

PARKERS RIDGE

82 SCHOOL STREET ROLESVILLE, NC 27571

STORMWATER MANAGEMENT CALCULATIONS

PREPARED FOR:

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#114- Update this with correct submittals, there have only been 2 CID submittals so far

1st Submittal: 4/3/2023 2nd Submittal: 6/1/2023 3RD Submittal: 8/1/2023



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INTRODUCTION

On behalf of our client, Lennar Corporation, BGE, Inc. (BGE) submits this Engineer's Report in support of Parker Ridge project. This report contains the approach and results of the stormwater design for the subject property. The subject property is located at 82 School Street in the Town of Rolesville (Town), North Carolina. The site is comprised of four (4) parcels identified by the following parcel identification numbers (PINs): 1758-98-8411, 1758-98-3710, 1758-88-4270 E, and 1758-88-4270 W. The project area is approximately 86.74-acre (see project aerial map).

EXISTING CONDITIONS

The existing site condition is primarily undeveloped and tree-covered with several existing ponds. The predominant soil types within the proposed limit of construction are Rawlings-Rion complex (RgD), Urban land (Ur), and Wake-Rolesville complex (WaD) as taken from the Web Soil Survey 2.1 – National Cooperative Soil Survey by NRCS).

For the western parcel most of the site drains to the stream that runs through the site and into the southwest corner shown as POA #3 on the Pre-Development Exhibit. For the east parcel majority of the site drains into the existing pond located in the center of the east parcel and flows into Harris Creek exiting south of our site with a small portion draining to a more southern stream connection. These areas are shown on the Pre-Development Exhibit as POA#1 and POA#2.

FLOODPLAIN, FLOODWAY AND WATERSHED

The proposed site does not lie within a 100-year floodplain boundary as determined by FEMA FIRM Panel(s): #3720176800K and #3720175800K dated July 18, 2022.

PROPOSED DEVELOPMENT

The overall proposed project will include the development of 114 attached townhouse lots and 161 single-family lots with associated infrastructure. The proposed impervious buildout for the development is as follows:

Table 1 Impervious Area

POST-DEVELOPMENT IMPERVIOUS AREAS			
PAVEMENT	7.44	AC	
SIDEWALK	2.03	AC	
LOTS - TOWNHOMES	5.7	AC	
LOTS - SINGLE-FAMILY (MAX.)	9.66	AC _	
TOTAL ONSITE IMPERVIOUS AREA:	24.83	AC	

The project will have 7 full access points, two from the roundabor and one east. Two south connecting to Long Melford Drive and of Street H. There are also two access points from Alley 2 and Alley 3

#115- Doesn't match impervious indicated on cover sheet

ne west ast of Drive.

STORM DRAINAGE DESIGN

The existing topographic information was used to grade the property and identify the contributing drainage areas to the stormwater devices.

This project includes four (4) separate drainage systems that will drain to four (4) different proposed wet ponds located throughout the site. All four (4) of the proposed ponds will discharge to the existing Harris Creek located at the southern portion of both parcels. With Bypass also flowing into Harris Creek. The on-site storm sewer collection system was designed to capture and convey the 1-, 10, and 100- year storm event for the proposed development. Per local design standards, the Rational Method and Manning's Equation will be used for the storm sewer system design utilizing AutoDesk's Hydraflow Storm Sewers software. A Manning's n value of 0.013 will be used for the reinforced concrete pipe and 0.024 for HDPE. Runoff coefficients (C) used for open space and impervious cover were 0.35 and 0.95, respectively. The starting HGL used for the 10 yr calculations is the 10 yr WSE for the detention pond, and the starting HGL for the 100 yr WSE for the 100 yr calculations.

WATER QUALITY

The proposed wet detention ponds (SCM's) have been designed based on the town's water quantity requirements to attenuate the post-development peak runoff rates for the 1-, 10-, and 100-year storm events to pre-developed rates. The ponds are designed with weirs to safely pass the 100-year storm event and provides a minimum of one foot of freeboard above the peak stage to the top of the embankment.

The pre-development drainage area that was established for the project area includes stormwater runoff that will be conveyed to 5 points of analysis (POA's). The post-development drainage area was established based on proposed grading conditions, where all stormwater is either conveyed into a pond, and into a post-POA. The curve numbers (CN) and time of concentration (Tc) for each drainage basin were calculated based on existing and proposed conditions using the TR-55 method. The 4 proposed ponds (SCM's) were analyzed with Hydraflow modeling software for verification that the proposed design meets the Town of Rolesville's and NCDEQ's minimum requirements.

WATER QUANTITY

The proposed wet detention ponds (SCM's) have been designed based on both the NCDEQ's MDC and the town's water quantity requirements to attenuate the post-development peak runoff rates for the 1-, 10, and 100- year, 24-hour storm events. The post development flows are required to be less than the pre-developed rates by means of stormwater detention. The wet pond is designed to reduce the flows of each storm event mentioned above with a weir, the riser and an emergency spillway to safely pass the 100-year storm event.

The post-development drainage area was established based on existing and proposed site conditions. The curve numbers (CN) and time of concentration (Tc) for each drainage basin were calculated based on existing and proposed conditions using the TR-55 method. The 4 proposed ponds (SCM's) were analyzed with Hydraflow modeling software for verification that the proposed design meets the Town of Rolesville and NCDEQ's minimum requirements. For the pre-development condition and the tree save areas, the curve # of roughly 77 was used while 80 was used for the open space (grass) and 98 was used for the impervious areas. Information on Peak Flow Analysis is available below in Table 2.

Table 2 Peak Flow Analysis

	Pre-D	evelopmer	nt (cfs)	Post-Development (cfs)		Percent Difference			
POA#	1-yr	10-yr	100-yr	1-yr	10-yr	100-yr	1-yr	10-yr	100-yr
POA #1	34.25	89.35	157.92	15.95	63.14	141.43	-53%	-29%	-10%
POA #2	32.35	76.33	128.55	3.809	71.35	149.22	-88%	-7%	16%
POA #3	81.28	208.92	367.67	34.72	144.21	291.65	-57%	-31%	-21%
POA #4	10.04	25.45	44.48	1.021	2.701	4.793	-90%	-89%	-89%
POA #5	5.429	12.81	21.57	1.85	4.124	6.777	-66%	-68%	-69%
POA #6	3.604	8.504	14.32	1.037	2.484	4.212	-71%	-71%	-71%

SUMMARY

Based on the results of the stormwater models, all points of analysis are reduced in the post development condition. As a result, the proposed design meets the requirements for the Town of Rolesville and NCDEQ for stormwater conveyance, and stormwater treatment and detention. The stormwater detention information is as follows:

SCM #1	SCM #3
OCIVI #1	3CIVI #3

Drainage Area:	9.80 ac	Drainage Area:	11.17 ac
Impervious Area:	5.21 ac	Impervious Area:	4.63 ac
Average Pond Depth:	3.5 feet	Average Pond Depth:	3.5 feet
Surface Area Required:	7422 sf	Surface Area Required:	6884 sf
Surface Area Proposed:	8489 sf	Surface Area Proposed:	7226 sf
1" Detention Volume:	18800 cf	1" Detention Volume:	17154 cf

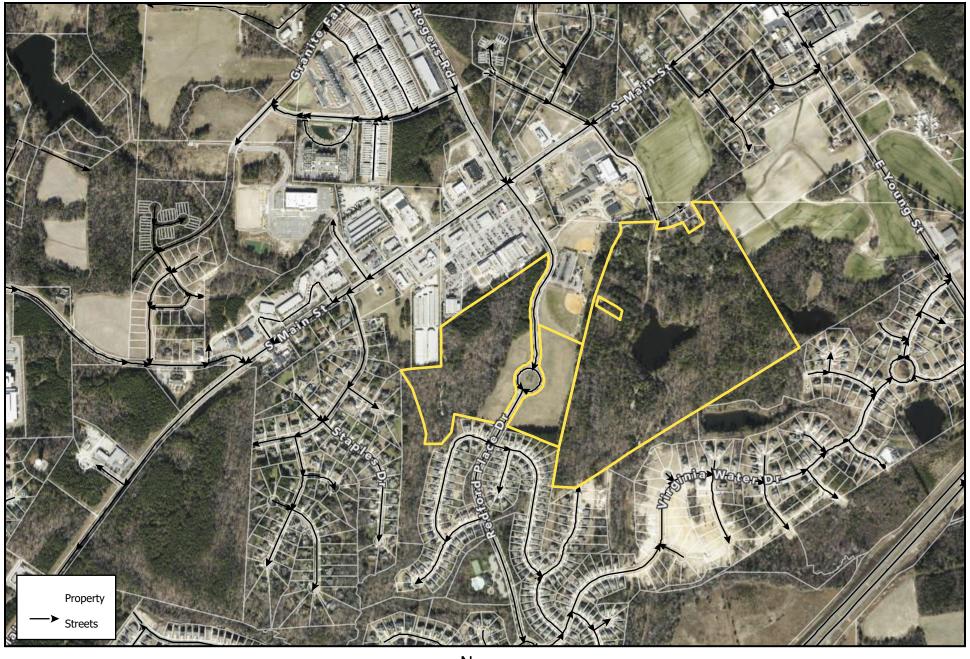
Top of Dam El: 390 at 10' wide Top of Dam El: 390 at 10' wide

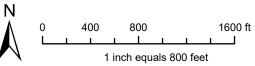
SCM #2 SCM #4

Drainage Area: 20.08 ac Drainage Area: 9.86 ac Impervious Area: 10.10 ac Impervious Area: 4.34 ac Average Pond Depth: 3.5 feet Average Pond Depth: 3.5 feet Surface Area Required: 18408 sf Surface Area Required: 8660 sf Surface Area Proposed: 20384 sf Surface Area Proposed: 14636 sf 1" Detention Volume: 36641 cf 1" Detention Volume: 15968 cf

Top of Dam El: 357 at 10' wide Top of Dam El: 386 at 10' wide

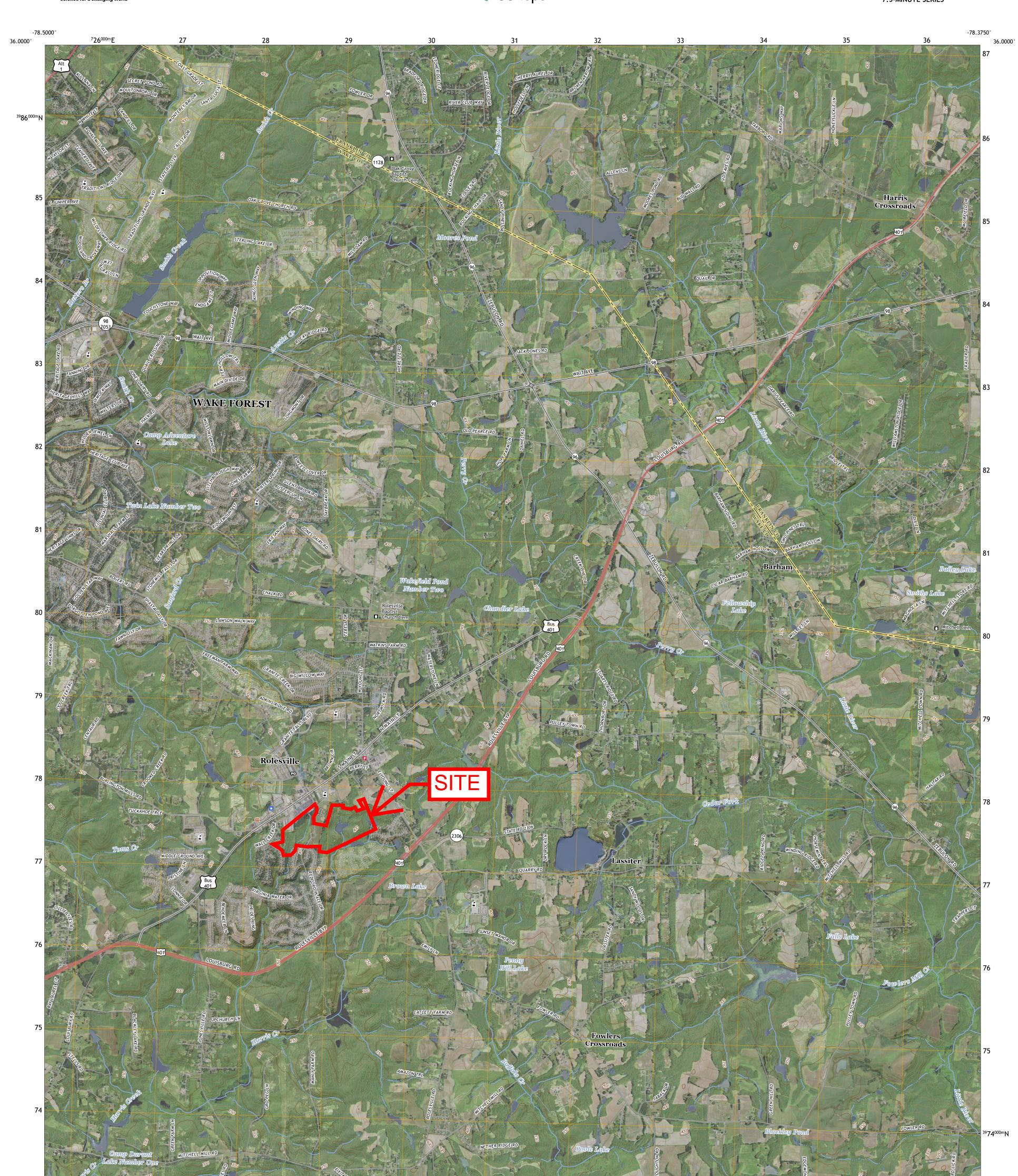
ATTACHMENT 1: PROJECT AERIAL MAP

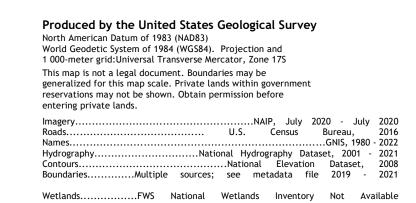




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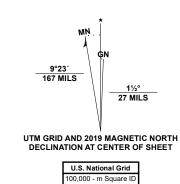
ATTACHMENT 2: USGS TOPO MAP





35.8750°

-78.5000°



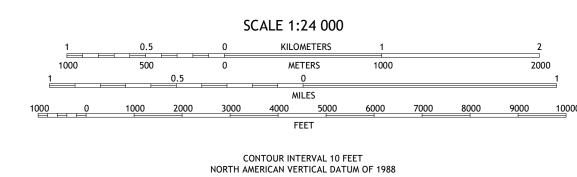
QV

Grid Zone Designation 17S

29

30

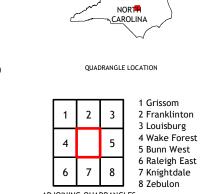
28



This map was produced to conform with the National Geospatial Program US Topo Product Standard.

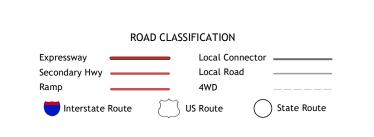
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32



ADJOINING QUADRANGLES

33



35

-78.3750° 35.8750°

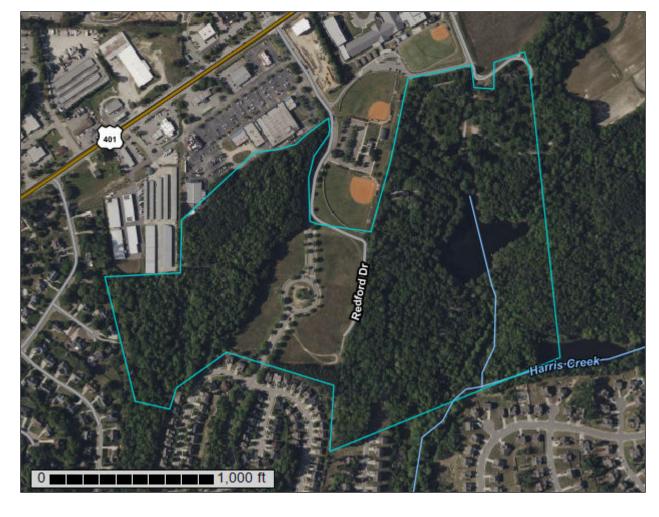
ATTACHMENT 3: SOIL SURVEY REPORT



NRCS

Natural Resources Conservation Service A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

Custom Soil Resource Report for Wake County, North Carolina



Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2_053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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How Soil Surveys Are Made

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



MAP LEGEND

Area of Interest (AOI)

Area of Interest (AOI)

Soils

Soil Map Unit Polygons

-

Soil Map Unit Lines

Soil Map Unit Points

Special Point Features

()

Blowout

 \boxtimes

Borrow Pit

Ж

Clay Spot

 \Diamond

Closed Depression

Š

Gravel Pit

.

Gravelly Spot

0

Landfill Lava Flow

٨.

Marsh or swamp

@

Mine or Quarry

0

Miscellaneous Water
Perennial Water

0

Rock Outcrop

+

Saline Spot

. .

Sandy Spot

Sodic Spot

_

Severely Eroded Spot

Sinkhole

Slide or Slip

Ø

8

Spoil Area Stony Spot

Ø

Very Stony Spot

3

Wet Spot Other

Δ

Special Line Features

Water Features

_

Streams and Canals

Transportation

ransp

Rails

~

Interstate Highways

__

US Routes

 \sim

Major Roads

~

Local Roads

Background

100

Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24.000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Wake County, North Carolina Survey Area Data: Version 23, Sep 12, 2022

Soil map units are labeled (as space allows) for map scales 1:50.000 or larger.

Date(s) aerial images were photographed: Apr 24, 2022—May 9, 2022

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI	
HeB	Helena sandy loam, 2 to 6 percent slopes	11.1	13.2%	
RgB	Rawlings-Rion complex, 2 to 6 percent slopes	6.1	7.2%	
RgC	Rawlings-Rion complex, 6 to 10 percent slopes	0.6	0.7%	
RgD	Rawlings-Rion complex, 10 to 15 percent slopes	17.4	20.5%	
Ur	Urban land	16.4	19.4%	
W	Water	3.9	4.6%	
WaD	Wake-Rolesville complex, 10 to 15 percent slopes, very rocky	13.4	15.8%	
WaE	Wake-Rolesville complex, 15 to 25 percent slopes, very rocky	11.6	13.7%	
WfB	Wedowee-Saw complex, 2 to 6 percent slopes	1.2	1.4%	
WgB	Wedowee-Urban land complex, 2 to 6 percent slopes	2.8	3.4%	
WgC	Wedowee-Urban land complex, 6 to 15 percent slopes	0.1	0.2%	
Totals for Area of Interest		84.7	100.0%	

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties

and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

Wake County, North Carolina

HeB—Helena sandy loam, 2 to 6 percent slopes

Map Unit Setting

National map unit symbol: 2qqqq

Elevation: 70 to 560 feet

Mean annual precipitation: 39 to 47 inches Mean annual air temperature: 55 to 63 degrees F

Frost-free period: 200 to 250 days

Farmland classification: All areas are prime farmland

Map Unit Composition

Helena and similar soils: 92 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Helena

Setting

Landform: Interfluves

Landform position (two-dimensional): Summit, shoulder Landform position (three-dimensional): Side slope

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Residuum weathered from granite and gneiss

Typical profile

Ap - 0 to 12 inches: sandy loam BE - 12 to 19 inches: sandy clay loam

Bt1 - 19 to 39 inches: clay Bt2 - 39 to 43 inches: clay loam BCg - 43 to 46 inches: clay loam C - 46 to 80 inches: sandy loam

Properties and qualities

Slope: 2 to 6 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Moderately well drained

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.06 in/hr)

Depth to water table: About 18 to 30 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Moderate (about 8.3 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: D

Ecological site: F136XY810SC - Acidic upland forest, seasonally wet

Hydric soil rating: No

RgB—Rawlings-Rion complex, 2 to 6 percent slopes

Map Unit Setting

National map unit symbol: 2xhb9

Elevation: 70 to 560 feet

Mean annual precipitation: 39 to 47 inches Mean annual air temperature: 55 to 63 degrees F

Frost-free period: 200 to 250 days

Farmland classification: Farmland of statewide importance

Map Unit Composition

Rawlings and similar soils: 55 percent Rion and similar soils: 35 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Rawlings

Setting

Landform: Interfluves

Landform position (two-dimensional): Summit, shoulder Landform position (three-dimensional): Interfluve

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Residuum weathered from granite

Typical profile

Ap - 0 to 8 inches: sandy loam

Bt - 8 to 20 inches: sandy clay loam

C - 20 to 40 inches: gravelly sandy loam

R - 40 to 80 inches: bedrock

Properties and qualities

Slope: 2 to 6 percent

Depth to restrictive feature: 20 to 40 inches to lithic bedrock

Drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.06 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Low (about 4.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: C

Ecological site: F136XY830NC - Acidic upland forest, dry-moist

Hydric soil rating: No

Description of Rion

Setting

Landform: Interfluves

Landform position (two-dimensional): Summit, shoulder Landform position (three-dimensional): Interfluve

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Saprolite derived from granite and gneiss

Typical profile

Ap - 0 to 8 inches: sandy loam
Bt1 - 8 to 17 inches: sandy clay loam
Bt2 - 17 to 38 inches: sandy loam
C - 38 to 80 inches: sandy loam

Properties and qualities

Slope: 2 to 6 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high

(0.57 to 1.98 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Moderate (about 7.3 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: B

Ecological site: F136XY820GA - Acidic upland forest, moist

Hydric soil rating: No

RgC—Rawlings-Rion complex, 6 to 10 percent slopes

Map Unit Setting

National map unit symbol: 2xhbb

Elevation: 70 to 560 feet

Mean annual precipitation: 39 to 47 inches
Mean annual air temperature: 55 to 63 degrees F

Frost-free period: 200 to 250 days

Farmland classification: Farmland of statewide importance

Map Unit Composition

Rawlings and similar soils: 55 percent Rion and similar soils: 35 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Rawlings

Setting

Landform: Interfluves

Landform position (two-dimensional): Shoulder, backslope

Landform position (three-dimensional): Interfluve

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Residuum weathered from granite

Typical profile

Ap - 0 to 8 inches: sandy loam

Bt - 8 to 20 inches: sandy clay loam

C - 20 to 40 inches: gravelly sandy loam

R - 40 to 80 inches: bedrock

Properties and qualities

Slope: 6 to 10 percent

Depth to restrictive feature: 20 to 40 inches to lithic bedrock

Drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.06 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Low (about 4.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3e

Hydrologic Soil Group: C

Ecological site: F136XY830NC - Acidic upland forest, dry-moist

Hydric soil rating: No

Description of Rion

Setting

Landform: Interfluves

Landform position (two-dimensional): Shoulder, backslope

Landform position (three-dimensional): Interfluve

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Saprolite derived from granite and gneiss

Typical profile

Ap - 0 to 8 inches: sandy loam

Bt1 - 8 to 17 inches: sandy clay loam

Bt2 - 17 to 38 inches: sandy loam

C - 38 to 80 inches: sandy loam

Properties and qualities

Slope: 6 to 10 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high

(0.57 to 1.98 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Moderate (about 7.3 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3e

Hydrologic Soil Group: B

Ecological site: F136XY820GA - Acidic upland forest, moist

Hydric soil rating: No

RgD—Rawlings-Rion complex, 10 to 15 percent slopes

Map Unit Setting

National map unit symbol: 2xhb8

Elevation: 70 to 560 feet

Mean annual precipitation: 39 to 47 inches
Mean annual air temperature: 55 to 63 degrees F

Frost-free period: 200 to 250 days

Farmland classification: Farmland of statewide importance

Map Unit Composition

Rawlings and similar soils: 55 percent Rion and similar soils: 35 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Rawlings

Setting

Landform: Interfluves

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Interfluve

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Residuum weathered from granite

Typical profile

Ap - 0 to 8 inches: sandy loam

Bt - 8 to 20 inches: sandy clay loam

C - 20 to 40 inches: gravelly sandy loam

R - 40 to 80 inches: bedrock

Properties and qualities

Slope: 10 to 15 percent

Depth to restrictive feature: 20 to 40 inches to lithic bedrock

Drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.06 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Low (about 4.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4e

Hydrologic Soil Group: C

Ecological site: F136XY830NC - Acidic upland forest, dry-moist

Hydric soil rating: No

Description of Rion

Setting

Landform: Interfluves

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Interfluve

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Saprolite derived from granite and gneiss

Typical profile

Ap - 0 to 8 inches: sandy loam
Bt1 - 8 to 17 inches: sandy clay loam
Bt2 - 17 to 38 inches: sandy loam
C - 38 to 80 inches: sandy loam

Properties and qualities

Slope: 10 to 15 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high

(0.57 to 1.98 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Moderate (about 7.3 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4e

Hydrologic Soil Group: B

Ecological site: F136XY820GA - Acidic upland forest, moist

Hydric soil rating: No

Ur—Urban land

Map Unit Setting

National map unit symbol: 2qwpc

Elevation: 70 to 1,400 feet

Mean annual precipitation: 39 to 51 inches Mean annual air temperature: 54 to 63 degrees F

Frost-free period: 190 to 250 days

Farmland classification: Not prime farmland

Map Unit Composition

Urban land: 100 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Urban Land

Setting

Parent material: Impervious layers over human-transported material

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8

Hydric soil rating: No

W-Water

Map Unit Setting

National map unit symbol: 2qqjv

Elevation: 70 to 450 feet

Mean annual precipitation: 39 to 51 inches Mean annual air temperature: 55 to 63 degrees F

Frost-free period: 200 to 250 days

Farmland classification: Not prime farmland

Map Unit Composition

Water: 100 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Water

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8

Hydric soil rating: No

WaD—Wake-Rolesville complex, 10 to 15 percent slopes, very rocky

Map Unit Setting

National map unit symbol: 2xhbf

Elevation: 70 to 560 feet

Mean annual precipitation: 39 to 47 inches Mean annual air temperature: 55 to 63 degrees F

Frost-free period: 200 to 250 days

Farmland classification: Not prime farmland

Map Unit Composition

Wake, very rocky, and similar soils: 50 percent Rolesville, very rocky, and similar soils: 40 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Wake, Very Rocky

Setting

Landform: Interfluves

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Interfluve

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Residuum weathered from granite and gneiss

Typical profile

Ap - 0 to 7 inches: gravelly loamy coarse sand C - 7 to 11 inches: gravelly loamy sand

R - 11 to 80 inches: bedrock

Properties and qualities

Slope: 10 to 15 percent

Depth to restrictive feature: 10 to 20 inches to lithic bedrock

Drainage class: Excessively drained

Capacity of the most limiting layer to transmit water (Ksat): Very low to low (0.00 to

0.01 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Very low (about 1.9 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4s

Hydrologic Soil Group: D

Ecological site: F136XY870GA - Outer piedmont acidic upland woodlands and

glades, dry *Hydric soil rating:* No

Description of Rolesville, Very Rocky

Settina

Landform: Interfluves

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Interfluve

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Residuum weathered from granite and gneiss

Typical profile

Ap - 0 to 12 inches: loamy sand Bw - 12 to 26 inches: loamy sand C - 26 to 32 inches: loamy coarse sand

Cr - 32 to 38 inches: bedrock R - 38 to 80 inches: bedrock

Properties and qualities

Slope: 10 to 15 percent

Depth to restrictive feature: 20 to 40 inches to paralithic bedrock; 20 to 80 inches

to lithic bedrock

Drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): Very low to low (0.00 to

0.01 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Moderate (about 6.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4e

Hydrologic Soil Group: A

Ecological site: F136XY870GA - Outer piedmont acidic upland woodlands and

glades, dry *Hydric soil rating:* No

WaE—Wake-Rolesville complex, 15 to 25 percent slopes, very rocky

Map Unit Setting

National map unit symbol: 2xhbg

Elevation: 70 to 560 feet

Mean annual precipitation: 39 to 47 inches Mean annual air temperature: 55 to 63 degrees F

Frost-free period: 200 to 250 days

Farmland classification: Not prime farmland

Map Unit Composition

Wake, very rocky, and similar soils: 50 percent Rolesville, very rocky, and similar soils: 40 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Wake, Very Rocky

Setting

Landform: Interfluves

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Residuum weathered from granite and gneiss

Typical profile

Ap - 0 to 7 inches: gravelly loamy coarse sand C - 7 to 11 inches: gravelly loamy sand

R - 11 to 80 inches: bedrock

Properties and qualities

Slope: 15 to 25 percent

Depth to restrictive feature: 10 to 20 inches to lithic bedrock

Drainage class: Excessively drained

Capacity of the most limiting layer to transmit water (Ksat): Very low to low (0.00 to

0.01 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Very low (about 1.9 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4s

Hydrologic Soil Group: D

Ecological site: F136XY870GA - Outer piedmont acidic upland woodlands and

glades, dry *Hydric soil rating:* No

Description of Rolesville, Very Rocky

Setting

Landform: Interfluves

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Residuum weathered from granite and gneiss

Typical profile

Ap - 0 to 12 inches: loamy sand Bw - 12 to 26 inches: loamy sand C - 26 to 32 inches: loamy coarse sand

Cr - 32 to 38 inches: bedrock R - 38 to 80 inches: bedrock

Properties and qualities

Slope: 15 to 25 percent

Depth to restrictive feature: 20 to 40 inches to paralithic bedrock; 20 to 80 inches

to lithic bedrock

Drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): Very low to low (0.00 to

0.01 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Moderate (about 6.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6e

Hydrologic Soil Group: A

Ecological site: F136XY870GA - Outer piedmont acidic upland woodlands and

glades, dry *Hydric soil rating:* No

WfB—Wedowee-Saw complex, 2 to 6 percent slopes

Map Unit Setting

National map unit symbol: 2xn42

Elevation: 70 to 560 feet

Mean annual precipitation: 39 to 47 inches Mean annual air temperature: 55 to 63 degrees F

Frost-free period: 200 to 250 days

Farmland classification: Farmland of statewide importance

Map Unit Composition

Wedowee and similar soils: 60 percent Saw and similar soils: 35 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Wedowee

Setting

Landform: Interfluves

Landform position (two-dimensional): Summit, shoulder Landform position (three-dimensional): Interfluve

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Saprolite residuum weathered from granite and gneiss and/or

saprolite residuum weathered from schist

Typical profile

Ap - 0 to 4 inches: sandy loam
E - 4 to 7 inches: sandy loam
BC - 23 to 35 inches: clay loam
C - 35 to 80 inches: sandy clay loam

Properties and qualities

Slope: 2 to 6 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high

(0.57 to 1.98 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Moderate (about 6.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: B

Ecological site: F136XY820GA - Acidic upland forest, moist

Hydric soil rating: No

Description of Saw

Setting

Landform: Interfluves

Landform position (two-dimensional): Summit, shoulder Landform position (three-dimensional): Interfluve

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Residuum weathered from granite and gneiss

Typical profile

Ap - 0 to 8 inches: sandy loam Bt - 8 to 20 inches: clay

BC - 20 to 26 inches: sandy clay loam
C - 26 to 29 inches: sandy loam
R - 29 to 80 inches: bedrock

Properties and qualities

Slope: 2 to 6 percent

Depth to restrictive feature: 20 to 40 inches to lithic bedrock

Drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): Very low to low (0.00 to

0.01 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Low (about 3.6 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: C

Ecological site: F136XY830NC - Acidic upland forest, dry-moist

Hydric soil rating: No

WgB-Wedowee-Urban land complex, 2 to 6 percent slopes

Map Unit Setting

National map unit symbol: 2xn43

Elevation: 70 to 560 feet

Mean annual precipitation: 39 to 47 inches
Mean annual air temperature: 55 to 63 degrees F

Frost-free period: 200 to 250 days

Farmland classification: Not prime farmland

Map Unit Composition

Wedowee and similar soils: 55 percent

Urban land: 40 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Wedowee

Setting

Landform: Interfluves

Landform position (two-dimensional): Summit, shoulder Landform position (three-dimensional): Interfluve

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Saprolite residuum weathered from granite and gneiss and/or

saprolite residuum weathered from schist

Typical profile

Ap - 0 to 4 inches: sandy loam
E - 4 to 7 inches: sandy loam
BC - 23 to 35 inches: clay loam
C - 35 to 80 inches: sandy clay loam

Properties and qualities

Slope: 2 to 6 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high

(0.57 to 1.98 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Moderate (about 6.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: B

Ecological site: F136XY820GA - Acidic upland forest, moist

Hydric soil rating: No

Description of Urban Land

Setting

Parent material: Impervious layers over human transported material

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8

Hydric soil rating: No

WgC—Wedowee-Urban land complex, 6 to 15 percent slopes

Map Unit Setting

National map unit symbol: 2xn44

Elevation: 70 to 560 feet

Mean annual precipitation: 39 to 47 inches

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Mean annual air temperature: 55 to 63 degrees F

Frost-free period: 200 to 250 days

Farmland classification: Not prime farmland

Map Unit Composition

Wedowee and similar soils: 55 percent

Urban land: 40 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Wedowee

Setting

Landform: Interfluves

Landform position (two-dimensional): Shoulder, backslope

Landform position (three-dimensional): Interfluve

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Saprolite residuum weathered from granite and gneiss and/or

saprolite residuum weathered from schist

Typical profile

Ap - 0 to 4 inches: sandy loam
E - 4 to 7 inches: sandy loam
BC - 23 to 35 inches: clay loam
C - 35 to 80 inches: sandy clay loam

Properties and qualities

Slope: 6 to 15 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high

(0.57 to 1.98 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Moderate (about 6.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4e

Hydrologic Soil Group: B

Ecological site: F136XY820GA - Acidic upland forest, moist

Hydric soil rating: No

Description of Urban Land

Setting

Parent material: Impervious layers over human transported material

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8

Hydric soil rating: No

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References

American Association of State Highway and Transportation Officials (AASHTO). 2004. Standard specifications for transportation materials and methods of sampling and testing. 24th edition.

American Society for Testing and Materials (ASTM). 2005. Standard classification of soils for engineering purposes. ASTM Standard D2487-00.

Cowardin, L.M., V. Carter, F.C. Golet, and E.T. LaRoe. 1979. Classification of wetlands and deep-water habitats of the United States. U.S. Fish and Wildlife Service FWS/OBS-79/31.

Federal Register. July 13, 1994. Changes in hydric soils of the United States.

Federal Register. September 18, 2002. Hydric soils of the United States.

Hurt, G.W., and L.M. Vasilas, editors. Version 6.0, 2006. Field indicators of hydric soils in the United States.

National Research Council. 1995. Wetlands: Characteristics and boundaries.

Soil Survey Division Staff. 1993. Soil survey manual. Soil Conservation Service. U.S. Department of Agriculture Handbook 18. http://www.nrcs.usda.gov/wps/portal/nrcs/detail/national/soils/?cid=nrcs142p2 054262

Soil Survey Staff. 1999. Soil taxonomy: A basic system of soil classification for making and interpreting soil surveys. 2nd edition. Natural Resources Conservation Service, U.S. Department of Agriculture Handbook 436. http://www.nrcs.usda.gov/wps/portal/nrcs/detail/national/soils/?cid=nrcs142p2 053577

Soil Survey Staff. 2010. Keys to soil taxonomy. 11th edition. U.S. Department of Agriculture, Natural Resources Conservation Service. http://www.nrcs.usda.gov/wps/portal/nrcs/detail/national/soils/?cid=nrcs142p2 053580

Tiner, R.W., Jr. 1985. Wetlands of Delaware. U.S. Fish and Wildlife Service and Delaware Department of Natural Resources and Environmental Control, Wetlands Section.

United States Army Corps of Engineers, Environmental Laboratory. 1987. Corps of Engineers wetlands delineation manual. Waterways Experiment Station Technical Report Y-87-1.

United States Department of Agriculture, Natural Resources Conservation Service. National forestry manual. http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/home/?cid=nrcs142p2 053374

United States Department of Agriculture, Natural Resources Conservation Service. National range and pasture handbook. http://www.nrcs.usda.gov/wps/portal/nrcs/detail/national/landuse/rangepasture/?cid=stelprdb1043084

Custom Soil Resource Report

United States Department of Agriculture, Natural Resources Conservation Service. National soil survey handbook, title 430-VI. http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/scientists/?cid=nrcs142p2_054242

United States Department of Agriculture, Natural Resources Conservation Service. 2006. Land resource regions and major land resource areas of the United States, the Caribbean, and the Pacific Basin. U.S. Department of Agriculture Handbook 296. http://www.nrcs.usda.gov/wps/portal/nrcs/detail/national/soils/?cid=nrcs142p2_053624

United States Department of Agriculture, Soil Conservation Service. 1961. Land capability classification. U.S. Department of Agriculture Handbook 210. http://www.nrcs.usda.gov/Internet/FSE_DOCUMENTS/nrcs142p2_052290.pdf

ATTACHMENT 4: FEMA FLOOD MAP

DATUM INFORMATION

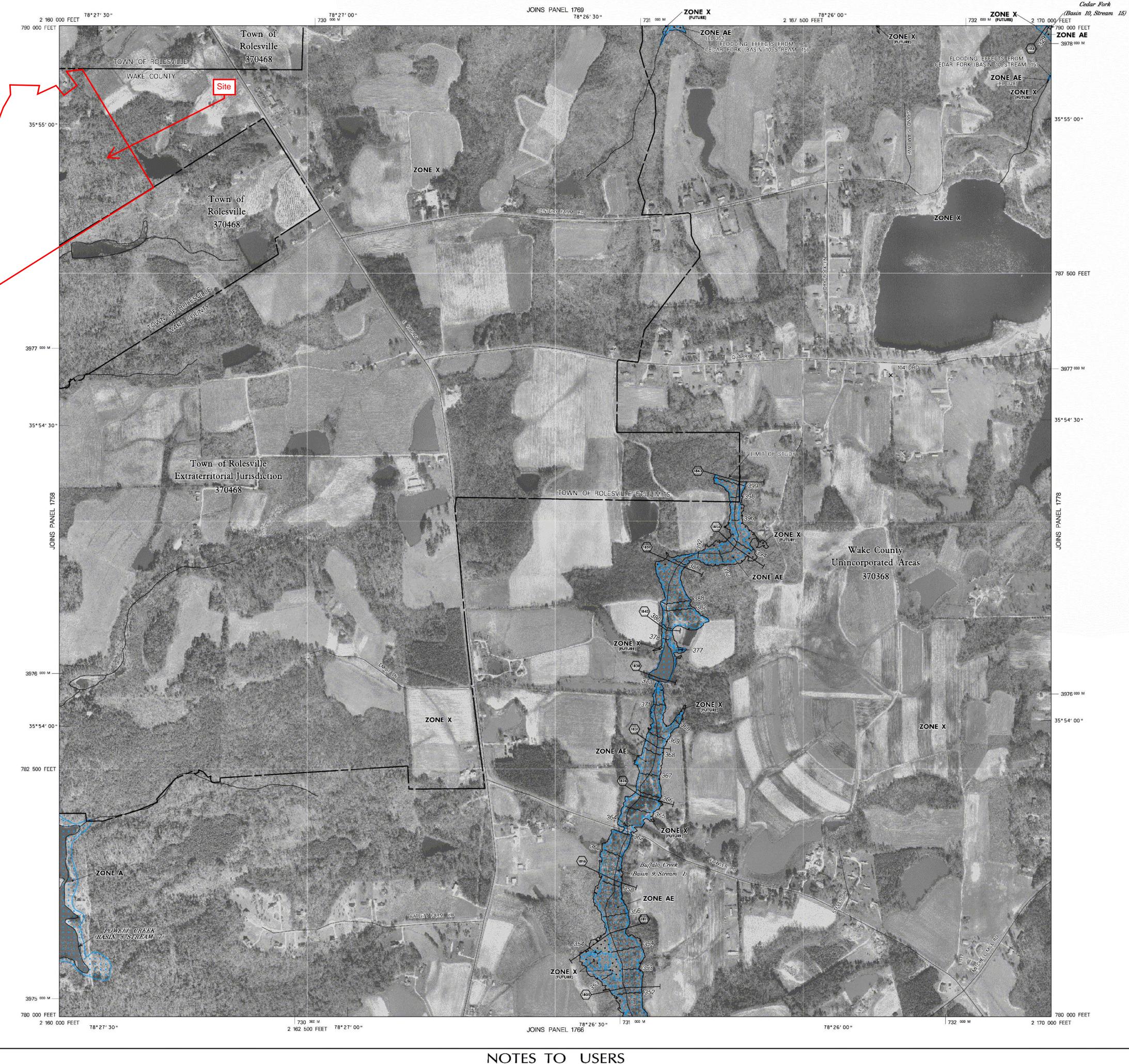
The projection used in the preparation of this map was the North Carolina State Plane (FIPSZONE 3200). The horizontal datum was the North American Datum of 1983, GRS80 ellipsoid. Differences in datum, ellipsoid, projection, or Universal Transverse Mercator zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdictional boundaries. These differences do not affect the accuracy of this FIRM. All coordinates on this map are in U.S. Survey Feet, where 1 U.S. Survey Foot = 1200/3937 Meters.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988 (NAVD 88). These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. An average offset between NAVD 88 and the National Geodetic Vertical Datum of 1929 (NGVD 29) has been computed for each North Carolina county. This offset was then applied to the NGVD 29 flood elevations that were not revised during the creation of this statewide format FIRM. The offsets for each county shown on this FIRM panel are shown in the vertical datum offset table below. Where a county boundary and a flooding source with unrevised NGVD 29 flood elevations are coincident, an individual offset has been calculated and applied during the creation of this statewide format FIRM. See Section 6.1 of the accompanying Flood Insurance Study report to obtain further information on the conversion of elevations between NAVD 88 and NGVD 29. To obtain current elevation, description, and/or location information for bench marks shown on this map, please contact the North Carolina Geodetic Survey at the address shown below. You may also contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242, or visit its website at www.ngs.noaa.gov.

North Carolina Geodetic Survey 121 West Jones Street Raleigh, NC 27601 (919) 733-3836 www.ncgs.state.nc.us

County Average Vertical Datum Offset Table Vertical Datum Offset (ft) Example: NAVD 88 = NGVD 29 + (-0.88)

All streams listed in the Flood Hazard Data Table below were studied by detailed methods using field survey. Other flood hazard data shown on this map may have been derived using either a coastal analysis or limited detailed riverine analysis. More information on the flooding sources studied by these analyses is contained in the Flood Insurance Study report.







This digital Flood Insurance Rate Map (FIRM) was produced through a unique cooperative partnership between the State of North Carolina and the Federal Emergency Management Agency (FEMA). The State of North Carolina has implemented a long term approach of floodplain management to decrease the costs associated with flooding. This is demonstrated by the State's commitment to map floodplain areas at the local level. As a part of this effort, the State of North Carolina has joined in a Cooperating Technical State agreement with FEMA to produce and maintain this digital FIRM.

www.ncfloodmaps.com

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible

updated or additional flood hazard information. To obtain more detailed information in areas where Base Flood Elevations (BFEs) and/or floodways have been determined, users are encouraged to consult the Flood Profiles, Floodway Data, Limited Detailed Flood Hazard Data, and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Boundaries of regulatory floodways shown on the FIRM for flooding sources studied by detailed methods were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data for flooding sources studied by detailed methods as well as non-encroachment widths for flooding sources studied by limited detailed methods are provided in the FIS report for this jurisdiction. The FIS report also provides instructions for determining a floodway using non-encroachment widths for flooding sources studied by limited detailed methods.

Certain areas not in Special Flood Hazard Areas may be protected by flood control structures. Refer to Section 4.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures in this jurisdiction.

Base map information and geospatial data used to develop this FIRM were obtained from various organizations, including the participating local community(ies), state and federal agencies, and/or other sources. The primary base for this FIRM is aerial imagery acquired by Wake County. The time period of collection for the imagery is 1999. Information and geospatial data supplied by the local community(ies) that met FEMA base map specifications were considered the preferred source for development of the base map. See geospatial metadata for the associated digital FIRM for additional information about base map

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This map reflects more detailed and up-to-date stream channel configurations than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map.

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If you have questions about this map, or questions concerning the National Flood Insurance Program in general, please call 1-877-FEMA MAP (1-877-336-2627) or visit the FEMA website at www.fema.gov.

An accompanying Flood Insurance Study report, Letter of Map Revision (LOMR) or Letter of Map Amendment (LOMA) revising portions of this panel, and digital versions of this FIRM may be available. Visit the North Carolina Floodplain Mapping Program website at www.ncfloodmaps.com, or contact the FEMA Map Service Center at 1-800-358-9616 for information on all related products associated with this FIRM. The FEMA Map Service Center may also be reached by Fax at 1-800-358-9620 and its website at www.msc.fema.gov.

MAP REPOSITORY Refer to listing of Map Repositories on Map Index or visit www.ncfloodmaps.com.

> EFFECTIVE DATE OF FLOOD INSURANCE RATE MAP PANEL MAY 2, 2006

EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL

For community map revision history prior to statewide mapping, refer to the Community Map History table located in the Flood Insurance Study report for this jurisdiction. To determine if flood insurance is available in this community, contact your insurance agent, the North Carolina Division of Emergency Management or the National Flood Insurance Program at the

following phone numbers or websites: National Flood Insurance Program NC Division of Emergency Management (919) 715–8000 <u>www.nccrimecontrol.org/nfip</u> 1–800–638–6620 <u>www.fema.gov/nfip</u>

LEGEND

SPECIAL FLOOD HAZARD AREAS (SFHAs) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD

The 1% annual chance flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equaled or exceeded in any given year. The Special Flood Hazard Area is the area subject to flooding by the 1% annual chance flood. Areas of Special Flood Hazard include Zones A, AE, AH, AO, AR, A99, V, and VE. The Base Flood Elevation is the water-surface elevation of the 1% annual chance flood.

No Base Flood Elevations determined. Base Flood Elevations determined. ZONE AE

Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations determined. Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities

Special Flood Hazard Area formerly protected from the 1% annual chance flood by a flood control system that was subsequently decertified. Zone AR indicates that the former flood control system is being restored to provide protection from the 1% annual chance or

greater flood. Area to be protected from 1% annual chance flood by a Federal flood protection system under construction; no Base Flood Elevations

Coastal flood zone with velocity hazard (wave action); Base Flood Elevations FLOODWAY AREAS IN ZONE AE

The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood heights.

OTHER FLOOD AREAS

Areas of 0.2% annual chance flood; areas of future conditions 1% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.

OTHER AREAS Areas determined to be outside the 0.2% annual chance and future conditions 1% annual chance floodplain.

COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS

Areas in which flood hazards are undetermined, but possible.

OTHERWISE PROTECTED AREAS (OPAs) CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas.

1% annual chance floodplain boundary 0.2% annual chance floodplain boundary and future conditions 1% annual chance floodplain boundary

Floodway boundary _______ Zone D Boundary

CBRS and OPA boundary Boundary dividing Special Flood Hazard Area Zones and boundary dividing Special Flood Hazard Areas of different

Base Flood Elevations, flood depths or flood velocities. ----513----Base Flood Elevation line and value; elevation in feet* Base Flood Elevation value where uniform within zone; (EL 987) elevation in feet*

*Referenced to the North American Vertical Datum of 1988 Cross section line

(23)-----(23) Transect line

97°07′30", 32°22′30" 4276000 M

• M1.5

ZONE X

1 477 500 FEET BM5510 🗸

Geographic coordinates referenced to the North American Datum of 1983 (NAD 83) 1000-meter Universal Transverse Mercator grid ticks, zone 17 2500-foot grid values: North Carolina State Plane coordinate system (FIPSZONE 3200, State Plane NAD 83 feet)

North Carolina Geodetic Survey bench mark (see explanation in the Datum Information section of this FIRM panel). National Geodetic Survey bench mark (see explanation in the Datum Information section of this FIRM panel). River Mile



MAP SCALE 1" = 500' (1 : 6,000)

PANEL 1768J

FIRM FLOOD INSURANCE RATE MAP

(1)(0)(0)

PANEL 1768 (SEE LOCATOR DIAGRAM OR MAP INDEX FOR FIRM

NORTH CAROLINA

PANEL LAYOUT)

ROLESVILLE, TOWN OF 370468 1768 J WAKE COUNTY 370368 1768

Notice to User: The Map Number shown below should be used when placing map orders; the Community Number shown above should be used on insurance applications for the subject

EFFECTIVE DATE MAY 2, 2006



MAP NUMBER

State of North Carolina Federal Emergency Management Agency



DATUM INFORMATION

The projection used in the preparation of this map was the North Carolina State Plane (FIPSZONE 3200). The horizontal datum was the North American Datum of 1983, GRS80 ellipsoid. Differences in datum, ellipsoid, projection, or Universal Transverse Mercator zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdictional boundaries. These differences do not affect the accuracy of this FIRM. All coordinates on this map are in U.S. Survey Feet, where 1 U.S. Survey Foot = 1200/3937 Meters.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988 (NAVD 88). These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. An average offset between NAVD 88 and the National Geodetic Vertical Datum of 1929 (NGVD 29) has been computed for each North Carolina county. This offset was then applied to the NGVD 29 flood elevations that were not revised during the creation of this statewide format FIRM. The offsets for each county shown on this FIRM panel are shown in the vertical datum offset table below. Where a county boundary and a flooding source with unrevised NGVD 29 flood elevations are coincident, an individual offset has been calculated and applied during the creation of this statewide format FIRM. See Section 6.1 of the accompanying Flood Insurance Study report to obtain further information on the conversion of elevations between NAVD 88 and NGVD 29. To obtain current elevation, description, and/or location information for bench marks shown on this map, please contact the North Carolina Geodetic Survey at the address shown below. You may also contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242, or visit its website at www.ngs.noaa.gov.

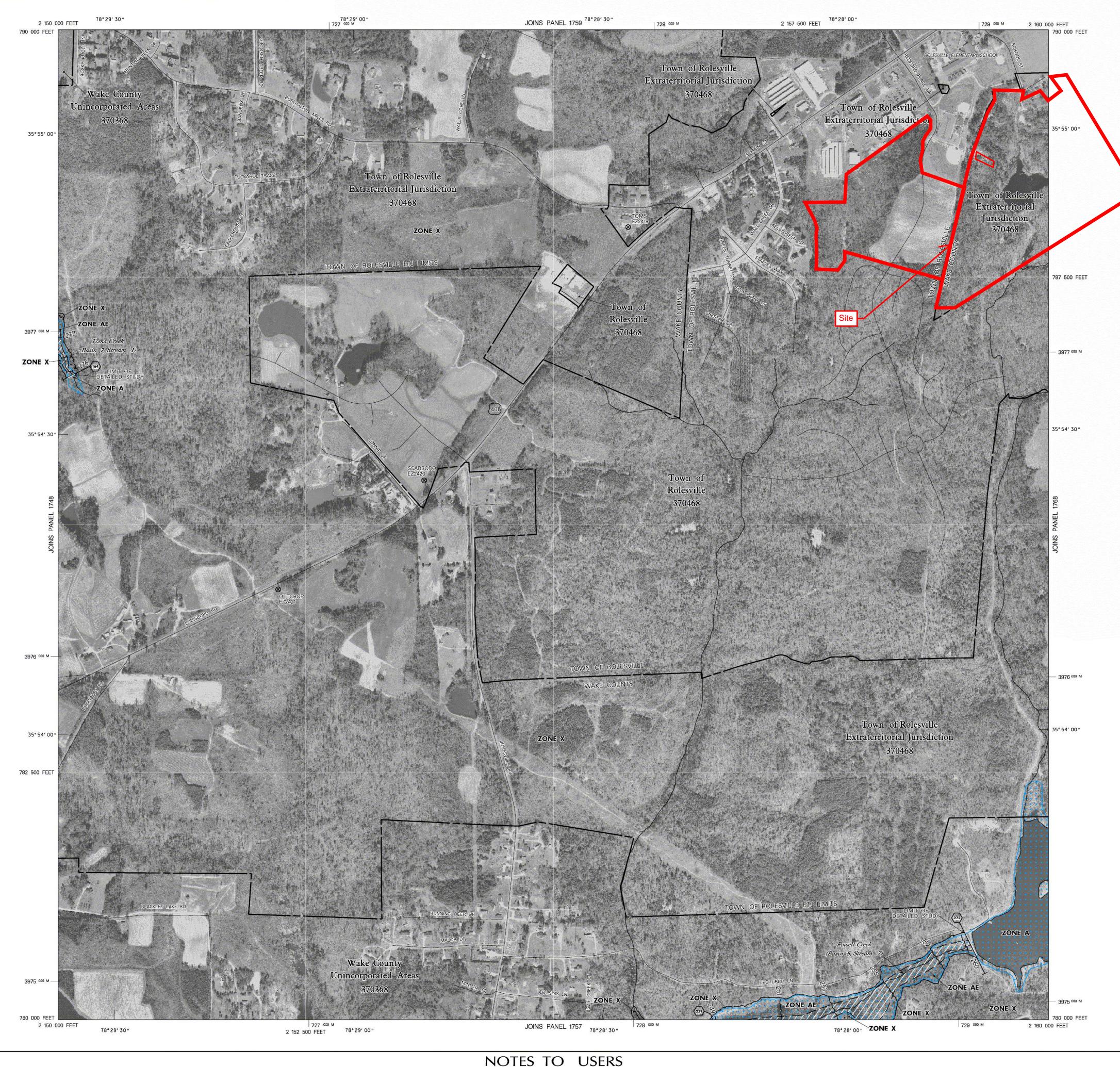
North Carolina Geodetic Survey 121 West Jones Street Raleigh, NC 27601 (919) 733-3836 www.ncgs.state.nc.us

	et (ft)
Wake - 0.88	

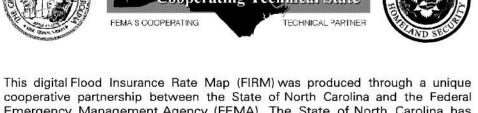
All streams listed in the Flood Hazard Data Table below were studied by detailed methods using field survey. Other flood hazard data shown on this map may have been derived using either a coastal analysis or limited detailed riverine analysis. More information on the flooding sources studied by these analyses is contained in the Flood Insurance Study report.

Fl	OOD HAZ	ZARD DAT	A TABLE	Floodway Width (feet) Left/Right Distance From			
Cross Section	Stream Station	Flood Discharge (cfs)	1 % Annual Chance (100-year) Water-Surface Elevation (feet NAVD 88)	the Center of Stream to Encroachment Boundary (Looking Downstream) of Total Floodway Width			
TOMS CRI	EEK (BASIN 7	, STREAM 1)					
164	16,350 ¹	NA	275.5	50			
POWELL	CREEK (BASII	N 8, STREAM 7	' }				
239	23,890 ²	NA	248.7	120			
272	27,200 ²	NA	259.9	110			

² Feet above confluence with Hodges Creek (Basin 8, Stream 1)







cooperative partnership between the State of North Carolina and the Federal Emergency Management Agency (FEMA). The State of North Carolina has implemented a long term approach of floodplain management to decrease the costs associated with flooding. This is demonstrated by the State's commitment to map floodplain areas at the local level. As a part of this effort, the State of North Carolina has joined in a Cooperating Technical State agreement with FEMA to produce and maintain this digital FIRM.

www.ncfloodmaps.com

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updated or additional flood hazard information. To obtain more detailed information in areas where Base Flood Elevations (BFEs) and/or floodways have been determined, users are encouraged to consult the Flood Profiles, Floodway Data, Limited Detailed Flood Hazard Data, and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

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> EFFECTIVE DATE OF FLOOD INSURANCE RATE MAP PANEL MAY 2, 2006

EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL

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(919) 715–8000 <u>www.nccrimecontrol.org/nfip</u> 1–800–638–6620 <u>www.fema.gov/nfip</u>

LEGEND

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No Base Flood Elevations determined. Base Flood Elevations determined.

greater flood.

Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations determined. Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities

Special Flood Hazard Area formerly protected from the 1% annual chance flood by a flood control system that was subsequently decertified. Zone AR indicates that the former flood control system is being restored to provide protection from the 1% annual chance or

Area to be protected from 1% annual chance flood by a Federal flood protection system under construction; no Base Flood Elevations Coastal flood zone with velocity hazard (wave action); Base Flood Elevations

FLOODWAY AREAS IN ZONE AE

The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood heights.

OTHER FLOOD AREAS

Areas of 0.2% annual chance flood; areas of future conditions 1% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.

OTHER AREAS

ZONE X Areas determined to be outside the 0.2% annual chance and future conditions 1% annual chance floodplain. Areas in which flood hazards are undetermined, but possible.

COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS

OTHERWISE PROTECTED AREAS (OPAs) CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas.

1% annual chance floodplain boundary 0.2% annual chance floodplain boundary and future conditions 1% annual chance floodplain boundary

_ _ _ _ _ Floodway boundary Zone D Boundary CBRS and OPA boundary

Boundary dividing Special Flood Hazard Area Zones and boundary dividing Special Flood Hazard Areas of different Base Flood Elevations, flood depths or flood velocities. Base Flood Elevation line and value; elevation in feet* ----513----Base Flood Elevation value where uniform within zone;

elevation in feet* *Referenced to the North American Vertical Datum of 1988

> Cross section line Transect line

(23)-----(23) 97°07′30", 32°22′30"

(EL 987)

4276000 M 1 477 500 FEET BM5510 🗸

M1.5

Geographic coordinates referenced to the North American Datum of 1983 (NAD 83) 1000-meter Universal Transverse Mercator grid ticks, zone 17 2500-foot grid values: North Carolina State Plane coordinate system (FIPSZONE 3200, State Plane NAD 83 feet)

North Carolina Geodetic Survey bench mark (see explanation in the Datum Information section of this FIRM panel). National Geodetic Survey bench mark (see explanation in the Datum Information section of this FIRM panel). River Mile



MAP SCALE 1" = 500' (1 : 6,000)

PANEL 1758J

FIRM FLOOD INSURANCE RATE MAP

PANEL 1758

(100)

(SEE LOCATOR DIAGRAM OR MAP INDEX FOR FIRM PANEL LAYOUT)

NORTH CAROLINA

COMMUNITY ROLESVILLE, TOWN OF

CID No. PANEL SUFFIX 370468 1758 J WAKE COUNTY

when placing map orders; the Community Number shown above should be used on insurance applications for the subject EFFECTIVE DATE MAP NUMBER

Notice to User: The Map Number shown below should be used





3720175800J

State of North Carolina Federal Emergency Management Agency

ATTACHMENT 5: RAINFALL DATA

#116- Please also include precipitation intensity (in/hr) NOAA rainfall data



NOAA Atlas 14, Volume 2, Version 3 Location name: Rolesville, North Carolina, USA* Latitude: 35.9195°, Longitude: -78.4618° Elevation: m/ft**

* source: ESRI Maps ** source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

 $G.M.\ Bonnin,\ D.\ Martin,\ B.\ Lin,\ T.\ Parzybok,\ M.Yekta,\ and\ D.\ Riley$

NOAA, National Weather Service, Silver Spring, Maryland

PF tabular | PF graphical | Maps & aerials

PF tabular

PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches) ¹										
Duration				Avera	ge recurren	ce interval (years)			
Duration	1	2	5	10	25	50	100	200	500	1000
5-min	0.403 (0.369-0.441)	0.468 (0.429-0.512)	0.534 (0.489-0.582)	0.599 (0.548-0.654)	0.665 (0.606-0.725)	0.718 (0.651-0.782)	0.764 (0.689-0.832)	0.805 (0.722-0.879)	0.851 (0.756-0.929)	0.892 (0.786-0.976)
10-min	0.644 (0.590-0.704)	0.749 (0.687-0.818)	0.855 (0.783-0.933)	0.959 (0.877-1.05)	1.06 (0.965-1.16)	1.14 (1.04-1.25)	1.21 (1.09-1.32)	1.28 (1.14-1.39)	1.35 (1.20-1.47)	1.41 (1.24-1.54)
15-min	0.805 (0.738-0.880)	0.942 (0.863-1.03)	1.08 (0.991-1.18)	1.21 (1.11-1.32)	1.34 (1.22-1.46)	1.45 (1.31-1.58)	1.53 (1.38-1.67)	1.61 (1.44-1.76)	1.69 (1.51-1.85)	1.76 (1.55-1.93)
30-min	1.10 (1.01-1.21)	1.30 (1.19-1.42)	1.54 (1.41-1.68)	1.76 (1.61-1.92)	1.99 (1.81-2.17)	2.18 (1.98-2.38)	2.35 (2.12-2.56)	2.51 (2.25-2.74)	2.70 (2.40-2.94)	2.86 (2.52-3.12)
60-min	1.38 (1.26-1.51)	1.63 (1.50-1.78)	1.97 (1.81-2.15)	2.29 (2.09-2.50)	2.65 (2.41-2.89)	2.95 (2.68-3.22)	3.24 (2.92-3.53)	3.52 (3.15-3.84)	3.87 (3.44-4.22)	4.17 (3.67-4.56)
2-hr	1.61 (1.46-1.78)	1.91 (1.75-2.10)	2.34 (2.13-2.56)	2.74 (2.49-3.01)	3.23 (2.91-3.53)	3.65 (3.28-3.99)	4.06 (3.62-4.43)	4.47 (3.96-4.89)	5.01 (4.40-5.48)	5.49 (4.78-6.02)
3-hr	1.71 (1.55-1.89)	2.03 (1.85-2.24)	2.49 (2.26-2.74)	2.94 (2.67-3.24)	3.49 (3.15-3.84)	3.99 (3.57-4.38)	4.47 (3.97-4.91)	4.99 (4.40-5.46)	5.67 (4.94-6.21)	6.29 (5.42-6.91)
6-hr	2.05 (1.87-2.26)	2.44 (2.23-2.68)	2.99 (2.72-3.28)	3.54 (3.22-3.88)	4.22 (3.81-4.62)	4.83 (4.34-5.28)	5.45 (4.85-5.95)	6.10 (5.37-6.65)	6.98 (6.07-7.61)	7.79 (6.68-8.50)
12-hr	2.41 (2.21-2.66)	2.87 (2.64-3.15)	3.54 (3.24-3.88)	4.21 (3.84-4.61)	5.06 (4.59-5.53)	5.84 (5.25-6.35)	6.62 (5.90-7.20)	7.47 (6.57-8.11)	8.64 (7.48-9.37)	9.72 (8.29-10.6)
24-hr	2.86 (2.66-3.08)	3.45 (3.22-3.72)	4.34 (4.04-4.68)	5.04 (4.68-5.43)	6.00 (5.56-6.46)	6.77 (6.25-7.28)	7.56 (6.95-8.14)	8.37 (7.67-9.02)	9.50 (8.66-10.2)	10.4 (9.42-11.2)
2-day	3.32 (3.09-3.57)	3.99 (3.72-4.30)	4.98 (4.63-5.36)	5.76 (5.35-6.20)	6.81 (6.31-7.34)	7.65 (7.06-8.24)	8.51 (7.84-9.17)	9.40 (8.62-10.1)	10.6 (9.68-11.5)	11.6 (10.5-12.6)
3-day	3.52 (3.28-3.77)	4.23 (3.95-4.53)	5.24 (4.89-5.62)	6.05 (5.63-6.48)	7.15 (6.63-7.67)	8.02 (7.42-8.60)	8.91 (8.22-9.57)	9.84 (9.03-10.6)	11.1 (10.1-12.0)	12.1 (11.0-13.1)
4-day	3.72 (3.48-3.98)	4.46 (4.17-4.77)	5.51 (5.15-5.89)	6.34 (5.91-6.77)	7.48 (6.95-7.99)	8.39 (7.77-8.97)	9.32 (8.60-9.97)	10.3 (9.45-11.0)	11.6 (10.6-12.4)	12.6 (11.5-13.6)
7-day	4.31 (4.04-4.60)	5.15 (4.82-5.50)	6.28 (5.88-6.70)	7.18 (6.71-7.66)	8.41 (7.83-8.98)	9.39 (8.72-10.0)	10.4 (9.63-11.1)	11.4 (10.5-12.3)	12.9 (11.8-13.8)	14.0 (12.8-15.0)
10-day	4.91 (4.61-5.23)	5.84 (5.48-6.23)	7.04 (6.59-7.49)	7.97 (7.46-8.49)	9.24 (8.62-9.84)	10.2 (9.53-10.9)	11.2 (10.4-12.0)	12.3 (11.4-13.1)	13.7 (12.6-14.6)	14.7 (13.5-15.8)
20-day	6.59 (6.20-7.01)	7.78 (7.32-8.28)	9.21 (8.66-9.80)	10.3 (9.71-11.0)	11.9 (11.1-12.6)	13.1 (12.2-13.9)	14.3 (13.3-15.2)	15.5 (14.4-16.6)	17.2 (15.9-18.4)	18.5 (17.0-19.8)
30-day	8.18 (7.72-8.68)	9.62 (9.07-10.2)	11.2 (10.6-11.9)	12.4 (11.7-13.2)	14.1 (13.2-14.9)	15.3 (14.3-16.3)	16.6 (15.5-17.6)	17.8 (16.6-19.0)	19.5 (18.1-20.8)	20.7 (19.2-22.2)
45-day	10.4 (9.89-11.0)	12.2 (11.6-12.9)	14.0 (13.3-14.8)	15.4 (14.6-16.2)	17.2 (16.2-18.1)	18.5 (17.5-19.5)	19.9 (18.7-21.0)	21.2 (19.9-22.4)	22.9 (21.4-24.3)	24.2 (22.6-25.7)
60-day	12.5 (11.9-13.1)	14.6 (13.9-15.3)	16.5 (15.7-17.4)	18.0 (17.1-19.0)	20.0 (18.9-21.0)	21.4 (20.2-22.5)	22.8 (21.5-24.0)	24.2 (22.8-25.5)	25.9 (24.4-27.4)	27.3 (25.6-28.8)

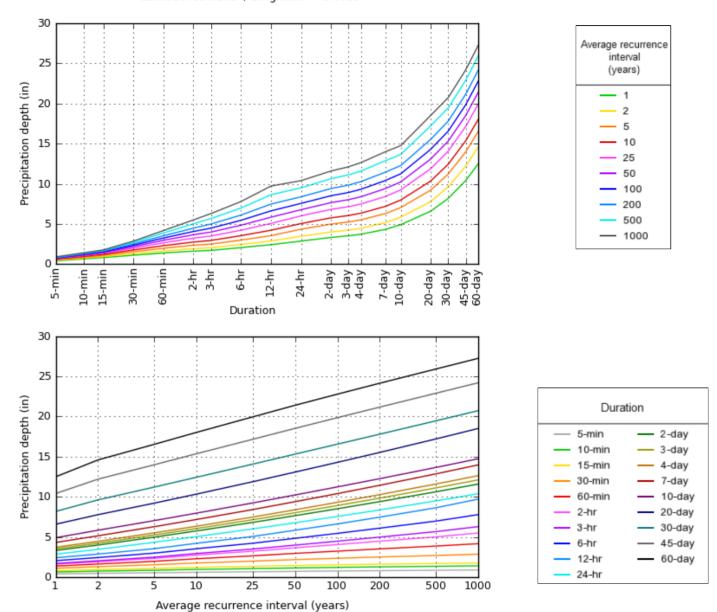
Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

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PDS-based depth-duration-frequency (DDF) curves Latitude: 35.9195°, Longitude: -78.4618°



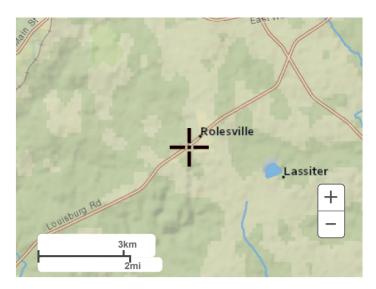
NOAA Atlas 14, Volume 2, Version 3

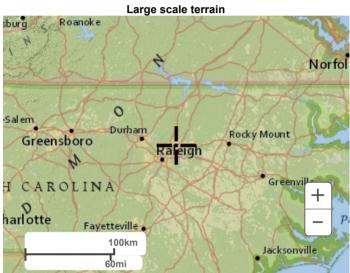
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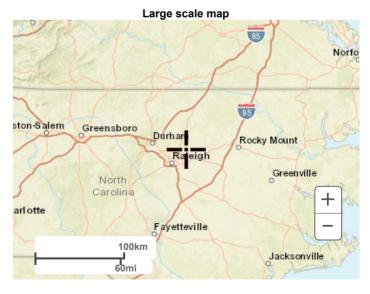
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Maps & aerials

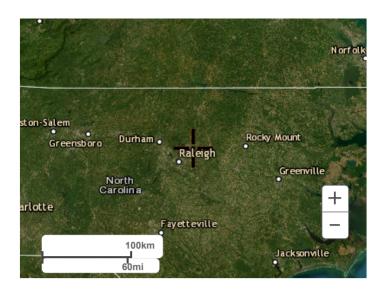
Small scale terrain







Large scale aerial



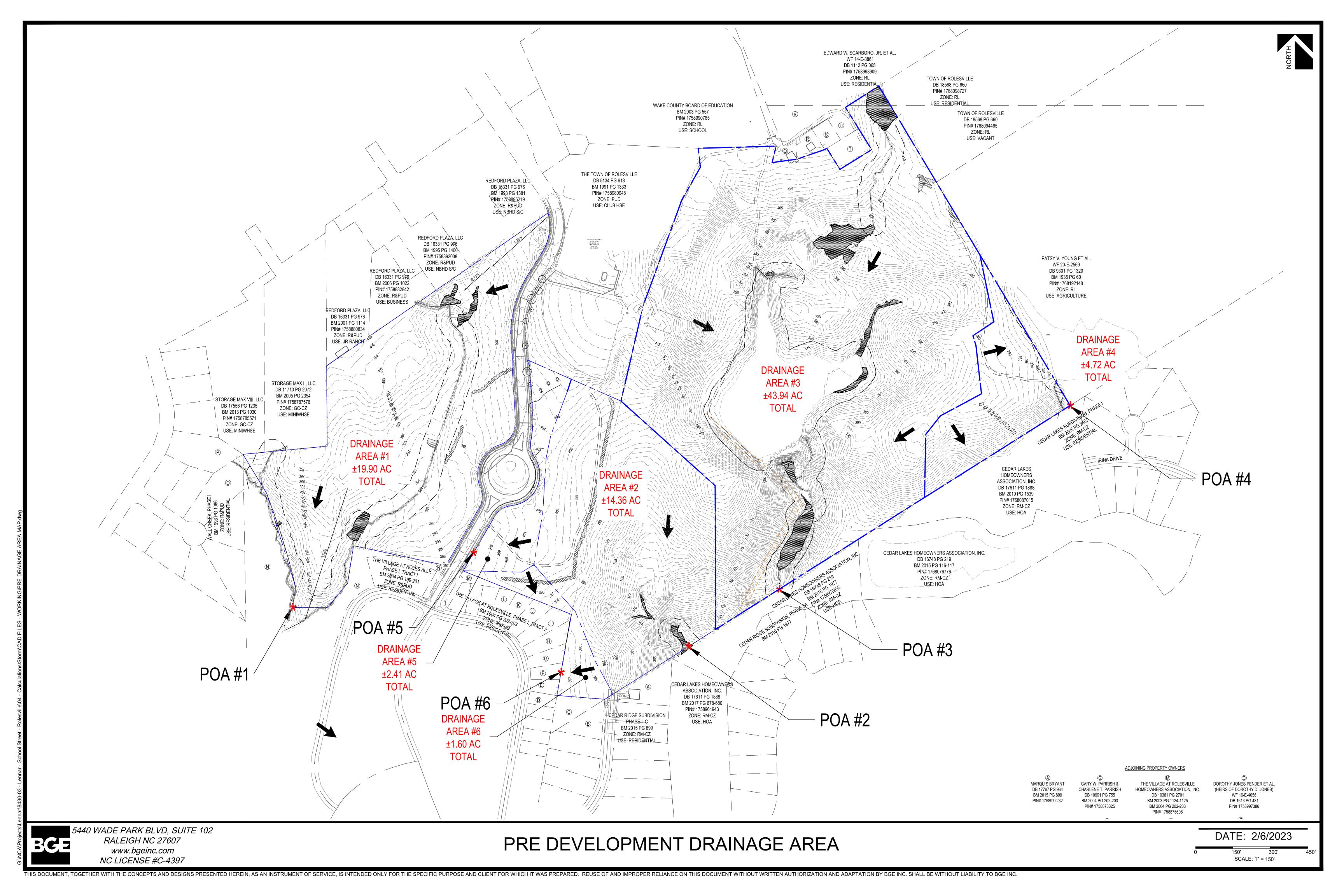
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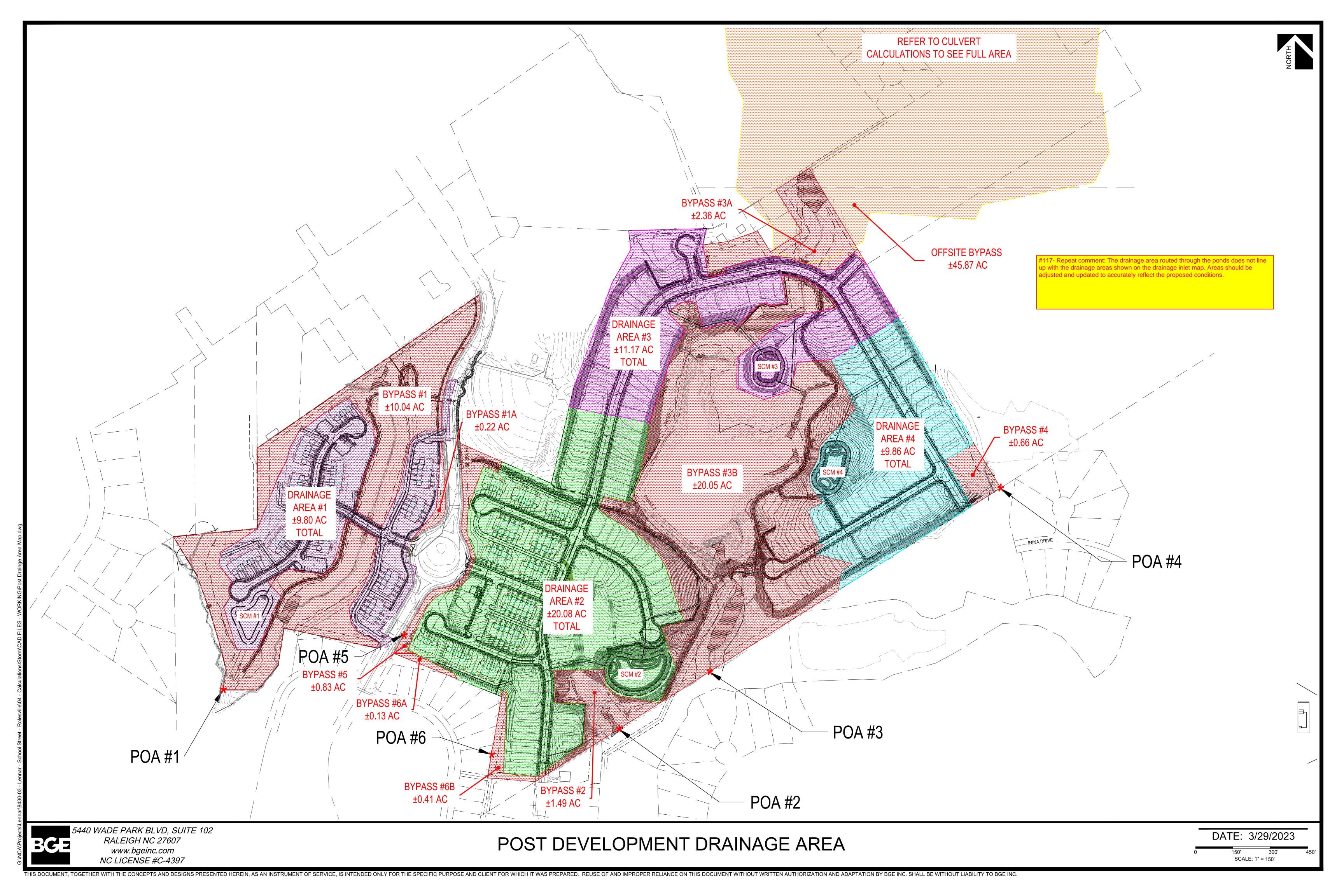
US Department of Commerce
National Oceanic and Atmospheric Administration
National Weather Service
National Water Center
1325 East West Highway

1325 East West Highway Silver Spring, MD 20910 Questions?: <u>HDSC.Questions@noaa.gov</u>

<u>Disclaimer</u>

ATTACHMENT 6: PRE- AND POST-DEVELOPMENT DRAINAGE AREA MAPS





ATTACHMENT 7: SCM CALCULATIONS

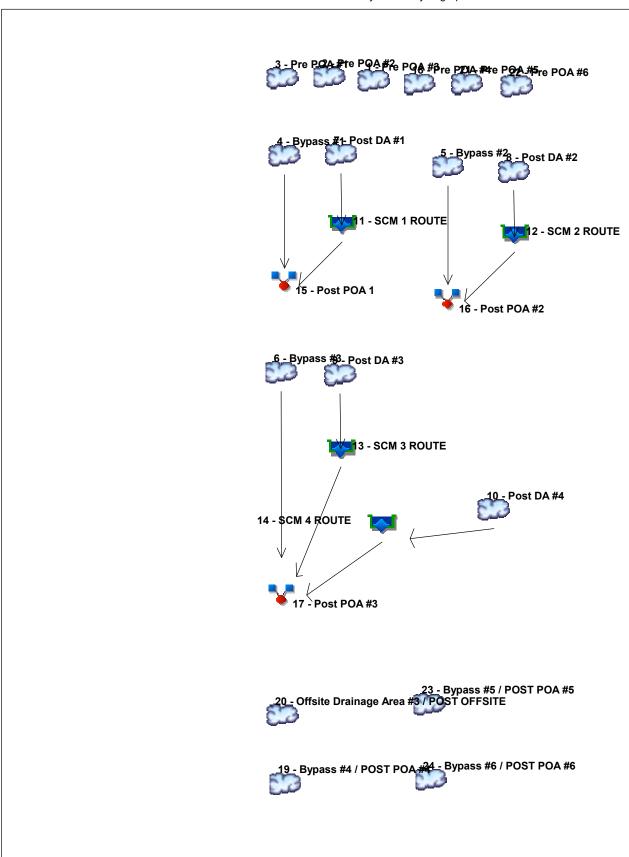
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Project: SCMs.gpw Tuesday, 08 / 1 / 2023

Hydrograph Return Period Recap

-	Hydrograph	Inflow				Hydrograph					
lo.	type (origin)	hyd(s)	1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	100-yr	Description
1	SCS Runoff		81.28	113.63			208.92	268.97		367.67	Pre POA #3
2	SCS Runoff		32.35	43.89			76.33	96.21		128.55	Pre POA #2
3	SCS Runoff		34.25	48.19			89.35	115.26		157.92	Pre POA #1
4	SCS Runoff		15.87	22.47			41.99	54.27		74.51	Bypass #1
5	SCS Runoff		2.861	3.908			6.855	8.668		11.62	Bypass #2
6	SCS Runoff		34.65	49.08			91.72	118.54		162.74	Bypass #3
7	SCS Runoff		22.87	30.09			49.85	61.80		81.12	Post DA #1
8	SCS Runoff		46.87	61.65			102.14	126.62		166.21	Post DA #2
9	SCS Runoff		24.89	33.04			55.50	69.13		91.20	Post DA #3
10	SCS Runoff		21.97	29.17			48.99	61.02		80.50	Post DA #4
11	Reservoir	7	2.495	5.265			31.49	50.04		70.93	SCM 1 ROUTE
12	Reservoir	8	3.566	8.895			66.55	95.97		139.06	SCM 2 ROUTE
13	Reservoir	9	2.885	10.15			49.73	63.92		85.19	SCM 3 ROUTE
14	Reservoir	10	1.909	4.021			12.07	30.17		58.87	SCM 4 ROUTE
15	Combine	4, 11,	15.95	24.25			63.14	98.20		141.43	Post POA 1
16	Combine	5, 12,	3.809	9.499			71.35	102.38		149.22	Post POA #2
17	Combine	6, 13, 14,	34.72	52.38			144.21	192.27		291.65	Post POA #3
18	SCS Runoff		10.04	14.02			25.45	32.66		44.48	Pre POA #4
19	SCS Runoff		1.021	1.446			2.701	3.491		4.793	Bypass #4 / POST POA #4
20	SCS Runoff		41.37	60.62			118.39	155.43		217.12	Offsite Drainage Area #3 / POST OFF
21	SCS Runoff		5.429	7.366			12.81	16.15		21.57	Pre POA #5
22	SCS Runoff		3.604	4.890			8.504	10.72		14.32	Pre POA #6
23	SCS Runoff		1.850	2.455			4.124	5.137		6.777	Bypass #5 / POST POA #5
24	SCS Runoff		1.037	1.416			2.484	3.141		4.212	Bypass #6 / POST POA #6

Proj. file: SCMs.gpw

Tuesday, 08 / 1 / 2023

Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

lyd. Io.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	81.28	2	718	162,567				Pre POA #3
2	SCS Runoff	32.35	2	718	65,226				Pre POA #2
3	SCS Runoff	34.25	2	720	78,533				Pre POA #1
4	SCS Runoff	15.87	2	722	41,755				Bypass #1
5	SCS Runoff	2.861	2	720	7,445				Bypass #2
6	SCS Runoff	34.65	2	722	91,203				Bypass #3
7	SCS Runoff	22.87	2	720	59,338				Post DA #1
3	SCS Runoff	46.87	2	720	121,582				Post DA #2
9	SCS Runoff	24.89	2	720	64,527				Post DA #3
10	SCS Runoff	21.97	2	720	56,960				Post DA #4
11	Reservoir	2.495	2	754	39,436	7	386.92	31,712	SCM 1 ROUTE
12	Reservoir	3.566	2	774	90,493	8	353.89	68,186	SCM 2 ROUTE
13	Reservoir	2.885	2	752	42,452	9	387.41	33,658	SCM 3 ROUTE
14	Reservoir	1.909	2	764	38,884	10	382.32	30,945	SCM 4 ROUTE
5	Combine	15.95	2	722	81,191	4, 11,			Post POA 1
6	Combine	3.809	2	766	97,937	5, 12,			Post POA #2
17	Combine	34.72	2	722	172,539	6, 13, 14,			Post POA #3
18	SCS Runoff	10.04	1	716	17,463				Pre POA #4
19	SCS Runoff	1.021	2	722	2,686				Bypass #4 / POST POA #4
20	SCS Runoff	41.37	2	730	159,839				Offsite Drainage Area #3 / POST OF
21	SCS Runoff	5.429	2	718	10,947				Pre POA #5
22	SCS Runoff	3.604	2	718	7,267				Pre POA #6
23	SCS Runoff	1.850	2	720	4,795				Bypass #5 / POST POA #5
24	SCS Runoff	1.037	2	720	2,698				Bypass #6 / POST POA #6
SC	Ms.gpw				Return F	Period: 1 Ye	ear	Tuesday, 0	08 / 1 / 2023

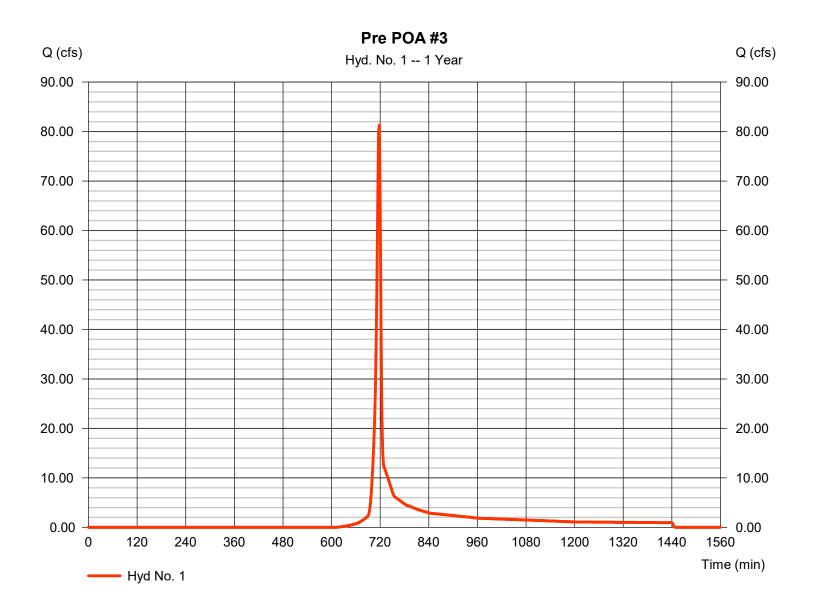
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Tuesday, 08 / 1 / 2023

Hyd. No. 1

Pre POA #3

= 81.28 cfsHydrograph type = SCS Runoff Peak discharge Storm frequency Time to peak = 1 yrs= 718 min = 162,567 cuft Time interval = 2 min Hyd. volume Drainage area = 43.940 acCurve number = 79 Hydraulic length = 0 ftBasin Slope = 0.0 %Tc method = TR55 Time of conc. (Tc) $= 3.10 \, \text{min}$ Total precip. = 2.86 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Hyd. No. 1

Pre POA #3

<u>Description</u>	<u>A</u>		<u>B</u>		<u>C</u>		<u>Totals</u>	
Sheet Flow Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	= 0.011 = 300.0 = 2.20 = 7.06		0.011 0.0 0.00 0.00		0.011 0.0 0.00 0.00			
Travel Time (min)	= 2.12	+	0.00	+	0.00	=	2.12	
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	= 193.00 = 4.30 = Paved =4.22		0.00 0.00 Paved 0.00		0.00 0.00 Paved 0.00			
Travel Time (min)	= 0.76	+	0.00	+	0.00	=	0.76	
Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s)	= 30.00 = 16.00 = 5.00 = 0.015 =33.84		0.00 0.00 0.00 0.015 0.00		0.00 0.00 0.00 0.015			
Flow length (ft)	({0})500.0		0.0		0.0			
Travel Time (min)	= 0.25	+	0.00	+	0.00	=	0.25	
Total Travel Time, Tc								

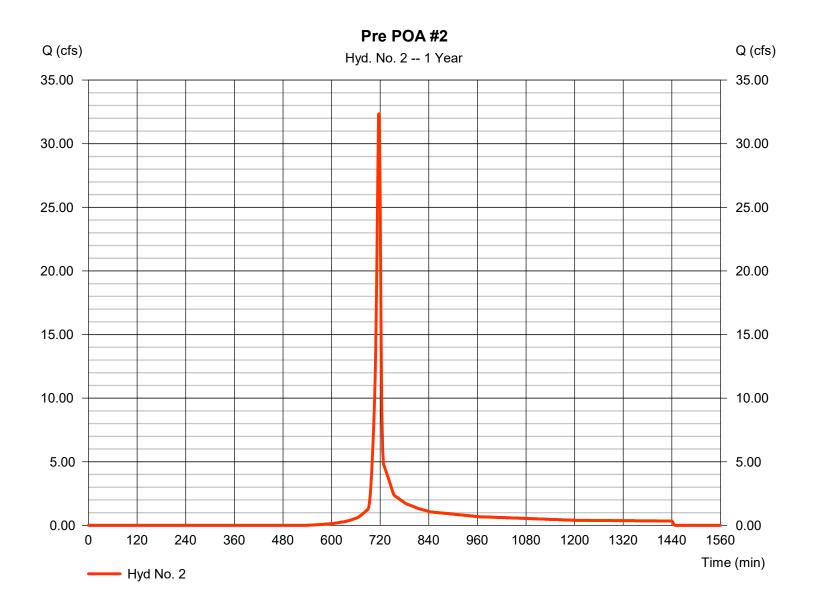
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Tuesday, 08 / 1 / 2023

Hyd. No. 2

Pre POA #2

Hydrograph type = SCS Runoff Peak discharge = 32.35 cfsStorm frequency Time to peak = 1 yrs= 718 min Time interval = 2 min Hyd. volume = 65.226 cuft Drainage area = 14.360 ac Curve number = 83 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) $= 5.60 \, \text{min}$ = TR55 Total precip. = 2.86 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



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Hyd. No. 2

Pre POA #2

<u>Description</u>	<u>A</u>		<u>B</u>		<u>C</u>		<u>Totals</u>		
Sheet Flow Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	= 0.011 = 300.0 = 2.20 = 3.80		0.011 0.0 0.00 0.00		0.011 0.0 0.00 0.00				
Travel Time (min)	= 2.72	+	0.00	+	0.00	=	2.72		
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	= 850.00 = 6.00 = Paved =4.98		0.00 0.00 Paved 0.00		0.00 0.00 Paved 0.00				
Travel Time (min)	= 2.85	+	0.00	+	0.00	=	2.85		
Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s)	= 0.00 = 0.00 = 0.00 = 0.015 =0.00		0.00 0.00 0.00 0.015 0.00		0.00 0.00 0.00 0.015				
Flow length (ft)	({0})0.0		0.0		0.0				
Travel Time (min)	= 0.00	+	0.00	+	0.00	=	0.00		
Total Travel Time, Tc									

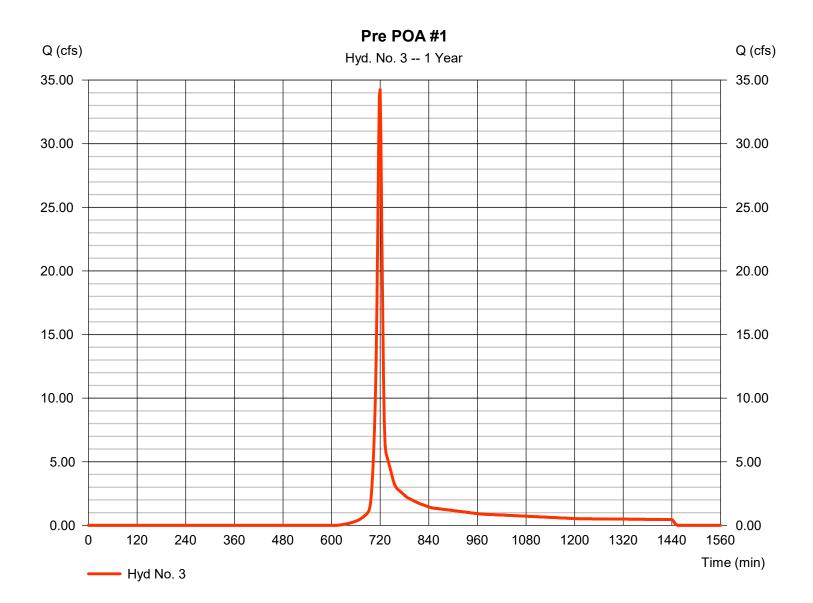
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Hyd. No. 3

Pre POA #1

Hydrograph type = SCS Runoff Peak discharge = 34.25 cfsStorm frequency Time to peak = 1 yrs= 720 min = 78,533 cuft Time interval = 2 min Hyd. volume Drainage area Curve number = 19.900 ac = 79 Hydraulic length = 0 ftBasin Slope = 0.0 %Tc method Time of conc. (Tc) $= 9.70 \, \text{min}$ = TR55 Total precip. = 2.86 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



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Hyd. No. 3

Pre POA #1

<u>Description</u>	<u>A</u>		<u>B</u>		<u>C</u>		<u>Totals</u>	
Sheet Flow Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	= 0.011 = 300.0 = 2.20 = 4.60		0.011 0.0 0.00 0.00		0.011 0.0 0.00 0.00			
Travel Time (min)	= 2.52	+	0.00	+	0.00	=	2.52	
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	= 150.00 = 3.50 = Unpaved =3.02		0.00 0.00 Paved 0.00		0.00 0.00 Paved 0.00			
Travel Time (min)	= 0.83	+	0.00	+	0.00	=	0.83	
Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s)	= 16.00 = 20.00 = 1.00 = 0.015 =8.55		0.00 0.00 0.00 0.015 0.00		0.00 0.00 0.00 0.015			
Flow length (ft)	({0})3240.0		0.0		0.0			
Travel Time (min)	= 6.31	+	0.00	+	0.00	=	6.31	
Total Travel Time, Tc								

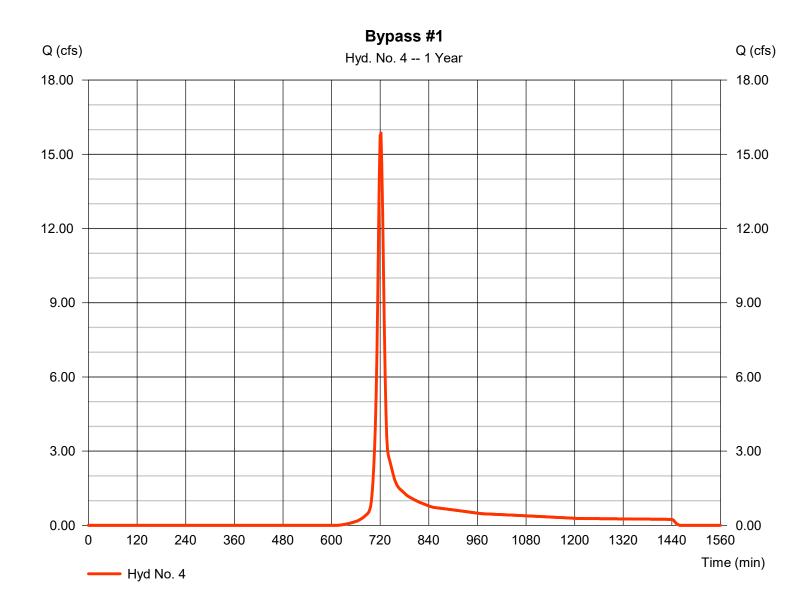
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Hyd. No. 4

Bypass #1

Hydrograph type = SCS Runoff Peak discharge = 15.87 cfsStorm frequency = 1 yrsTime to peak = 722 min Time interval = 2 min Hyd. volume = 41,755 cuft Drainage area Curve number = 10.260 ac= 79 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 10.00 \, \text{min}$ = User Total precip. = 2.86 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



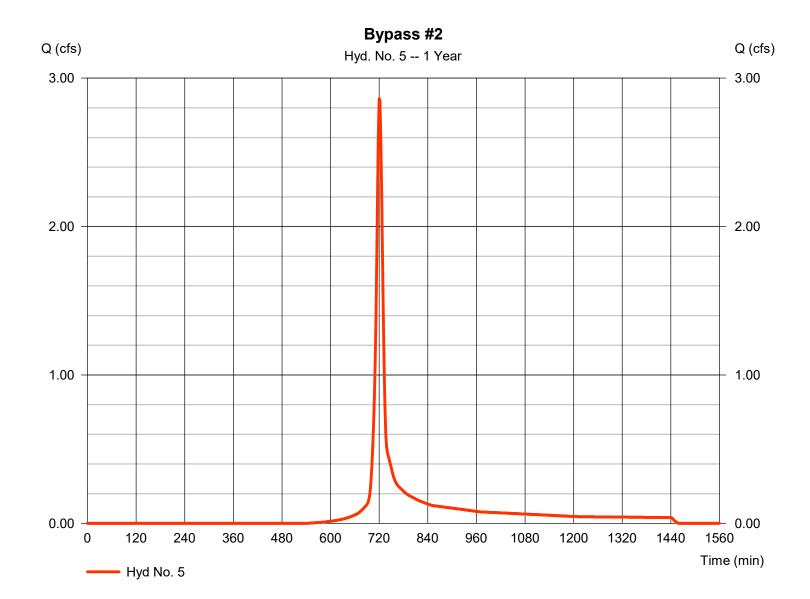
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Tuesday, 08 / 1 / 2023

Hyd. No. 5

Bypass #2

Hydrograph type = SCS Runoff Peak discharge = 2.861 cfsStorm frequency = 1 yrsTime to peak = 720 min Time interval = 2 min Hyd. volume = 7,445 cuftDrainage area Curve number = 1.490 ac= 83 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 10.00 \, \text{min}$ = User Total precip. = 2.86 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



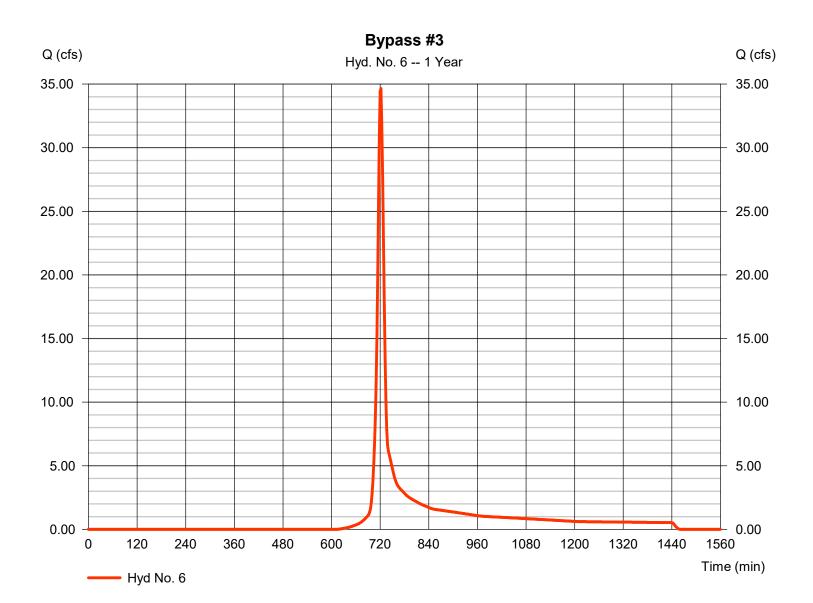
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Tuesday, 08 / 1 / 2023

Hyd. No. 6

Bypass #3

Hydrograph type = SCS Runoff Peak discharge = 34.65 cfsStorm frequency = 1 yrsTime to peak = 722 min Time interval = 2 min Hyd. volume = 91,203 cuft Drainage area Curve number = 22.410 ac= 79 Hydraulic length Basin Slope = 0.0 %= 0 ftTc method Time of conc. (Tc) $= 10.00 \, \text{min}$ = User Total precip. = 2.86 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



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= 24 hrs

Tuesday, 08 / 1 / 2023

= 484

Hyd. No. 7

Storm duration

120

Hyd No. 7

240

360

480

600

720

840

960

1080

1200

1320

1440

1560

Time (min)

Post DA #1

Hydrograph type = SCS Runoff Peak discharge = 22.87 cfsStorm frequency = 1 yrsTime to peak = 720 min Time interval = 2 min Hyd. volume = 59,338 cuft Drainage area Curve number = 9.800 ac= 87 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 10.00 \, \text{min}$ = User Total precip. = 2.86 inDistribution = Type II

Shape factor

Post DA #1 Q (cfs) Q (cfs) Hyd. No. 7 -- 1 Year 24.00 24.00 20.00 20.00 16.00 16.00 12.00 12.00 8.00 8.00 4.00 4.00 0.00 0.00

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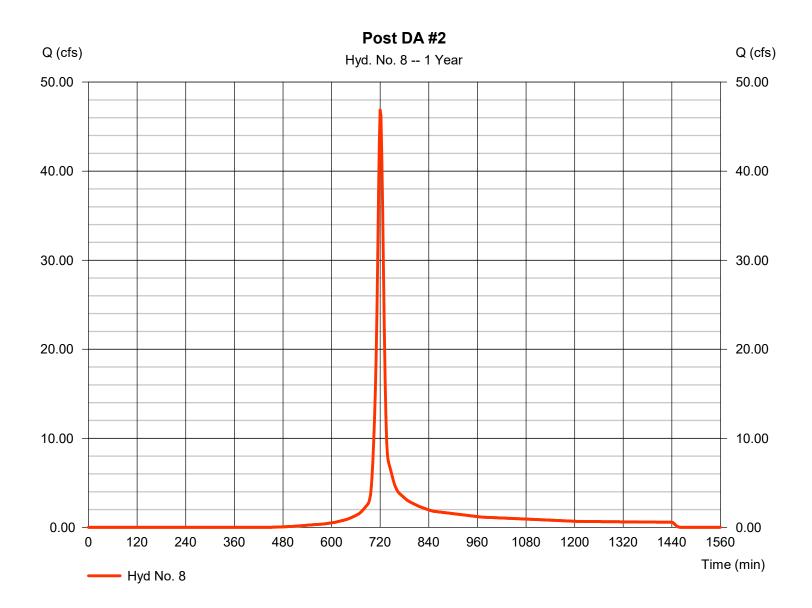
Hyd. No. 8

Post DA #2

Hydrograph type= SCS RunoffPeak discharge= 46.87 cfsStorm frequency= 1 yrsTime to peak= 720 minTime interval= 2 minHyd. volume= 121,582 cuft

Drainage area = 20.080 ac Curve number = 87 Basin Slope = 0.0 % Hydraulic length = 0 ft

Tc method = User Time of conc. (Tc) = 10.00 min
Total precip. = 2.86 in Distribution = Type II
Storm duration = 24 hrs Shape factor = 484



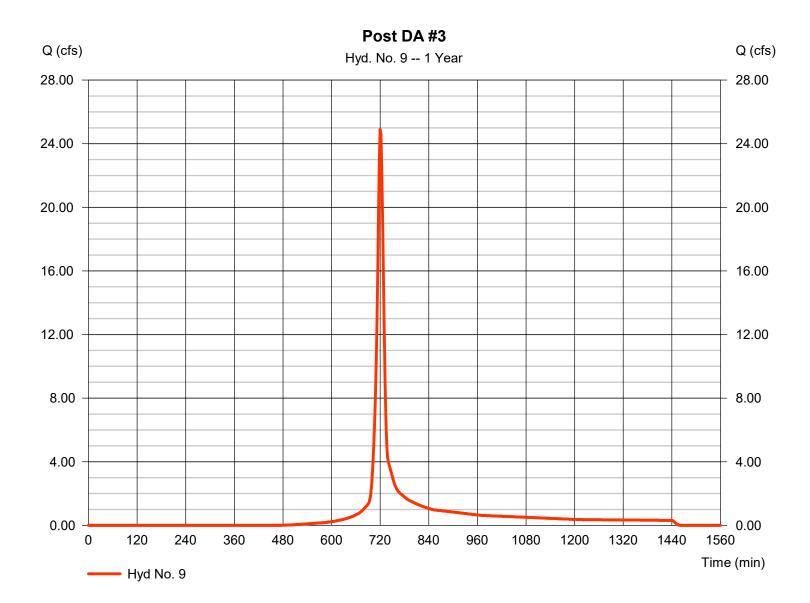
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Hyd. No. 9

Post DA #3

Hydrograph type = SCS Runoff Peak discharge = 24.89 cfsStorm frequency = 1 yrsTime to peak = 720 min Time interval = 2 min Hyd. volume = 64,527 cuftDrainage area = 11.170 ac Curve number = 86 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 10.00 \, \text{min}$ = User Total precip. = 2.86 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

= 24 hrs

Tuesday, 08 / 1 / 2023

= 484

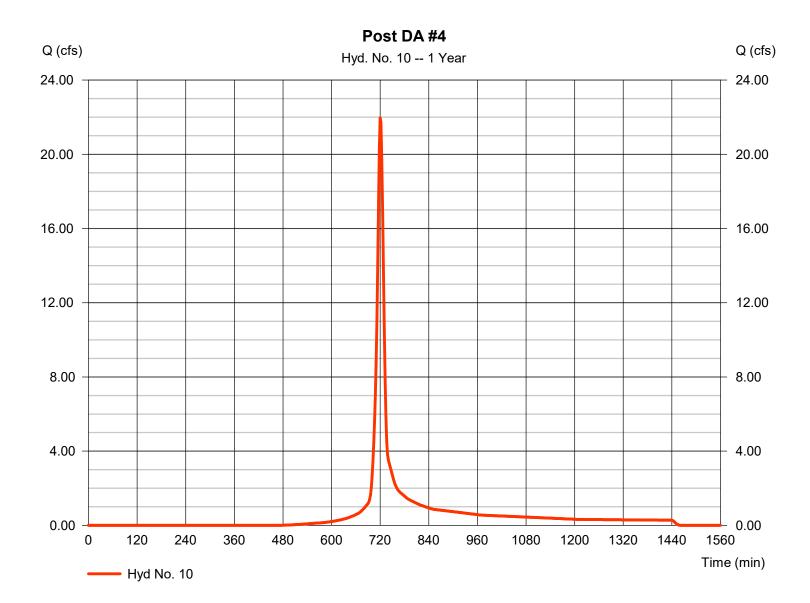
Hyd. No. 10

Storm duration

Post DA #4

Hydrograph type = SCS Runoff Peak discharge = 21.97 cfsStorm frequency = 1 yrsTime to peak = 720 min Time interval = 2 min Hyd. volume = 56,960 cuftDrainage area Curve number = 9.860 ac= 86 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 10.00 \, \text{min}$ = User Total precip. = 2.86 inDistribution = Type II

Shape factor



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

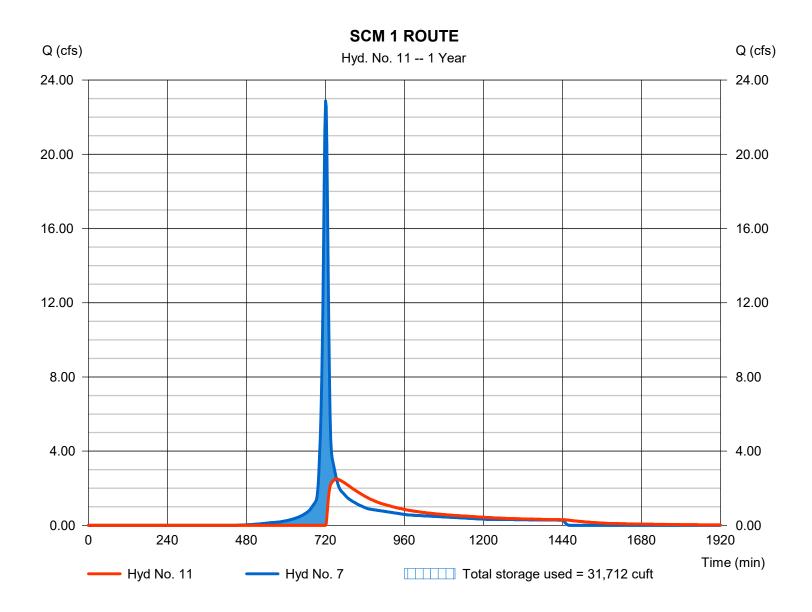
Tuesday, 08 / 1 / 2023

Hyd. No. 11

SCM 1 ROUTE

Hydrograph type Peak discharge = 2.495 cfs= Reservoir Storm frequency = 1 yrsTime to peak = 754 min Time interval = 2 min Hyd. volume = 39,436 cuft Inflow hyd. No. = 7 - Post DA #1 Max. Elevation = 386.92 ft= SCM 1 Reservoir name Max. Storage = 31,712 cuft

Storage Indication method used.



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Tuesday, 08 / 1 / 2023

Pond No. 1 - SCM 1

Pond Data

Contours -User-defined contour areas. Conic method used for volume calculation. Begining Elevation = 384.50 ft

Stage / Storage Table

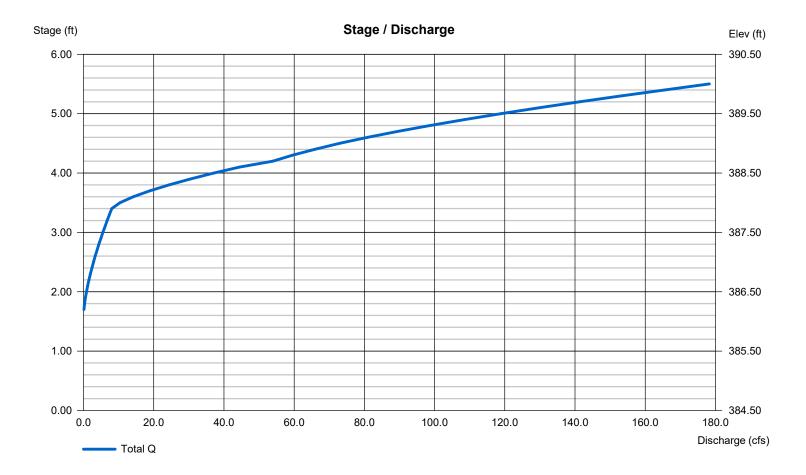
Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft		
0.00	384.50	10,590	0	0		
0.50	385.00	12,050	5,656	5,656		
1.50	386.00	13,565	12,799	18,454		
2.50	387.00	15,138	14,343	32,797		
3.50	388.00	16,767	15,944	48,741		
4.50	389.00	18,453	17,602	66,343		
5.50	390.00	20,196	19,316	85,659		

Culvert / Orifice Structures

Weir Structures

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 24.00	1.00	0.00	0.00	Crest Len (ft)	= 16.00	1.00	20.00	Inactive
Span (in)	= 24.00	0.00	0.00	0.00	Crest El. (ft)	= 387.90	386.10	388.60	0.00
No. Barrels	= 1	1	0	0	Weir Coeff.	= 3.33	3.33	3.33	3.33
Invert El. (ft)	= 379.00	384.50	0.00	0.00	Weir Type	= 1	Rect	Rect	
Length (ft)	= 165.00	1.00	0.00	0.00	Multi-Stage	= Yes	No	No	No
Slope (%)	= 0.61	0.00	0.00	n/a					
N-Value	= .013	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 0.000 (by	Contour)		
Multi-Stage	= n/a	No	No	No	TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



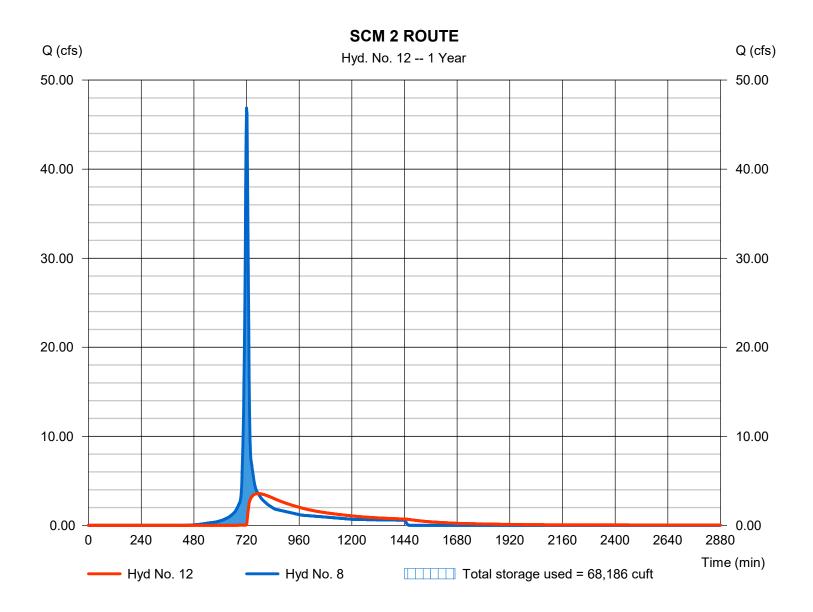
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Tuesday, 08 / 1 / 2023

Hyd. No. 12

SCM 2 ROUTE

Hydrograph type Peak discharge = 3.566 cfs= Reservoir Storm frequency = 1 yrsTime to peak = 774 min Time interval = 2 min Hyd. volume = 90,493 cuftInflow hyd. No. Max. Elevation = 8 - Post DA #2 = 353.89 ftReservoir name = SCM 2 Max. Storage = 68,186 cuft



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Tuesday, 08 / 1 / 2023

Pond No. 2 - SCM 2

Pond Data

Contours -User-defined contour areas. Conic method used for volume calculation. Begining Elevation = 351.50 ft

Stage / Storage Table

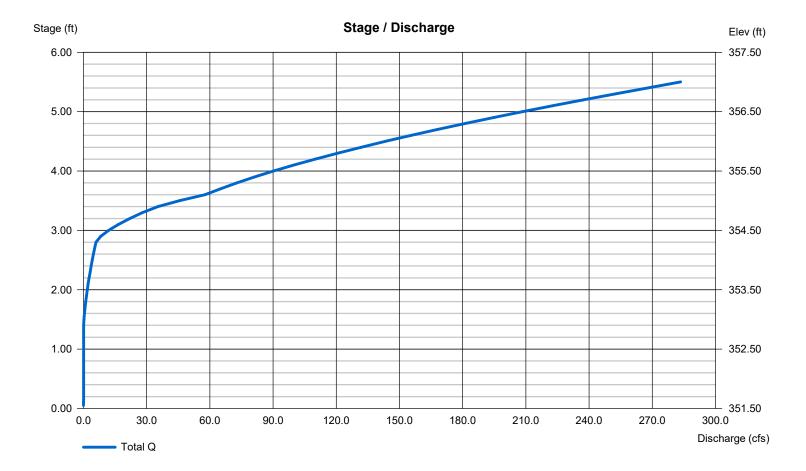
Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	351.50	25,295	0	0
0.50	352.00	27,224	13,125	13,125
1.50	353.00	29,209	28,208	41,333
2.50	354.00	31,251	30,221	71,555
3.50	355.00	33,350	32,292	103,846
4.50	356.00	35,504	34,418	138,264
5.50	357.00	37,716	36,601	174,865

Culvert / Orifice Structures

Weir Structures

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 24.00	1.00	0.00	0.00	Crest Len (ft)	= 16.00	1.00	20.00	Inactive
Span (in)	= 24.00	1.00	0.00	0.00	Crest El. (ft)	= 354.30	352.85	354.85	0.00
No. Barrels	= 1	1	0	0	Weir Coeff.	= 3.33	3.33	3.33	3.33
Invert El. (ft)	= 347.00	351.50	0.00	0.00	Weir Type	= 1	Rect	Rect	
Length (ft)	= 87.00	1.00	0.00	0.00	Multi-Stage	= Yes	No	No	No
Slope (%)	= 1.15	0.00	0.00	n/a					
N-Value	= .013	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 0.000 (by	Contour)		
Multi-Stage	= n/a	No	No	No	TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



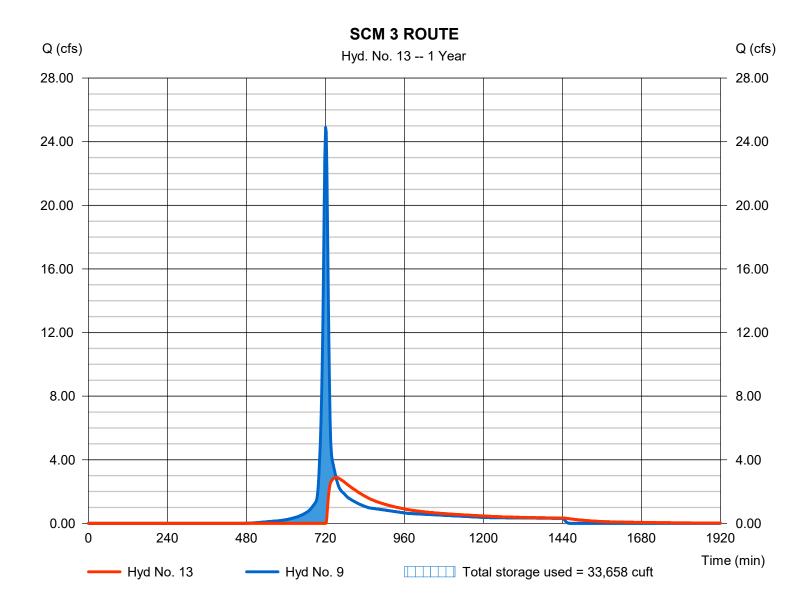
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Tuesday, 08 / 1 / 2023

Hyd. No. 13

SCM 3 ROUTE

Hydrograph type Peak discharge = 2.885 cfs= Reservoir Storm frequency = 1 yrsTime to peak = 752 min Time interval = 2 min Hyd. volume = 42,452 cuft Inflow hyd. No. Max. Elevation = 387.41 ft= 9 - Post DA #3 Reservoir name = SCM 3 Max. Storage = 33,658 cuft



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Tuesday, 08 / 1 / 2023

Pond No. 3 - SCM 3

Pond Data

Contours -User-defined contour areas. Conic method used for volume calculation. Begining Elevation = 384.50 ft

Stage / Storage Table

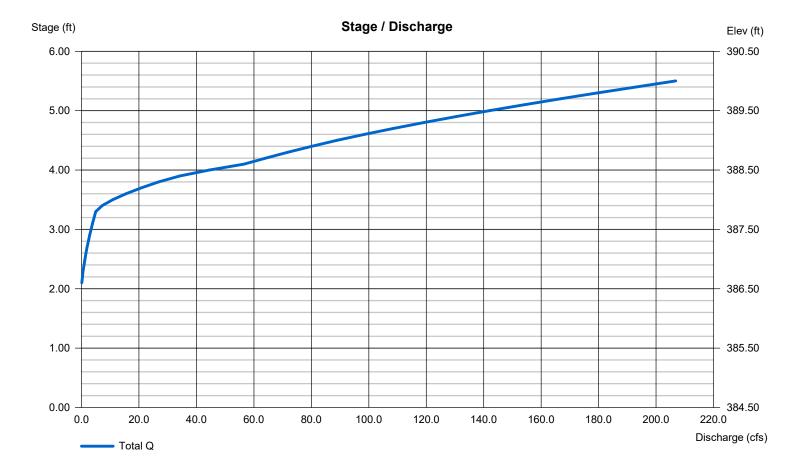
Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	384.50	9,342	0	0
0.50	385.00	10,446	4,944	4,944
1.50	386.00	11,603	11,018	15,962
2.50	387.00	12,816	12,203	28,166
3.50	388.00	14,086	13,445	41,610
4.50	389.00	15,412	14,743	56,353
5.50	390.00	16,783	16,091	72,444

Culvert / Orifice Structures

Weir Structures

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 24.00	1.00	0.00	0.00	Crest Len (ft)	= 16.00	1.00	20.00	Inactive
Span (in)	= 24.00	0.00	0.00	0.00	Crest El. (ft)	= 387.80	386.50	388.35	0.00
No. Barrels	= 1	1	0	0	Weir Coeff.	= 3.33	3.33	3.33	3.33
Invert El. (ft)	= 380.00	384.50	0.00	0.00	Weir Type	= 1	Rect	Rect	
Length (ft)	= 118.00	1.00	0.00	0.00	Multi-Stage	= Yes	No	No	No
Slope (%)	= 0.85	0.00	0.00	n/a					
N-Value	= .013	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 0.000 (by	Contour)		
Multi-Stage	= n/a	No	No	No	TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



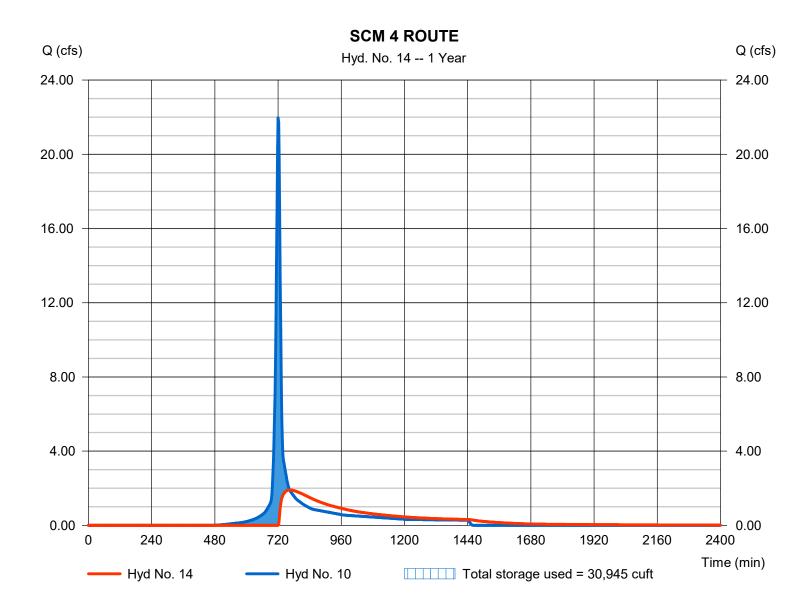
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Tuesday, 08 / 1 / 2023

Hyd. No. 14

SCM 4 ROUTE

Hydrograph type Peak discharge = 1.909 cfs= Reservoir Storm frequency = 1 yrsTime to peak = 764 min Time interval = 2 min Hyd. volume = 38,884 cuft Inflow hyd. No. Max. Elevation = 382.32 ft= 10 - Post DA #4 Reservoir name = SCM 4 Max. Storage = 30,945 cuft



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Tuesday, 08 / 1 / 2023

Pond No. 4 - SCM 4

Pond Data

Contours -User-defined contour areas. Conic method used for volume calculation. Begining Elevation = 380.50 ft

Stage / Storage Table

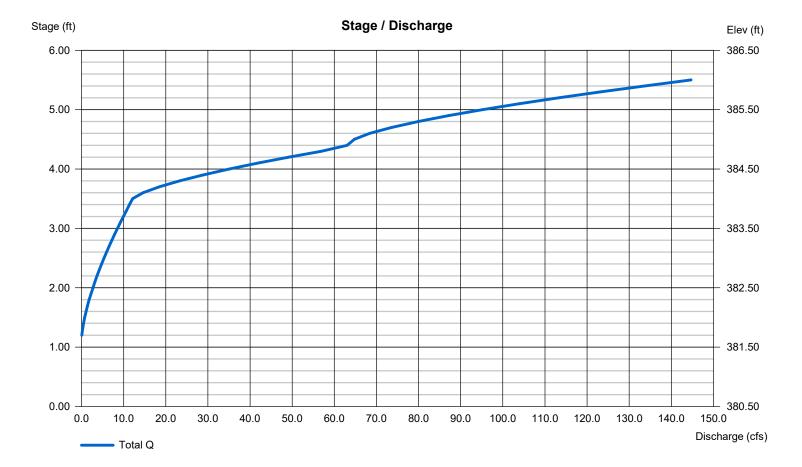
Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	380.50	14,636	0	0
0.50	381.00	16,358	7,744	7,744
1.50	382.00	18,005	17,173	24,917
2.50	383.00	19,735	18,862	43,778
3.50	384.00	21,522	20,620	64,398
4.50	385.00	22,548	22,031	86,429
5.50	386.00	24,300	23,416	109,845

Culvert / Orifice Structures

Weir Structures

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 24.00	1.00	0.00	0.00	Crest Len (ft)	= 16.00	1.00	20.00	Inactive
Span (in)	= 24.00	0.00	0.00	0.00	Crest El. (ft)	= 384.00	381.63	385.00	0.00
No. Barrels	= 1	1	0	0	Weir Coeff.	= 3.33	3.33	3.33	3.33
Invert El. (ft)	= 375.00	380.50	0.00	0.00	Weir Type	= 1	Rect	Rect	
Length (ft)	= 63.00	1.00	0.00	0.00	Multi-Stage	= Yes	No	No	No
Slope (%)	= 1.60	0.00	0.00	n/a					
N-Value	= .013	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 0.000 (by	Contour)		
Multi-Stage	= n/a	No	No	No	TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



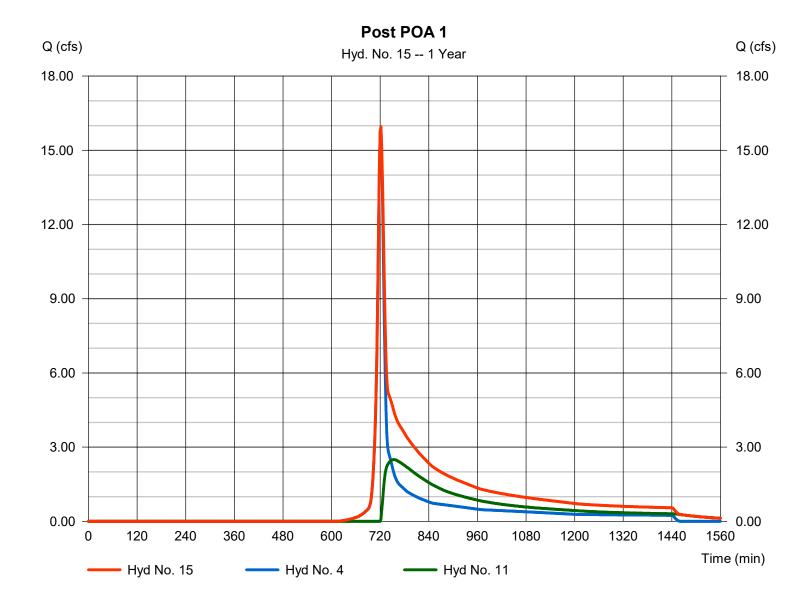
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Tuesday, 08 / 1 / 2023

Hyd. No. 15

Post POA 1

Hydrograph type = Combine Peak discharge = 15.95 cfsStorm frequency Time to peak = 1 yrs= 722 min Time interval = 2 min Hyd. volume = 81,191 cuft Inflow hyds. = 4, 11 Contrib. drain. area = 10.260 ac



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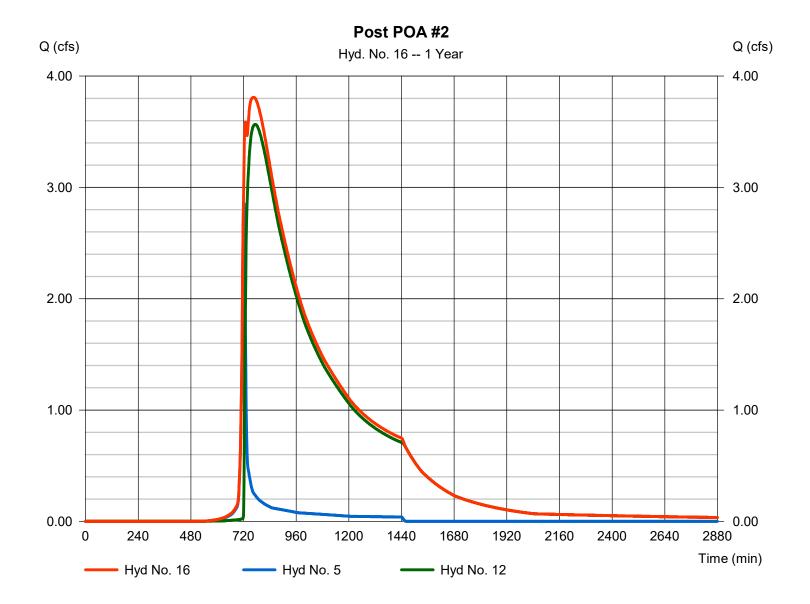
Tuesday, 08 / 1 / 2023

Hyd. No. 16

Post POA #2

Hydrograph type = Combine
Storm frequency = 1 yrs
Time interval = 2 min
Inflow hyds. = 5, 12

Peak discharge = 3.809 cfs
Time to peak = 766 min
Hyd. volume = 97,937 cuft
Contrib. drain. area = 1.490 ac



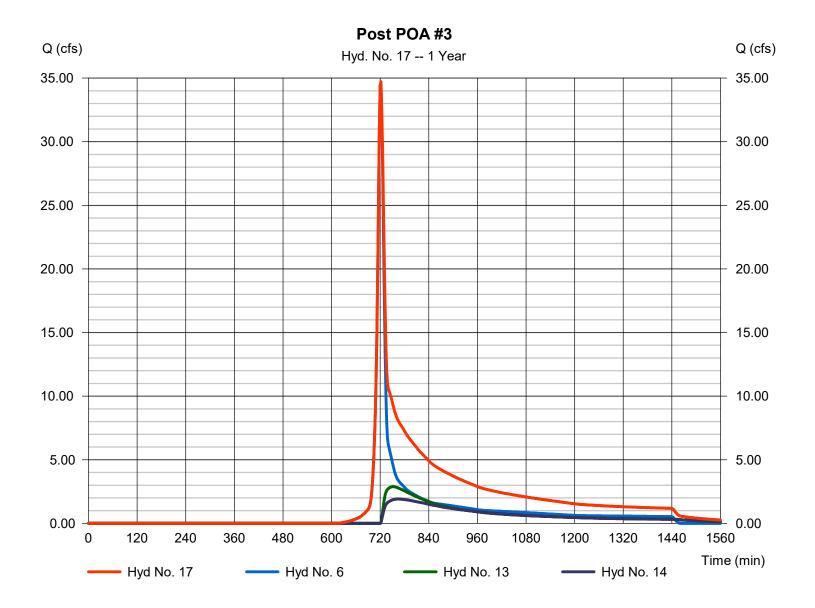
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Tuesday, 08 / 1 / 2023

Hyd. No. 17

Post POA #3

Hydrograph type = Combine Peak discharge = 34.72 cfsStorm frequency Time to peak = 1 yrs= 722 min Time interval = 2 min Hyd. volume = 172,539 cuft Inflow hyds. = 6, 13, 14 Contrib. drain. area = 22.410 ac



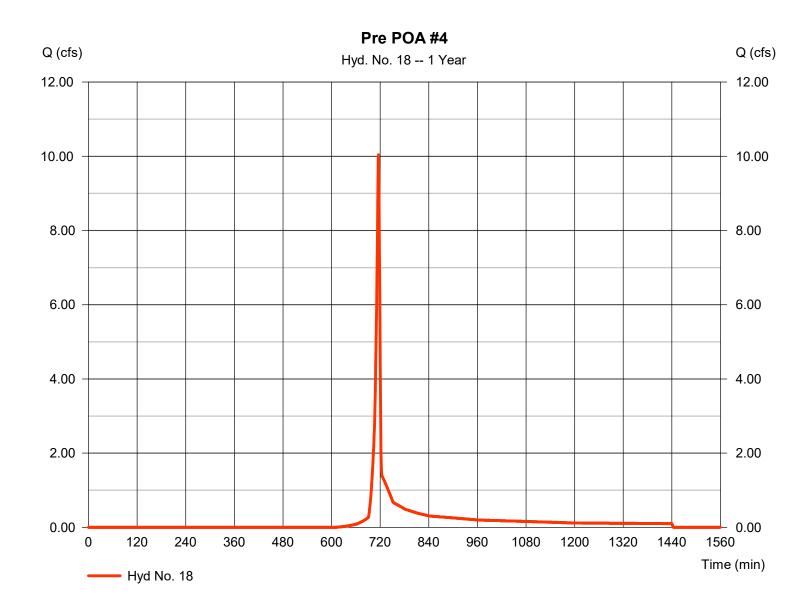
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Tuesday, 08 / 1 / 2023

Hyd. No. 18

Pre POA #4

Hydrograph type = SCS Runoff Peak discharge = 10.04 cfsStorm frequency = 1 yrsTime to peak = 716 min Time interval = 1 min Hyd. volume = 17,463 cuft Drainage area Curve number = 4.720 ac= 79 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) = 2.10 min = TR55 Total precip. = 2.86 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Hyd. No. 18

Pre POA #4

<u>Description</u>	<u>A</u>		<u>B</u>		<u>C</u>		<u>Totals</u>
Sheet Flow Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	= 0.011 = 300.0 = 2.20 = 8.00		0.011 0.0 0.00 0.00		0.011 0.0 0.00 0.00		
Travel Time (min)	= 2.02	+	0.00	+	0.00	=	2.02
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	= 30.00 = 8.00 = Unpaved =4.56	d	0.00 0.00 Paved 0.00		0.00 0.00 Paved 0.00		
Travel Time (min)	= 0.11	+	0.00	+	0.00	=	0.11
Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s)	= 0.00 = 0.00 = 0.00 = 0.015 =0.00		0.00 0.00 0.00 0.015 0.00		0.00 0.00 0.00 0.015		
Flow length (ft)	({0})0.0		0.0		0.0		
Travel Time (min)	= 0.00	+	0.00	+	0.00	=	0.00
Total Travel Time, Tc							2.10 min

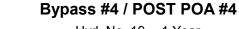
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

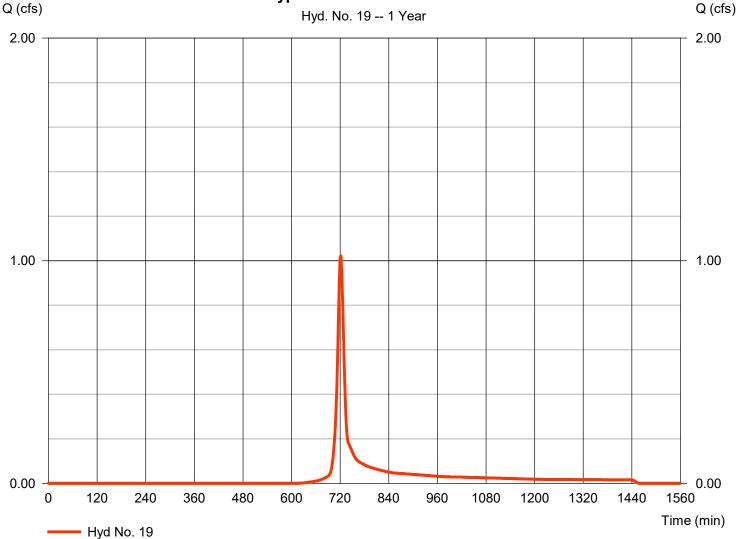
Tuesday, 08 / 1 / 2023

Hyd. No. 19

Bypass #4 / POST POA #4

Hydrograph type = SCS Runoff Peak discharge = 1.021 cfsStorm frequency = 1 yrsTime to peak = 722 min Time interval = 2 min Hyd. volume = 2.686 cuft Curve number = 79 Drainage area = 0.660 acBasin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 10.00 \, \text{min}$ = User Total precip. = 2.86 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484





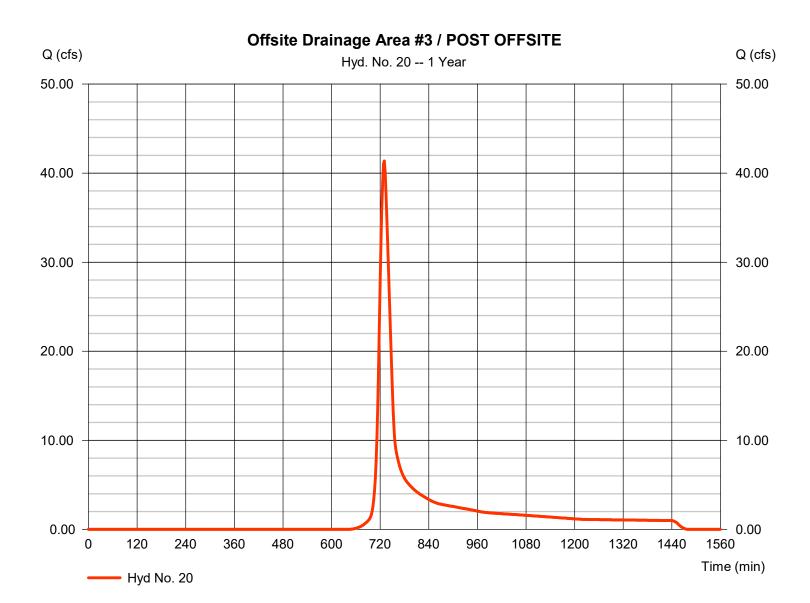
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Tuesday, 08 / 1 / 2023

Hyd. No. 20

Offsite Drainage Area #3 / POST OFFSITE

Hydrograph type = SCS Runoff Peak discharge = 41.37 cfsStorm frequency Time to peak = 730 min = 1 yrsTime interval = 2 min Hyd. volume = 159,839 cuft Curve number Drainage area = 45.870 ac = 77 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) = 25.00 min = User Total precip. = 2.86 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484



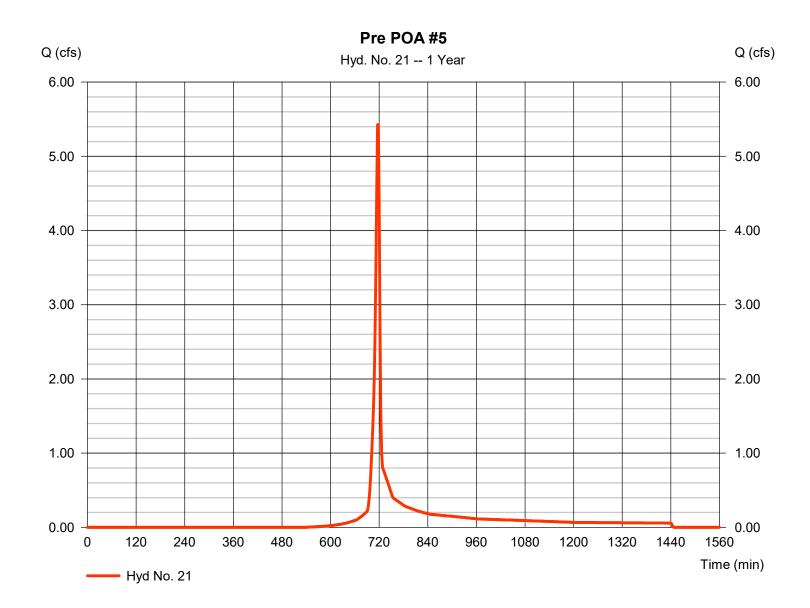
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Tuesday, 08 / 1 / 2023

Hyd. No. 21

Pre POA #5

Hydrograph type = SCS Runoff Peak discharge = 5.429 cfsStorm frequency = 1 yrsTime to peak = 718 min Time interval = 2 min Hyd. volume = 10,947 cuftDrainage area Curve number = 2.410 ac= 83 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 4.50 \, \text{min}$ = TR55 Total precip. = 2.86 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



TR55 Tc Worksheet

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Hyd. No. 21

Pre POA #5

<u>Description</u>	<u>A</u>		<u>B</u>		<u>C</u>		<u>Totals</u>	
Sheet Flow Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	= 0.011 = 300.0 = 3.45 = 2.09		0.011 0.0 0.00 0.00		0.011 0.0 0.00 0.00			
Travel Time (min)	= 2.76	+	0.00	+	0.00	=	2.76	
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	= 253.00 = 2.32 = Unpaved =2.46	t	0.00 0.00 Paved 0.00		0.00 0.00 Paved 0.00			
Travel Time (min)	= 1.72	+	0.00	+	0.00	=	1.72	
Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s)	= 0.00 = 0.00 = 0.00 = 0.015 =0.00		0.00 0.00 0.00 0.015 0.00		0.00 0.00 0.00 0.015			
Flow length (ft)	({0})0.0		0.0		0.0			
Travel Time (min)	= 0.00	+	0.00	+	0.00	=	0.00	
Total Travel Time, Tc							4.50 min	

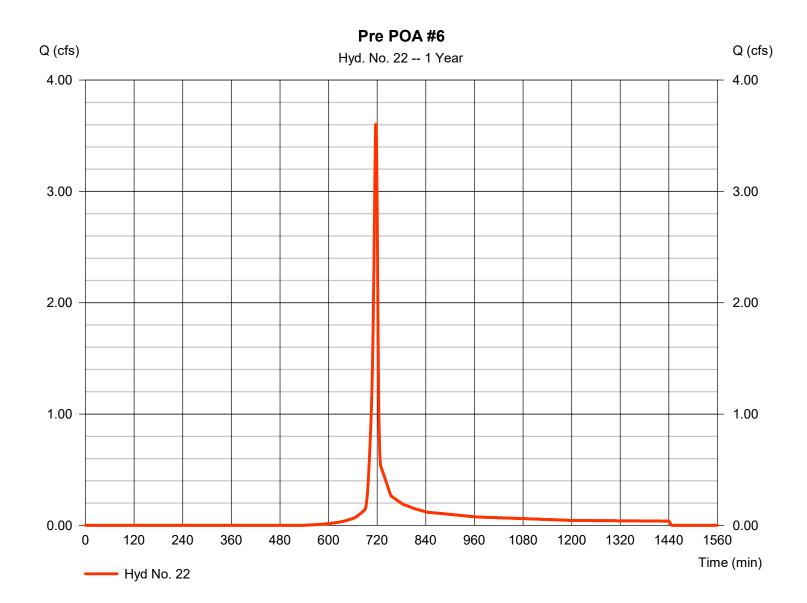
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Tuesday, 08 / 1 / 2023

Hyd. No. 22

Pre POA #6

Hydrograph type = SCS Runoff Peak discharge = 3.604 cfsStorm frequency = 1 yrsTime to peak = 718 min Time interval = 2 min Hyd. volume = 7.267 cuftDrainage area Curve number = 1.600 ac= 83 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 4.20 \, \text{min}$ = TR55 Total precip. = 2.86 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



TR55 Tc Worksheet

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Hyd. No. 22

Pre POA #6

<u>Description</u>	<u>A</u>		<u>B</u>		<u>C</u>		<u>Totals</u>
Sheet Flow Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%)	= 0.011 = 146.0 = 3.45 = 3.87		0.011 0.0 0.00 0.00		0.011 0.0 0.00 0.00		
Travel Time (min)	= 1.21	+	0.00	+	0.00	=	1.21
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	= 437.00 = 2.35 = Unpaved =2.47	d	0.00 0.00 Paved 0.00		0.00 0.00 Paved 0.00		
Travel Time (min)	= 2.94	+	0.00	+	0.00	=	2.94
Channel Flow X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s)	= 0.00 = 0.00 = 0.00 = 0.015 =0.00		0.00 0.00 0.00 0.015 0.00		0.00 0.00 0.00 0.015		
Flow length (ft)	({0})0.0		0.0		0.0		
Travel Time (min)	= 0.00	+	0.00	+	0.00	=	0.00
Total Travel Time, Tc							4.20 min

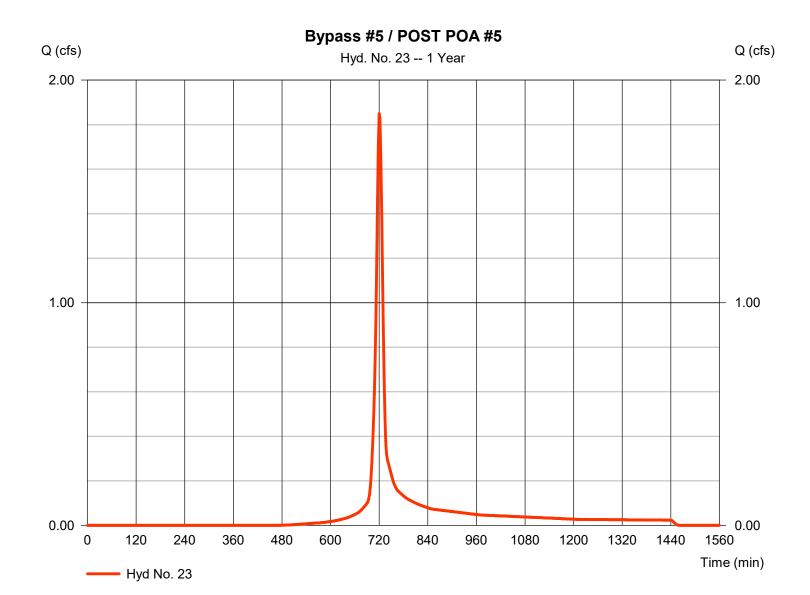
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Tuesday, 08 / 1 / 2023

Hyd. No. 23

Bypass #5 / POST POA #5

Hydrograph type = SCS Runoff Peak discharge = 1.850 cfsStorm frequency = 1 yrsTime to peak = 720 min Time interval = 2 min Hyd. volume = 4,795 cuftDrainage area Curve number = 0.830 ac= 86 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 10.00 \, \text{min}$ = User Total precip. = 2.86 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Tuesday, 08 / 1 / 2023

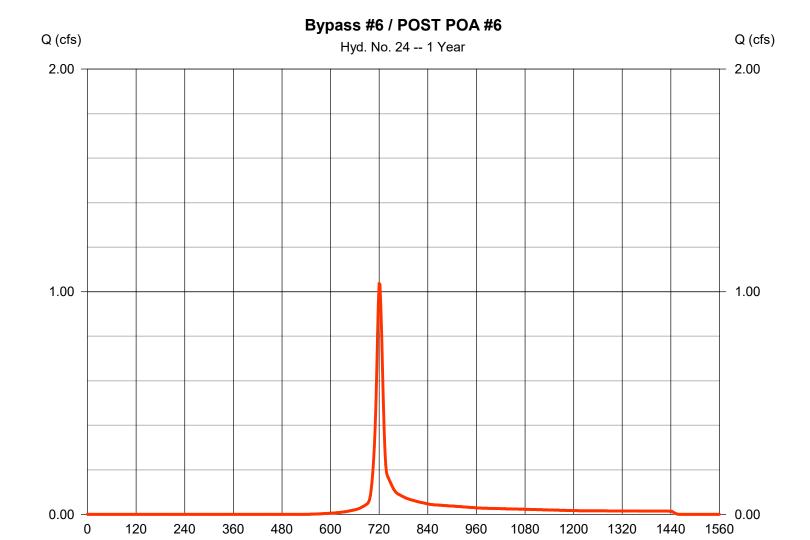
Time (min)

Hyd. No. 24

Bypass #6 / POST POA #6

Hyd No. 24

Hydrograph type = SCS Runoff Peak discharge = 1.037 cfsStorm frequency = 1 yrsTime to peak = 720 min Time interval = 2 min Hyd. volume = 2.698 cuft Drainage area Curve number = 0.540 ac= 83 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 10.00 \, \text{min}$ = User Total precip. = 2.86 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

	Hydrailow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, inc								utodesko civil 30o by Autodesk, Ilic. vz
Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	208.92	2	716	424,093				Pre POA #3
2	SCS Runoff	76.33	2	716	156,884				Pre POA #2
3	SCS Runoff	89.35	2	718	204,872				Pre POA #1
4	SCS Runoff	41.99	2	720	108,929				Bypass #1
5	SCS Runoff	6.855	2	720	17,906				Bypass #2
6	SCS Runoff	91.72	2	720	237,923				Bypass #3
7	SCS Runoff	49.85	2	720	132,251				Post DA #1
8	SCS Runoff	102.14	2	720	270,980				Post DA #2
9	SCS Runoff	55.50	2	720	146,532				Post DA #3
10	SCS Runoff	48.99	2	720	129,347				Post DA #4
11	Reservoir	31.49	2	728	112,349	7	388.42	56,055	SCM 1 ROUTE
12	Reservoir	66.55	2	728	239,739	8	355.22	111,397	SCM 2 ROUTE
13	Reservoir	49.73	2	724	124,456	9	388.54	49,620	SCM 3 ROUTE
14	Reservoir	12.07	2	734	111,271	10	383.99	64,173	SCM 4 ROUTE
15	Combine	63.14	2	724	221,278	4, 11,			Post POA 1
16	Combine	71.35	2	726	257,645	5, 12,			Post POA #2
17	Combine	144.21	2	722	473,650	6, 13, 14,			Post POA #3
18	SCS Runoff	25.45	1	715	45,556				Pre POA #4
19	SCS Runoff	2.701	2	720	7,007				Bypass #4 / POST POA #4
20	SCS Runoff	118.39	2	728	435,415				Offsite Drainage Area #3 / POST OFF
21	SCS Runoff	12.81	2	716	26,329				Pre POA #5
22	SCS Runoff	8.504	2	716	17,480				Pre POA #6
23	SCS Runoff	4.124	2	720	10,888				Bypass #5 / POST POA #5
24	SCS Runoff	2.484	2	720	6,490				Bypass #6 / POST POA #6
sc	SCMs.gpw Return Period: 10 Year Tuesday, 08 / 1 / 2023			08 / 1 / 2023					

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

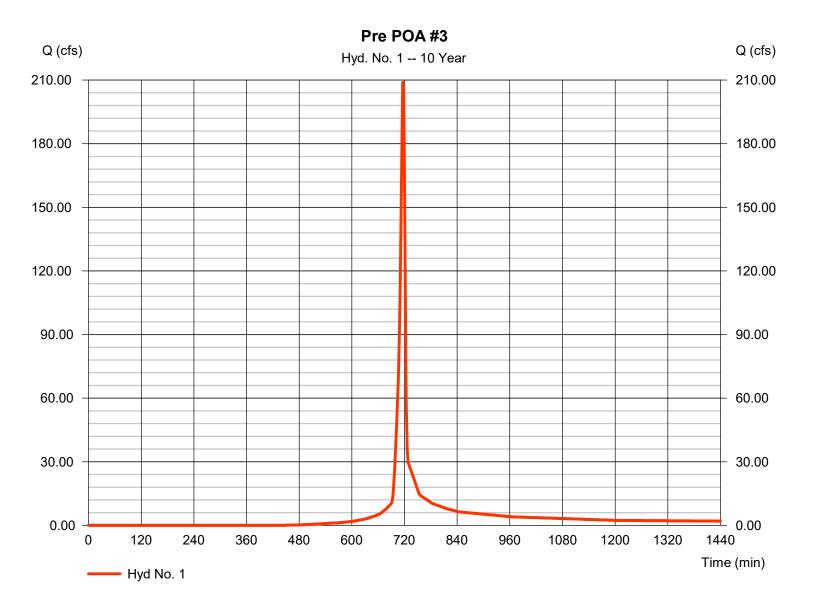
Tuesday, 08 / 1 / 2023

Hyd. No. 1

Pre POA #3

Hydrograph type = SCS Runoff Peak discharge = 208.92 cfsStorm frequency = 10 yrsTime to peak = 716 min Time interval = 2 min Hyd. volume = 424,093 cuft Drainage area Curve number = 43.940 ac= 79

Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 3.10 \, \text{min}$ = TR55 Total precip. = 5.04 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

= 24 hrs

Tuesday, 08 / 1 / 2023

= 484

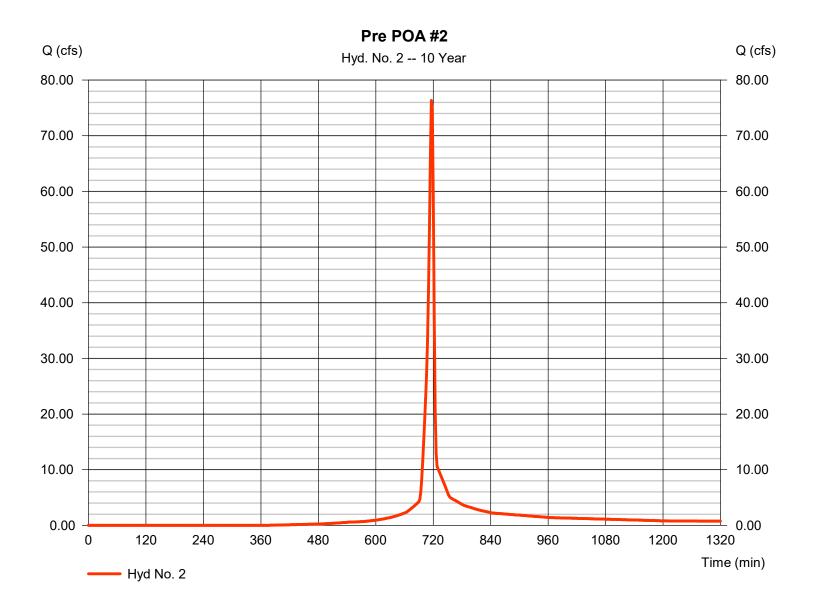
Hyd. No. 2

Pre POA #2

Storm duration

Hydrograph type = SCS Runoff Peak discharge = 76.33 cfsStorm frequency = 10 yrsTime to peak = 716 min Time interval = 2 min Hyd. volume = 156,884 cuft Drainage area = 14.360 ac Curve number = 83 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) $= 5.60 \, \text{min}$ = TR55 Total precip. = 5.04 inDistribution = Type II

Shape factor



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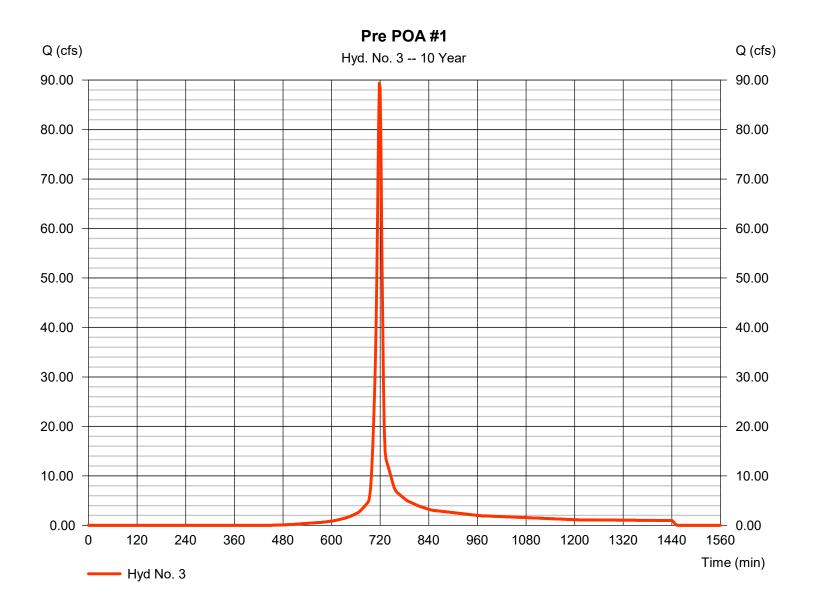
Tuesday, 08 / 1 / 2023

Hyd. No. 3

Pre POA #1

Hydrograph type = SCS Runoff Peak discharge = 89.35 cfsStorm frequency = 10 yrsTime to peak = 718 min Time interval = 2 min Hyd. volume = 204,872 cuft Drainage area = 19.900 ac Curve number = 79

Hydraulic length = 0 ftBasin Slope = 0.0 %Tc method Time of conc. (Tc) $= 9.70 \, \text{min}$ = TR55 Total precip. = 5.04 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

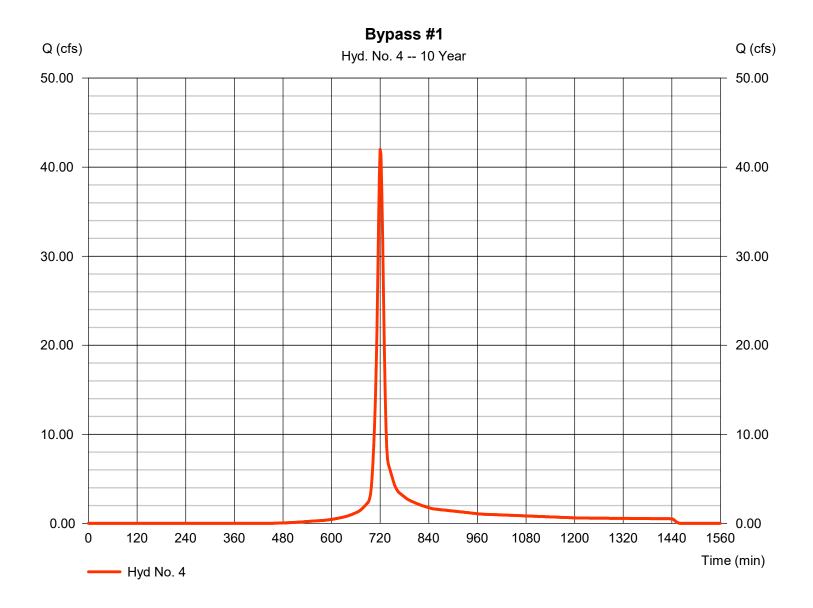
Tuesday, 08 / 1 / 2023

Hyd. No. 4

Bypass #1

Hydrograph type= SCS RunoffPeak discharge= 41.99 cfsStorm frequency= 10 yrsTime to peak= 720 minTime interval= 2 minHyd. volume= 108,929 cuft

Drainage area = 10.260 ac Curve number = 79 Basin Slope = 0.0 % Hydraulic length = 0 ft



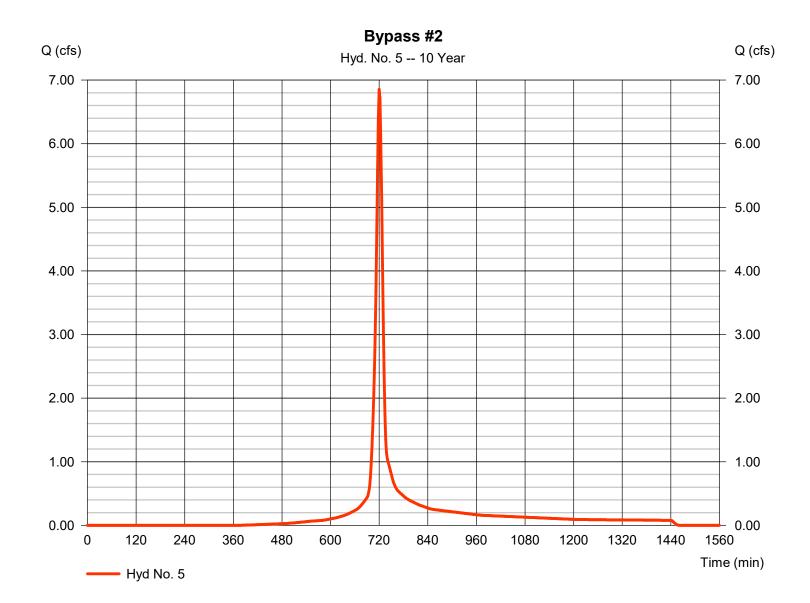
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Tuesday, 08 / 1 / 2023

Hyd. No. 5

Bypass #2

Hydrograph type = SCS Runoff Peak discharge = 6.855 cfsStorm frequency = 10 yrsTime to peak = 720 min Time interval = 2 min Hyd. volume = 17,906 cuft Drainage area Curve number = 83 = 1.490 acBasin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 10.00 min = User Total precip. = 5.04 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



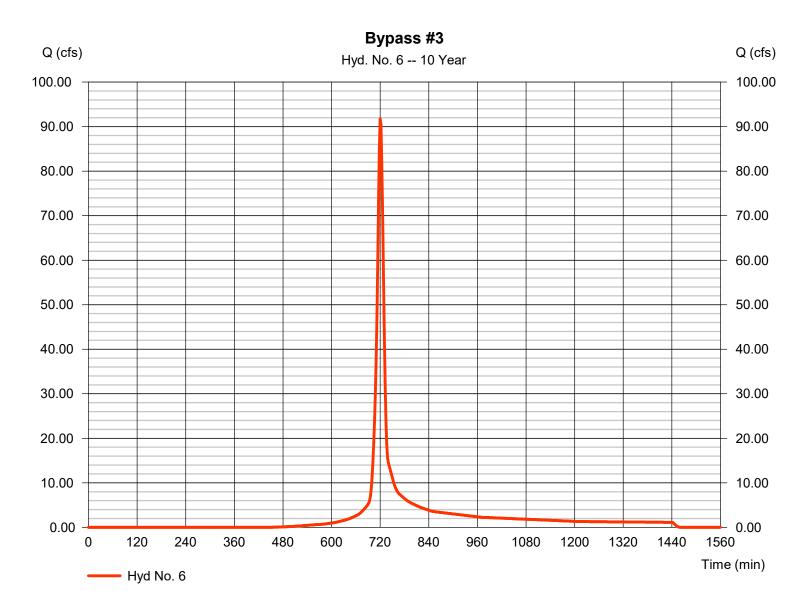
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Tuesday, 08 / 1 / 2023

Hyd. No. 6

Bypass #3

Hydrograph type = SCS Runoff Peak discharge = 91.72 cfsStorm frequency = 10 yrsTime to peak = 720 min Time interval = 2 min Hyd. volume = 237,923 cuft Drainage area Curve number = 22.410 ac= 79 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) = 10.00 min = User Total precip. = 5.04 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



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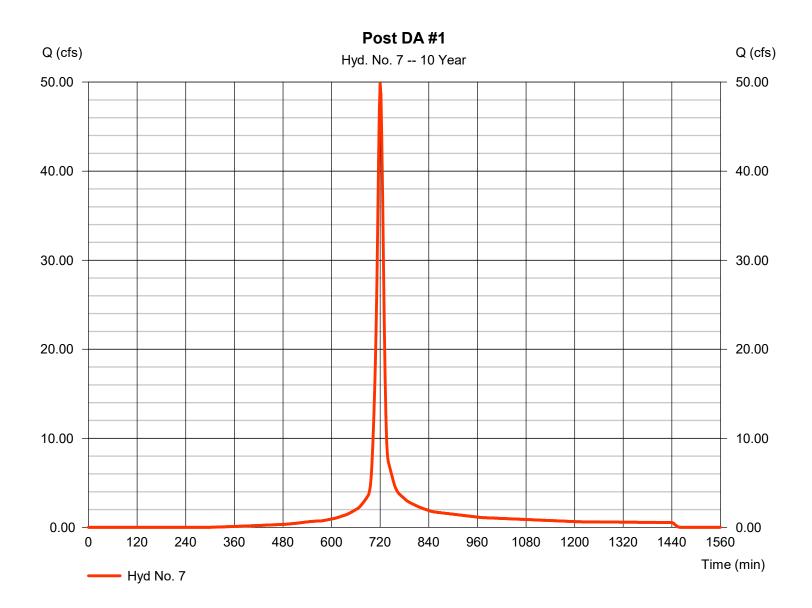
Tuesday, 08 / 1 / 2023

Hyd. No. 7

Post DA #1

Hydrograph type= SCS RunoffPeak discharge= 49.85 cfsStorm frequency= 10 yrsTime to peak= 720 minTime interval= 2 minHyd. volume= 132,251 cuft

Drainage area = 9.800 ac Curve number = 87 Basin Slope = 0.0 % Hydraulic length = 0.0 ft



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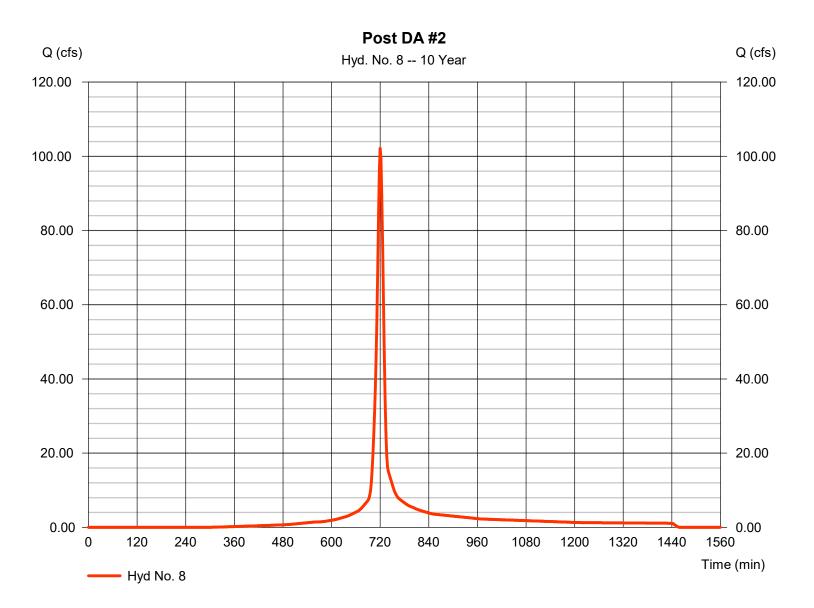
Tuesday, 08 / 1 / 2023

Hyd. No. 8

Post DA #2

Hydrograph type= SCS RunoffPeak discharge= 102.14 cfsStorm frequency= 10 yrsTime to peak= 720 minTime interval= 2 minHyd. volume= 270,980 cuft

Drainage area = 20.080 ac Curve number = 87 Basin Slope = 0.0 % Hydraulic length = 0 ft



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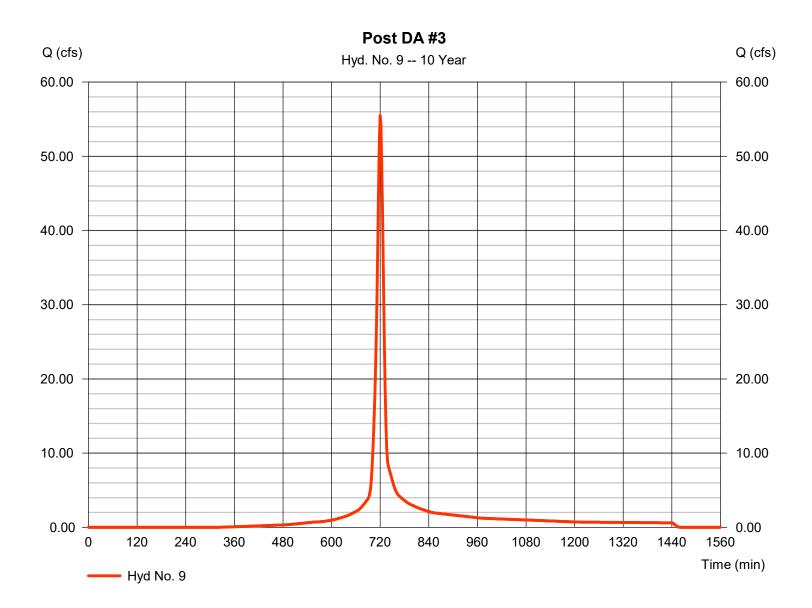
Tuesday, 08 / 1 / 2023

Hyd. No. 9

Post DA #3

Hydrograph type= SCS RunoffPeak discharge= 55.50 cfsStorm frequency= 10 yrsTime to peak= 720 minTime interval= 2 minHyd. volume= 146,532 cuft

Drainage area = 11.170 ac Curve number = 86 Basin Slope = 0.0 % Hydraulic length = 0 ft



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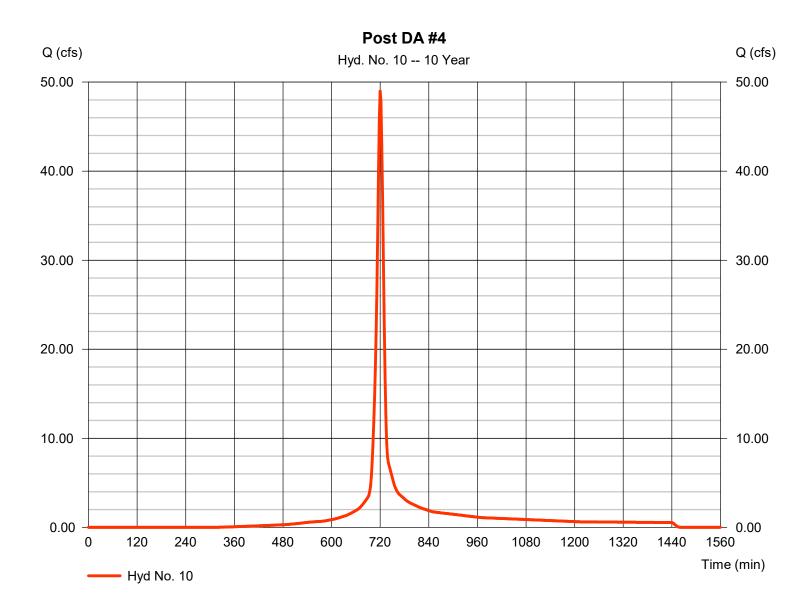
Tuesday, 08 / 1 / 2023

Hyd. No. 10

Post DA #4

Hydrograph type= SCS RunoffPeak discharge= 48.99 cfsStorm frequency= 10 yrsTime to peak= 720 minTime interval= 2 minHyd. volume= 129,347 cuft

Drainage area = 9.860 ac Curve number = 86 Basin Slope = 0.0 % Hydraulic length = 0 ft



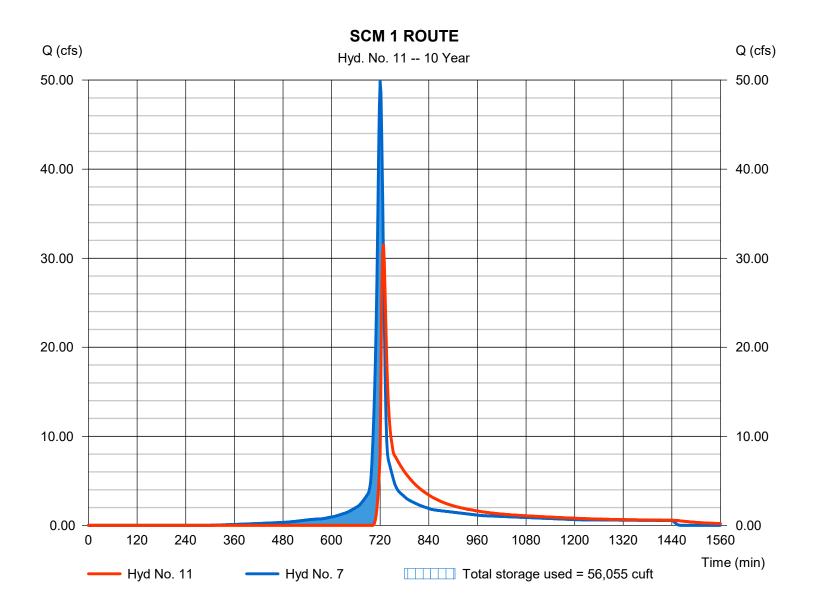
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Tuesday, 08 / 1 / 2023

Hyd. No. 11

SCM 1 ROUTE

Hydrograph type Peak discharge = 31.49 cfs= Reservoir Storm frequency = 10 yrsTime to peak = 728 min Time interval = 2 min Hyd. volume = 112,349 cuftMax. Elevation Inflow hyd. No. = 7 - Post DA #1 = 388.42 ftReservoir name = SCM 1 Max. Storage = 56,055 cuft



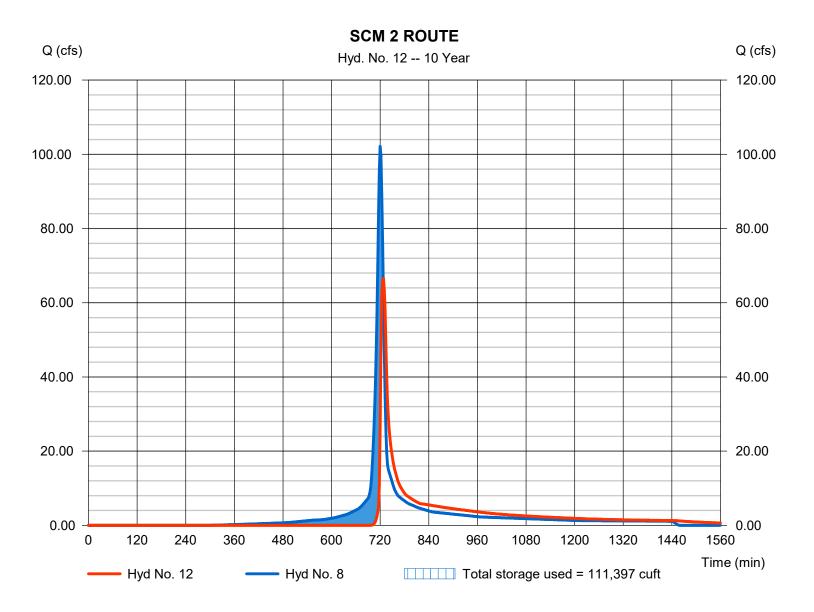
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Tuesday, 08 / 1 / 2023

Hyd. No. 12

SCM 2 ROUTE

Hydrograph type Peak discharge = 66.55 cfs= Reservoir Storm frequency = 10 yrsTime to peak = 728 min Time interval = 2 min Hyd. volume = 239,739 cuft Inflow hyd. No. Max. Elevation = 8 - Post DA #2 = 355.22 ftReservoir name = SCM 2 Max. Storage = 111,397 cuft



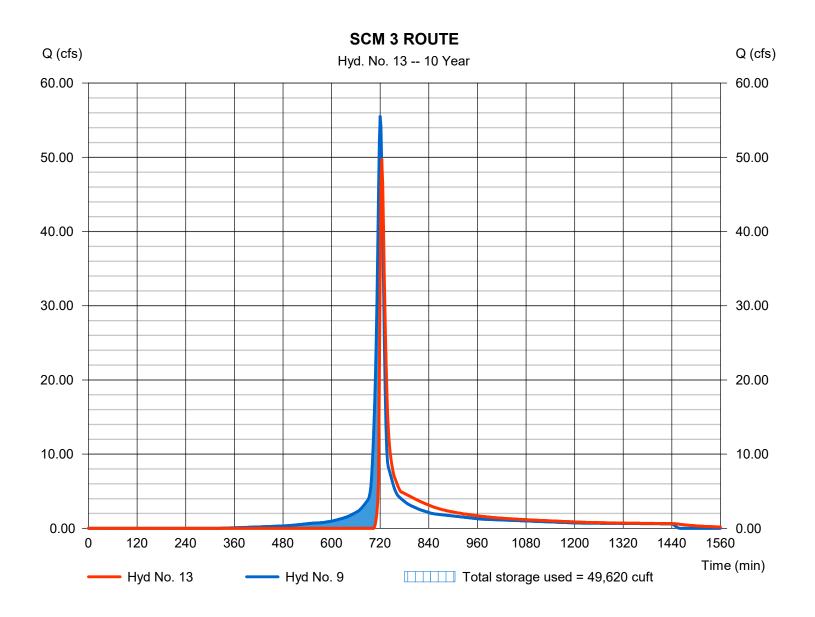
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Tuesday, 08 / 1 / 2023

Hyd. No. 13

SCM 3 ROUTE

Hydrograph type Peak discharge = 49.73 cfs= Reservoir Storm frequency = 10 yrsTime to peak = 724 min Time interval = 2 min Hyd. volume = 124,456 cuft Inflow hyd. No. Max. Elevation = 9 - Post DA #3 = 388.54 ftReservoir name = SCM 3 Max. Storage = 49,620 cuft



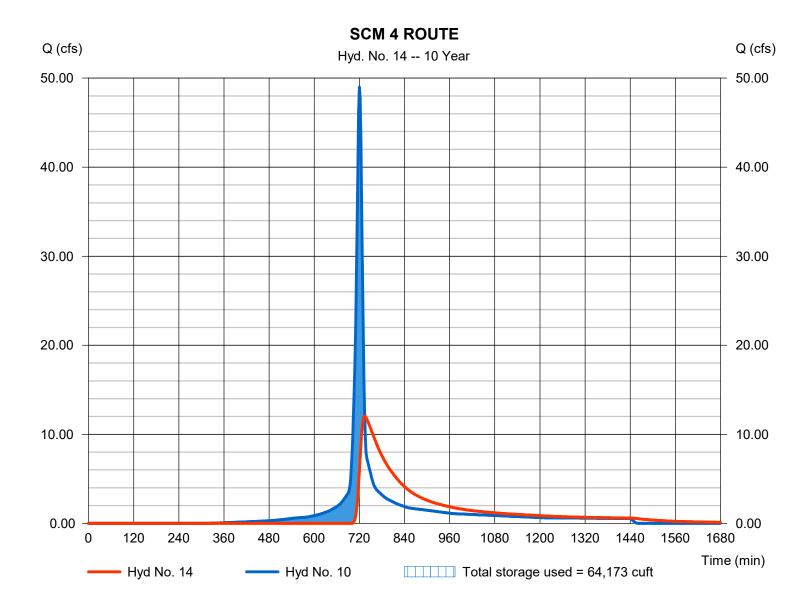
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Tuesday, 08 / 1 / 2023

Hyd. No. 14

SCM 4 ROUTE

Hydrograph type Peak discharge = 12.07 cfs= Reservoir Storm frequency = 10 yrsTime to peak = 734 min Time interval = 2 min Hyd. volume = 111,271 cuft Inflow hyd. No. Max. Elevation = 10 - Post DA #4 = 383.99 ftReservoir name = SCM 4 Max. Storage = 64,173 cuft



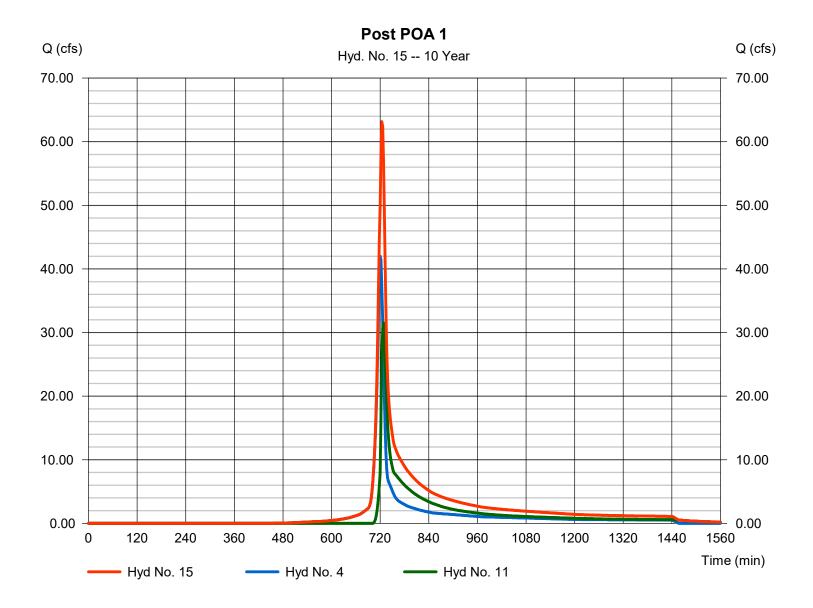
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Tuesday, 08 / 1 / 2023

Hyd. No. 15

Post POA 1

Hydrograph type = Combine Peak discharge = 63.14 cfsStorm frequency Time to peak = 10 yrs= 724 min Time interval = 2 min Hyd. volume = 221,278 cuft Inflow hyds. = 4, 11 Contrib. drain. area = 10.260 ac



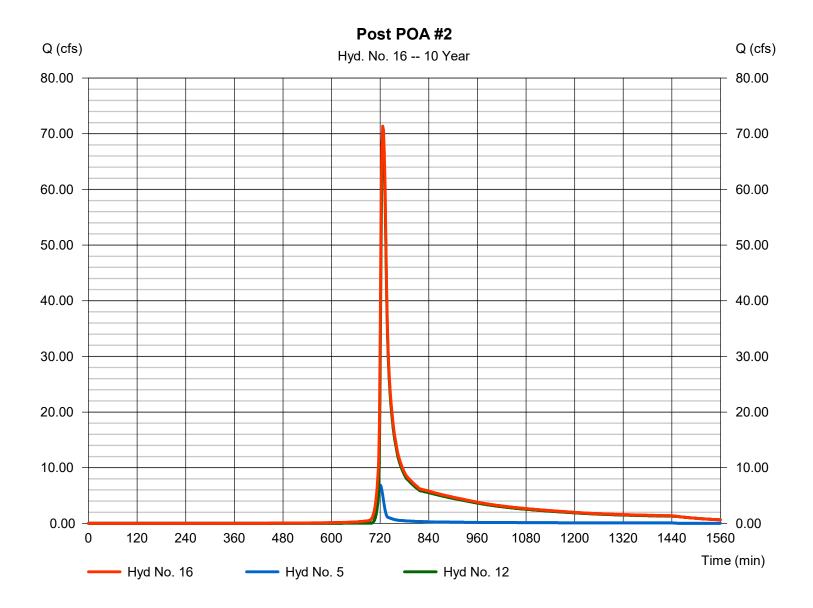
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Tuesday, 08 / 1 / 2023

Hyd. No. 16

Post POA #2

= 71.35 cfsHydrograph type = Combine Peak discharge Storm frequency Time to peak = 10 yrs= 726 min Time interval = 2 min Hyd. volume = 257,645 cuft Inflow hyds. = 5, 12 Contrib. drain. area = 1.490 ac



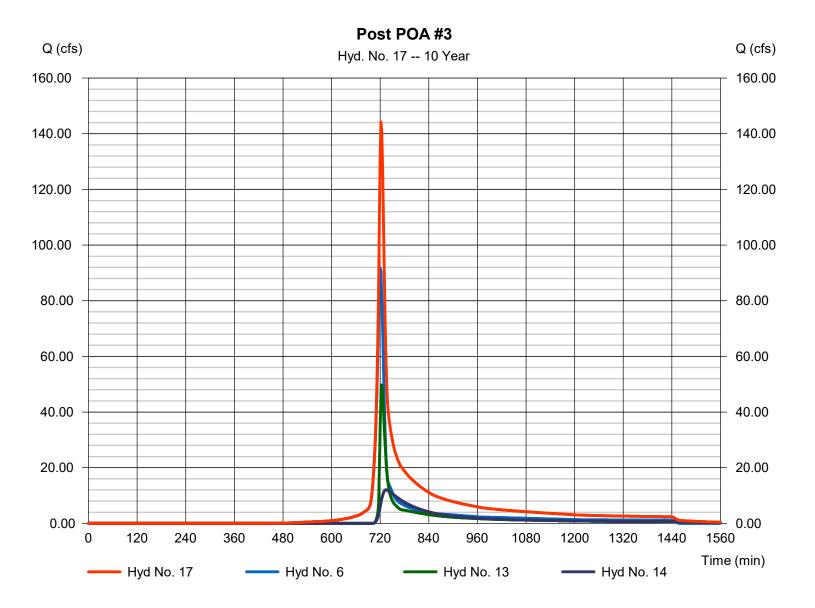
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Tuesday, 08 / 1 / 2023

Hyd. No. 17

Post POA #3

Hydrograph type = Combine Peak discharge = 144.21 cfsStorm frequency Time to peak = 10 yrs= 722 min Time interval = 2 min Hyd. volume = 473,650 cuft Inflow hyds. = 6, 13, 14 Contrib. drain. area = 22.410 ac



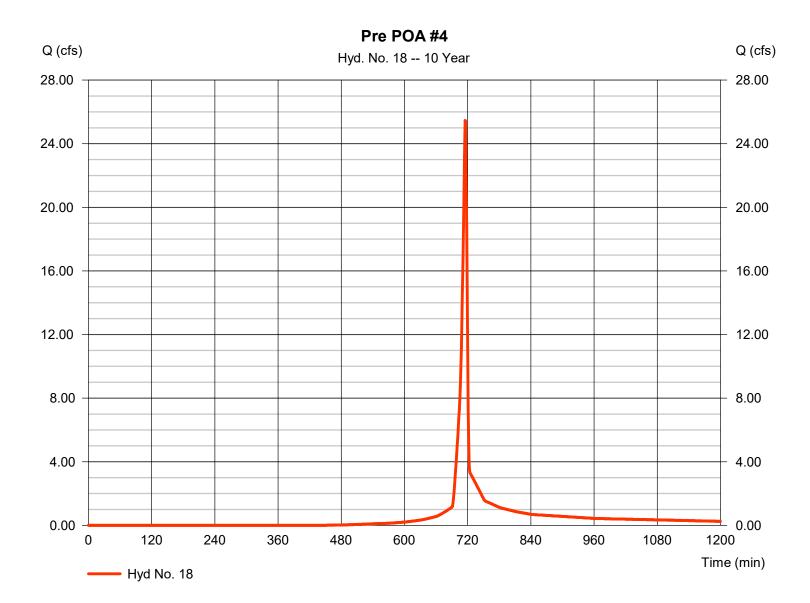
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Tuesday, 08 / 1 / 2023

Hyd. No. 18

Pre POA #4

Hydrograph type = SCS Runoff Peak discharge = 25.45 cfsStorm frequency = 10 yrsTime to peak = 715 min Time interval = 1 min Hyd. volume = 45,556 cuft Drainage area Curve number = 4.720 ac= 79 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 2.10 min = TR55 Total precip. = 5.04 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



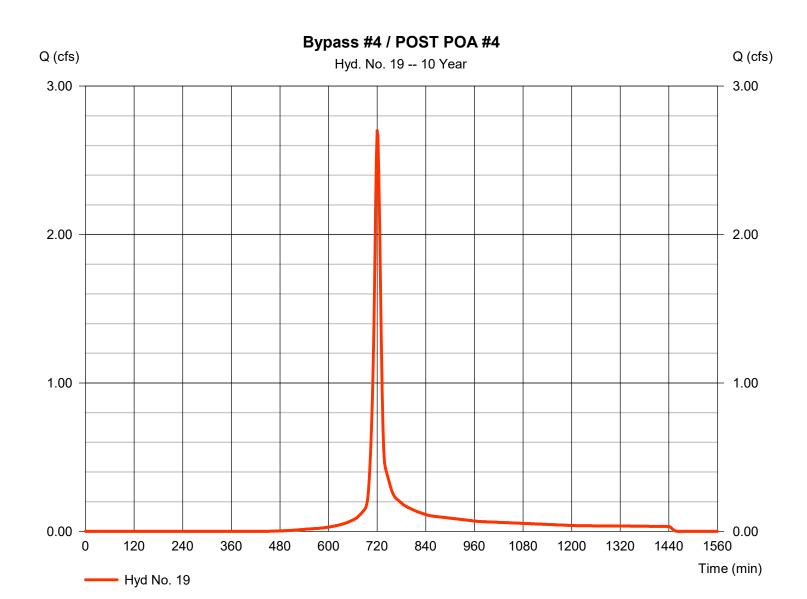
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Tuesday, 08 / 1 / 2023

Hyd. No. 19

Bypass #4 / POST POA #4

Hydrograph type = SCS Runoff Peak discharge = 2.701 cfsStorm frequency = 10 yrsTime to peak = 720 min Time interval = 2 min Hyd. volume = 7.007 cuftDrainage area Curve number = 0.660 ac= 79 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) = 10.00 min = User Total precip. = 5.04 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



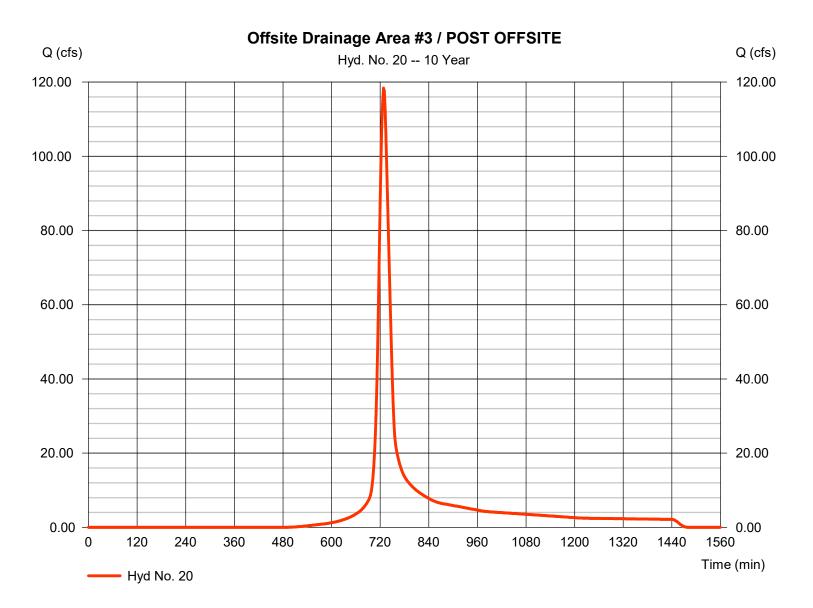
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Tuesday, 08 / 1 / 2023

Hyd. No. 20

Offsite Drainage Area #3 / POST OFFSITE

Hydrograph type = SCS Runoff Peak discharge = 118.39 cfsStorm frequency = 10 yrsTime to peak = 728 min Time interval = 2 min Hyd. volume = 435.415 cuft Curve number Drainage area = 45.870 ac = 77 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 25.00 min = User Total precip. = 5.04 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



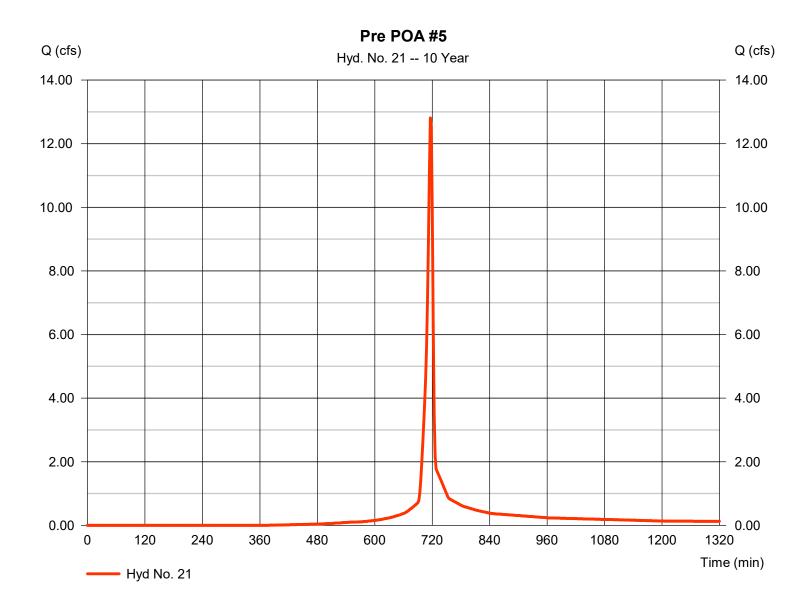
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Tuesday, 08 / 1 / 2023

Hyd. No. 21

Pre POA #5

Hydrograph type = SCS Runoff Peak discharge = 12.81 cfsStorm frequency = 10 yrsTime to peak = 716 min Time interval = 2 min Hyd. volume = 26.329 cuft Drainage area Curve number = 2.410 ac= 83 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 4.50 \, \text{min}$ = TR55 Total precip. = 5.04 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484



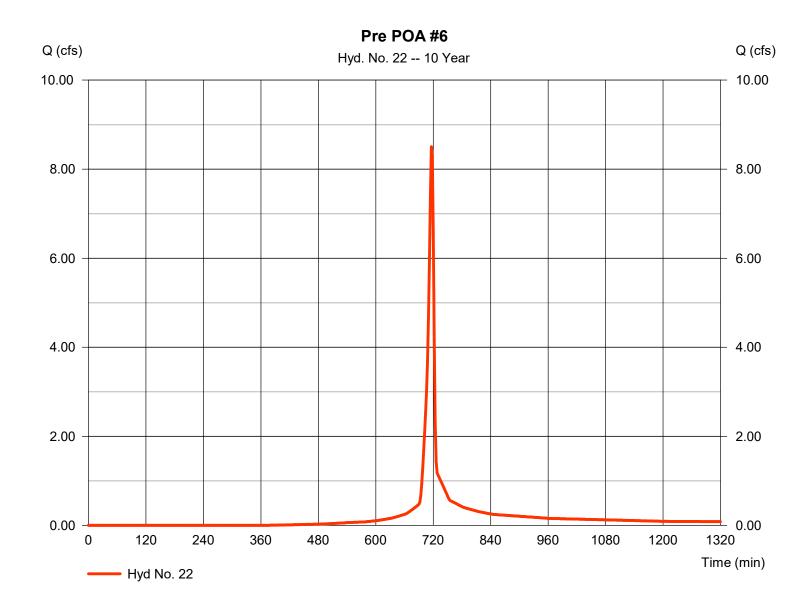
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Tuesday, 08 / 1 / 2023

Hyd. No. 22

Pre POA #6

Hydrograph type = SCS Runoff Peak discharge = 8.504 cfsStorm frequency = 10 yrsTime to peak = 716 min Time interval = 2 min Hyd. volume = 17,480 cuftDrainage area Curve number = 1.600 ac= 83 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 4.20 \, \text{min}$ = TR55 Total precip. = 5.04 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



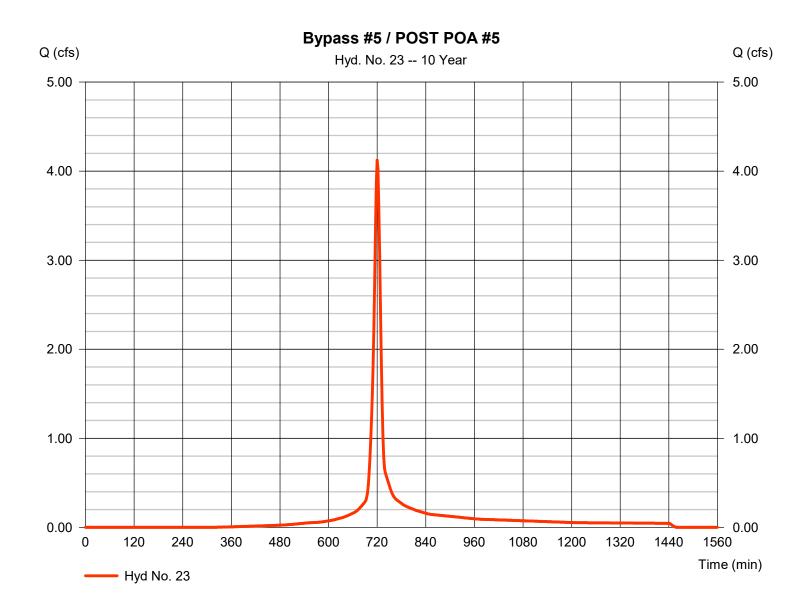
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Tuesday, 08 / 1 / 2023

Hyd. No. 23

Bypass #5 / POST POA #5

Hydrograph type = SCS Runoff Peak discharge = 4.124 cfsStorm frequency = 10 yrsTime to peak = 720 min Time interval = 2 min Hyd. volume = 10.888 cuft Curve number Drainage area = 0.830 ac= 86 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 10.00 min = User Total precip. = 5.04 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484



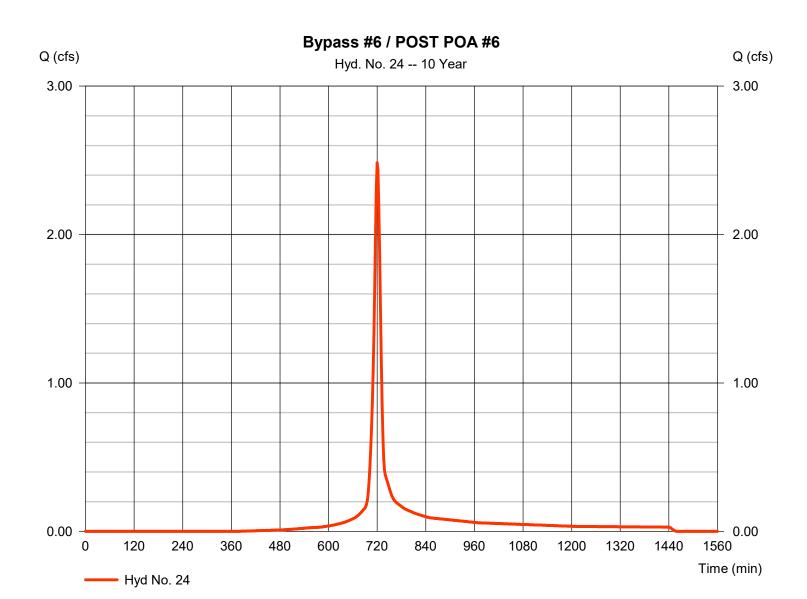
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Tuesday, 08 / 1 / 2023

Hyd. No. 24

Bypass #6 / POST POA #6

Hydrograph type = SCS Runoff Peak discharge = 2.484 cfsStorm frequency = 10 yrsTime to peak = 720 min Time interval = 2 min Hyd. volume = 6,490 cuftDrainage area Curve number = 0.540 ac= 83 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 10.00 min = User Total precip. = 5.04 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	367.67	2	716	762,560				Pre POA #3
2	SCS Runoff	128.55	2	716	271,624				Pre POA #2
3	SCS Runoff	157.92	2	718	368,380				Pre POA #1
4	SCS Runoff	74.51	2	720	195,864				Bypass #1
5	SCS Runoff	11.62	2	720	31,002				Bypass #2
6	SCS Runoff	162.74	2	720	427,808				Bypass #3
7	SCS Runoff	81.12	2	720	220,918				Post DA #1
8	SCS Runoff	166.21	2	720	452,656				Post DA #2
9	SCS Runoff	91.20	2	720	246,935				Post DA #3
10	SCS Runoff	80.50	2	720	217,975				Post DA #4
11	Reservoir	70.93	2	724	201,016	7	388.97	65,840	SCM 1 ROUTE
12	Reservoir	139.06	2	724	421,328	8	355.96	136,997	SCM 2 ROUTE
13	Reservoir	85.19	2	722	224,860	9	388.96	55,721	SCM 3 ROUTE
14	Reservoir	58.87	2	726	199,900	10	384.83	82,726	SCM 4 ROUTE
15	Combine	141.43	2	722	396,880	4, 11,			Post POA 1
16	Combine	149.22	2	724	452,331	5, 12,			Post POA #2
17	Combine	291.65	2	722	852,568	6, 13, 14,			Post POA #3
18	SCS Runoff	44.48	1	715	81,914				Pre POA #4
19	SCS Runoff	4.793	2	720	12,599				Bypass #4 / POST POA #4
20	SCS Runoff	217.12	2	728	798,606				Offsite Drainage Area #3 / POST OFF
21	SCS Runoff	21.57	2	716	45,586				Pre POA #5
22	SCS Runoff	14.32	2	716	30,265				Pre POA #6
23	SCS Runoff	6.777	2	720	18,349				Bypass #5 / POST POA #5
24	SCS Runoff	4.212	2	720	11,236				Bypass #6 / POST POA #6
SCMs.gpw				Return F	Period: 100	Year	Tuesday, 0	8 / 1 / 2023	

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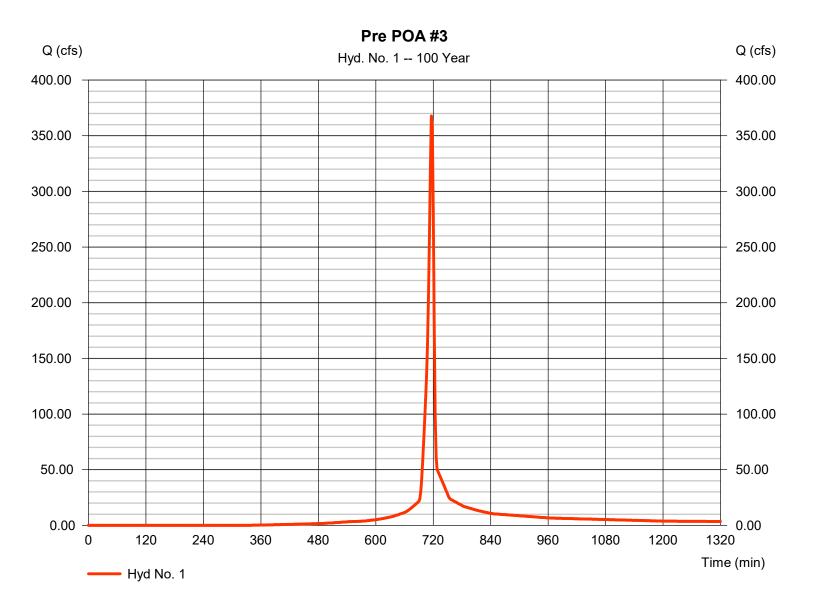
Tuesday, 08 / 1 / 2023

Hyd. No. 1

Pre POA #3

Hydrograph type = SCS Runoff Peak discharge = 367.67 cfsStorm frequency = 100 yrsTime to peak = 716 min Time interval = 2 min Hyd. volume = 762,560 cuftDrainage area Curve number = 43.940 ac= 79 = 0 ft= 0.0 %

Basin Slope= 0.0 %Hydraulic length= 0 ftTc method= TR55Time of conc. (Tc)= 3.10 minTotal precip.= 7.56 inDistribution= Type IIStorm duration= 24 hrsShape factor= 484



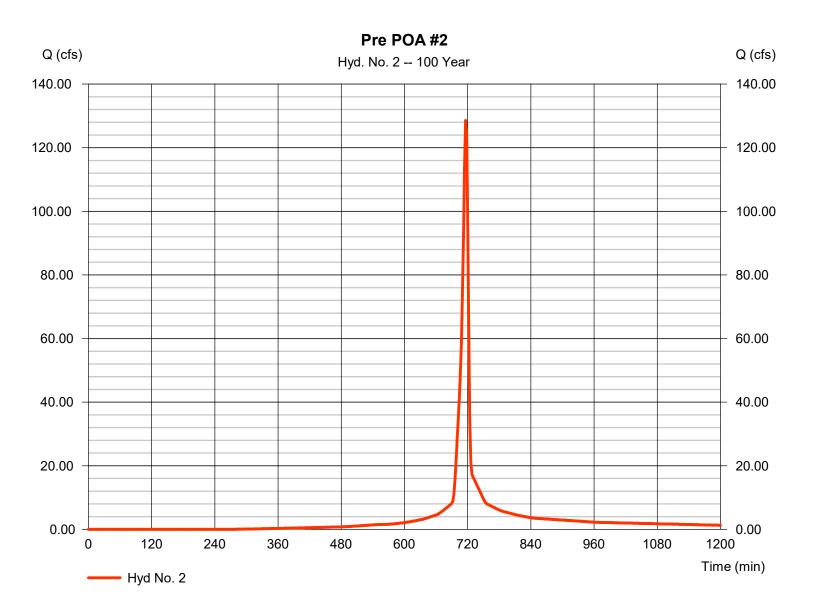
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Tuesday, 08 / 1 / 2023

Hyd. No. 2

Pre POA #2

Hydrograph type = SCS Runoff Peak discharge = 128.55 cfsStorm frequency = 100 yrsTime to peak = 716 min Time interval = 2 min Hyd. volume = 271,624 cuft Drainage area Curve number = 14.360 ac = 83 = 0 ftBasin Slope = 0.0 %Hydraulic length



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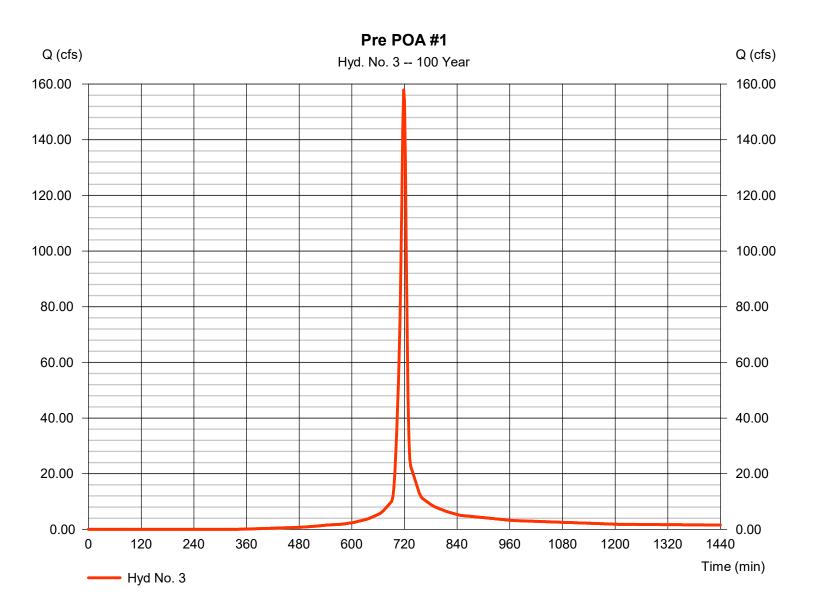
Tuesday, 08 / 1 / 2023

Hyd. No. 3

Pre POA #1

Hydrograph type = SCS Runoff Peak discharge = 157.92 cfsStorm frequency = 100 yrsTime to peak = 718 min Time interval = 2 min Hyd. volume = 368,380 cuft Drainage area Curve number = 19.900 ac = 79

= 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) $= 9.70 \, \text{min}$ = TR55 Total precip. = 7.56 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484



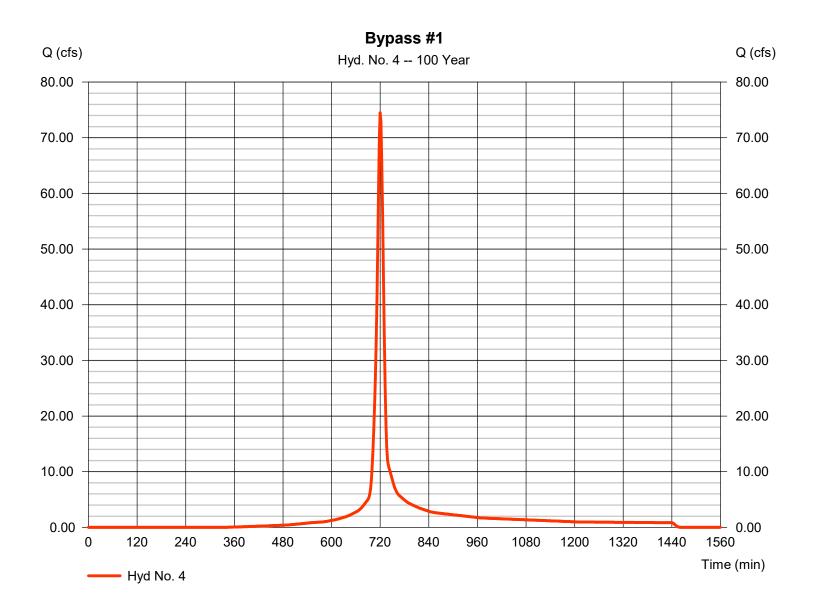
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Tuesday, 08 / 1 / 2023

Hyd. No. 4

Bypass #1

Hydrograph type = SCS Runoff Peak discharge = 74.51 cfsStorm frequency = 100 yrsTime to peak = 720 min Time interval = 2 min Hyd. volume = 195,864 cuft Drainage area Curve number = 10.260 ac= 79 Hydraulic length = 0 ftBasin Slope = 0.0 %



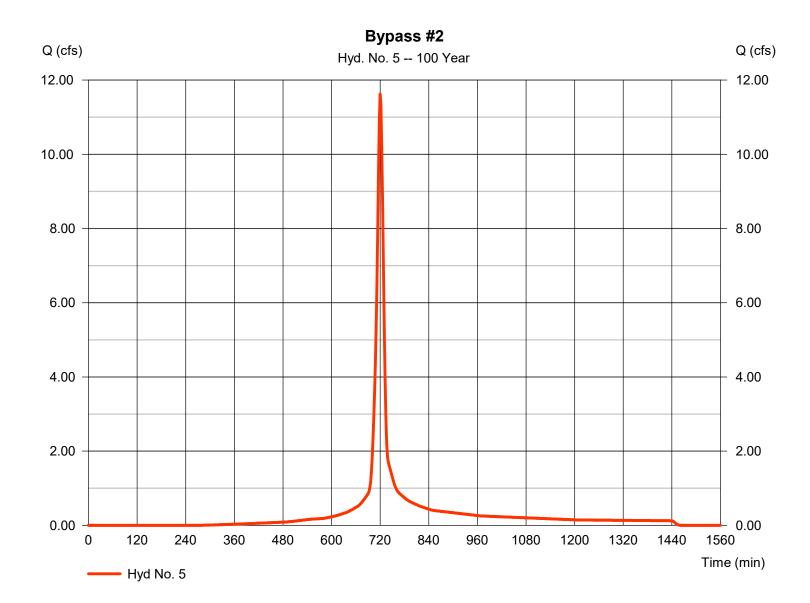
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Tuesday, 08 / 1 / 2023

Hyd. No. 5

Bypass #2

Hydrograph type = SCS Runoff Peak discharge = 11.62 cfsStorm frequency = 100 yrsTime to peak = 720 min Time interval = 2 min Hyd. volume = 31,002 cuftDrainage area Curve number = 1.490 ac= 83 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 10.00 min = User Total precip. = 7.56 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



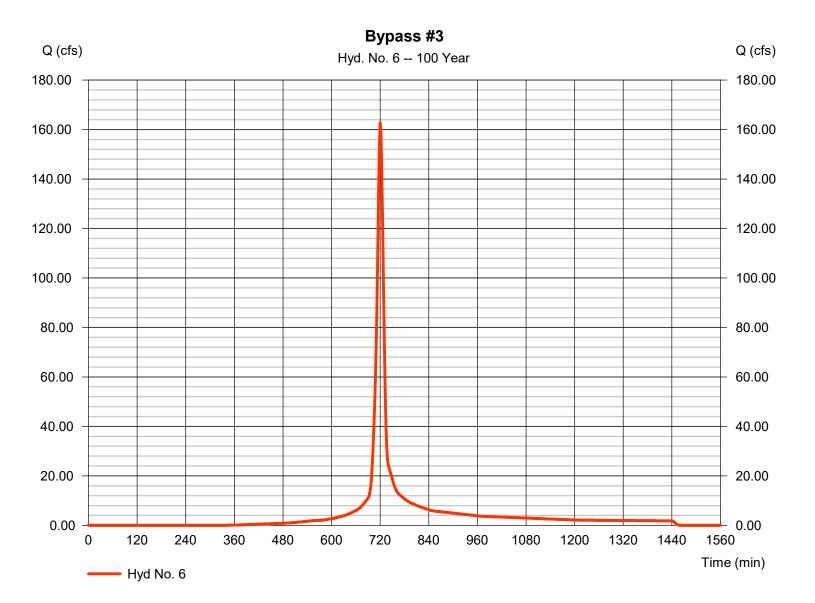
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Tuesday, 08 / 1 / 2023

Hyd. No. 6

Bypass #3

Hydrograph type= SCS RunoffPeak discharge= 162.74 cfsStorm frequency= 100 yrsTime to peak= 720 minTime interval= 2 minHyd. volume= 427,808 cuft



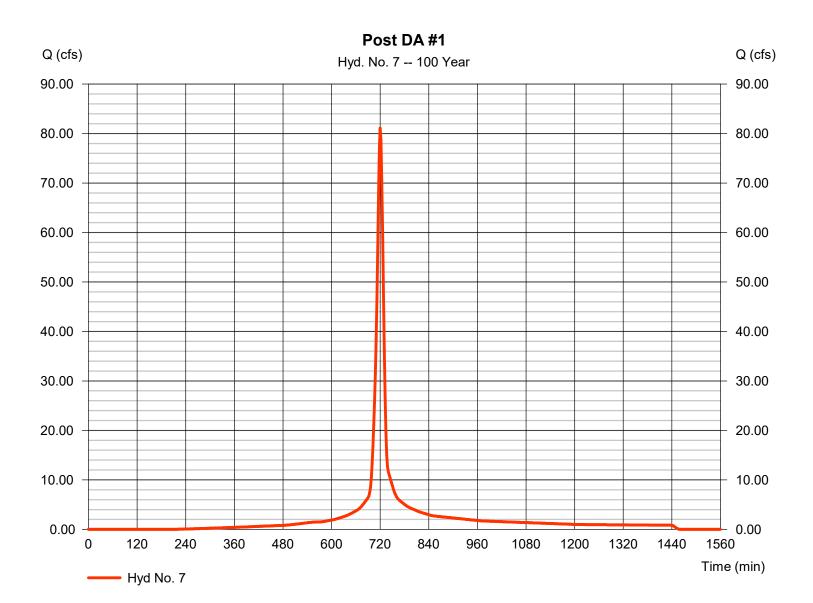
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Tuesday, 08 / 1 / 2023

Hyd. No. 7

Post DA #1

Hydrograph type = SCS Runoff Peak discharge = 81.12 cfsStorm frequency = 100 yrsTime to peak = 720 min Time interval = 2 min Hyd. volume = 220,918 cuft Drainage area = 9.800 acCurve number = 87



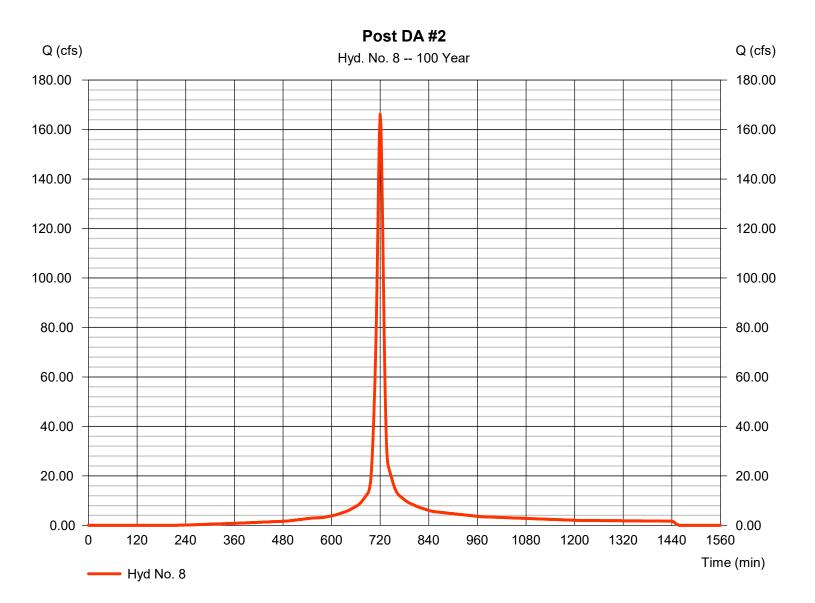
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Tuesday, 08 / 1 / 2023

Hyd. No. 8

Post DA #2

Hydrograph type = SCS Runoff Peak discharge = 166.21 cfsStorm frequency Time to peak = 100 yrs= 720 min Time interval = 2 min Hyd. volume = 452,656 cuft Drainage area Curve number = 20.080 ac= 87



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Tuesday, 08 / 1 / 2023

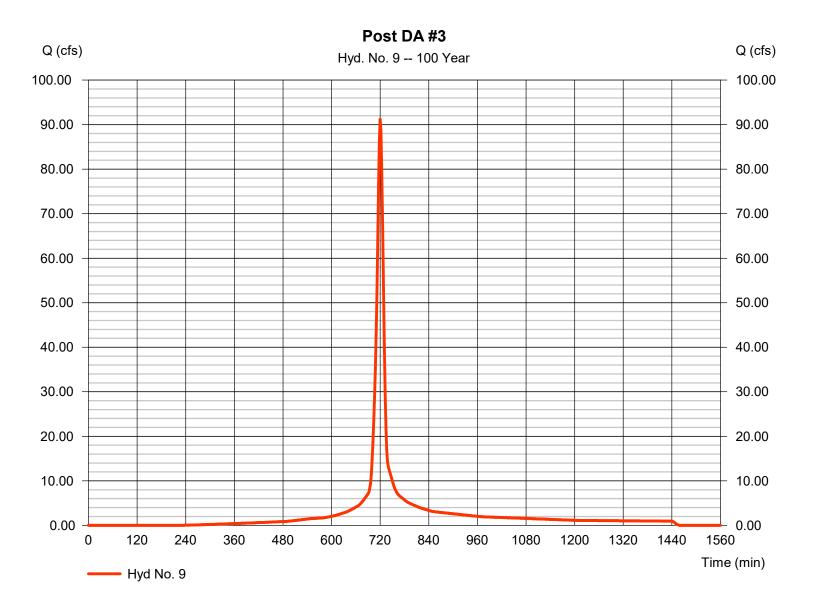
Hyd. No. 9

Post DA #3

= 91.20 cfsHydrograph type = SCS Runoff Peak discharge Storm frequency Time to peak = 100 yrs= 720 min Time interval = 2 min Hyd. volume = 246.935 cuft Drainage area Curve number = 11.170 ac = 86

Basin Slope = 0.0 % Hydraulic length = 0 ft
Tc method = User Time of conc. (Tc) = 10.00 min

Total precip. = 7.56 in Distribution = Type II Storm duration = 24 hrs Shape factor = 484



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

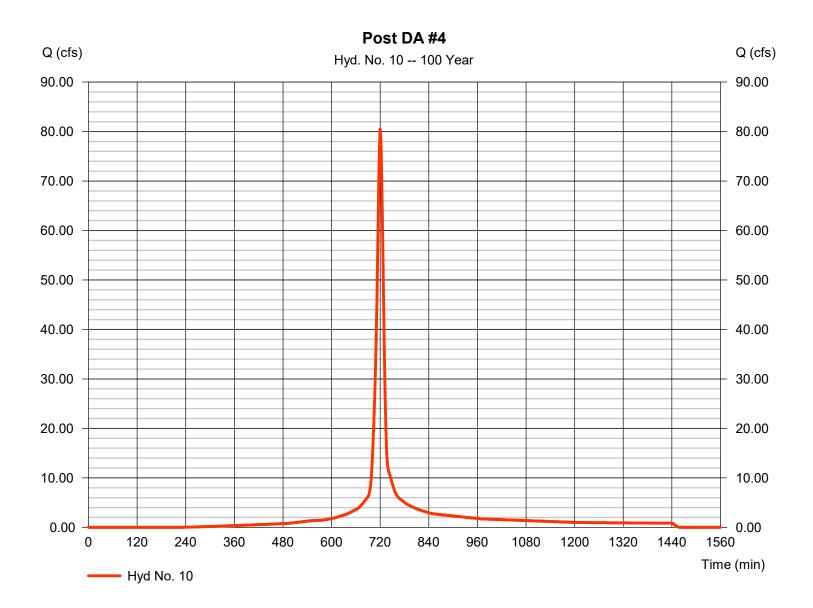
Tuesday, 08 / 1 / 2023

Hyd. No. 10

Post DA #4

Hydrograph type= SCS RunoffPeak discharge= 80.50 cfsStorm frequency= 100 yrsTime to peak= 720 minTime interval= 2 minHyd. volume= 217,975 cuftDrainage area= 9.860 acCurve number= 86

Drainage area = 9.860 ac Curve number = 86 Basin Slope = 0.0 % Hydraulic length = 0.0 ft



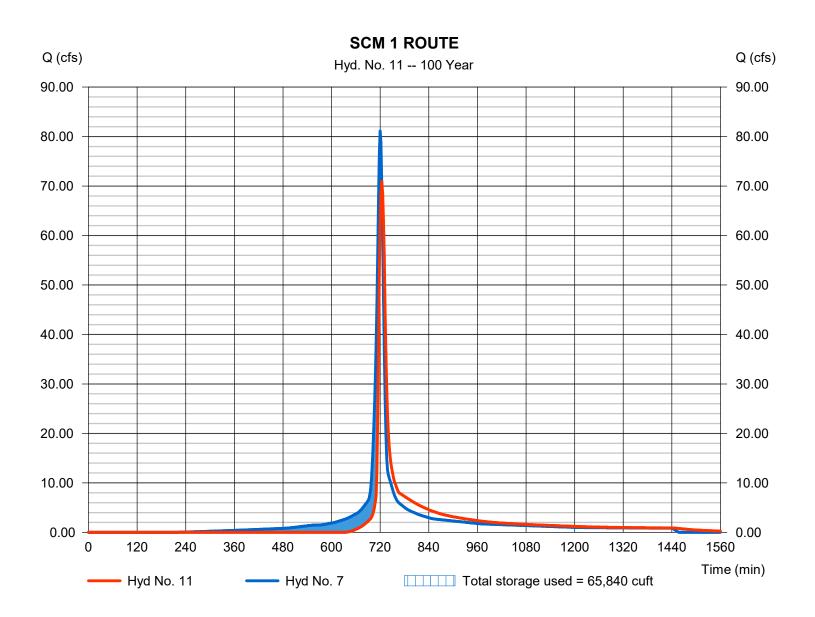
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Tuesday, 08 / 1 / 2023

Hyd. No. 11

SCM 1 ROUTE

Hydrograph type = Reservoir Peak discharge = 70.93 cfsStorm frequency = 100 yrsTime to peak = 724 min Time interval = 2 min Hyd. volume = 201,016 cuft Inflow hyd. No. Max. Elevation = 7 - Post DA #1 = 388.97 ft= SCM 1 Reservoir name Max. Storage = 65,840 cuft



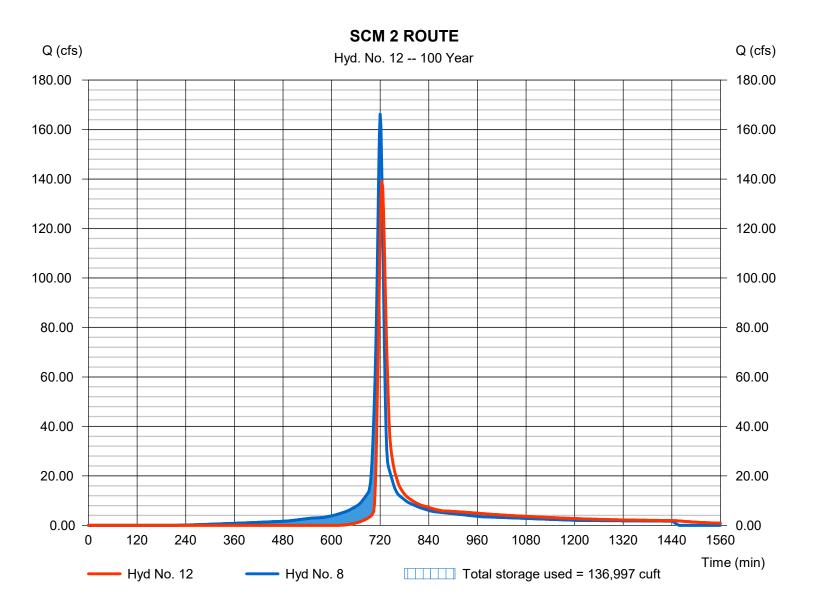
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Tuesday, 08 / 1 / 2023

Hyd. No. 12

SCM 2 ROUTE

Hydrograph type Peak discharge = 139.06 cfs= Reservoir Storm frequency = 100 yrsTime to peak = 724 min Time interval = 2 min Hyd. volume = 421,328 cuft Inflow hyd. No. Max. Elevation = 8 - Post DA #2 = 355.96 ftReservoir name = SCM 2 Max. Storage = 136,997 cuft



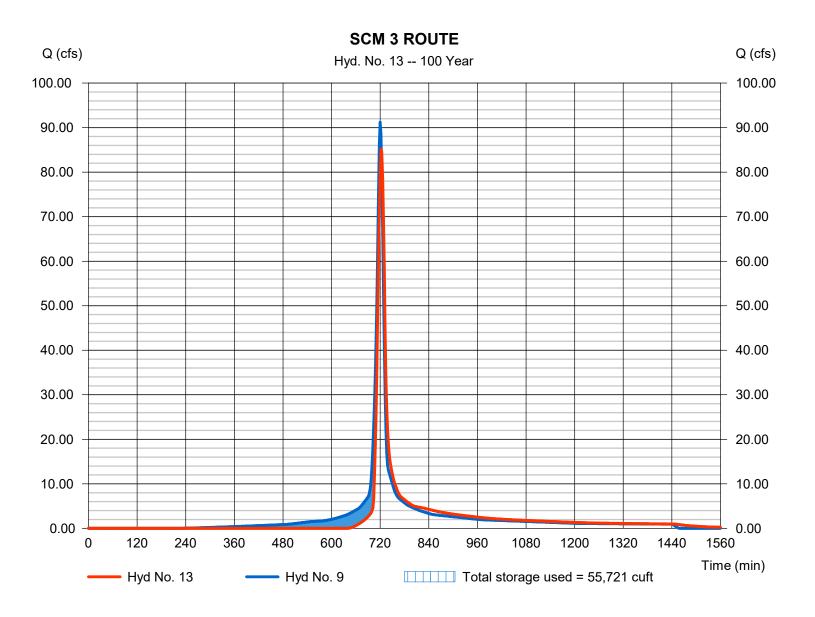
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Tuesday, 08 / 1 / 2023

Hyd. No. 13

SCM 3 ROUTE

Hydrograph type Peak discharge = 85.19 cfs= Reservoir Storm frequency = 100 yrsTime to peak = 722 min Time interval = 2 min Hyd. volume = 224,860 cuft Inflow hyd. No. Max. Elevation = 9 - Post DA #3 = 388.96 ft= 55,721 cuft Reservoir name = SCM 3Max. Storage



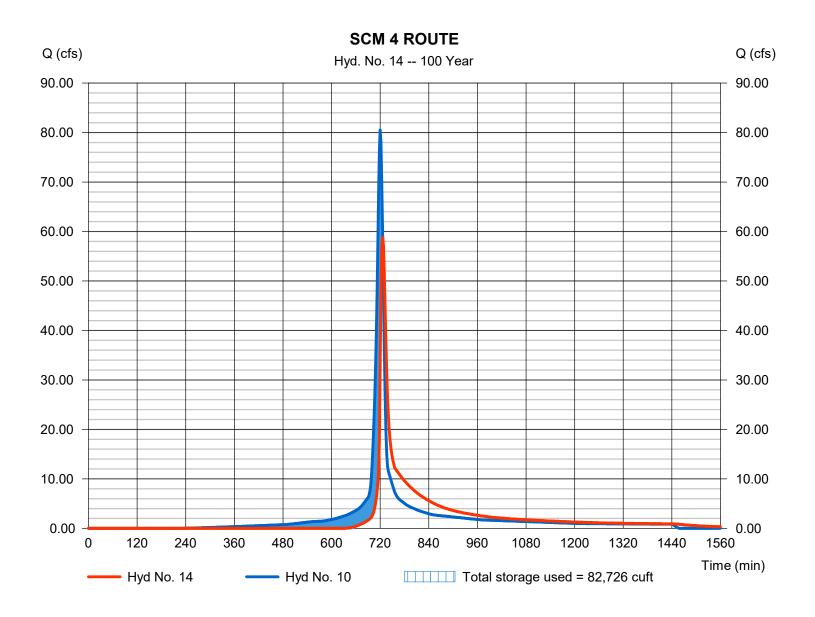
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Tuesday, 08 / 1 / 2023

Hyd. No. 14

SCM 4 ROUTE

Hydrograph type = Reservoir Peak discharge = 58.87 cfsStorm frequency = 100 yrsTime to peak = 726 min Time interval = 2 min Hyd. volume = 199,900 cuft Inflow hyd. No. Max. Elevation = 10 - Post DA #4 = 384.83 ft= 82,726 cuft Reservoir name = SCM 4 Max. Storage



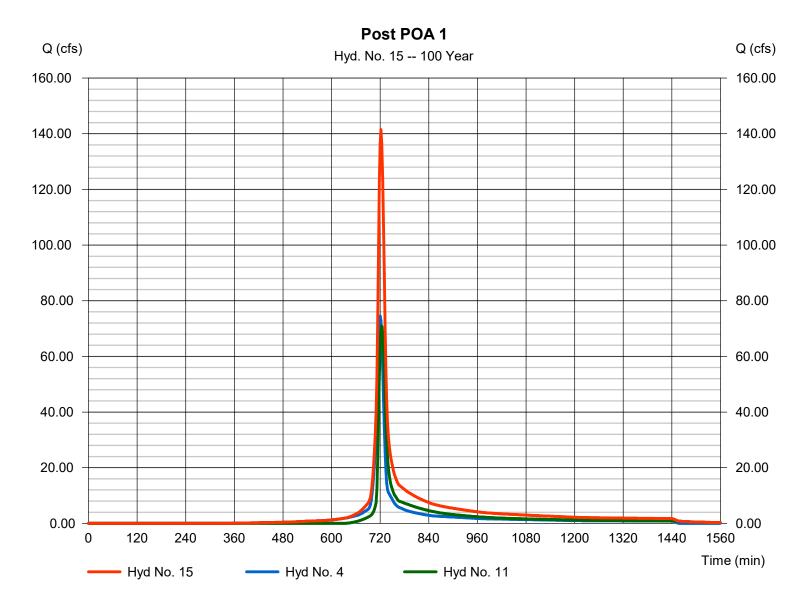
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Tuesday, 08 / 1 / 2023

Hyd. No. 15

Post POA 1

Hydrograph type = Combine Peak discharge = 141.43 cfsStorm frequency Time to peak = 100 yrs= 722 min Time interval = 2 min Hyd. volume = 396,880 cuft Inflow hyds. = 4, 11 Contrib. drain. area = 10.260 ac



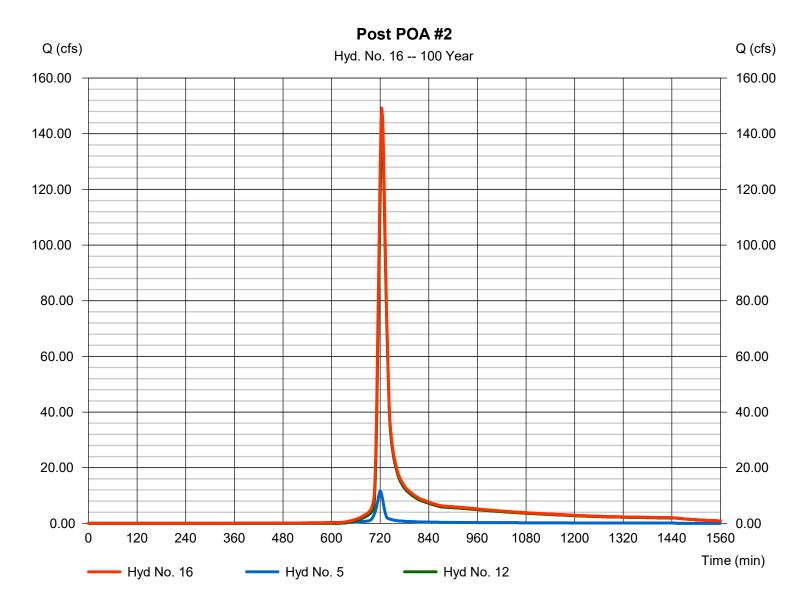
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Tuesday, 08 / 1 / 2023

Hyd. No. 16

Post POA #2

Hydrograph type = Combine Peak discharge = 149.22 cfsStorm frequency Time to peak = 100 yrs= 724 min Time interval = 2 min Hyd. volume = 452,331 cuft Inflow hyds. = 5, 12 Contrib. drain. area = 1.490 ac



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

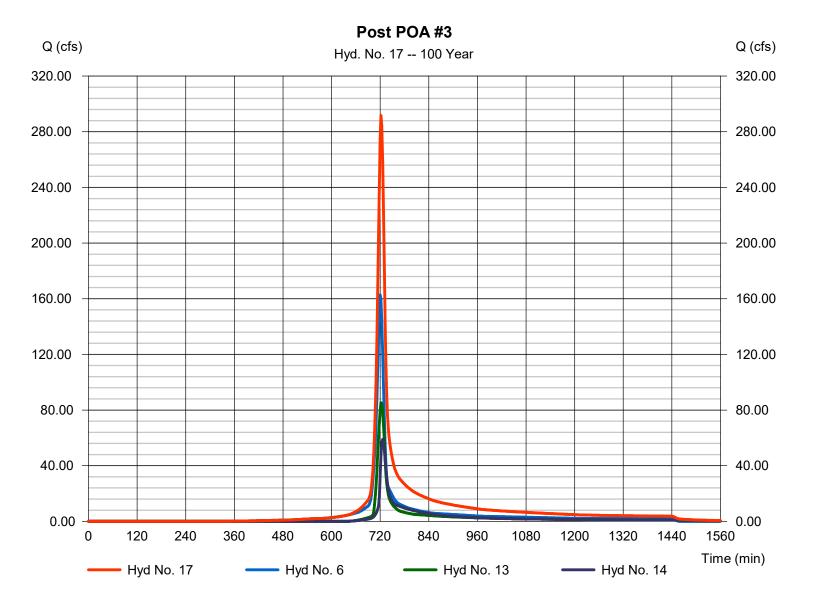
Tuesday, 08 / 1 / 2023

Hyd. No. 17

Post POA #3

Hydrograph type = Combine
Storm frequency = 100 yrs
Time interval = 2 min
Inflow hyds. = 6, 13, 14

Peak discharge = 291.65 cfs
Time to peak = 722 min
Hyd. volume = 852,568 cuft
Contrib. drain. area = 22.410 ac



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

= 24 hrs

Tuesday, 08 / 1 / 2023

= 484

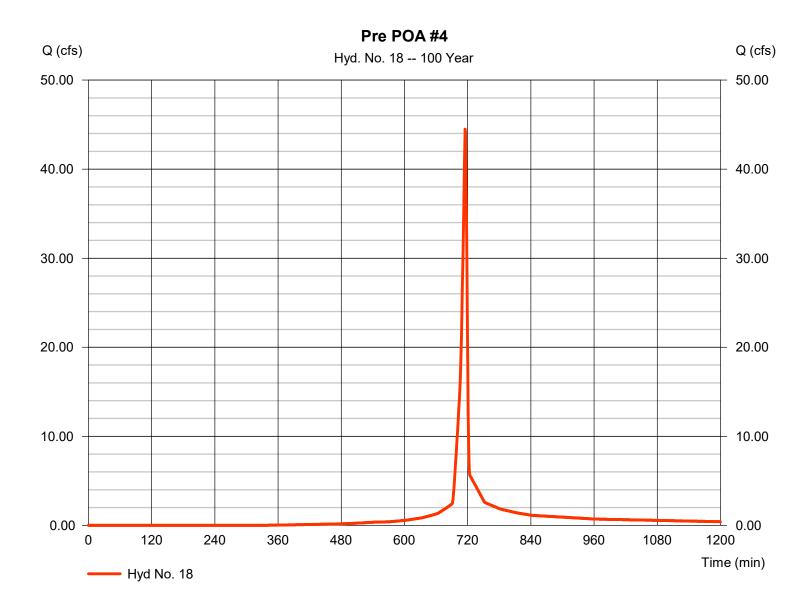
Hyd. No. 18

Storm duration

Pre POA #4

Hydrograph type = SCS Runoff Peak discharge = 44.48 cfsStorm frequency = 100 yrsTime to peak = 715 min Time interval = 1 min Hyd. volume = 81,914 cuft Drainage area Curve number = 4.720 ac= 79 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 2.10 min = TR55 Total precip. = 7.56 inDistribution = Type II

Shape factor



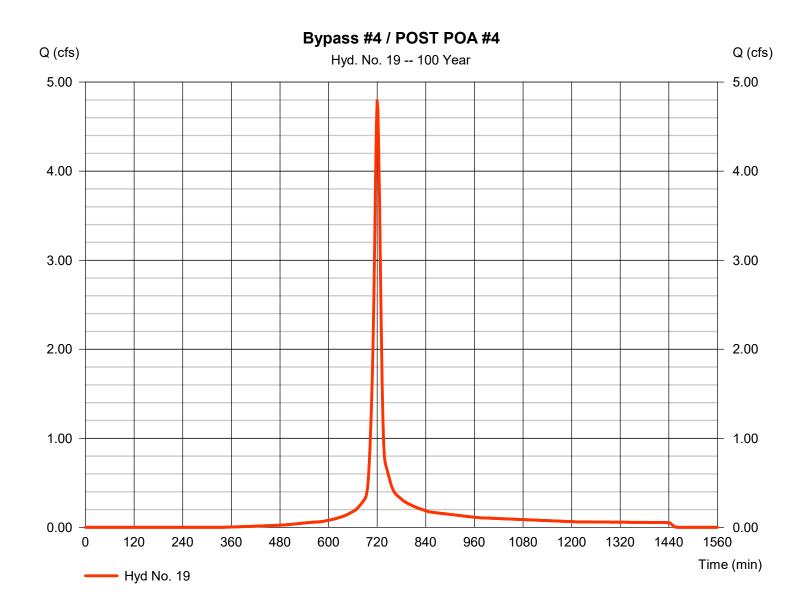
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Tuesday, 08 / 1 / 2023

Hyd. No. 19

Bypass #4 / POST POA #4

Hydrograph type = SCS Runoff Peak discharge = 4.793 cfsStorm frequency = 100 yrsTime to peak = 720 min Time interval = 2 min Hyd. volume = 12,599 cuftCurve number Drainage area = 0.660 ac= 79 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = User $= 10.00 \, \text{min}$ Total precip. = 7.56 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484



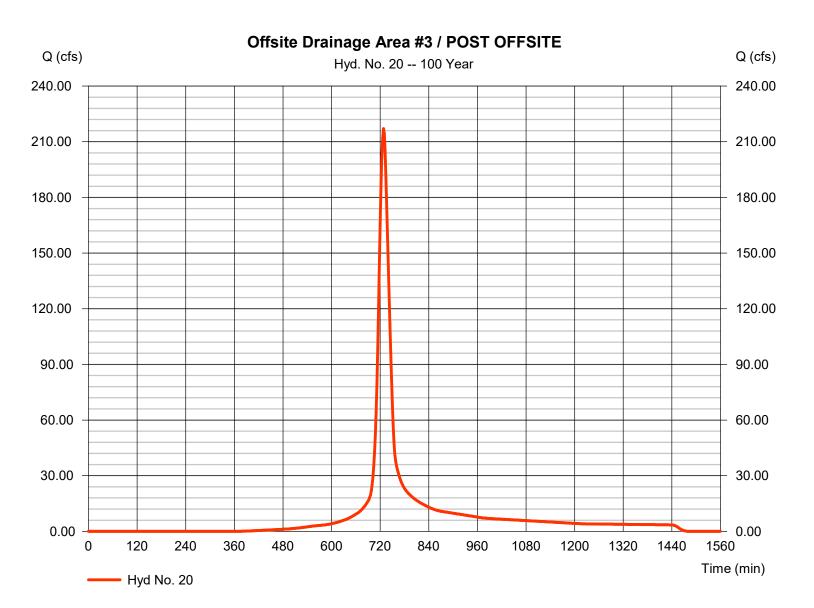
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Tuesday, 08 / 1 / 2023

Hyd. No. 20

Offsite Drainage Area #3 / POST OFFSITE

Hydrograph type = SCS Runoff Peak discharge = 217.12 cfsStorm frequency = 100 yrsTime to peak = 728 min Time interval = 2 min Hyd. volume = 798,606 cuft Drainage area Curve number = 45.870 ac = 77 = 0 ftBasin Slope = 0.0 %Hydraulic length Tc method Time of conc. (Tc) = 25.00 min = User Total precip. = 7.56 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



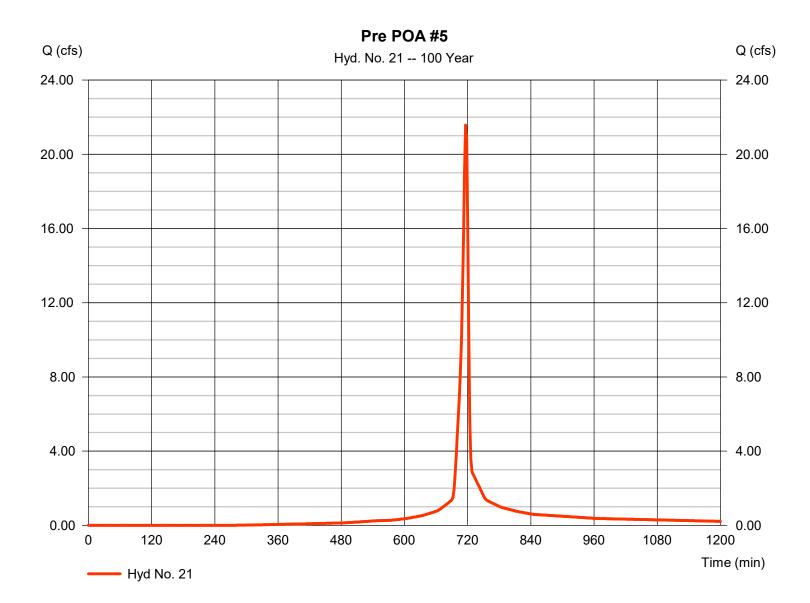
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Tuesday, 08 / 1 / 2023

Hyd. No. 21

Pre POA #5

Hydrograph type = SCS Runoff Peak discharge = 21.57 cfsStorm frequency = 100 yrsTime to peak = 716 min Time interval = 2 min Hyd. volume = 45,586 cuft Drainage area Curve number = 2.410 ac= 83 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 4.50 \, \text{min}$ = TR55 Total precip. = 7.56 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



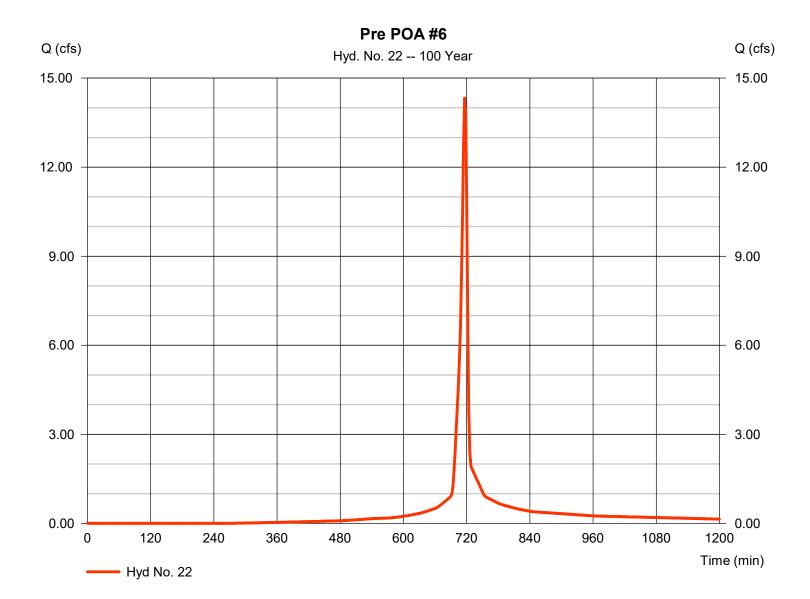
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Tuesday, 08 / 1 / 2023

Hyd. No. 22

Pre POA #6

Hydrograph type = SCS Runoff Peak discharge = 14.32 cfsStorm frequency = 100 yrsTime to peak = 716 min Time interval = 2 min Hyd. volume = 30,265 cuftDrainage area Curve number = 1.600 ac= 83 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) $= 4.20 \, \text{min}$ = TR55 Total precip. = 7.56 inDistribution = Type II Storm duration = 24 hrs Shape factor = 484



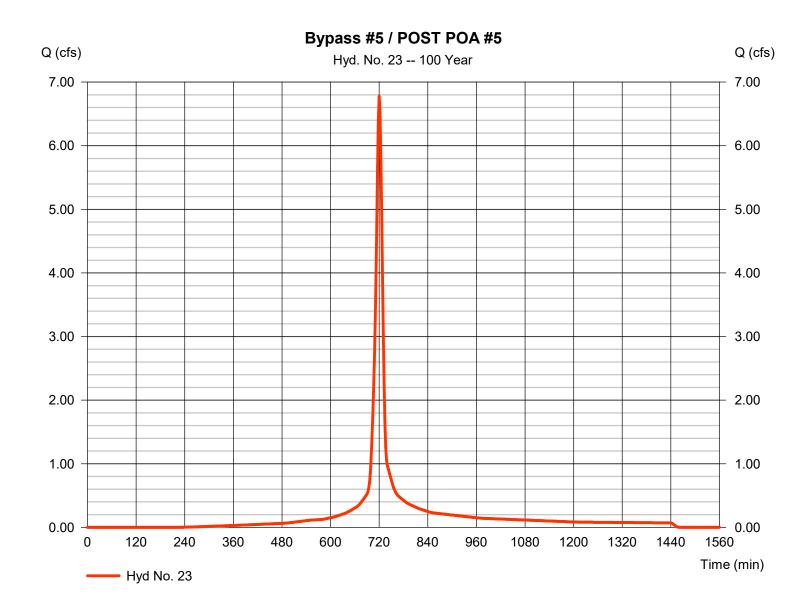
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Tuesday, 08 / 1 / 2023

Hyd. No. 23

Bypass #5 / POST POA #5

Hydrograph type = SCS Runoff Peak discharge = 6.777 cfsStorm frequency = 100 yrsTime to peak = 720 min Time interval = 2 min Hyd. volume = 18,349 cuftDrainage area Curve number = 0.830 ac= 86 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 10.00 min = User Total precip. = 7.56 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484



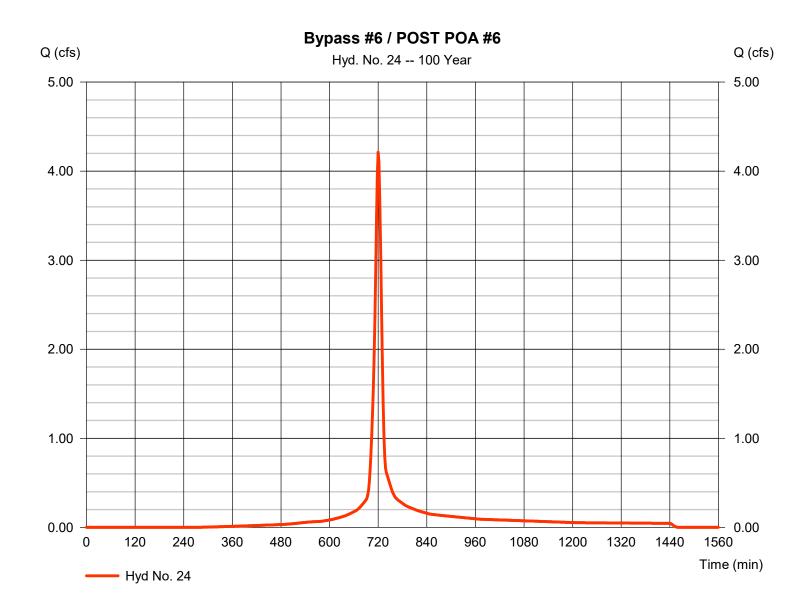
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Tuesday, 08 / 1 / 2023

Hyd. No. 24

Bypass #6 / POST POA #6

Hydrograph type = SCS Runoff Peak discharge = 4.212 cfsStorm frequency = 100 yrsTime to peak = 720 min Time interval = 2 min Hyd. volume = 11,236 cuft Curve number Drainage area = 0.540 ac= 83 Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc) = 10.00 min = User Total precip. = 7.56 inDistribution = Type II Shape factor Storm duration = 24 hrs = 484



Hydraflow Rainfall Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Tuesday, 08 / 1 / 2023

Return Period	Intensity-Duration-Frequency Equation Coefficients (FHA)							
(Yrs)	В	D	E	(N/A)				
1	0.0000	0.0000	0.0000					
2	51.0918	10.3000	0.8101					
3	0.0000	0.0000	0.0000					
5	49.6368	10.3000	0.7553					
10	51.1095	10.4000	0.7327					
25	54.6954	10.5000	0.7118					
50	58.0360	10.6000	0.7004					
100	61.9189	10.8000	0.6926					

File name: rolesville.IDF

Intensity = $B / (Tc + D)^E$

Return	Intensity Values (in/hr)											
Period (Yrs)	5 min	10	15	20	25	30	35	40	45	50	55	60
1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	5.61	4.46	3.73	3.22	2.85	2.56	2.33	2.14	1.98	1.85	1.73	1.63
3	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5	6.33	5.11	4.33	3.78	3.36	3.04	2.79	2.57	2.40	2.24	2.11	2.00
10	6.89	5.61	4.78	4.19	3.75	3.40	3.12	2.89	2.70	2.53	2.39	2.26
25	7.77	6.37	5.46	4.80	4.31	3.92	3.61	3.35	3.14	2.95	2.79	2.65
50	8.47	6.97	5.99	5.29	4.75	4.34	4.00	3.72	3.48	3.28	3.10	2.94
100	9.16	7.57	6.52	5.77	5.20	4.75	4.38	4.08	3.82	3.60	3.41	3.24

Tc = time in minutes. Values may exceed 60.

name: G:\NCA\Projects\Lennar\8430-03 - Lennar - School Street - Rolesville\04 - Calculations\Storm\rolesville prec.pcp

		Rainfall Precipitation Table (in)									
Storm Distribution	1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	100-yr			
SCS 24-hour	2.86	3.45	0.00	3.30	5.04	6.00	6.80	7.56			
SCS 6-Hr	2.04	2.44	0.00	0.00	3.54	4.22	0.00	5.45			
Huff-1st	0.00	0.00	0.00	2.75	0.00	0.00	6.50	0.00			
Huff-2nd	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00			
Huff-3rd	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00			
Huff-4th	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00			
Huff-Indy	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00			
Custom	0.00	0.00	0.00	2.80	0.00	0.00	6.00	0.00			



#118- Label what SCM this corresponds to. This comment applies to all SCM calculation sheets

Project Name: Parker Ridge City/State: Rolesville, NC

Project #: <u>8430-03</u> Date: <u>8/1/23</u>

Table 1 Surface Area to Drainage Area Ratio for Permanent Pool Sizing

Piedmont and Mountain SA/DA Table (Adapted from Driscoll, 1986)

	Permanent Pool Depth (feet)							
% Impervious	3.0	4.0	5.0	6.0	7.0	8.0		
10	0.51	0.43	0.37	0.30	0.27	0.25		
20	0.84	0.69	0.61	0.51	0.44	0.40		
30	1.17	0.94	0.84	0.72	0.61	0.56		
40	1.51	1.24	1.09	0.91	0.78	0.71		
50	1.79	1.51	1.31	1.13	0.95	0.87		
60	2.09	1.77	1.49	1.31	1.12	1.03		
70	2.51	2.09	1.80	1.56	1.34	1.17		
80	2.92	2.41	2.07	1.82	1.62	1.40		
90	3.25	2.64	2.31	2.04	1.84	1.59		
100	3.55	2.79	2.52	2.34	2.04	1.75		

Source: NCDEQ Stormwater Design Manual Minimum Design Criteria C-3 Wet Pond (4.18.2017)

Drainage Area Information

Total Drainage Area = 9.80 acres

Total Impervious Area = 5.21 acres

% Impervious Surface Area = 53.16 %

Normal Pool Information

Minimum Required Permanent Pool Surface Area	Provided Permanent Pool Surface Area		
Avg Depth = 3.50 ft	Normal Pool Elevation =	384.5	
SA/DA ratio = 1.74 From Table 1	Main Pool SA Provided =	8489 sq. ft.	
Minimum pond surface area $(SA) = \frac{DA \times SA \div DA \ ratio}{100}$		0.195 acres	
SA = 7422 sq. ft.			
0.170 acres			

Water Quality Information

1-Inch Runoff Volume	Calculation (Water Quality Volume)	Provided Water Quali	ty Volume
Using "Simple Method" Runo	ff Volume Calculations	Water Quality Pool Elev =	386.02 ft
As described by Schueler (1987)		Overflow Elev =	387.90 ft
$Rv = 0.05 + 0.9 \times I$	Where: Rv = Runoff coefficient (in./in.)	torage Volume Provided =	66349 cu. ft.
$RV = 0.03 + 0.3 \times 1$	I = Percent impervious		1.523 acre-ft
Rv =	0.53 in/in		
Total runoff volume from 1-in	nch precipitation:		
Runoff Volume $(S) = Des$	ign Rainfall $\times Rv \times$ Drainage Area		
S =	18800 cu. ft.		
	0.432 acre-ft		



Project Name: Parker Ridge Project #: 8430-03

City/State: Rolesville, NC Date: 8/1/23

Total Drainage Area = AVERAGE DEPTH

9.8

Per NCDEQ "Stormwater Design Manual" Minimum Design Criteria:

The average depth of a wet pond is to be calculated by one of these two options:

	Below Normal Pool Contours (feet)	Contour Area (SF)	Incremental Contour Volume (CF)	Accumulated Contour Volume (CF)	
$A_{\text{bot pond}} \rightarrow$	379.00	4017			_
	380.00	4627	4318	4318	←Sediment Storage Volume
	381.00	5266	4943	9261	
$A_{\text{bot shelf}} \rightarrow$	384.00	7367	18862	28123	
$A_{perm_pool} \rightarrow$	384.50	8489	3961	32084	←Total Pond Volume

V_{perm pool} = Total Volume - Sediment Storage Volume = 27,765 cf

OPTION 1: Use the following equation:

$$D_{avg} = \frac{V_{perm_pool}}{A_{perm_pool}}$$

Where:

 D_{avg} = Average Depth (ft)

 V_{perm_pool} = Volume of Permanent Pool (ft³)

 $A_{perm_pool} = Area of Permanent Pool (ft²)$

$$D_{avg} = 3.27 \text{ ft}$$

OPTION 2: Use the following equation:

$$D_{avg} = 0.25 \times \left(1 + \frac{A_{bot_shelf}}{A_{perm_pool}}\right) + \frac{A_{bot_shelf} + A_{bot_pond}}{2} \times \frac{Depth}{A_{bot_shelf}}$$

Where:

 D_{avg} = Average Depth (ft)

 A_{bot_shelf} = Area of Wet Pond at the Bottom of the Shelf (ft²)

A_{bot pond} = Area of Wet Pond Bottom above Sediment Storage (ft2)

 A_{perm_pool} = Area of Permanent Pool (ft²)

Depth = Depth of Wet Pond from Bottom of Shelf to Sediment Storage (ft)

$$D_{avg} = 3.72 \text{ ft}$$

Use Average Depth = 3.50 ft



Total Drainage Area =

FOREBAY DESIGN

Per NCDEQ "Stormwater Design Manual" Minimum Design Criteria:

The forebay volume shall be 15-20% of the main pool.

Project Name:Parker RidgeProject #:8430-03City/State:Rolesville, NCDate:8/1/23

70 Runoff Storage Volume Information

	Countour	Contour	Incremental	Accumulated	ı
Pond Area	Elevation	Area	Contour	Contour	
	(ft)	(sf)	Volume	Volume	
	390.00	20,196	19,318	85,667	←Top of Dam
	389.00	18,453	17,603	66,349	
Storage	388.00	16,767	15,946	48,746	
Volume	387.00	15,138	14,344	32,800	
	386.00	13,565	12,800	18,456	
	385.00	12,050	5,656	5,656	
Normal Pool	384.50	10,590	0	0	←Normal Pool

70 Pond Volume Information

70 Pond Vol	ume Information	n			_
	Countour	Contour	Incremental	Accumulated	
Pond Area	Elevation	Area	Contour	Contour	
	(ft)	(sf)	Volume	Volume	
	384.50	8,489	3,961	32,109	←Normal Pool
	384.00	7,367	7,001	28,148	←Bottom of Litoral Shelf
	383.00	6,641	6,287	21,147	Control of Entoral official
Main Pool	382.00	5,939	5,599	14,861	1
	381.00	5,266	4,943	9,261	1
	380.00	4,627	4,318	4,318	←Sediment Storage Volume
	379.00	4,017	0	0	←Pond Bottom
					1
	384.50	2,101	927	5,775	←Normal Pool
	384.00	1,617	1,470	4,848	←Bottom of Litoral Shelf
	383.00	1,328	1,194	3,378	1
Forebay	382.00	1,064	942	2,184	1
	381.00	826	718	1,242	
	380.00	616	523	523	←Sediment Storage Volume
	379.00	436	0	0	←Forebay Bottom
					1
	384.50	10,590	4,888	37,887	1
	384.00	8,984	8,471	32,999	1
	383.00	7,969	7,481	24,528	1
Total	382.00	7,003	6,542	17,047]
	381.00	6,092	5,662	10,505]
	380.00	5,243	4,843	4,843]
	379.00	4,453	0	0	1



Project Name:	Parker Ridge	Project #: 8430-0	ЭЗ
City/State:	Rolesville, NC	Date: 8/1/23	3

Total Drainage Area =

9.8 acres

OS-A Anti-Floatation Sizing Calulations

Outlet Structure Dimension

Inside Riser Width: 4 ft **Outside Riser Width:** 5 **ft** 6 in Wall Thickness: **Top Elevation:** 387.9 ft **Invert Elevation:** 384.5 ft **Bottom Elevation:** 379 ft 12 in 7 ft **Extended Base: Extended Base Width**

Displaced Volume: 222 cu ft
Displaced Weight: 13884 lbs

Volume of Actual Structure: 31 cu ft
Weight of Concrete Structure: 4590 lbs
Weight of Earth with Extended Base: 4488 lbs
Weight of Extra Depth: 20625 lbs
Total Weight of Structure: 29703 lbs

Factor of Safety: 2.1 Ok



Table 1 Surface Area to Drainage Area Ratio for Permanent Pool Sizing
Piedmont and Mountain SA/DA Table (Adapted from Driscoll, 1986)

	Permanent Pool Depth (feet)					
% Impervious	3.0	4.0	5.0	6.0	7.0	8.0
10	0.51	0.43	0.37	0.30	0.27	0.25
20	0.84	0.69	0.61	0.51	0.44	0.40
30	1.17	0.94	0.84	0.72	0.61	0.56
40	1.51	1.24	1.09	0.91	0.78	0.71
50	1.79	1.51	1.31	1.13	0.95	0.87
60	2.09	1.77	1.49	1.31	1.12	1.03
70	2.51	2.09	1.80	1.56	1.34	1.17
80	2.92	2.41	2.07	1.82	1.62	1.40
90	3.25	2.64	2.31	2.04	1.84	1.59
100	3.55	2.79	2.52	2.34	2.04	1.75

Source: NCDEQ Stormwater Design Manual Minimum Design Criteria C-3 Wet Pond (4.18.2017)

Drainage Area Information

Total Drainage Area = 20.08 acres
Total Impervious Area = 10.10 acres
% Impervious Surface Area = 50.30 %

Normal Pool Information

Minim	um Require	d Permanent Pool Surface Ar	Provided Permanent Pool	Surface Area	
Avg Depth =	3.50 ft			Normal Pool Elevation =	351.5
SA/DA ratio =	2.10	From Table 1		Main Pool SA Provided =	20384 sq. ft.
Minimum po	nd surface	$area (SA) = \frac{DA \times SA \div DA}{100}$		0.468 acres	
	SA =	18408 sq. ft.	_		
		0.423 acres			

Water Quality Information

1-Inch Runoff Volume Calculation (Water Quality Volume)	Provided Water Quali	ity Volume
Using "Simple Method" Runoff Volume Calculations	Water Quality Pool Elev =	352.83 ft
As described by Schueler (1987)	Overflow Elev =	354.82 ft
$Rv = 0.05 + 0.9 \times I \qquad \text{Where: Rv = Runoff coefficient (in./in.)} \\ Rv = 0.50 \text{ in/in} \\ \text{Total runoff volume from 1-inch precipitation:}$	Storage Volume Provided =	138278 cu. ft. 3.174 acre-ft
Runoff Volume (S) = Design Rainfall $\times Rv \times$ Drainage Area		
S = 36641 cu. ft.		
0.841 acre-ft		

Interpolation from table 10.1:

sno	Permanent Pool Depth			
Š		3.0	3.5	4.0
Jec	50.0	1.79		1.51
<u>.</u> E	50.3	1.80	2.10	2.41
%	60.0	2.09		1.77



Project Name: Parker Ridge Project #: 8430-03

City/State: Rolesville, NC Date: 8/1/23

Total Drainage Area =

AVERAGE DEPTH

Per NCDEQ "Stormwater Design Manual" Minimum Design Criteria:

The average depth of a wet pond is to be calculated by one of these two options:

	Below Normal Pool Contours (feet)	Contour Area (SF)	Incremental Contour Volume (CF)	Accumulated Contour Volume (CF)	
$A_{\text{bot pond}} \rightarrow$	346.00	12020			
	347.00	13231	12621	12621	←Sediment Storage Volume
	348.00	14468	13845	26466	
$A_{\text{bot_shelf}} \rightarrow$	351.00	18329	49081	75547	
$A_{perm pool} \rightarrow$	351.50	20384	9674	85221	←Total Pond Volume

V_{perm pool} = Total Volume - Sediment Storage Volume = 72,600 cf

OPTION 1: Use the following equation:

$$D_{avg} = \frac{V_{perm_pool}}{A_{perm_pool}}$$

Where:

D_{avg} = Average Depth (ft)

 $V_{perm pool}$ = Volume of Permanent Pool (ft³)

 $A_{perm_pool} = Area of Permanent Pool (ft²)$

$$D_{avg} = 3.56 \text{ ft}$$

OPTION 2: Use the following equation:

$$D_{avg} = 0.25 \times \left(1 + \frac{A_{bot_shelf}}{A_{perm_pool}}\right) + \frac{A_{bot_shelf} + A_{bot_pond}}{2} \times \frac{Depth}{A_{bot_shelf}}$$

Where:

 D_{avg} = Average Depth (ft)

 A_{bot_shelf} = Area of Wet Pond at the Bottom of the Shelf (ft²)

A_{bot_pond} = Area of Wet Pond Bottom above Sediment Storage (ft2)

 $A_{perm pool} = Area of Permanent Pool (ft²)$

Depth = Depth of Wet Pond from Bottom of Shelf to Sediment Storage (ft)

$$D_{avg} = 3.92 \text{ ft}$$

Use Average Depth = 3.50 ft



 Project Name:
 Project #: 8430-03

 City/State:
 Rolesville, NC

 Date:
 8/1/23

Total Drainage Area =

FOREBAY DESIGN

Per NCDEQ "Stormwater Design Manual" Minimum Design Criteria:

The forebay volume shall be 15-20% of the main pool.

 Project Name:
 Parker Ridge
 Project #:
 8430-03

 City/State:
 Rolesville, NC
 Date:
 8/1/23

50 Runoff Storage Volume Information

	Countour	Contour	Incremental	Accumulated	
Pond Area	Elevation	Area	Contour	Contour	
	(ft)	(sf)	Volume	Volume	
	357.00	37,716	36,604	174,882	←Top of Dam
	356.00	35,504	34,421	138,278	
Storage	355.00	33,350	32,295	103,857	
Volume	354.00	31,251	30,224	71,562	
	353.00	29,209	28,211	41,337	
	352.00	27,224	13,127	13,127	
Normal Pool	351.50	25,295	0	0	←Normal Pool

50 Pond Volume Information

50 Pond Vol	ume information	n			_
	Countour	Contour	Incremental	Accumulated	
Pond Area	Elevation	Area	Contour	Contour	
	(ft)	(sf)	Volume	Volume	
	351.50	20,384	9,674	85,272	←Normal Pool
	351.00	18,329	17,669	75,598	←Bottom of Litoral Shelf
	350.00	17,017	16,369	57,929	
Main Pool	349.00	15,730	15,095	41,560	
	348.00	14,468	13,845	26,466	
	347.00	13,231	12,621	12,621	←Sediment Storage Volume
	346.00	12,020	0	0	←Pond Bottom
	351.50	4,911	2,185	12,993	←Normal Pool
	351.00	3,849	3,477	10,809	←Bottom of Litoral Shelf
	350.00	3,117	2,768	7,332	
Forebay	349.00	2,434	2,111	4,564	
	348.00	1,803	1,504	2,453	
	347.00	1,224	949	949	←Sediment Storage Volume
	346.00	698	0	0	←Forebay Bottom
	351.50	25,295	11,860	98,288]
	351.00	22,178	21,148	86,428	15.2%
	350.00	20,134	19,141	65,281	
Total	349.00	18,164	17,209	46,140	
	348.00	16,271	15,354	28,931	
	347.00	14,455	13,577	13,577	
	346.00	12,718	0	0	



Total Drainage Area =

OS-A Anti-Floatation Sizing Calulations

Outlet Structure Dimension

Inside Riser Width: 4 ft Outside Riser Width: 5 ft

Wall Thickness: 6 in
Top Elevation: 354.85 ft
Invert Elevation: 351.5 ft
Bottom Elevation: 347 ft

Extended Base: 12 in Extended Base Width 7 ft

Displaced Volume: 196 cu ft
Displaced Weight: 12246 lbs

Volume of Actual Structure: 30 cu ft
leight of Concrete Structure: 4523 lbs

of Earth with Extended Base: 4422 lbs

Weight of Extra Depth: 16875 lbs

Total Weight of Structure: 25820 lbs

Factor of Safety: 2.1 OK



Table 1 Surface Area to Drainage Area Ratio for Permanent Pool Sizing
Piedmont and Mountain SA/DA Table (Adapted from Driscoll, 1986)

	Permanent Pool Depth (feet)					
% Impervious	3.0	4.0	5.0	6.0	7.0	8.0
10	0.51	0.43	0.37	0.30	0.27	0.25
20	0.84	0.69	0.61	0.51	0.44	0.40
30	1.17	0.94	0.84	0.72	0.61	0.56
40	1.51	1.24	1.09	0.91	0.78	0.71
50	1.79	1.51	1.31	1.13	0.95	0.87
60	2.09	1.77	1.49	1.31	1.12	1.03
70	2.51	2.09	1.80	1.56	1.34	1.17
80	2.92	2.41	2.07	1.82	1.62	1.40
90	3.25	2.64	2.31	2.04	1.84	1.59
100	3.55	2.79	2.52	2.34	2.04	1.75

Source: NCDEQ Stormwater Design Manual Minimum Design Criteria C-3 Wet Pond (4.18.2017)

Drainage Area Information

Total Drainage Area = 11.17 acres

Total Impervious Area = 4.63 acres

% Impervious Surface Area = 41.45 %

Input Output

Normal Pool Information

Minimum Required Permanent Pool Surface Area	Provided Permanent Pool Surface Area
Avg Depth = 3.50 ft	Normal Pool Elevation = 384.5
SA/DA ratio = 1.41 From Table 1	Main Pool SA Provided = 7226 sq. ft.
Minimum pond surface area $(SA) = \frac{DA \times SA \div DA \ ratio}{100}$	0.166 acres
SA = 6884 sq. ft.	
0.158 acres	

Water Quality Information 1-Inch Runoff Volume Calculation (Water Quality Volume) **Provided Water Quality Volume** Using "Simple Method" Runoff Volume Calculations Water Quality Pool Elev = 386.10 ft Overflow Elev = 387.80 ft As described by Schueler (1987) Where: Rv = Runoff coefficient (in./in.) Storage Volume Provided = 41614 cu. ft. $Rv = 0.05 + 0.9 \times I$ I = Percent impervious 0.955 acre-ft Rv = 0.42 in/in Total runoff volume from 1-inch precipitation: Runoff Volume (S) = Design Rainfall $\times Rv \times$ Drainage Area S = 17154 cu. ft. 0.394 acre-ft



Project Name: Parker Ridge Project #: 8430-03

City/State: Rolesville, NC Date: 8/1/23

Total Drainage Area =

AVERAGE DEPTH

Per NCDEQ "Stormwater Design Manual" Minimum Design Criteria:

The average depth of a wet pond is to be calculated by one of these two options:

	Below Normal Pool Contours (feet)	Contour Area (SF)	Incremental Contour Volume (CF)	Accumulated Contour Volume (CF)	
$A_{\text{bot pond}} \rightarrow$	379.00	3496			_
	380.00	4003	3747	3747	←Sediment Storage Volume
	381.00	4531	4264	8011	
$A_{\text{bot_shelf}} \rightarrow$	384.00	6265	16124	24135	
$A_{perm_pool} \rightarrow$	384.50	7226	3370	27505	←Total Pond Volume

V_{perm pool} = Total Volume - Sediment Storage Volume = 23,758 cf

OPTION 1: Use the following equation:

$$D_{avg} = \frac{V_{perm_pool}}{A_{perm_pool}}$$

Where:

D_{avg} = Average Depth (ft)

 V_{perm_pool} = Volume of Permanent Pool (ft³)

 $A_{perm pool} = Area of Permanent Pool (ft²)$

$$D_{avg} = 3.29 \text{ ft}$$

OPTION 2: Use the following equation:

$$D_{avg} = 0.25 \times \left(1 + \frac{A_{bot_shelf}}{A_{perm_pool}}\right) + \frac{A_{bot_shelf} + A_{bot_pond}}{2} \times \frac{Depth}{A_{bot_shelf}}$$

Where:

 D_{avg} = Average Depth (ft)

 $A_{\text{bot_shelf}}$ = Area of Wet Pond at the Bottom of the Shelf (ft²)

 A_{bot_pond} = Area of Wet Pond Bottom above Sediment Storage (ft2)

 $A_{perm pool} = Area of Permanent Pool (ft²)$

Depth = Depth of Wet Pond from Bottom of Shelf to Sediment Storage (ft)

$$D_{avg} = 3.74 \text{ ft}$$

Use Average Depth = 3.50 ft



Total Drainage Area =

FOREBAY DESIGN

Per NCDEQ "Stormwater Design Manual" Minimum Design Criteria:

11.17

The forebay volume shall be 15-20% of the main pool.

Project Name:Parker Ridge SubdivisionProject #:8430-03City/State:Rolesville, NCDate:8/1/23

70 Runoff Storage Volume Information

	Countour	Contour	Incremental	Accumulated	I
Pond Area	Elevation	Area	Contour	Contour	
	(ft)	(sf)	Volume	Volume	
	390.00	16,783	16,086	72,439	←Top of Dam
	389.00	15,400	14,738	56,352	
Storage	388.00	14,086	13,446	41,614	
Volume	387.00	12,816	12,204	28,168	
	386.00	11,603	11,019	15,964	
	385.00	10,446	4,944	4,944	
Normal Pool	384.50	9,342	0	0	←Normal Pool

70 Pond Volume Information

70 Pond Vo	lume Informatio	n			_
	Countour	Contour	Incremental	Accumulated	
Pond Area	Elevation	Area	Contour	Contour	
	(ft)	(sf)	Volume	Volume	
	384.50	7,226	3,370	27,517	←Normal Pool
	384.00	6,265	5,961	24,147	←Bottom of Litoral Shelf
	383.00	5,662	5,370	18,186	
Main Pool	382.00	5,084	4,805	12,816	1
	381.00	4,531	4,264	8,011	1
	380.00	4,003	3,747	3,747	←Sediment Storage Volume
	379.00	3,496	0	0	←Pond Bottom
	384.50	2,116	927	5,417	←Normal Pool
	384.00	1,604	1,445	4,490	←Bottom of Litoral Shelf
	383.00	1,292	1,143	3,045	
Forebay	382.00	1,000	866	1,902	
	381.00	738	622	1,037	
	380.00	512	415	415	←Sediment Storage Volume
	379.00	325	0	0	←Forebay Bottom
	384.50	9,342	4,297	32,940	
	384.00	7,869	7,407	28,643	
	383.00	6,954	6,514	21,236	
Total	382.00	6,084	5,672	14,722	
	381.00	5,269	4,887	9,050	
	380.00	4,515	4,163	4,163	
	379.00	3,821	0	0	



Project Name:	Parker Ridge	Project #:	8430-03
City/State:	Rolesville, NC	Date:	8/1/23

Total Drainage Area =

OS-A Anti-Floatation Sizing Calulations

Outlet Structure Dimension

Inside Riser Width: 4 ft Outside Riser Width: 5 ft Wall Thickness: 6 in

Top Elevation: 388.35 ft
Invert Elevation: 384.5 ft
Bottom Elevation: 380 ft

Extended Base: 12 in Extended Base Width: 7 ft

Displaced Volume: 209 cu ft
Displaced Weight: 13026 lbs

Volume of Actual Structure: 35 cu ft
leight of Concrete Structure: 5198 lbs

of Earth with Extended Base: 5082 lbs

Weight of Extra Depth: 16875 lbs

Total Weight of Structure: 27155 lbs

Factor of Safety: 2.1 Ok



Table 1 Surface Area to Drainage Area Ratio for Permanent Pool Sizing
Piedmont and Mountain SA/DA Table (Adapted from Driscoll, 1986)

	Permanent Pool Depth (feet)					
% Impervious	3.0	4.0	5.0	6.0	7.0	8.0
10	0.51	0.43	0.37	0.30	0.27	0.25
20	0.84	0.69	0.61	0.51	0.44	0.40
30	1.17	0.94	0.84	0.72	0.61	0.56
40	1.51	1.24	1.09	0.91	0.78	0.71
50	1.79	1.51	1.31	1.13	0.95	0.87
60	2.09	1.77	1.49	1.31	1.12	1.03
70	2.51	2.09	1.80	1.56	1.34	1.17
80	2.92	2.41	2.07	1.82	1.62	1.40
90	3.25	2.64	2.31	2.04	1.84	1.59
100	3.55	2.79	2.52	2.34	2.04	1.75

Source: NCDEQ Stormwater Design Manual Minimum Design Criteria C-3 Wet Pond (4.18.2017)

Drainage Area Information

Total Drainage Area = 9.86 acres
Total Impervious Area = 4.34 acres
% Impervious Surface Area = 44.02 %

Input Output

Normal Pool Information

Minimum Required Permanent Pool Surface Area	Provided Permanent Pool	Surface Area
Avg Depth = 3.50 ft	Normal Pool Elevation =	380.5
SA/DA ratio = 2.02 From Table 1	Main Pool SA Provided =	14636 sq. ft.
Minimum pond surface area $(SA) = \frac{DA \times SA \div DA \ ratio}{100}$		0.336 acres
SA = 8660 sq. ft.		
0.199 acres		

Water Quality Information

Provided Water Quali	ty Volume
Water Quality Pool Elev =	381.49 ft
Overflow Elev =	385.00 ft
Storage Volume Provided =	84687 cu. ft. 1.944 acre-ft
	Overflow Elev =



Total Drainage Area =

AVERAGE DEPTH

Per NCDEQ "Stormwater Design Manual" Minimum Design Criteria:

The average depth of a wet pond is to be calculated by one of these two options:

	Below Normal Pool Contours (feet)	Contour Area (SF)	Incremental Contour Volume (CF)	Accumulated Contour Volume (CF)	
$A_{\text{bot pond}} \rightarrow$	375.00	5047			
	376.00	5697	5369	5369	←Sediment Storage Volume
	377.00	6373	6032	11401	
$A_{\text{bot shelf}} \rightarrow$	380.00	8550	22305	33705	
$A_{perm_pool} \rightarrow$	380.50	10901	4851	38556	←Total Pond Volume

V_{perm pool} = Total Volume - Sediment Storage Volume = 33,187 cf

OPTION 1: Use the following equation:

$$D_{avg} = \frac{V_{perm_pool}}{A_{perm_pool}}$$

Where:

 D_{avg} = Average Depth (ft)

 V_{perm_pool} = Volume of Permanent Pool (ft³)

 $A_{perm pool} = Area of Permanent Pool (ft²)$

 $D_{avg} = 3.04 \text{ ft}$

OPTION 2: Use the following equation:

$$D_{avg} = 0.25 \times \left(1 + \frac{A_{bot_shelf}}{A_{perm_pool}}\right) + \frac{A_{bot_shelf} + A_{bot_pond}}{2} \times \frac{Depth}{A_{bot_shelf}}$$

Where:

 D_{avg} = Average Depth (ft)

 A_{bot_shelf} = Area of Wet Pond at the Bottom of the Shelf (ft²)

A_{bot_pond} = Area of Wet Pond Bottom above Sediment Storage (ft2)

 A_{perm_pool} = Area of Permanent Pool (ft²)

Depth = Depth of Wet Pond from Bottom of Shelf to Sediment Storage (ft)

 $D_{avg} = 3.78 \text{ ft}$

Use Average Depth = 3.50 ft



 Project Name:
 Project #: 8430-03

 City/State:
 Rolesville, NC

 Date:
 8/1/23

Total Drainage Area =

9.86

FOREBAY DESIGN

Per NCDEQ "Stormwater Design Manual" Minimum Design Criteria:

The forebay volume shall be 15-20% of the main pool.

Project Name: Parker Ridge
City/State: Rolesville, NC

Project #: 8430-03
Date: 8/1/23

70 Runoff Storage Volume Information

	Countour	Contour	Incremental	Accumulated	
Pond Area	Elevation	Area	Contour	Contour	
	(ft)	(sf)	Volume	Volume	
	386.00	24,300	23,419	108,106	←Top of Dam
	385.00	22,548	21,695	84,687	
Storage	384.00	20,853	20,028	62,992	
Volume	383.00	19,214	18,418	42,964	
	382.00	17,634	16,864	24,546	
	381.00	16,105	7,682	7,682	
Normal Pool	380.50	14,636	0	0	←Normal Pool

70 Pond Volume Information

70 1 Olla VO	iume imormatio				•
	Countour	Contour	Incremental	Accumulated	
Pond Area	Elevation	Area	Contour	Contour	
	(ft)	(sf)	Volume	Volume	
	380.50	10,901	4,851	38,576	←Normal Pool
	380.00	8,550	8,172	33,725	←Bottom of Litoral Shelf
	379.00	7,799	7,433	25,554	
Main Pool	378.00	7,073	6,720	18,121	
	377.00	6,373	6,032	11,401	
	376.00	5,697	5,369	5,369	←Sediment Storage Volume
	375.00	5,047	0	0	←Pond Bottom
	380.50	3,735	1,638	9,851	←Normal Pool
	380.00	2,839	2,566	8,212	←Bottom of Litoral Shelf
	379.00	2,302	2,054	5,647	
Forebay	378.00	1,816	1,592	3,592	
	377.00	1,379	1,181	2,000	
	376.00	993	819	819	←Sediment Storage Volume
	375.00	657	0	0	←Forebay Bottom
	380.50	14,636	6,489	48,435	1
	380.00	11,389	10,739	41,946	1
	379.00	10,101	9,489	31,208	1
Total	378.00	8,889	8,314	21,719]
	377.00	7,752	7,214	13,405]
	376.00	6,690	6,190	6,190]
	375.00	5,704	0	0	1



Project Name: Parker Ridge	Project #: 8430-03
City/State: Rolesville, NC	Date: 8/1/23

Total Drainage Area =

OS-A Anti-Floatation Sizing Calulations

Outlet Structure Dimension

Inside Riser Width: 4 ft Outside Riser Width: 5 ft

Wall Thickness: 6 in
Top Elevation: 386 ft
Invert Elevation: 380.5 ft
Bottom Elevation: 375 ft

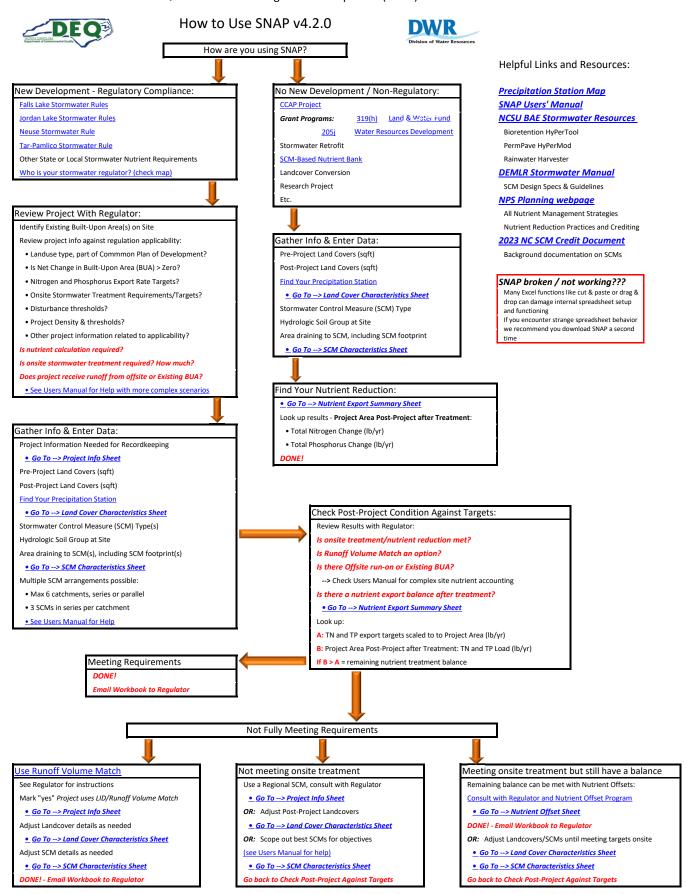
Extended Base: 12 in Extended Base Width: 7 ft

Displaced Volume: 275 cu ft
Displaced Weight: 17160 lbs

Volume of Actual Structure: 50 cu ft
leight of Concrete Structure: 7425 lbs
of Earth with Extended Base: 7260 lbs
Weight of Extra Depth: 20625 lbs
Total Weight of Structure: 35310 lbs

Factor of Safety: 2.1 Ok

ATTACHMENT 8: NUTRIENT CALCULATIONS



Project Information

Complete this sheet if required by your reviewing authority. Contact them for any questions. Grey boxes/text are optional.

SNAP v4.2.0

LOCATION

Project Name (optional):	Parker Ridge		Parcel ID (optional):
Submission Date (optional):		date	Nutrient Management Watershed:
Local Jurisdiction / Reviewing Agency:	Rolesville	menu	Subwatershed:
Project Latitude Coordinates (optional):		N	Phosphorus Delivery Zone:
Project Longitude Coordinates (optional):		W	Nitrogen Delivery Zone:

Parcel ID (optional):		
Nutrient Management Watershed:	Neuse	menu
Subwatershed:	Neuse-Upper	menu
Phosphorus Delivery Zone:	Neuse - Upper 03020201	menu
Nitrogen Delivery Zone:	Neuse - Upper 03020201	menu

PROJECT DETAILS

Development Land Use Type:	Single Family Residential	menu
Part of Common Development Plan?	no	y/n
Designated Downtown Area?	no	y/n
Public Linear Road/Sidewalk Project?	no	y/n
Project Owner Type:	Private	menu

	Disturbed Area:	2,596,176	ft ²
	Project Activity:	New Development	menu
1	Project Drains to SA Waters?	no	y/n
1	Pre-Project Land Use:	fallow/open	menu
	Project Description (optional):		

STORMWATER DETAILS

(Falls ONLY) Onsite Reduction % Req.		%
Existing BUA/Development Onsite?	no	y/n
Local Gov't cutoff date for Existing BUA:	05/01/2005	date
Nitrogen Export Rate Target:	3.60	lb/ac/yr
Phosphorus Export Rate Target:	0.40	lb/ac/yr

Project Uses LID/Runoff Volume Match?	no	y/n
Local Gov't nutrient req's same as State?	yes	y/n
Project Drains to Regional SCM?	no	y/n
Total Nitrogen Offset Credits Needed:	312.8	lb/yr
Total Phosphorus Offset Credits Needed:	34.8	lb/yr

Project Area and Offsite Land Cover Characteristics

Precipitation
Station:

Raleigh

Copy & Paste VALUES ONLY for Best Results

Click here to scroll down to error messages on this sheet.

PROJECT AREA LAND COVERS	TN EMC (mg/L)	TP EMC (mg/L)	Pre-Project Area (ft²)	Post-Project Area (ft²)	Change pre-to-post (ft ²)
Roof	1.18	0.11	2,810	669,081	666,271
Roadway	1.64	0.34	34,424	377,237	342,813
Parking/Driveway/Sidewalk	1.42	0.18	0	178,781	178,781
Protected Forest	0.97	0.03	3,115,651	0	-3,115,651
Managed Pervious/Landscaping	2.48	1.07	393,782	2,222,573	1,828,791
Offsite or Existing Roof	1.18	0.11			0
Offsite or Existing Roadway	1.64	0.34			0
Offsite or Existing Parking/Driveway/Sidewa	1.42	0.18			0
Offsite Protected Forest	0.97	0.03			0
Offsite Managed Pervious	2.48	1.07			0
CUSTOM LAND COVER 1					0
CUSTOM LAND COVER 2					0
CUSTOM LAND COVER 3					0
LAND TAKEN UP BY SCM	1.18	0.11		98,995	98,995
	Total (Regulate	d & UnReg) Area	3,546,667.00	3,546,667.00	
	Project (Regulated) Are		3,546,667.00	3,546,667.00	

SNAP v4.2.0	Copy & Paste for Best		SCM101's Land Cover Data	Click here to review Errors	Summary Data	top							
Catchment ID	1 000	ains to 102 Dra	ninr to 1	2 000	ains to 2	Orains to 2	3 000	ains to 3 Dra	ins to 3	4 Dr	ains to Dr.	ains to 4	5
SCM ID	101 Dra	102	103	201 Dra	202	203	301 Dra	ains to Dra	303	401 Dr.	ains to Dr.	403	501
Type of SCM	Wet Pond												
Hydrologic soil group at SCM location	D			D			D			D			
SCM Description													
Design Storm Size (inches/24hrs)													
Percent of Full Size	100%			100%			100%			100%			
% Annual Effluent	76%	0%	0%	76%	0%	0%	76%	0%	0%	76%	0%	0%	0%
% Annual Overflow	16%	0%	0%	16%	0%	0%	16%	0%	0%	16%	0%	0%	0%
% Annual ET/Infiltrated	8%	0%	0%	8%	0%	0%	8%	0%	0%	8%	0%	0%	0%
Custom % Annual Effluent	0,0	0,0	0,0	0,0	0,0	0,0	0,0	0,0	0.0	0.0	0.0	0,0	0,0
Custom % Annual Overflow													
Custom % Annual ET/Infiltrated										li			
SCM Effluent TP EMC (mg/L)	0.13	0.00	0.00	0.13	0.00	0.00	0.13	0.00	0.00	0.13	0.00	0.00	0.00
SCM Effluent TN EMC (mg/L)	0.86	0.00	0.00	0.86	0.00	0.00	0.86	0.00	0.00	0.86	0.00	0.00	0.00
Custom Effluent TP EMC													
Custom Effluent TN EMC													
SCM Land Cover TP EMC (mg/L)	0.11	0.00	0.00	0.11	0.00	0.00	0.11	0.00	0.00	0.11	0.00	0.00	0.00
SCM Land Cover TN EMC (mg/L)	1.18	0.00	0.00	1.18	0.00	0.00	1.18	0.00	0.00	1.18	0.00	0.00	0.00
This SCM Drains to Numbered SCM	0	0	0	0	0	0	0	0	0	0	0	0	0
	Catchments Draining to SCM 101	Catchments Draining to SCM 102	Catchments Draining to SCM 103	Catchments Draining to SCM 201	Catchments Draining to SCM 202	Catchments Draining to SCM 203	Catchments Draining to SCM 301	Catchments Draining to SCM 302	Catchments Draining to SCM 303	Catchments Draining to SCM 401	Catchments Draining to SCM 402	Catchments Draining to SCM 403	Catchments Drain
Catchment 1				no			no			no			
Catchment 2	no			110			no			no			
Catchment 3							110						
Catchment 4	no			no						no			
Catchment 5	no			no			no						
	no			no			no			no			
Catchment 6	no			no			no			no			
Error Check - Missing SCM Area:													
Error Check - Min/Max Size:													
Error Check - Hydrology:													
Error Check - Missing SCM Info:													
Error Check - Drainage Data w/o SCM:													
Error Checks - SCM Type:													
SCM ID:	101	102	103	201	202	203	301	302	303	401	402	403	501
SCM Drainage Area Land Covers	Area Draining Directly to SCM 101 (ft2)	Area Draining Directly to SCM 102 (ft2)	Area Draining Directly to SCM 103 (ft2)	Area Draining Directly to SCM 201 (ft2)	Area Draining Directly to SCM 202 (ft2)	Area Draining Directly to SCM 203 (ft2)	Area Draining Directly to SCM 301 (ft2)	Area Draining Directly to SCM 302 (ft2)	Area Draining Directly to SCM 303 (ft2)	Area Draining Directly to SCM 401 (ft2)	Area Draining Directly to SCM 402 (ft2)	Area Draining Directly to SCM 403 (ft2)	Area Draining Dire SCM 501 (ft2
pof	119,790			274,864			112,385			130,680			
adway	56,376			130,244			65,776			43,560			
rking/Driveway/Sidewalk	30,586			34,848			23,522			14,810			
otected Forest	0			0			0			0			
anaged Pervious/Landscaping	199,940			381,767			242,834			216,151			
fsite or Existing Roof													
fsite or Existing Roadway													
fsite or Existing Parking/Driveway/Sidewa	alk												
fsite Protected Forest						1							-
fsite Managed Pervious													
STOM LAND COVER 1													
			l			1						!	-
ISTOM LAND COVER 2													
JSTOM LAND COVER 2 JSTOM LAND COVER 3	20.196			37.716			16 783			24 300			
JSTOM LAND COVER 2 JSTOM LAND COVER 3 IND TAKEN UP BY SCM TOTAL AREA DRAINING TO SCM (R²):	20,196 426,888	0	0	37,716 859,439	0	0	16,783 461,300	0	0	24,300 429,501	0	0	0

Stormwater Control Measu

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Catchment ID SCM ID	ins to 502 Dra	5 503	6 601	6 Dr	ains to 6			
SCHI ID	<u> </u>	303	001	002	003			
Type of SCM								
Hydrologic soil group at SCM location								
SCM Description								
Design Storm Size (inches/24hrs)								
Percent of Full Size								
% Annual Effluent	0%	0%	0%	0%	0%			
% Annual Overflow	0%	0%	0%	0%	0%			
% Annual ET/Infiltrated	0%	0%	0%	0%	0%			
Custom % Annual Effluent	070	0,0	0,0	070	070			
Custom % Annual Overflow								
Custom % Annual ET/Infiltrated								
	0.00	0.00	0.00	0.00	0.00			
SCM Effluent TP EMC (mg/L)								
SCM Effluent TN EMC (mg/L)	0.00	0.00	0.00	0.00	0.00			
Custom Effluent TP EMC								
Custom Effluent TN EMC								
SCM Land Cover TP EMC (mg/L)	0.00	0.00	0.00	0.00	0.00			
SCM Land Cover TN EMC (mg/L)	0.00	0.00	0.00	0.00	0.00			
This SCM Drains to Numbered SCM	0	0	0	0	0		ก	
Catchment Routing	Catchments Draining to SCM 502	Catchments Draining to SCM 503	Catchments Draining to SCM 601	Catchments Draining to SCM 602	Catchments Draining to SCM 603			
Catchment 1								
Catchment 2								
Catchment 3								
Catchment 4								
Catchment 5								
Catchment 6								
Error Check - Missing SCM Area:								
Error Check - Min/Max Size:								
Error Check - Hydrology:								
Error Check - Missing SCM Info:								
Error Check - Drainage Data w/o SCM:								
Error Checks - SCM Type:								
SCM ID:	502	503	601	602	603			
SCM Drainage Area Land Covers	Area Draining Directly to SCM 502 (ft2)	Area Draining Directly to SCM 503 (ft2)	Area Draining Directly to SCM 601 (ft2)	Area Draining Directly to SCM 602 (ft2)	Area Draining Directly to SCM 603 (ft2)	Total Land Use Area Treated By All SCMs (ft²)	Allowable Total Land Use Area to be Treated Based on Post-Project Areas (ft²)	Post-Project Untreate Land Area (ft ²)
oof						637,719	669,081	31,362
oadway						295,956	377,237	81,281
arking/Driveway/Sidewalk						103,766	178,781	75,015
rotected Forest						0	0	0
Managed Pervious/Landscaping						1,040,692	2,222,573	1,181,881
ffsite or Existing Roof						0	0	0
ffsite or Existing Roadway						0	0	0
ffsite or Existing Parking/Driveway/Sidev ffsite Protected Forest						0	0	0
offsite Managed Pervious						0	0	0
USTOM LAND COVER 1						0	0	0
USTOM LAND COVER 2						0	0	0
USTOM LAND COVER 3						0	0	0
AND TAKEN UP BY SCM						98,995	98,995	0
TOTAL AREA DRAINING TO SCM (ft ²):	0	0	0	0	0	2,177,128	3,546,667	1,369,539

Nutrient Export Summary

Landcover & SCM Data Review

Errors / Advisories

Avg Annual precip (in) =	46.22	
Total (Regulated + Unregulated) Area (ft²) =	3,546,667	
Project (Regulated) Area (ft²) =	3,546,667	
Net BUA (Project Area BUA only ft ²) =	1,187,865	Net BUA indicates new development or expansion.
Custom Landcovers are present:		
Total Nitrogen Scaled to Project	•	293.11

Nutrient Export Summary	Total Area (Onsite + Offsite) P <u>re-Project</u>	Project Area (Onsite Only) <u>Pre-Project</u>	Total Area Post-Project before Treatment	Project Area Post-Project before Treatment
Area (All Landcover Types) (acres)	81.4203	81.4203	81.4203	81.4203
Percent Built-Upon Area (BUA) (%)	1%	1%	35%	35%
Built-Upon Area (BUA) (sqft)	37,234	37,234	1,225,099	1,225,099
Annual Runoff Volume (ft ³ /yr)	730,891	730,891	4,762,859	4,762,859
Annual Runoff % Change			552%	552%
Total Runoff Change (cuft/yr)			4,031,968	4,031,968
Total Nitrogen EMC (mg/L)	1.22	1.22	1.43	1.43
Total Nitrogen Load Leaving Site (lb/yr)	55.57	55.57	426.72	426.72
Total Nitrogen Loading Rate (lb/ac/yr)	0.68	0.68	5.24	5.24
Total Nitrogen % Change Pre-to-Post			668%	668%
Total Nitrogen Change (lb/yr) Pre-to-Post			371.15	371.15
Total Phosphorus EMC (mg/L)	0.18	0.18	0.26	0.26
Total Phosphorus Load Leaving Site (lb/yr)	8.04	8.04	76.22	76.22
Total Phosphorus Loading Rate (lb/ac/yr)	0.10	0.10	0.94	0.94
Total Phosphorus % Change Pre-to-Post			848%	848%
Total Phosphorus Change (lb/yr)Pre-to-Post			68.18	68.18

SCM/Catchment Summary

SCM ID and Type	Volume Reduction (%)	TN Reduction (%)	TP Reduction (%)	TN Out (lbs/ac/yr)	TP Out (lbs/ac/yr)
Catchment 1	8.44%	37.11%	38.77%	4.33	0.66
101: Wet Pond	8.44%	37.11%	38.77%	4.33	0.66
102: NA	0.00%	0.00%	0.00%	0.00	0.00
103: NA	0.00%	0.00%	0.00%	0.00	0.00
Catchment 2	8.44%	36.83%	38.28%	4.50	0.69
201: Wet Pond	8.44%	36.83%	38.28%	4.50	0.69
202: NA	0.00%	0.00%	0.00%	0.00	0.00
203: NA	0.00%	0.00%	0.00%	0.00	0.00
Catchment 3	8.44%	38.10%	42.55%	3.92	0.61
301: Wet Pond	8.44%	38.10%	42.55%	3.92	0.61
302: NA	0.00%	0.00%	0.00%	0.00	0.00
303: NA	0.00%	0.00%	0.00%	0.00	0.00
Catchment 4	8.44%	36.16%	36.91%	4.06	0.62
401: NA	8.44%	36.16%	36.91%	4.06	0.62
402: NA	0.00%	0.00%	0.00%	0.00	0.00
403: NA	0.00%	0.00%	0.00%	0.00	0.00
Catchment 5	0.00%	0.00%	0.00%	0.00	0.00
501: NA	0.00%	0.00%	0.00%	0.00	0.00
502: NA	0.00%	0.00%	0.00%	0.00	0.00
503: NA	0.00%	0.00%	0.00%	0.00	0.00
Catchment 6	0.00%	0.00%	0.00%	0.00	0.00
601: NA	0.00%	0.00%	0.00%	0.00	0.00
602: NA	0.00%	0.00%	0.00%	0.00	0.00
603: NA	0.00%	0.00%	0.00%	0.00	0.00

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Errors / Advisories

SCM Area (ft ²) =	98,995	
SCM Treated Area (ft ²) =	2,177,128	
Catchment Routing:	No errors	
Treating Runoff from Existing BUA or Offsite:	no	
Disturbed $\Delta rea (ft^2) = 11$		If using tool for Stormwater Compliance, check Project Info for missing Disturbed Area.
Total Phosphorus Scaled to Project	•	32.57

Total Area Post-Project after Treatment	Project Area Post-Project after Treatment	Total Area Post-Project SCM-Treated Area Only	Project Area Post-Project SCM-Treated Area Only	Total Area Post-Project Untreated Areas	Project Area Post-Project Untreated Areas
81.4203	81.4203	49.9800	49.9800	31.4403	31.4403
35%	35%	48%	48%	14%	14%
1,225,099	1,225,099	1,037,441	1,037,441	187,658	187,658
4,430,243	4,430,243	3,607,402	3,607,402	822,840	822,840
506%	506%				
3,699,352	3,699,352				
1.09	1.09	0.95	0.95	1.73	1.73
301.58	301.58	212.93	212.93	88.65	88.65
3.70	3.70	4.26	4.26	2.82	2.82
443%	443%				
246.01	246.01				
0.20	0.20	0.14	0.14	0.44	0.44
55.39	55.39	32.54	32.54	22.86	22.86
0.68	0.68	0.65	0.65	0.73	0.73
589%	589%				
47.35	47.35				

Nutrient Management Strategy Watershed - Nutrient Offset Credit Reporting Form

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Please complete and submit the following information to the local government permitting your development project to characterize it and assess the need to purchase nutrient offset credits. Contact and rule implementation information can be found online at:

http://deq.nc.gov/about/divisions/water-resources/planning/nonpoint-source-management/nutrient-offset-information

			PROJE	CT INFORM	ATION								
!	olicant Name:												
	Project Name:												
Project Address: 82 SCHOOL STREET ROLESVILLE NC 27571													
Date: ((mm/dd/yyyy)	BUILDSVII	Development Land Use Type										
	County:	IE	•		Activity Type:		ew Developme						
D	•	ct Area (sqft):	3,546,667		Project Latitude:		0.000000						
Post-P	Project Built-U	pon Area %:	34.54%		Projec	ct Longitude:	0.000	0.000000					
WATERSHED INFORMATION													
Nutrient	t Managemen	t Watershed:	Neuse N		N Tar	rget Export R	ate (lb/ac/yr):	3.60					
	Su	ubwatershed:	Neuse-Upper		P Tar	rget Export R	ate (lb/ac/yr):	0.40					
	•	elivery Zone:	Neuse - Upper 03020201			•	livery Factor:						
P	hosphorus D	elivery Zone:	Neuse - Upper 03020201		Ph	osphorus De	livery Factor:	100%					
PERMANENT NUTRIENT OFFSET REQUEST Post-Project Nitrogen Calculations - Projects with No Offsite or Built-Upon Area													
(A)	(B)	(C)	(D)		(F)	(G)	(Where						
(^)	(D)	(0)	(D)		(1)		Applicable)	THATTN					
TN Untreated Load (lb/yr)	TN Export Target Load (lb/yr)	TN Treated Load (lb/yr)	TN Remaining Reduction Need (lb/yr)		TN Delivery Factor (%)	TN Permanent Offsets Required (lb/yr)	Additional Local Gov't Offsets (lb/yr)	Total TN Permanent Offsets to Buy (lb/yr)					
426.7	293.1	301.6	8.5		1.0	8.5		8.5					
	Post-Pro	ject Phospho	rus Calculatio	ons - Projects	with No Offs	ite or Built-Ur	oon Area						
(A)	(B)	(C)	(D)		(F)	(G)	(Where Applicable)						
TP Untreated Load (lb/yr)	TP Export Target Load (lb/yr)	TP Treated Load (lb/yr)	TP Remaining Reduction Need (lb/yr)		TP Delivery Factor (%)	TP Permanent Offsets Required (lb/yr)	Additional Local Gov't Offsets (lb/yr)	Total TP Permanent Offsets to Buy (lb/yr)					
								#VALUE!					
LOCAL GOVERNMENT AUTHORIZATION Local Government Name:													
Staff Name:						Phone:							
Staff Email:						Date:							
Local Government Authorizing Signature:													