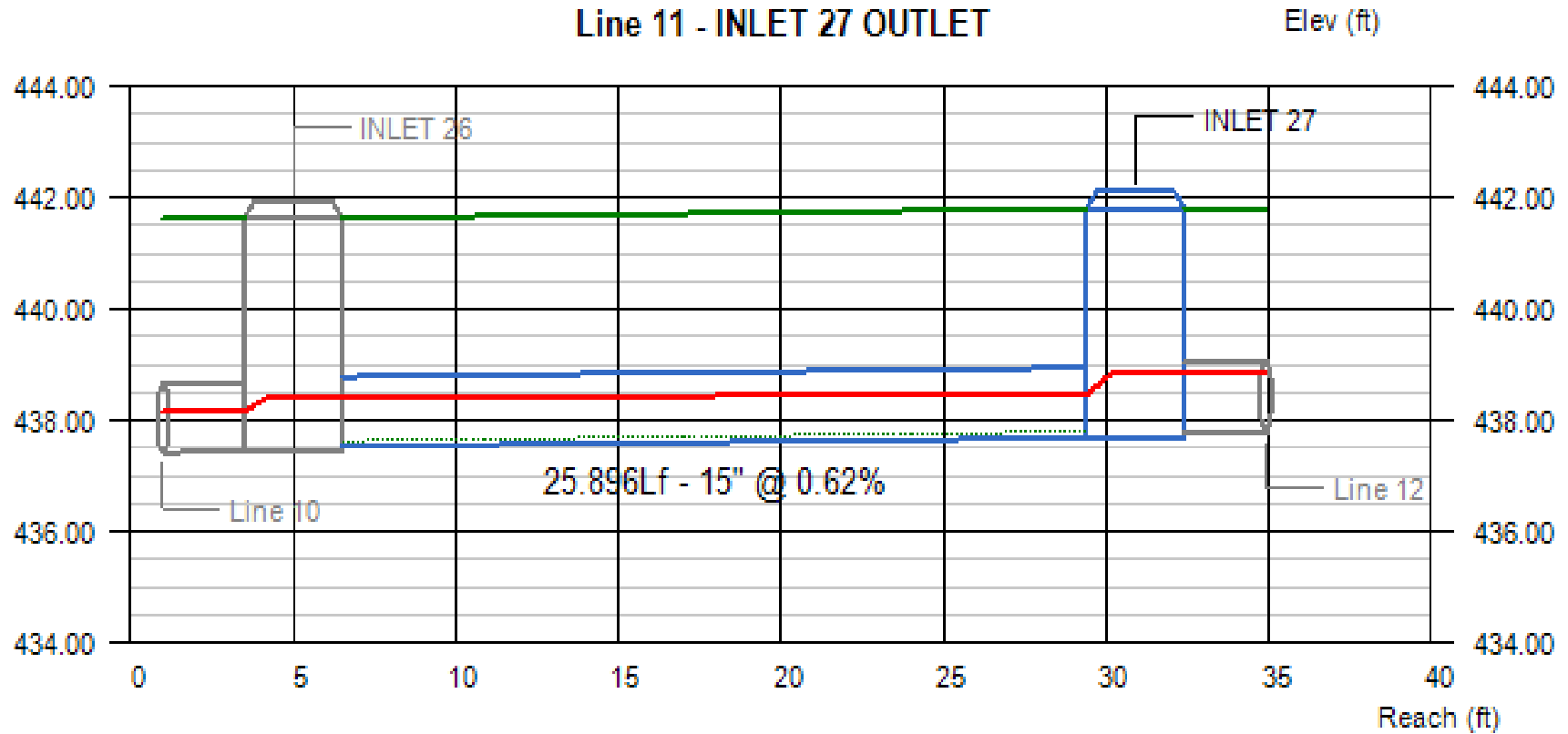


Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
10	3.26	436.71	437.43	0.74	0.73	0.99	437.45	438.16	438.42	4.35	4.36	2.87	2.95

Project File:

No. Lines: 30

Run Date: 2/12/2021



Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
11	3.22	437.53	437.69	0.89	0.77	1.14	438.42	438.46	438.83	3.43	4.07	2.85	2.86

Project File:

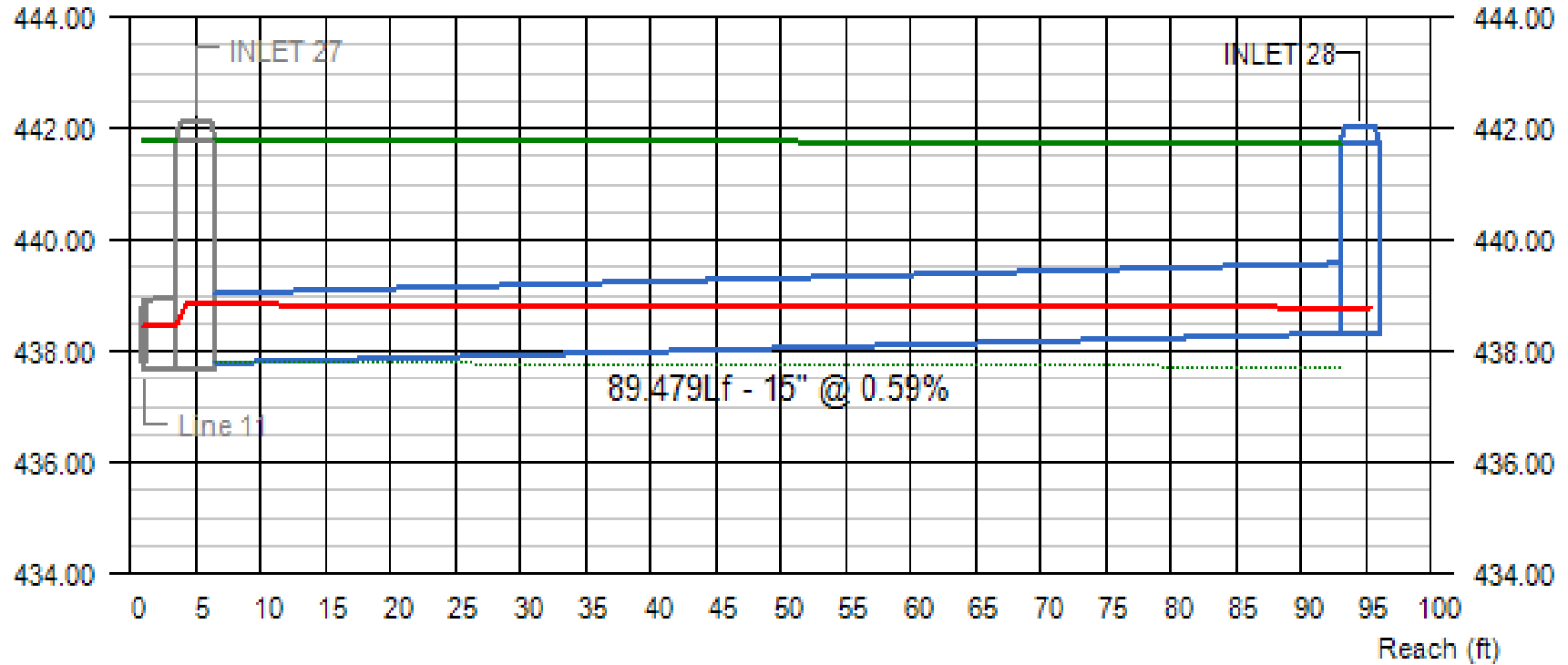
No. Lines: 30

Run Date: 2/12/2021

Line Profile (Line 12) - INLET 28 OUTLET

Line 12 - INLET 28 OUTLET

Elev (ft)



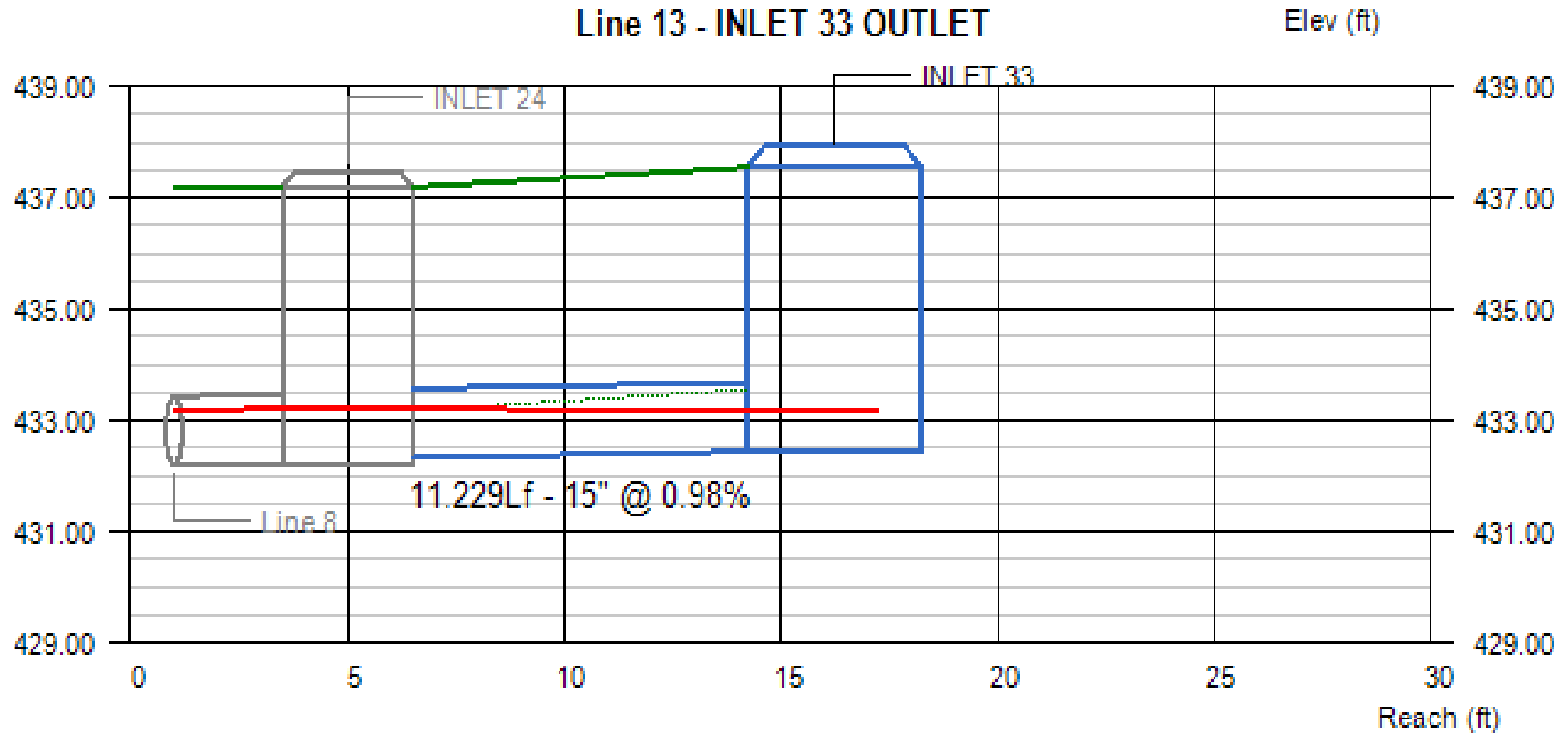
Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
12	1.36	437.79	438.32	1.04	0.46	0.46	438.83	438.78	438.78	1.24	3.31	2.76	2.15

Project File:

No. Lines: 30

Run Date: 2/12/2021

Line Profile (Line 13) - INLET 33 OUTLET



Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
13	3.26	432.32	432.43	0.89	0.73	0.73	433.21	433.16	433.16	3.48	4.40	3.61	3.87

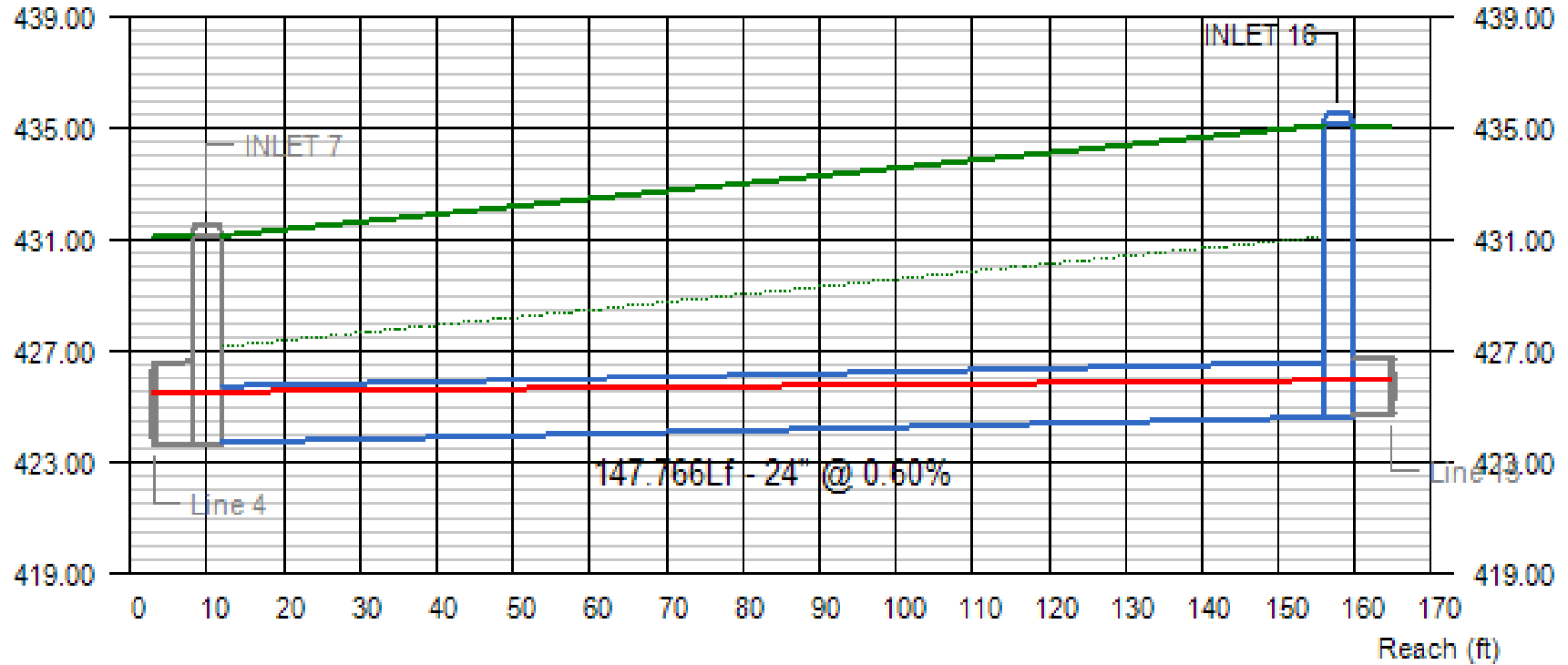
Project File:

No. Lines: 30

Run Date: 2/12/2021

Line 14 - INLET 16 OUTLET

Elev (ft)



Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
14	13.80	423.72	424.61	1.80	1.34	1.34	425.52	425.95	425.95	4.63	6.18	5.44	8.49

Project File:

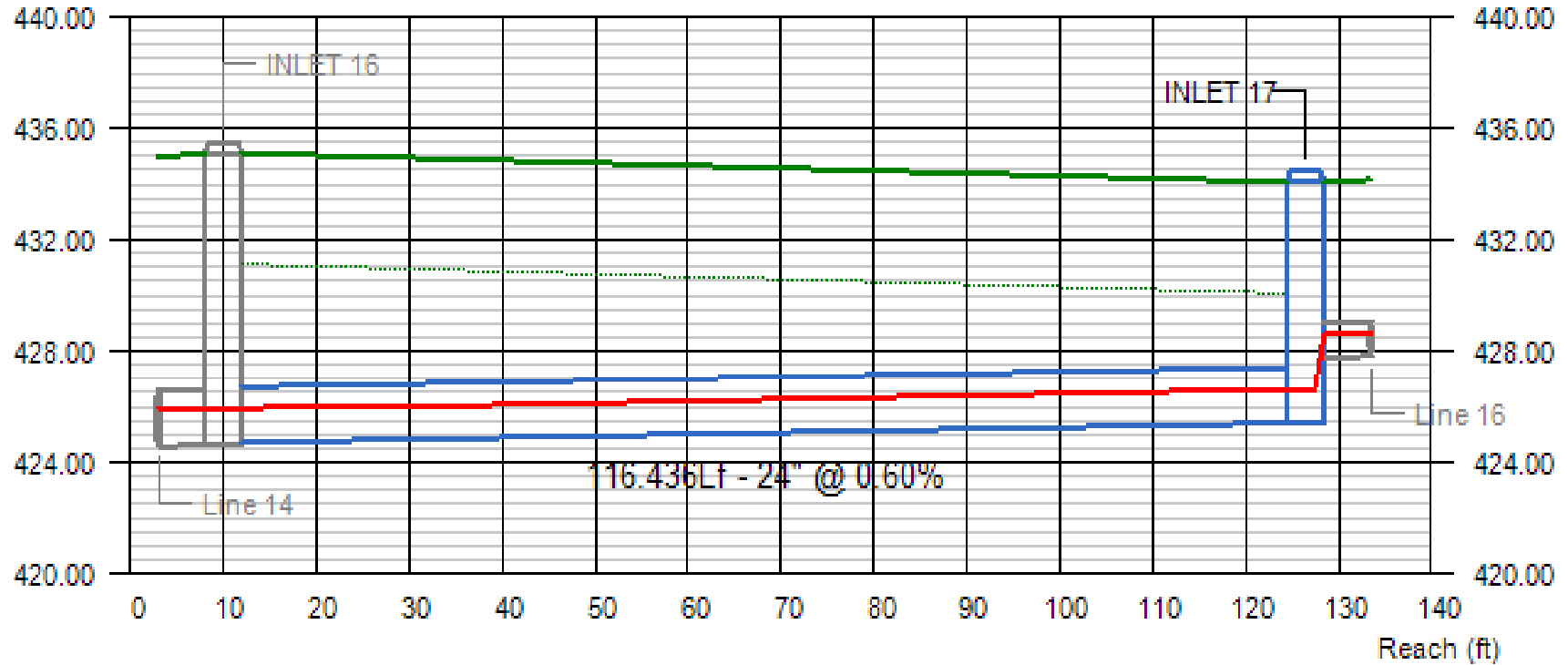
No. Lines: 30

Run Date: 2/12/2021

Line Profile (Line 15) - INLET 17 OUTLET

Line 15 - INLET 17 OUTLET

Elev (ft)



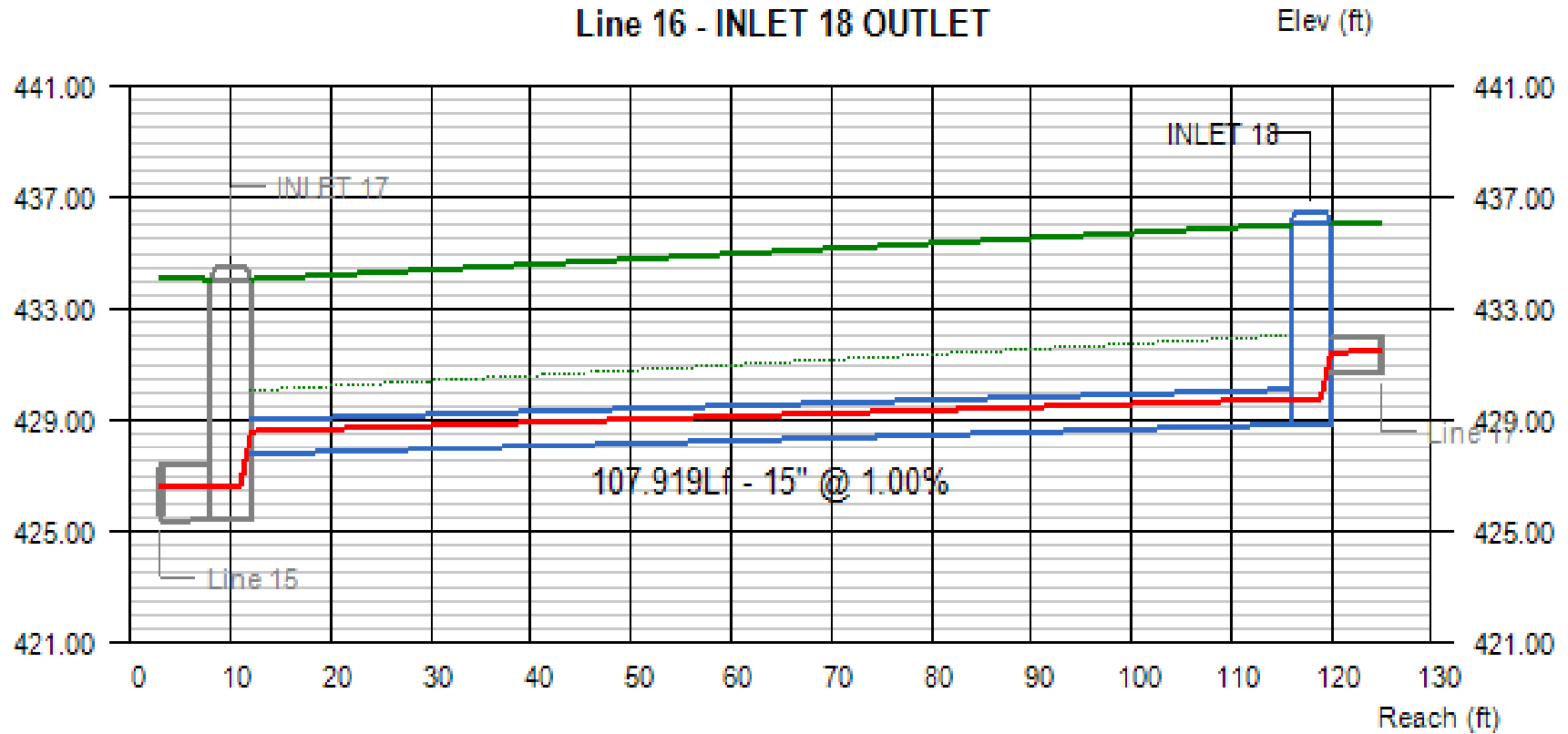
Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
15	11.54	424.71	425.41	1.24	1.22	1.22	425.95	426.63 j	426.63	5.66	5.76	8.39	6.66

Project File:

No. Lines: 30

Run Date: 2/12/2021

Line Profile (Line 16) - INLET 18 OUTLET



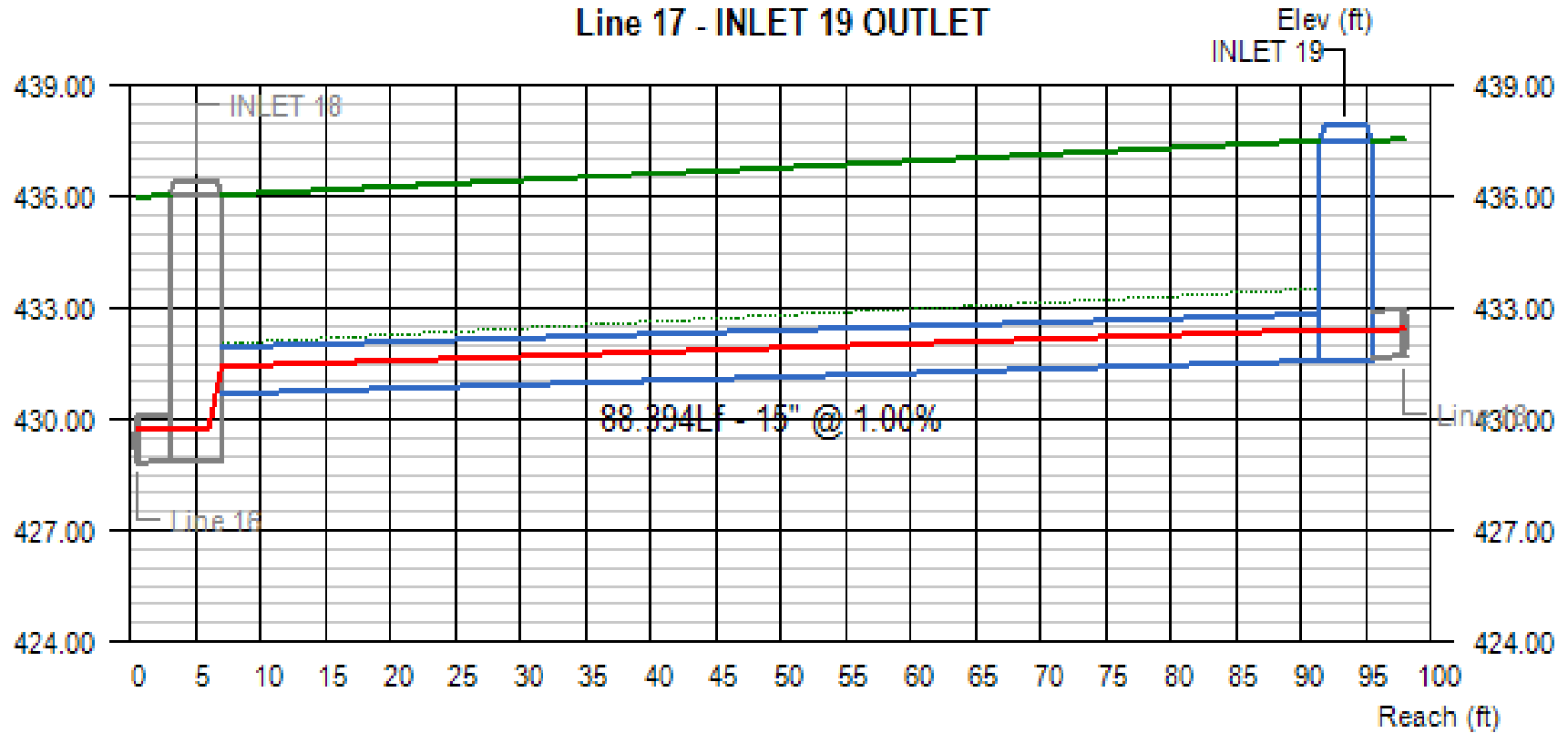
Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
16	5.12	427.77	428.85	0.84	0.92	0.92	428.61	429.77	429.77	5.84	5.31	5.05	5.93

Project File:

No. Lines: 30

Run Date: 2/12/2021

Line 17 - INLET 19 OUTLET



Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
17	4.18	430.69	431.57	0.73	0.83	0.83	431.42	432.40	432.40	5.58	4.85	4.09	4.70

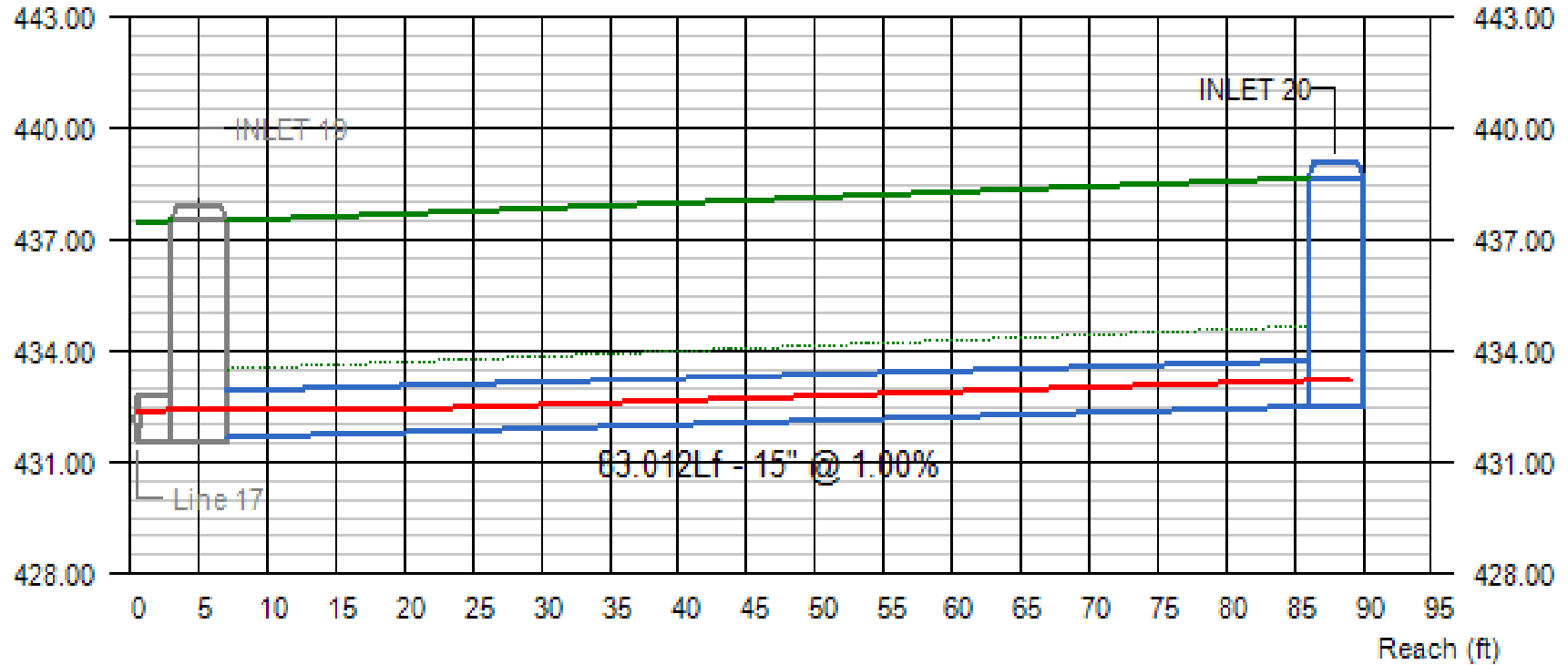
Project File:

No. Lines: 30

Run Date: 2/12/2021

Line 18 - INLET 20 OUTLET

Elev (ft)



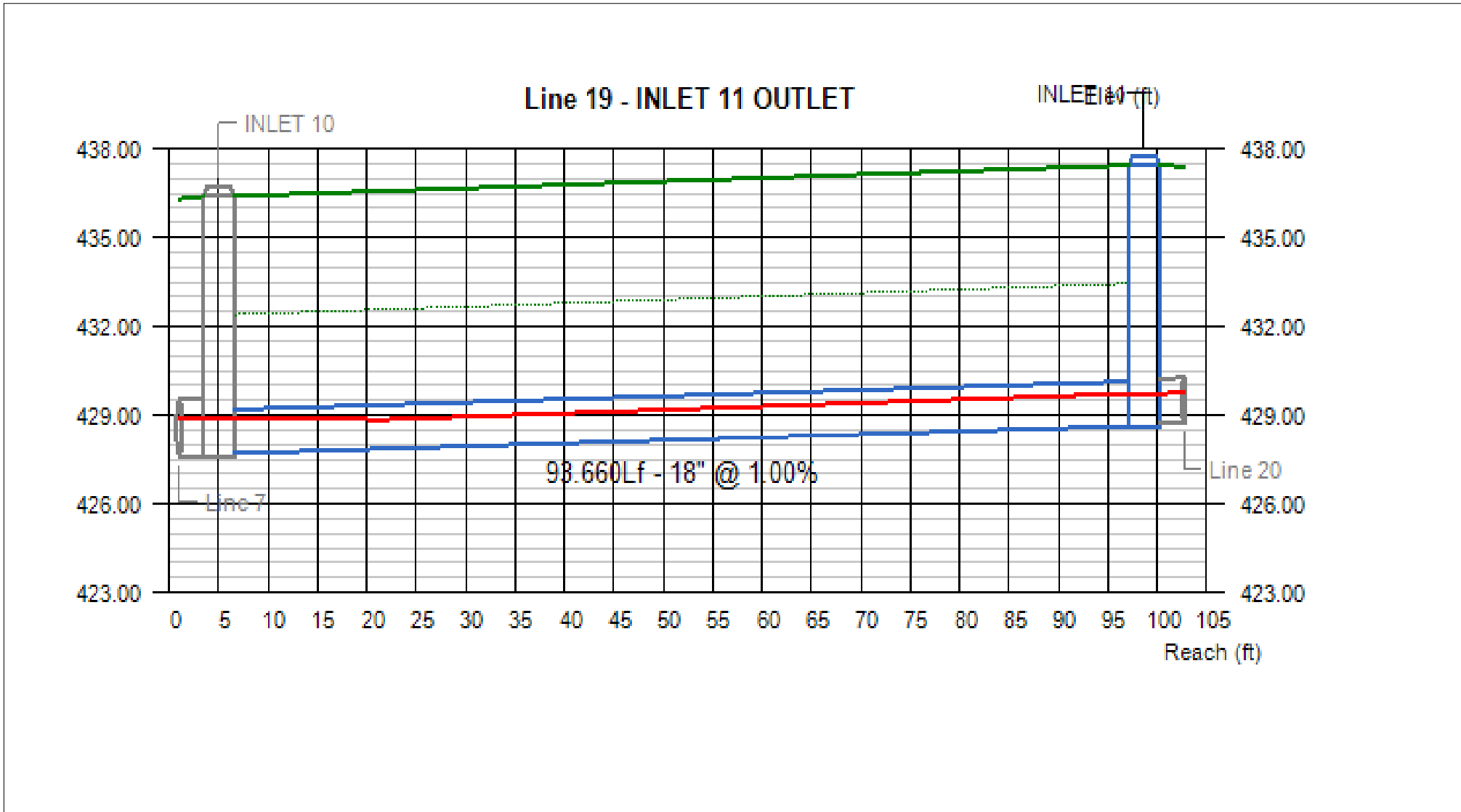
Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
18	3.05	431.67	432.50	0.73	0.70	0.70	432.40	433.20 j	433.20	4.12	4.30	4.60	4.92

Project File:

No. Lines: 30

Run Date: 2/12/2021

Line Profile (Line 19) - INLET 11 OUTLET

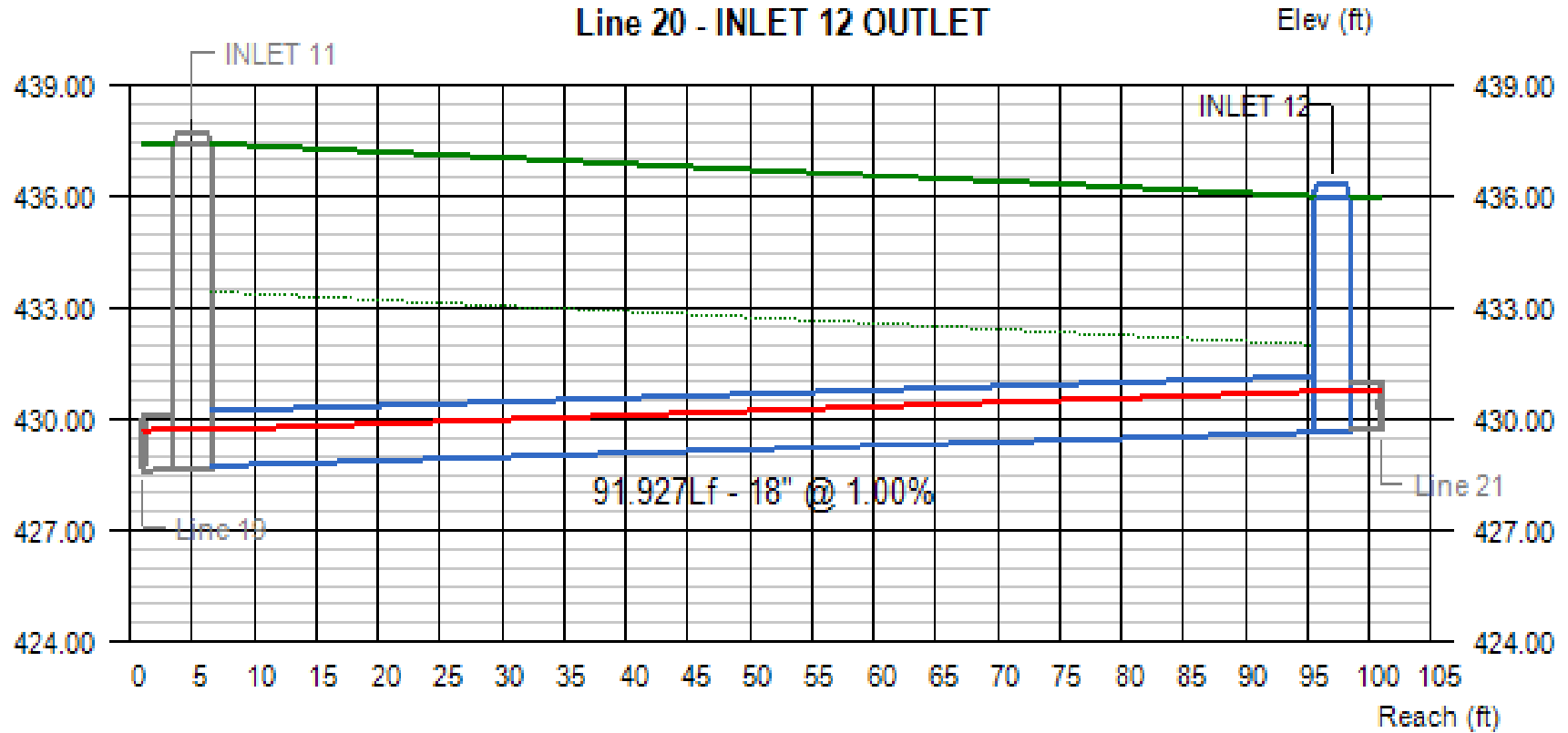


Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
19	8.03	427.69	428.63	1.21	1.10	1.10	428.90	429.73 j	429.73	5.25	5.80	7.21	7.31

Project File: _____ No. Lines: 30 Run Date: 2/12/2021

Line Profile (Line 20) - INLET 12 OUTLET

Line 20 - INLET 12 OUTLET



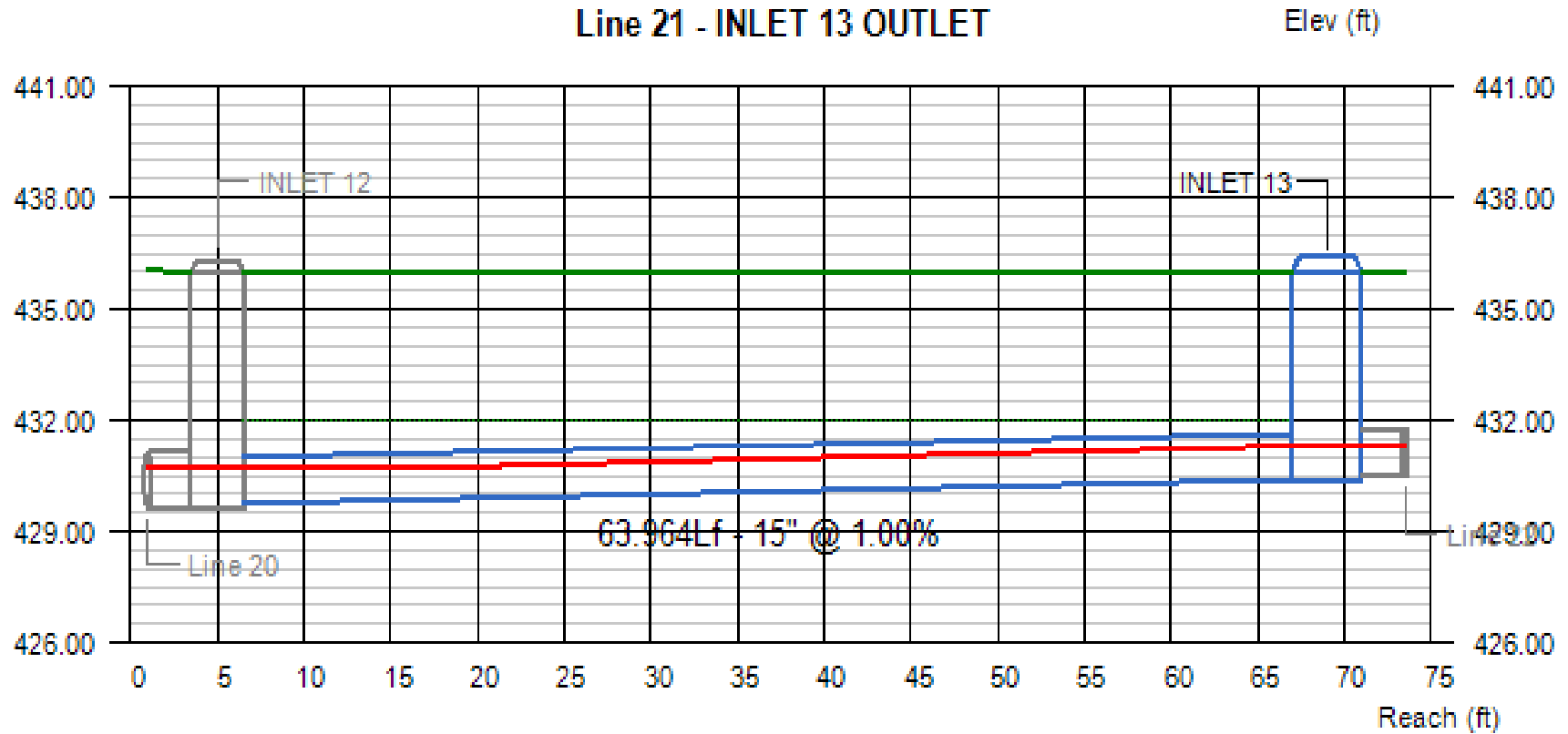
Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
20	8.08	428.73	429.65	1.00	1.10	1.10	429.73	430.75	430.75	6.48	5.82	7.21	4.85

Project File:

No. Lines: 30

Run Date: 2/12/2021

Line Profile (Line 21) - INLET 13 OUTLET



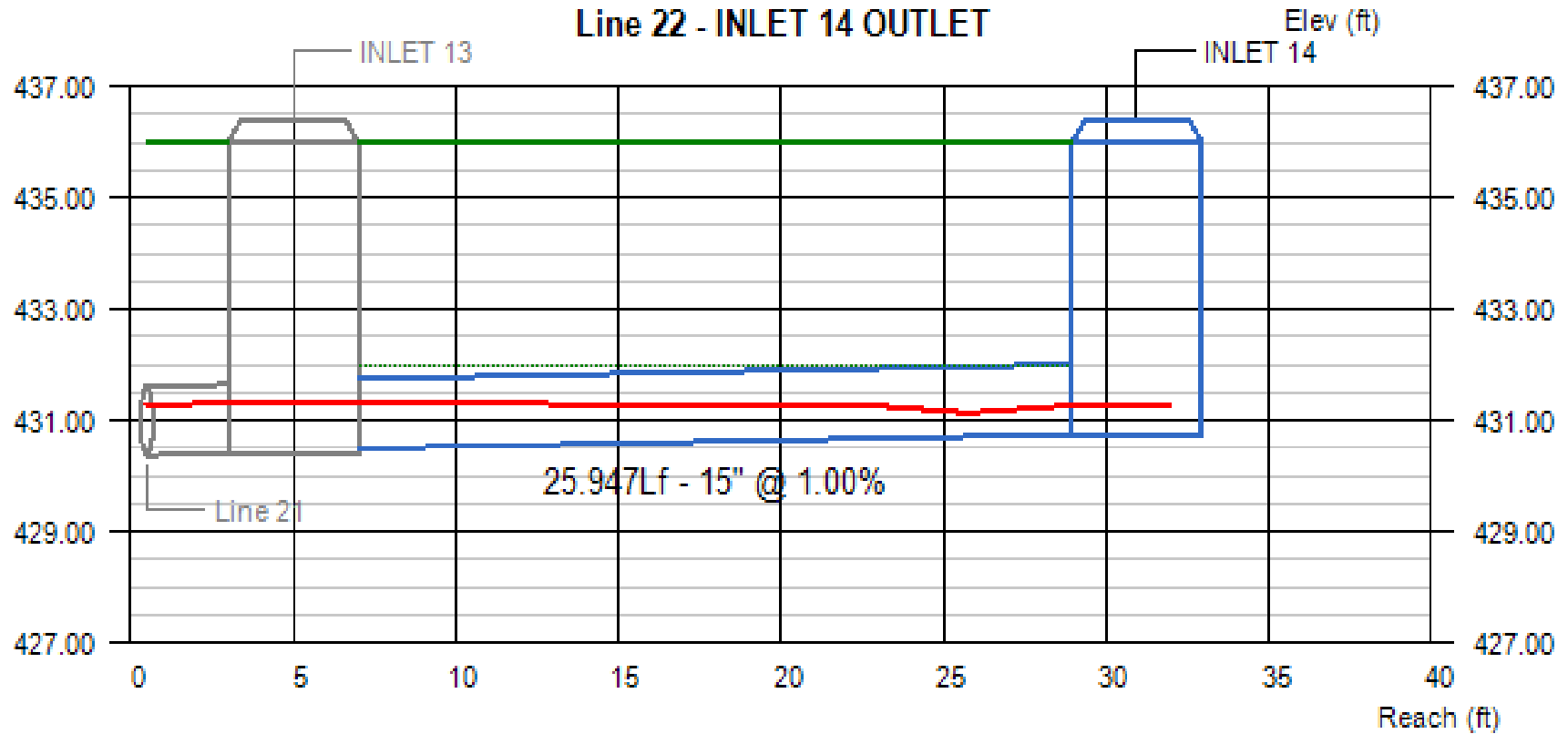
Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
21	5.10	429.75	430.39	1.00	0.92	0.92	430.75	431.31 j	431.31	4.85	5.30	5.00	4.36

Project File:

No. Lines: 30

Run Date: 2/12/2021

Line Profile (Line 22) - INLET 14 OUTLET



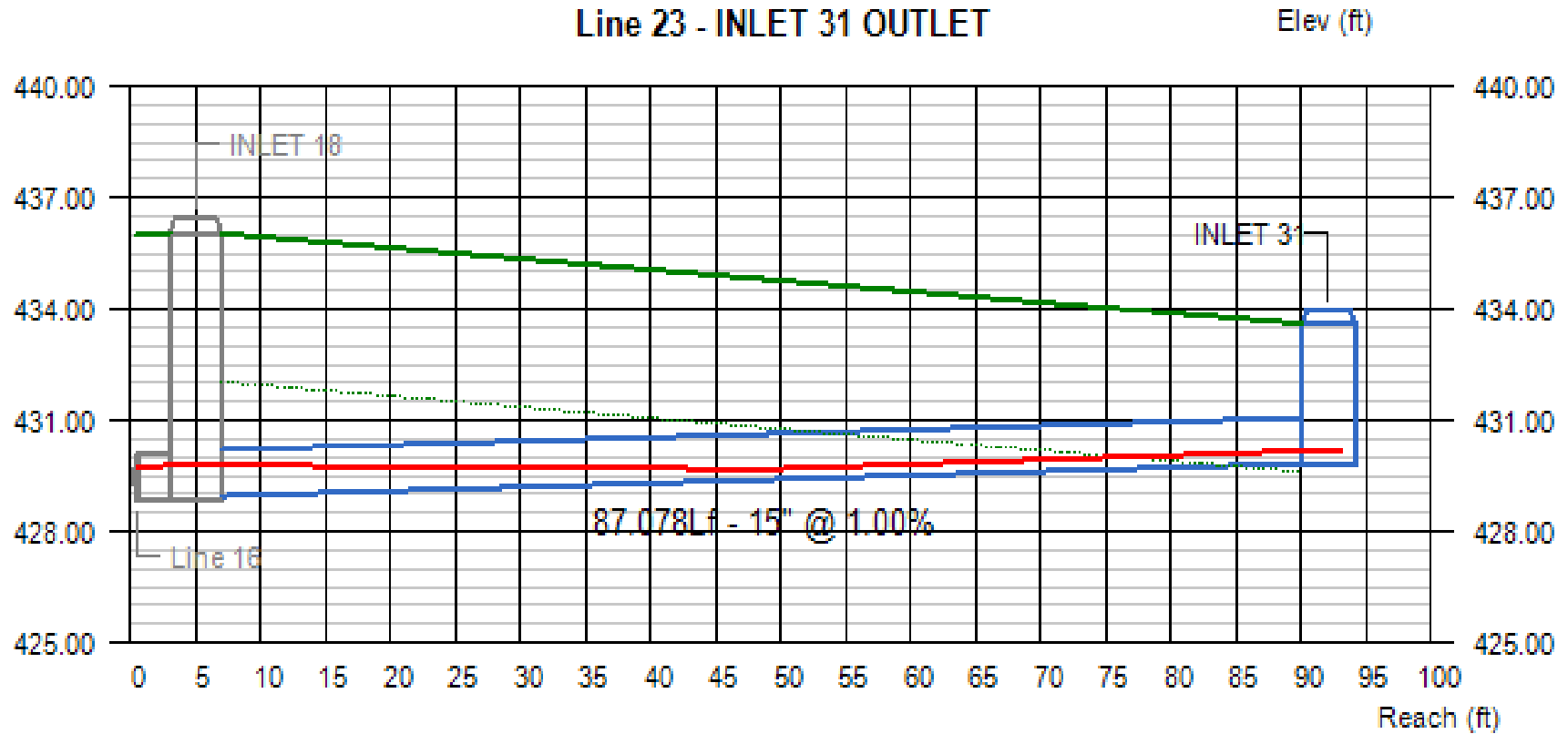
Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
22	1.72	430.49	430.75	0.82	0.52	0.52	431.31	431.27 j	431.27	2.04	3.56	4.26	4.00

Project File:

No. Lines: 30

Run Date: 2/12/2021

Line Profile (Line 23) - INLET 31 OUTLET



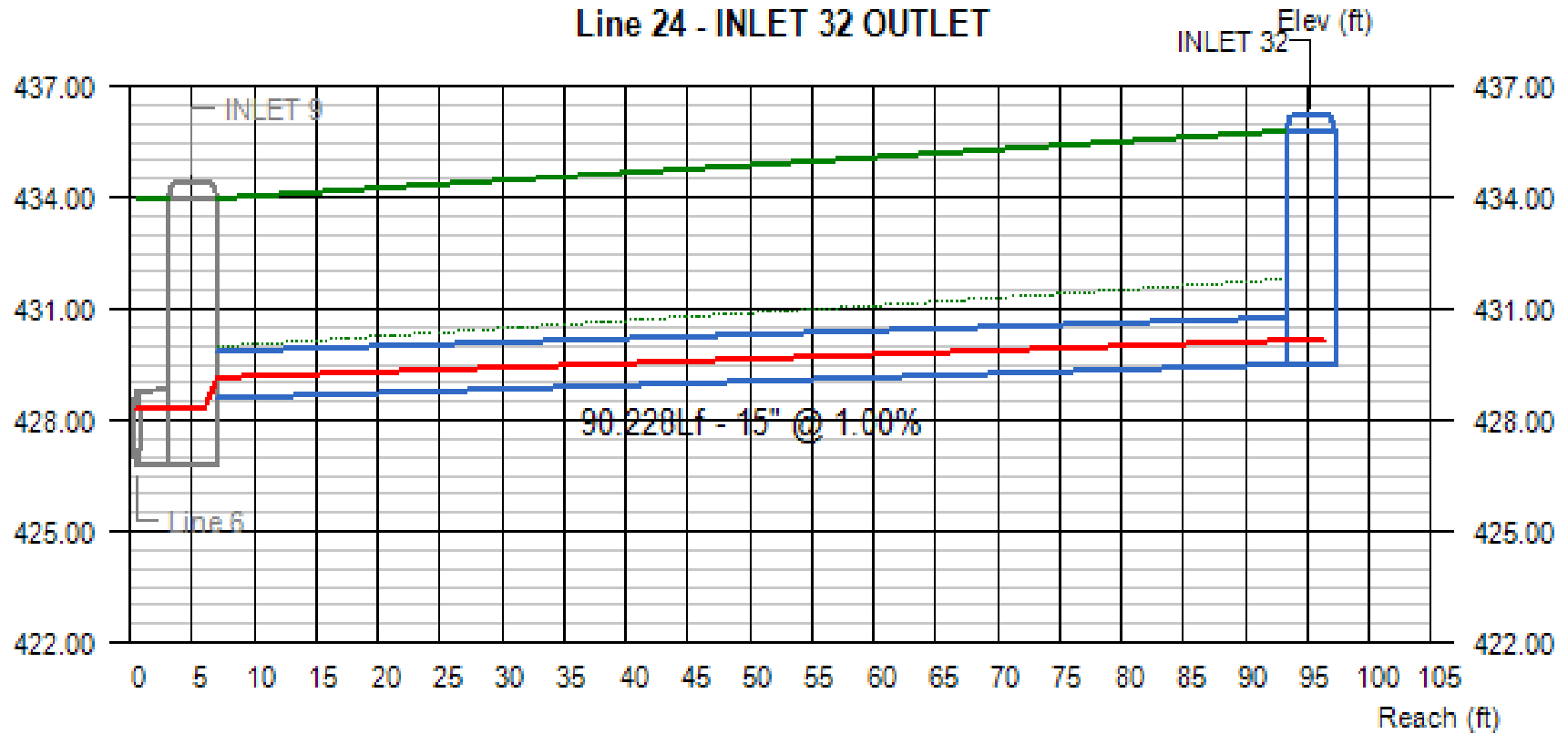
Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
23	0.78	428.95	429.82	0.82	0.34	0.34	429.77	430.16 j	430.16	0.91	2.82	5.83	2.52

Project File:

No. Lines: 30

Run Date: 2/12/2021

Line Profile (Line 24) - INLET 32 OUTLET

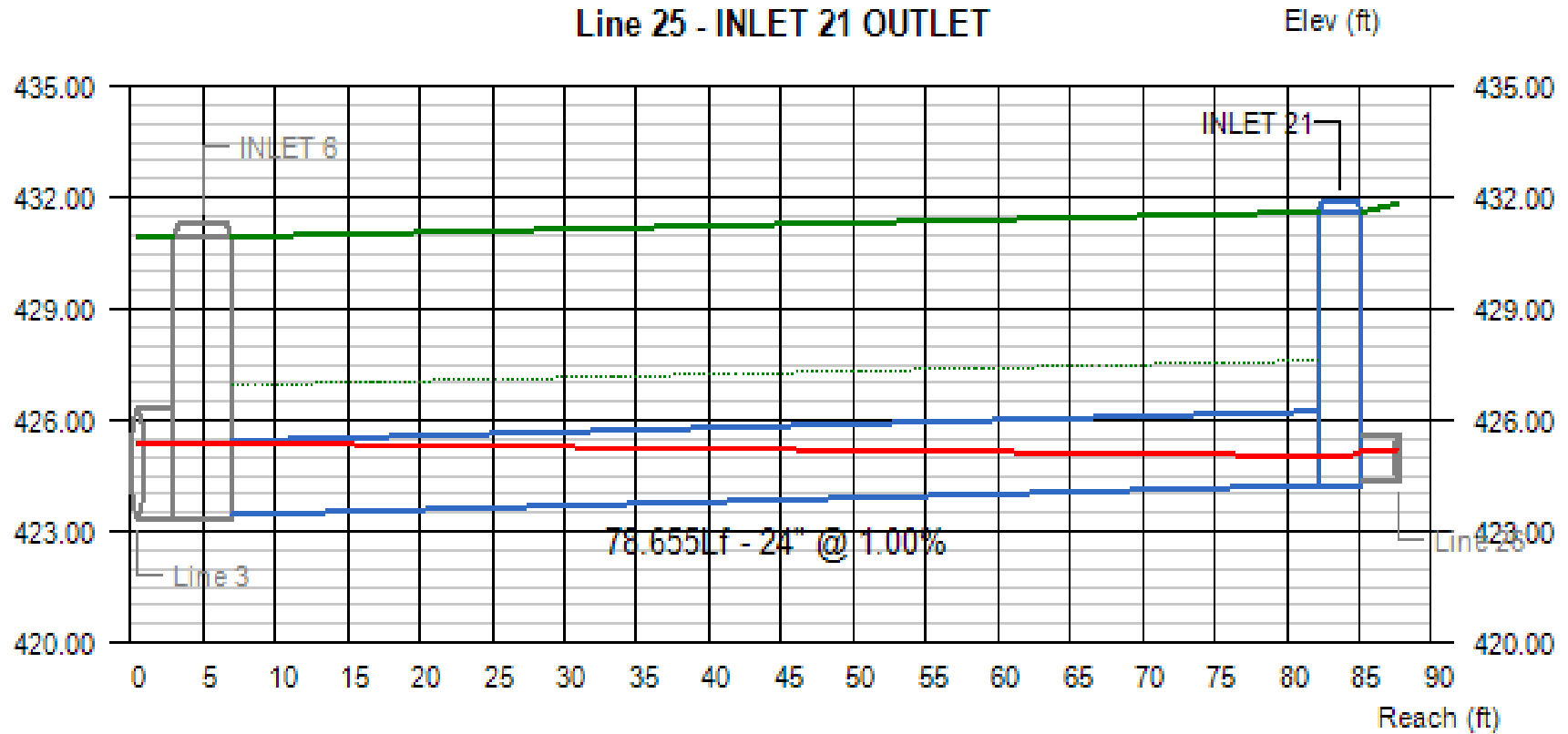


Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
24	2.59	428.60	429.50	0.55	0.64	0.64	429.15	430.14	430.14	4.96	4.06	4.12	5.05

Project File:

No. Lines: 30

Run Date: 2/12/2021



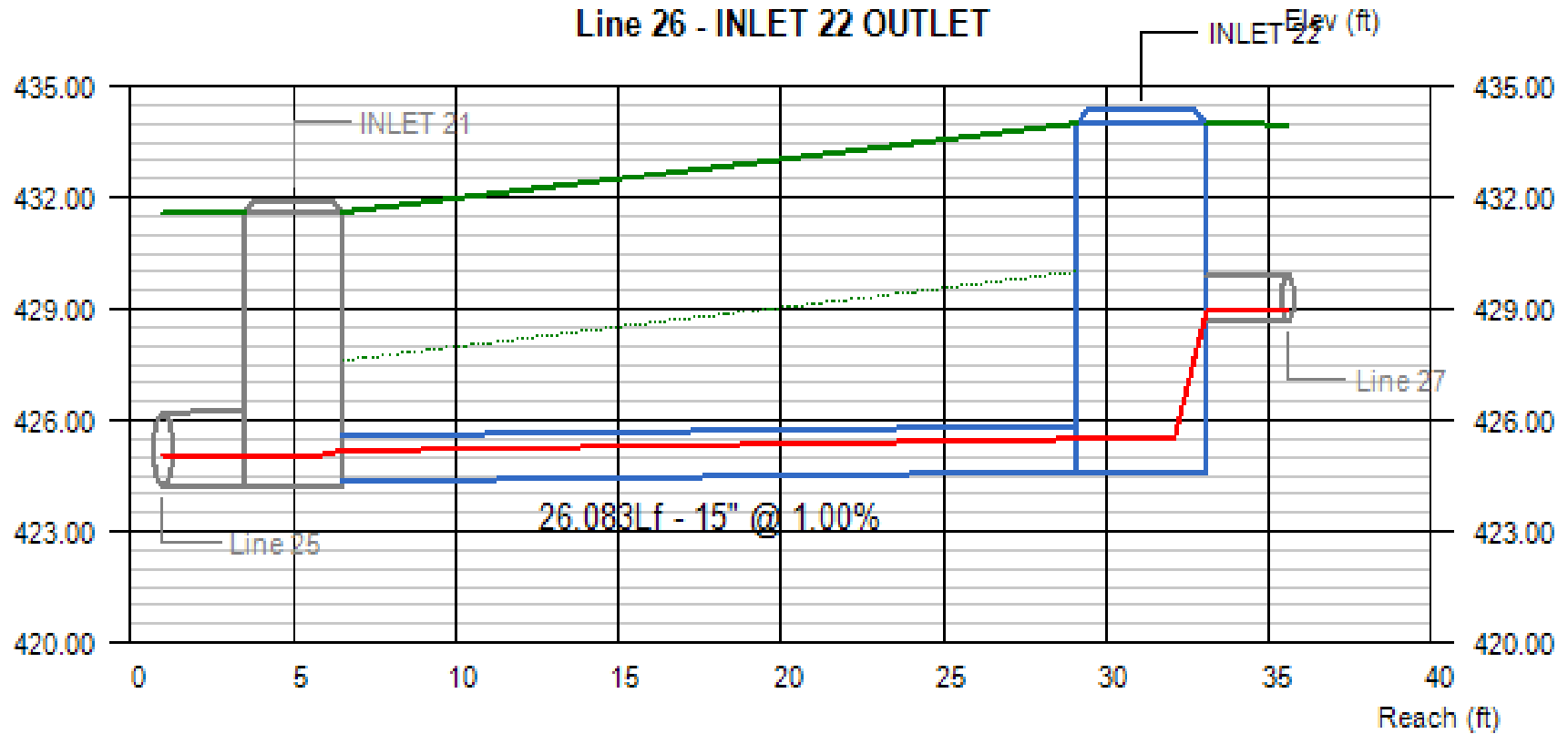
Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
25	4.99	423.45	424.24	1.93	0.79	0.79	425.38	425.03	425.03	1.60	4.35	5.49	5.36

Project File:

No. Lines: 30

Run Date: 2/12/2021

Line Profile (Line 26) - INLET 22 OUTLET



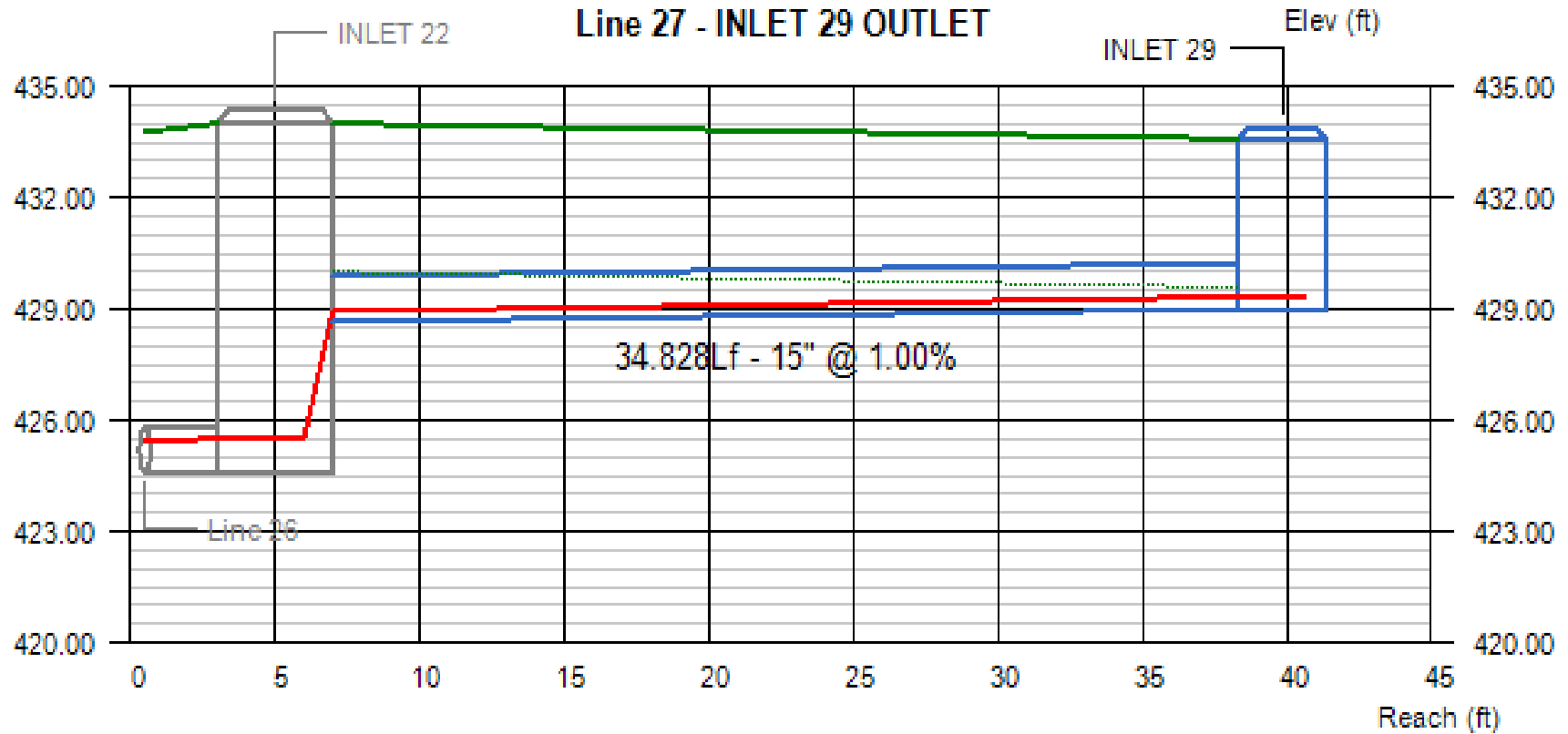
Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
26	4.94	424.34	424.60	0.82	0.90	0.90	425.16	425.50	425.50	5.79	5.22	6.01	8.15

Project File:

No. Lines: 30

Run Date: 2/12/2021

Line Profile (Line 27) - INLET 29 OUTLET



Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
27	0.77	428.64	428.99	0.29	0.34	0.34	428.93	429.33	429.33	3.54	2.81	4.11	3.35

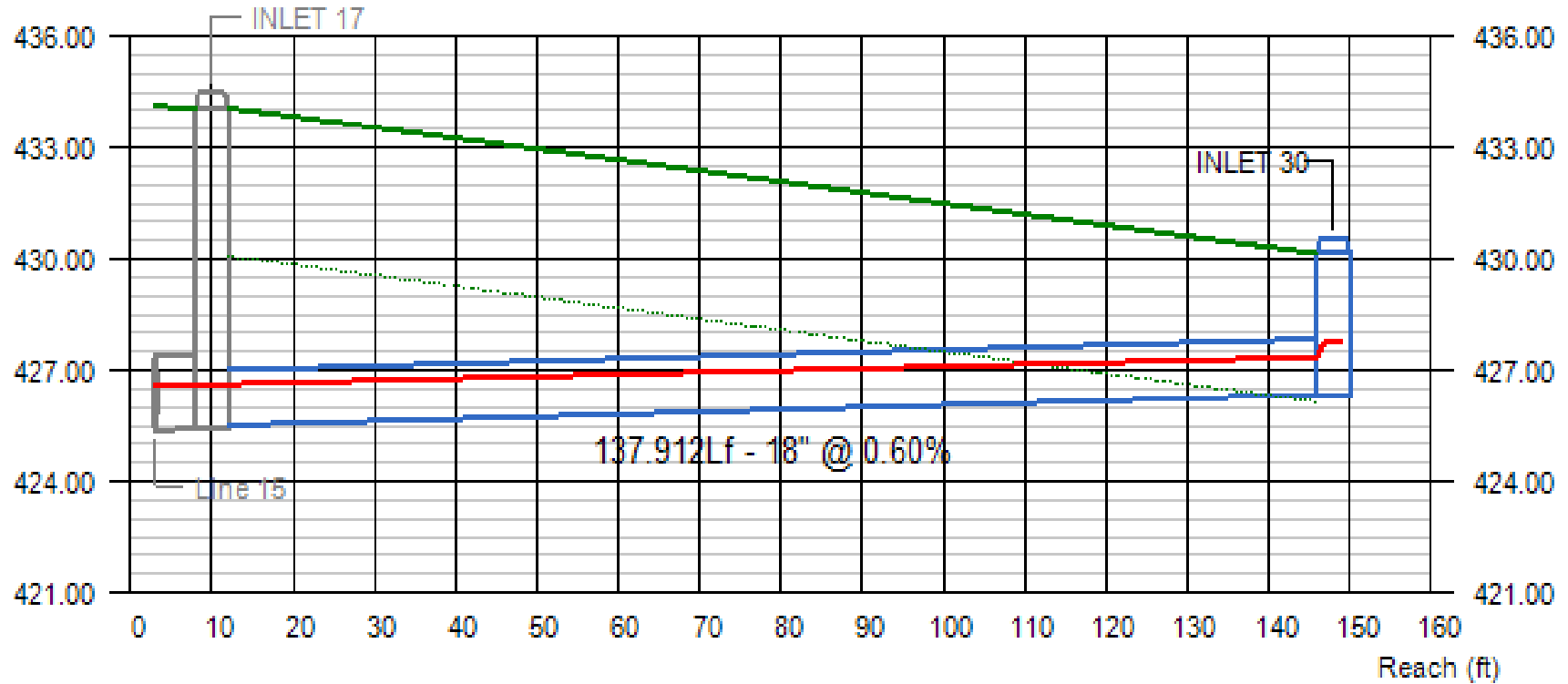
Project File:

No. Lines: 30

Run Date: 2/12/2021

Line 28 - INLET 30 OUTLET

Elev (ft)

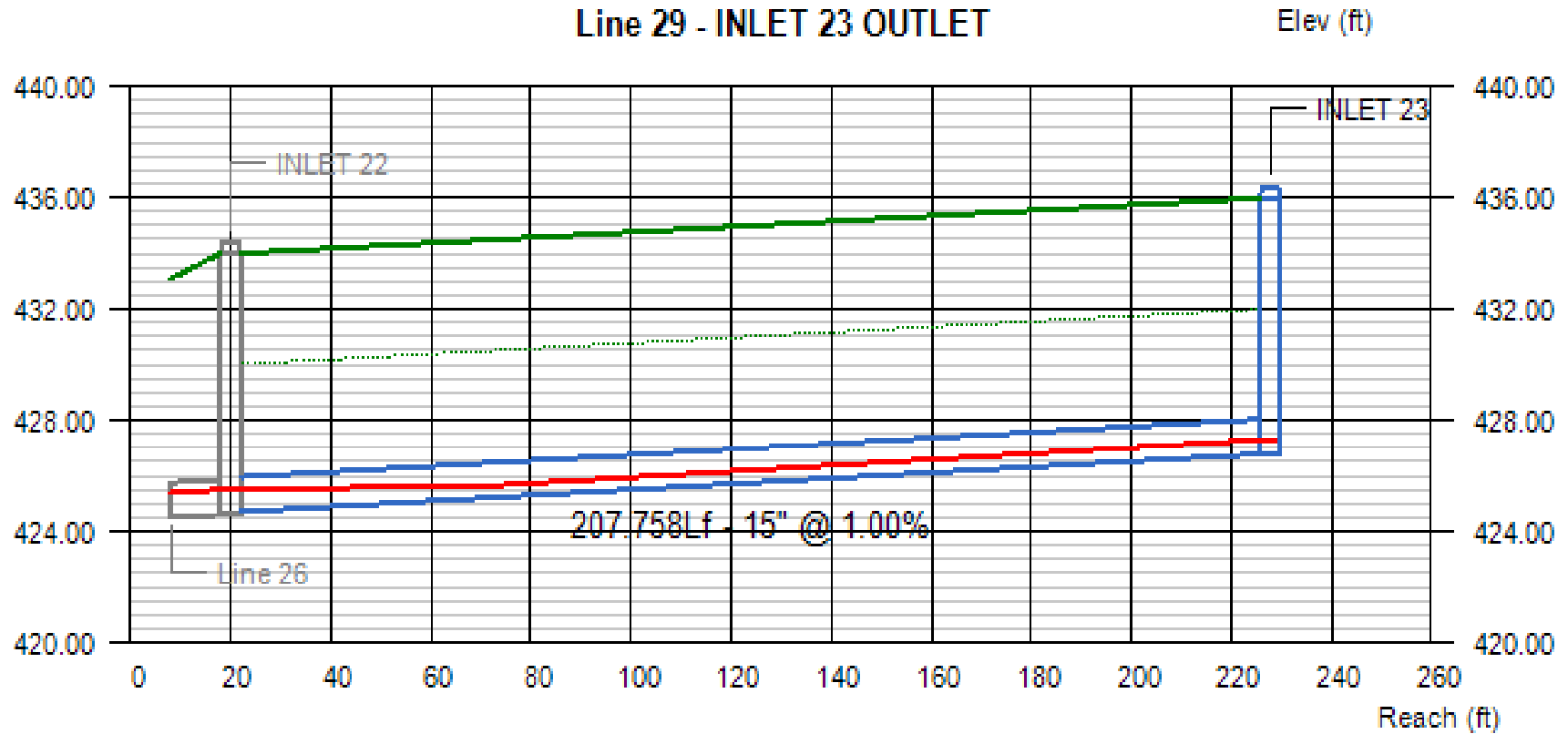


Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
28	6.81	425.51	426.34	1.12	1.01	1.46	426.63	427.35	427.80	4.82	5.37	7.06	2.31

Project File:

No. Lines: 30

Run Date: 2/12/2021

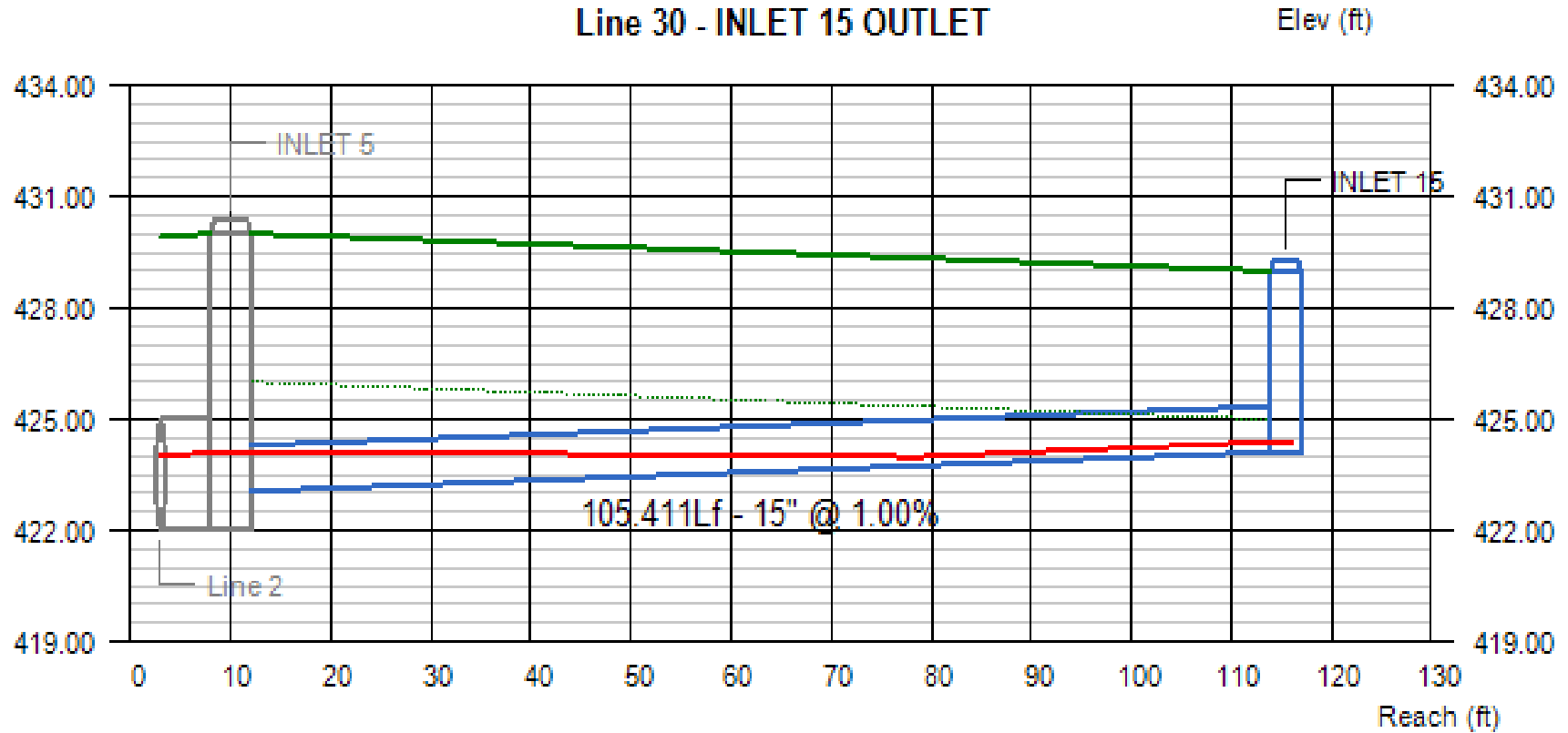


Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
29	1.66	424.70	426.78	0.80	0.51	0.51	425.50	427.29 j	427.29	1.99	3.52	8.05	7.94

Project File:

No. Lines: 30

Run Date: 2/12/2021



Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
30	0.58	423.05	424.10	1.02	0.30	0.30	424.07	424.40 j	424.40	0.55	2.61	5.70	3.65

Project File:

No. Lines: 30

Run Date: 2/12/2021

APPENDIX

**PRE-DEVELOPMENT DRAINAGE AREA MAP
POST-DEVELOPMENT DRAINAGE AREA MAP**

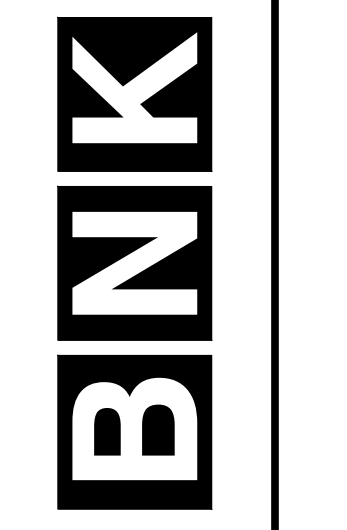
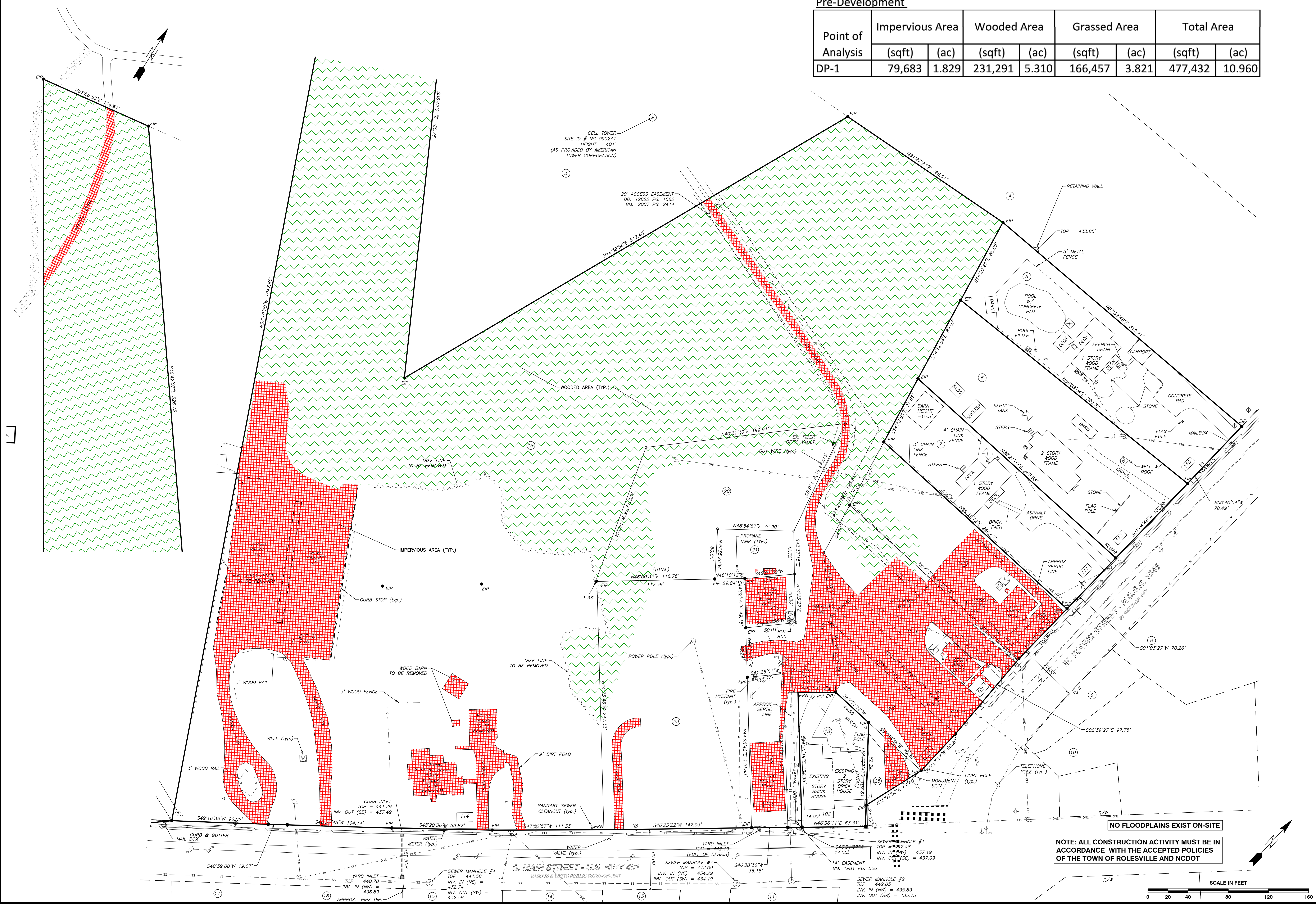
USGS MAP

FIRMETTE MAP

NOAA RAIN DATA

Pre-Development

Point of Analysis	Impervious Area		Wooded Area		Grassed Area		Total Area	
	(sqft)	(ac)	(sqft)	(ac)	(sqft)	(ac)	(sqft)	(ac)
DP-1	79,683	1.829	231,291	5.310	166,457	3.821	477,432	10.960



BASS, NIXON & KENNEDY, INC.
CONSULTING ENGINEERS
 6310 CHAPEL HILL ROAD, SUITE 250, RALEIGH, NC 27607
 TELEPHONE: (919) 851-1122 FAX: (919) 851-6888
 CERTIFICATION NUMBERS: NCBELS (C-0110); NCBOLA (C-0267)

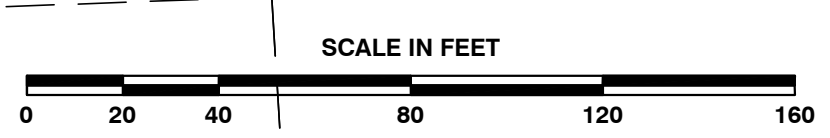
NO.	DATE	DESCRIPTION	BY

COBBLESTONE VILLAGE
MIXED USE DEVELOPMENT
 TOWN OF ROLESVILLE, WAKE COUNTY, NORTH CAROLINA

03-18881 PROGRESS RAB DATE DRAWN BY
 PRE-DEVELOPMENT DRAINAGE MAP
 SCALE: 1" = 40' CHK BY: MDB

R:\2019\19187 - Rolesville Town Center\CIVIL\04 Construction\40 - 19187_Drainage Maps.dwg, PRE DA MAP, 2/5/2021 12:23:25 PM, marc.muehler

NOTE: ALL CONSTRUCTION ACTIVITY MUST BE IN ACCORDANCE WITH THE ACCEPTED POLICIES OF THE TOWN OF ROLESVILLE AND NCDOT

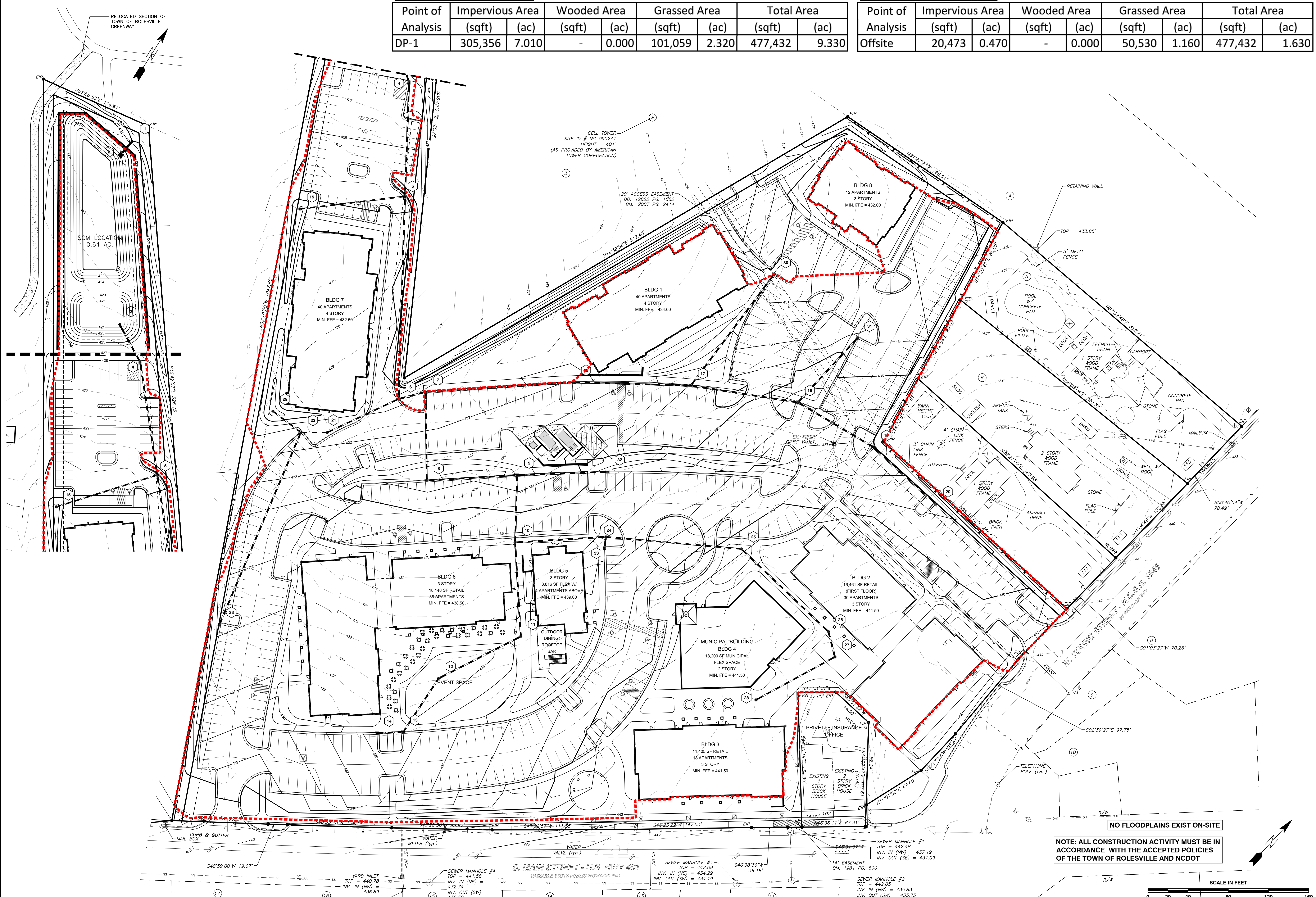


Post-Development - to SCM

Point of Analysis	Impervious Area		Wooded Area		Grassed Area		Total Area	
	(sqft)	(ac)	(sqft)	(ac)	(sqft)	(ac)	(sqft)	(ac)
DP-1	305,356	7.010	-	0.000	101,059	2.320	477,432	9.330

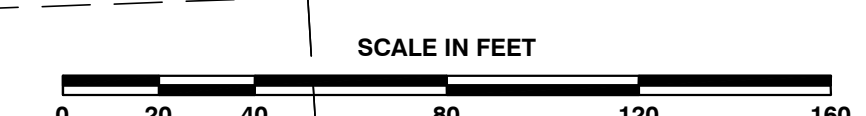
Post-Development - Bypass

Point of Analysis	Impervious Area		Wooded Area		Grassed Area		Total Area	
	(sqft)	(ac)	(sqft)	(ac)	(sqft)	(ac)	(sqft)	(ac)
Offsite	20,473	0.470	-	0.000	50,530	1.160	477,432	1.630



NOTE: ALL CONSTRUCTION ACTIVITY MUST BE IN ACCORDANCE WITH THE ACCEPTED POLICIES OF THE TOWN OF ROLESVILLE AND NCDOT

NO FLOODPLAINS EXIST ON-SITE



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 TELEPHONE: (919) 881-1122 FAX: (919) 881-8686
 CERTIFICATION NUMBERS: NCBELS (C-0110); NCBOLA (C-0267)

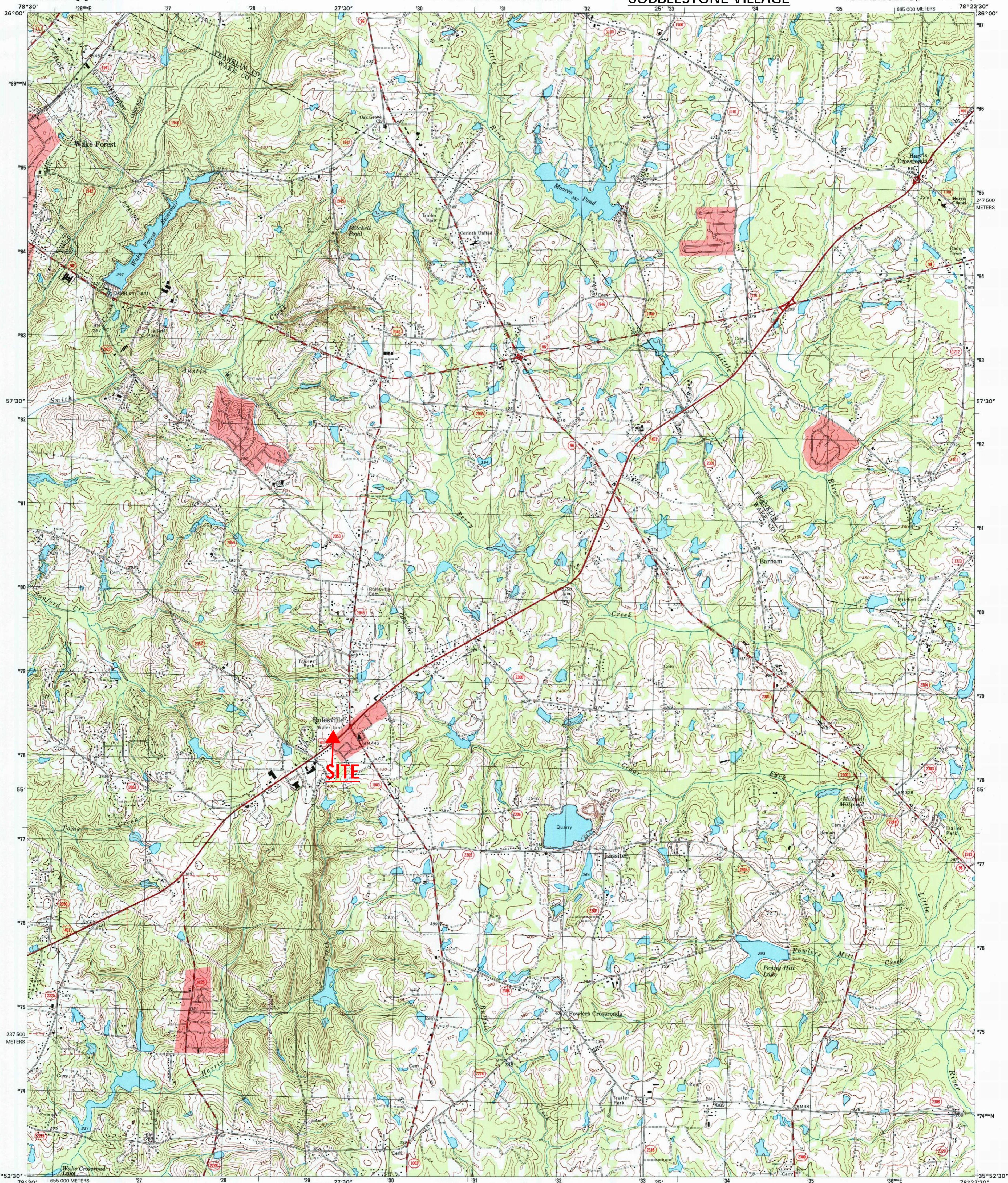
NO.	DATE	DESCRIPTION	BY

03-18881 PROGRESS RAB
 JOB NO. DATE DRAWN BY
POST-DEVELOPMENT DRAINAGE MAP
 SCALE: 1" = 40'
 CHK BY: MDB

COBBLESTONE VILLAGE
MIXED USE DEVELOPMENT
 TOWN OF ROLESVILLE, WAKE COUNTY, NORTH CAROLINA

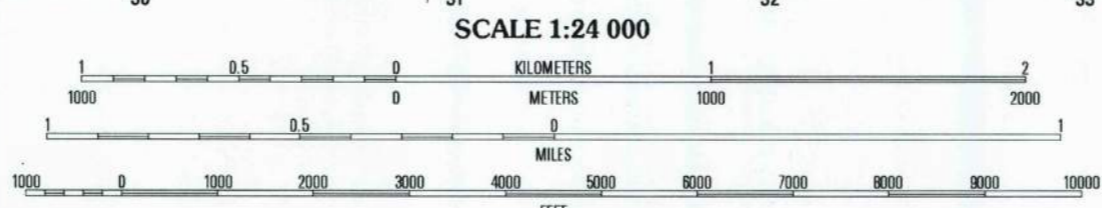
R:\2019\19187 - Rolesville Town Center\CIVIL\04 Construction\40 - 19187_Drainage Maps.dwg, POST DA MAD, 2/5/2021 12:24:06 PM, mrcmcmiller

NOT RELEASED FOR CONSTRUCTION OR BID SOLICITATION



Produced by the United States Geological Survey in cooperation with the North Carolina Department of Environment and Natural Resources. Topography compiled 1964. Planimetry derived from imagery taken 1993 and other sources. Survey control current as of 1967. North American Datum of 1983 (NAD 83). Projection and 1 000-meter grid: Universal Transverse Mercator, zone 17. 2 500-meter ticks: North Carolina Coordinate System of 1983. North American Datum of 1927 (NAD 27) is shown by dashed corner ticks. The values of the shift between NAD 83 and NAD 27 for 7.5-minute intersections are obtainable from National Geodetic Survey NADCON software. Landmark buildings verified 1967.

UTM GRID AND 1999 MAGNETIC NORTH DECLINATION AT CENTER OF SHEET RECEIVED JUN 3 0 1999 USGS NMD HISTORICAL MAP ARCHIVES



ROAD CLASSIFICATION Primary highway hard surface, Secondary highway hard surface, Light-duty road, hard or improved surface, Unimproved road, Interstate Route, U.S. Route, State Route

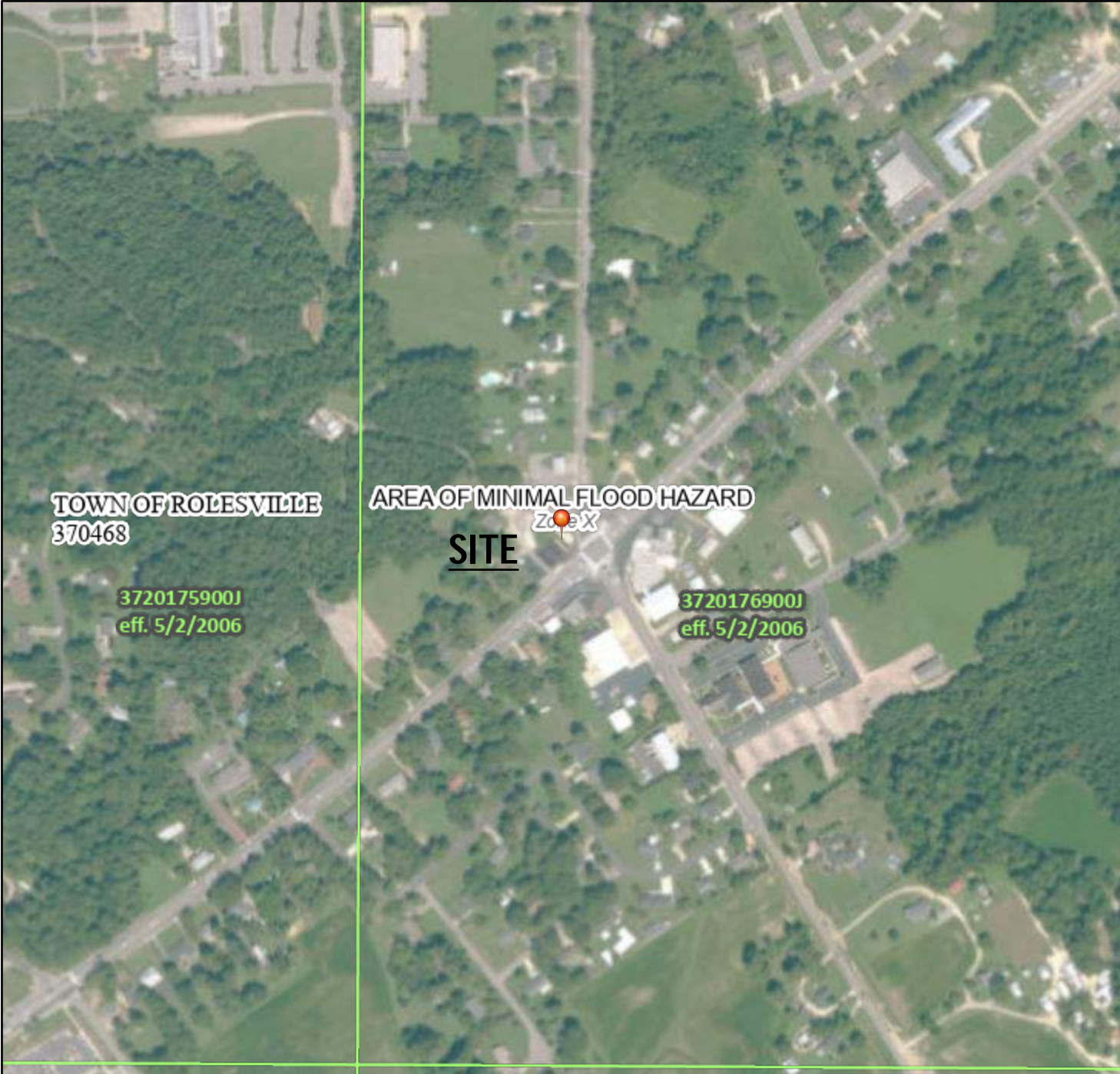
Table with 3 columns and 8 rows for adjoining 7.5' quadrangle names: 1 Glenasmole, 2 Franklinton, 3 Lenoir, 4 Wake Forest, 5 Bunn West, 6 Raleigh East, 7 Raleigh, 8 Zebulon

THIS MAP COMPLIES WITH NATIONAL MAP ACCURACY STANDARDS FOR SALE BY U.S. GEOLOGICAL SURVEY, P.O. BOX 25286, DENVER, COLORADO 80225 A FOLDER DESCRIBING TOPOGRAPHIC MAPS AND SYMBOLS IS AVAILABLE ON REQUEST

ROLESVILLE, NC 1993 NIMA 5355 IV NW-SERIES V842



ff1



FHOG

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 DFXUR WDDQJG/

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 UHOFRW FRQHV/RU DFRQVWV VEVHXQV WRWKLVDGWHDOG
 WLP 7KH%DOGHIFWLYHLQRUBMLRQBFRQHRU
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 UHKDWRUASUSRV



NOAA Atlas 14, Volume 2, Version 3
Location name: Rolesville, North Carolina, USA*
Latitude: 35.9233°, Longitude: -78.4579°
Elevation: 444.08 ft**



* source: ESRI Maps
 ** source: USGS

POINT PRECIPITATION FREQUENCY ESTIMATES

G.M. Bonnin, D. Martin, B. Lin, T. Parzybok, M. Yekta, and D. Riley

NOAA, National Weather Service, Silver Spring, Maryland

[PF tabular](#) | [PF graphical](#) | [Maps & aerials](#)

PF tabular

PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches/hour)¹										
Duration	Average recurrence interval (years)									
	1	2	5	10	25	50	100	200	500	1000
5-min	4.84 (4.43-5.29)	5.62 (5.15-6.13)	6.41 (5.87-6.98)	7.19 (6.58-7.85)	7.98 (7.27-8.70)	8.60 (7.81-9.38)	9.17 (8.26-9.98)	9.66 (8.65-10.5)	10.2 (9.07-11.1)	10.7 (9.43-11.7)
10-min	3.86 (3.54-4.22)	4.49 (4.12-4.91)	5.13 (4.70-5.60)	5.75 (5.26-6.27)	6.36 (5.79-6.93)	6.85 (6.22-7.47)	7.28 (6.56-7.93)	7.66 (6.86-8.35)	8.08 (7.18-8.82)	8.42 (7.42-9.22)
15-min	3.22 (2.95-3.52)	3.77 (3.45-4.11)	4.32 (3.96-4.72)	4.85 (4.44-5.29)	5.38 (4.89-5.86)	5.78 (5.25-6.30)	6.14 (5.53-6.68)	6.44 (5.77-7.03)	6.78 (6.02-7.40)	7.05 (6.21-7.71)
30-min	2.21 (2.02-2.41)	2.60 (2.38-2.84)	3.07 (2.82-3.35)	3.51 (3.21-3.83)	3.98 (3.62-4.34)	4.36 (3.95-4.75)	4.70 (4.24-5.12)	5.01 (4.49-5.47)	5.39 (4.79-5.89)	5.71 (5.03-6.25)
60-min	1.38 (1.26-1.51)	1.63 (1.50-1.78)	1.97 (1.81-2.15)	2.29 (2.09-2.50)	2.65 (2.41-2.89)	2.95 (2.68-3.22)	3.24 (2.92-3.53)	3.52 (3.15-3.84)	3.87 (3.44-4.22)	4.17 (3.67-4.56)
2-hr	0.804 (0.732-0.887)	0.957 (0.874-1.05)	1.17 (1.06-1.28)	1.37 (1.25-1.50)	1.61 (1.45-1.76)	1.83 (1.64-1.99)	2.03 (1.81-2.22)	2.24 (1.98-2.44)	2.51 (2.20-2.74)	2.74 (2.39-3.01)
3-hr	0.568 (0.516-0.629)	0.676 (0.617-0.746)	0.828 (0.754-0.913)	0.979 (0.888-1.08)	1.16 (1.05-1.28)	1.33 (1.19-1.46)	1.49 (1.32-1.63)	1.66 (1.46-1.82)	1.89 (1.65-2.07)	2.09 (1.81-2.30)
6-hr	0.342 (0.312-0.378)	0.407 (0.372-0.448)	0.499 (0.455-0.548)	0.591 (0.537-0.648)	0.704 (0.637-0.771)	0.807 (0.724-0.882)	0.910 (0.810-0.993)	1.02 (0.897-1.11)	1.17 (1.01-1.27)	1.30 (1.12-1.42)
12-hr	0.200 (0.183-0.221)	0.239 (0.219-0.262)	0.294 (0.269-0.322)	0.350 (0.319-0.383)	0.420 (0.381-0.459)	0.485 (0.436-0.527)	0.550 (0.489-0.597)	0.620 (0.546-0.673)	0.716 (0.621-0.778)	0.806 (0.688-0.876)
24-hr	0.119 (0.111-0.128)	0.144 (0.134-0.155)	0.181 (0.168-0.195)	0.210 (0.195-0.226)	0.250 (0.231-0.269)	0.282 (0.260-0.303)	0.314 (0.289-0.338)	0.348 (0.319-0.375)	0.395 (0.360-0.426)	0.432 (0.392-0.466)
2-day	0.069 (0.064-0.074)	0.083 (0.078-0.090)	0.104 (0.097-0.112)	0.120 (0.111-0.129)	0.142 (0.131-0.153)	0.159 (0.147-0.171)	0.177 (0.163-0.191)	0.196 (0.179-0.211)	0.221 (0.201-0.239)	0.241 (0.219-0.261)
3-day	0.049 (0.046-0.052)	0.059 (0.055-0.063)	0.073 (0.068-0.078)	0.084 (0.078-0.090)	0.099 (0.092-0.106)	0.111 (0.103-0.119)	0.124 (0.114-0.133)	0.136 (0.125-0.147)	0.154 (0.141-0.166)	0.168 (0.153-0.181)
4-day	0.039 (0.036-0.041)	0.046 (0.043-0.050)	0.057 (0.054-0.061)	0.066 (0.062-0.071)	0.078 (0.072-0.083)	0.087 (0.081-0.093)	0.097 (0.089-0.104)	0.107 (0.098-0.115)	0.121 (0.110-0.129)	0.131 (0.120-0.141)
7-day	0.026 (0.024-0.027)	0.031 (0.029-0.033)	0.037 (0.035-0.040)	0.043 (0.040-0.046)	0.050 (0.047-0.053)	0.056 (0.052-0.060)	0.062 (0.057-0.066)	0.068 (0.063-0.073)	0.076 (0.070-0.082)	0.083 (0.076-0.089)
10-day	0.020 (0.019-0.022)	0.024 (0.023-0.026)	0.029 (0.027-0.031)	0.033 (0.031-0.035)	0.038 (0.036-0.041)	0.043 (0.040-0.045)	0.047 (0.043-0.050)	0.051 (0.047-0.055)	0.057 (0.052-0.061)	0.061 (0.056-0.066)
20-day	0.014 (0.013-0.015)	0.016 (0.015-0.017)	0.019 (0.018-0.020)	0.022 (0.020-0.023)	0.025 (0.023-0.026)	0.027 (0.025-0.029)	0.030 (0.028-0.032)	0.032 (0.030-0.034)	0.036 (0.033-0.038)	0.039 (0.035-0.041)
30-day	0.011 (0.011-0.012)	0.013 (0.013-0.014)	0.016 (0.015-0.017)	0.017 (0.016-0.018)	0.020 (0.018-0.021)	0.021 (0.020-0.023)	0.023 (0.021-0.024)	0.025 (0.023-0.026)	0.027 (0.025-0.029)	0.029 (0.027-0.031)
45-day	0.010 (0.009-0.010)	0.011 (0.011-0.012)	0.013 (0.012-0.014)	0.014 (0.013-0.015)	0.016 (0.015-0.017)	0.017 (0.016-0.018)	0.018 (0.017-0.019)	0.020 (0.018-0.021)	0.021 (0.020-0.022)	0.022 (0.021-0.024)
60-day	0.009 (0.008-0.009)	0.010 (0.010-0.011)	0.011 (0.011-0.012)	0.013 (0.012-0.013)	0.014 (0.013-0.015)	0.015 (0.014-0.016)	0.016 (0.015-0.017)	0.017 (0.016-0.018)	0.018 (0.017-0.019)	0.019 (0.018-0.020)

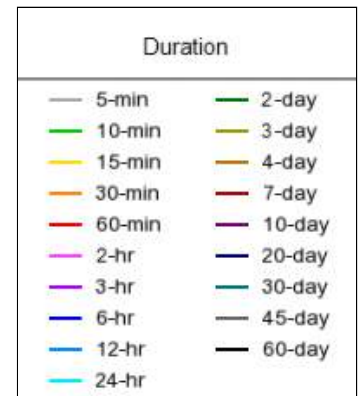
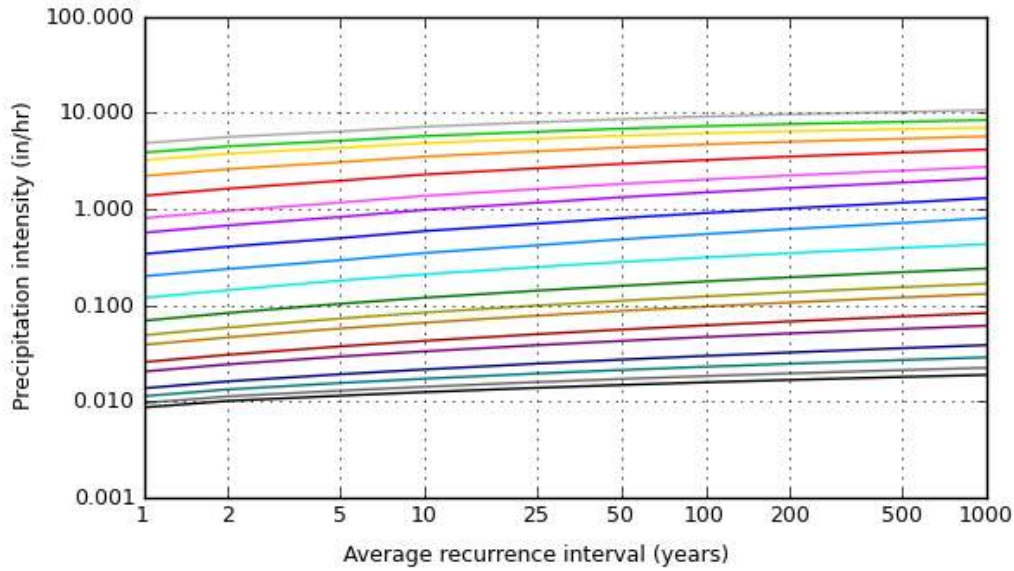
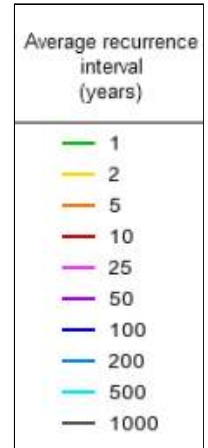
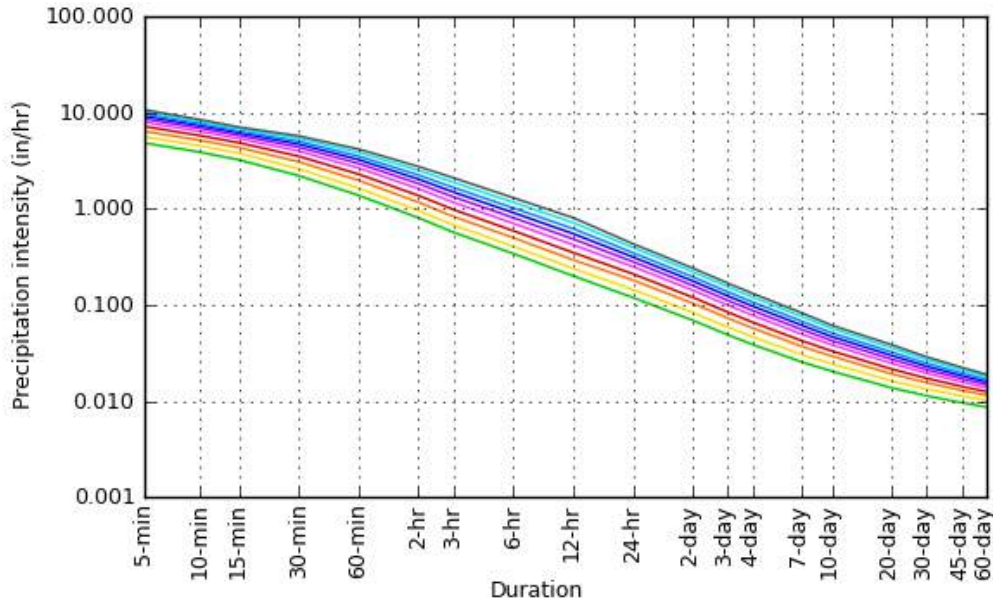
¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS). Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

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PF graphical

PDS-based intensity-duration-frequency (IDF) curves

Latitude: 35.9233°, Longitude: -78.4579°



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Maps & arials

Small scale terrain



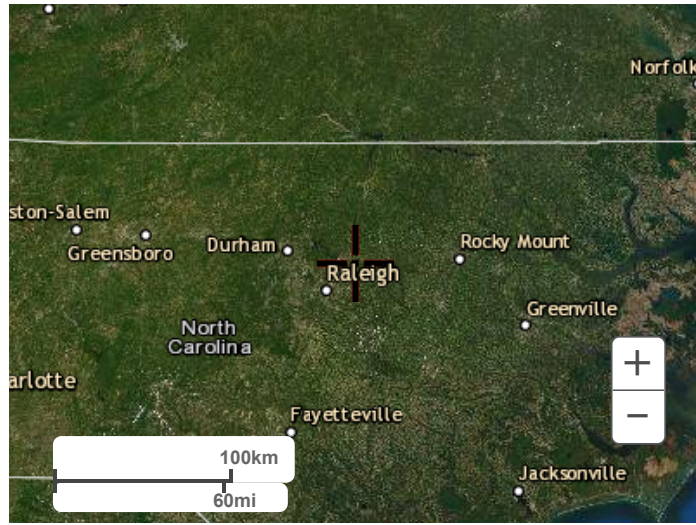
Large scale terrain



Large scale map



Large scale aerial



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