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| Harris Creek Farm
Traffic Impact Analysis
Rolesville, North Carolina

# TRAFFIC IMPACT ANALYSIS 

## FOR

## HARRIS CREEK FARM

## LOCATED

## IN

## ROLESVILLE, NORTH CAROLINA



MAY 2023

# TRAFFIC IMPACT ANALYSIS HARRIS CREEK FARM ROLESVILLE, NORTH CAROLINA 

## EXECUTIVE SUMMARY

## 1. Development Overview

A Traffic Impact Analysis (TIA) was conducted for the proposed Harris Creek Farm development in accordance with the Town of Rolesville (Town) Land Development Ordinance (LDO) and North Carolina Department of Transportation (NCDOT) capacity analysis guidelines. The proposed development, anticipated to be completed in 2027, is to be located on the west side of Jonesville Road near Universal Drive in Rolesville, NC. The proposed development is expected to consist of 68 single-family homes and 81 townhomes. Site access is proposed via two (2) fullmovement driveway connections: one on Universal Drive and one on Jonesville Road approximately 700 feet south of Universal Drive.

The study analyzes traffic conditions during the weekday AM and PM peak hours for the following scenarios:

- 2022 Existing Traffic Conditions
- 2027 No-Build Traffic Conditions
- 2027 Build Traffic Conditions
- 2027 Build-Improved Traffic Conditions


## 2. Existing Traffic Conditions

The study area for the TIA was determined through coordination with the Town and NCDOT and consists of the following existing intersections:

- US 401 Bypass and Jonesville Road
- US 401 Bypass and Eastern U-Turn Location
- Mitchell Mill Road and Jonesville Road / Peebles Road
- Jonesville Road and Universal Drive

Existing peak hour traffic volumes were determined based on traffic counts conducted at the study intersections listed above except for Jonesville Road and Universal Drive, in November of 2021 during typical weekday AM (7:00 AM - 9:00 AM) and PM (4:00 PM - 6:00 PM) peak periods, while schools were in session for in-person learning.

Existing peak hour turning movement volumes at the intersection of Jonesville Road and Universal Drive were estimated by generating and assigning trips for the nine (9) homes that are accessed via Universal Drive. It was estimated that there will be 8 AM trips: 2 enter 6 exit and 10 PM trips: 7 enter 3 exit. The trips were distributed to the north and south along Jonesville Road the same as site trips. Through traffic volumes were balanced from the Mitchell Mill Road/Jonesville Road intersection.

Previously collected counts from the year 2021 were projected to the 2022 existing analysis year using a compounded annual growth rate of $2 \%$. Weekday AM and PM traffic volumes were balanced between study intersections, where appropriate.

## 3. Site Trip Generation

The proposed development is assumed to consist of 68 single-family homes and 81 townhomes,. Average weekday daily, AM peak hour, and PM peak hour trips for the proposed development were estimated using methodology contained within the ITE Trip Generation Manual, 11 ${ }^{\text {th }}$ Edition. Table E-1 provides a summary of the trip generation potential for the site.

Table E-1: Site Trip Generation

| Land Use (ITE Code) | Intensity | Daily Traffic (vpd) | Weekday <br> AM Peak Hour Trips (vph) |  |  | Weekday PM Peak Hour Trips (vph) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Enter | Exit | Total | Enter | Exit | Total |
| Single-Family Home (210) | 68 DU | 708 | 13 | 39 | 52 | 44 | 25 | 69 |
| Single Family Attached (215) | 81 DU | 568 | 9 | 27 | 36 | 26 | 19 | 45 |
| Total Primary Trips |  | 1,276 | 22 | 66 | 88 | 70 | 44 | 114 |

## 4. Future Traffic Conditions

Through coordination with the Town and NCDOT, it was determined that an annual growth rate of $0 \%$ would be used to generate 2027 projected weekday AM and PM peak hour traffic volumes. A growth rate of $0 \%$ was used due to the number of developments included in the background traffic and the proximity of some of these developments to the proposed development. The following adjacent developments were identified to be considered under future conditions:

- Cobblestone Crossing Mixed-Use (Cobblestone)
- Young Street PUD (The Point)
- Wheeler Tract (Rolesville Crossing)
- Louisbury Road Assemblage
- Kalas / Watkins Family Property (Kalas Falls)
- 5109 Mitchell Mill
- Hills at Harris Creek


## 5. Capacity Analysis Summary

The analysis considered weekday AM and PM peak hour traffic for 2022 existing, 2027 no-build, 2027 build, and 2027 build-improved conditions. Refer to Section 7 of the TIA for the capacity analysis summary performed at each study intersection.

## 6. Recommendations

Based on the findings of this study, specific geometric and traffic control improvements have been identified at study intersections. The improvements are summarized below and are illustrated in Figure E-1.

## Recommended Improvements by Developer

US 401 Bypass and Jonesville Road

- Conduct a full signal warrant analysis prior to full build-out of the proposed development and install a traffic signal if warranted and approved by the Town and NCDOT.


## US 401 Bypass and Eastern U-Turn Location

- Conduct a full signal warrant analysis prior to full build-out of the proposed development and install a traffic signal if warranted and approved by the Town and NCDOT.


## Mitchell Mill Road and Jonesville Road / Peebles Road

- Construct a southbound (Jonesville Road) left-turn lane with at least 100 feet of storage and appropriate decel and taper.
- It should be noted that this improvement was also identified by the 5109 Mitchell Mill Road TIA and Hills at Harris Creek TIA
- Construct a westbound (Mitchell Mill Road) right-turn lane with at least 100 feet of storage and appropriate decel and taper.
- It should be noted that this improvement was also identified by the Hills at Harris Creek TIA
- Construct an eastbound (Mitchell Mill Road) left-turn lane with at least 100 feet of storage and appropriate decel and taper.
- It should be noted that this improvement was also identified by the 5109 Mitchell Mill Road TIA
- Conduct a full signal warrant analysis prior to full build-out of the proposed development and install a traffic signal if warranted and approved by the Town and NCDOT.


## Jonesville Road and Site Drive

- Construct the eastbound approach (Site Drive) with one ingress lane and one egress lane.
- Provide stop-control for the eastbound approach (Site Drive).



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# TRAFFIC IMPACT ANALYSIS <br> HARRIS CREEK FARM <br> ROLESVILLE, NORTH CAROLINA 

## 1. INTRODUCTION

The contents of this report present the findings of the Traffic Impact Analysis (TIA) conducted for the proposed Harris Creek Farm development in Rolesville, North Carolina. The proposed development, anticipated to be completed in 2027, is to be located on the west side of Jonesville Road near Universal Drive in Rolesville, NC. The proposed development is expected to consist of 68 single-family homes and 81 townhomes. The purpose of this study is to determine the potential impacts to the surrounding transportation system created by traffic generated by the proposed development, as well as recommend improvements to mitigate the impacts.

The study analyzes traffic conditions during the weekday AM and PM peak hours for the following scenarios:

- 2022 Existing Traffic Conditions
- 2027 No-Build Traffic Conditions
- 2027 Build Traffic Conditions


### 1.1. Site Location and Study Area

The proposed development is to be located on the west side of Jonesville Road near Universal Drive in Rolesville, NC. Refer to Figure 1 for the site location map. The study area for the TIA was determined through coordination with the North Carolina Department of Transportation (NCDOT) and the Town of Rolesville (Town) and consists of the following existing intersections:

- US 401 Bypass and Jonesville Road
- US 401 Bypass and Eastern U-Turn Location
- Jonesville Road and Universal Drive
- Mitchell Mill Road and Jonesville Road / Peebles Road

Refer to Appendix A for the approved scoping documentation.

### 1.2. Proposed Land Use and Site Access

The site is to be located on the west side of Jonesville Road near Universal Drive. The proposed development is anticipated to be completed in 2027, and is assumed to consist of the following uses:

- 68 single-family homes
- 81 townhomes

Site access to the proposed development is expected to be provided via two (2) full-movement driveway connections: one on Universal Drive and one on Jonesville Road approximately 700 feet south of Universal Drive. Refer to Figure 2 for a copy of the preliminary site plan.

### 1.3. Adjacent Land Uses

The proposed development is located in an area consisting primarily of undeveloped land and residential development.

### 1.4. Existing Roadways

Existing lane configurations (number of traffic lanes on each intersection approach), storage capacities, and other intersection and roadway information within the study area are shown in Figure 3. Table 1 provides a summary of this information, as well.

Table 1: Existing Roadway Inventory

| Road Name | Route <br> Number | Typical <br> Cross- <br> Section | Speed Limit | Maintained <br> By | 2019 AADT <br> (vpd) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| US 401 Bypass |  | 4-lane <br> divided | 55 mph | NCDOT | 17,500 |
| Jonesville Road | SR 2226 | 2-lane <br> undivided | $35 \mathrm{mph} /$ <br> 45 mph | NCDOT | $2,210^{*}$ |
| Mitchell Mill <br> Road | SR 2224 | 2-lane <br> undivided | 45 mph | NCDOT | 4,000 |
| Peebles Road | SR 2929 | 2-lane <br> undivided | 45 mph | NCDOT | $1,700^{*}$ |

*ADT based on 2022 existing traffic volumes and assuming the weekday PM peak hour volume is $10 \%$ of the average daily traffic.


## LEGEND

-     - I Proposed Site Location

O Existing Study Intersection

- -ı Study Area

|  | Harris Creek Farm <br> Rolesville, NC | Site Location Map |  |
| :---: | :---: | :---: | :---: |
|  |  | Scale: Not to Scale | Figure 1 |




|  | Harris Creek Farm <br> Rolesville, NC | 2022 Existing <br> Lane Configurations |  |
| :---: | :---: | :---: | :---: |
|  | Scale: Not to Scale | Figure 3 |  |

## 2. 2022 EXISTING PEAK HOUR CONDITIONS

### 2.1. 2022 Existing Peak Hour Traffic Volumes

Existing peak hour traffic volumes were determined based on previously collected traffic counts conducted at the study intersections listed below, in November of 2021 during typical weekday AM (7:00 AM - 9:00 AM) and PM (4:00 PM - 6:00 PM) peak periods, while schools were in session for in-person learning:

- US 401 Bypass and Jonesville Road
- US 401 Bypass and Eastern U-Turn Location
- Mitchell Mill Road and Jonesville Road / Peebles Road

Previously collected counts from the year 2021 were projected to the 2022 existing analysis year using a compounded annual growth rate of $2 \%$.

Existing peak hour turning movement volumes at the intersection of Jonesville Road and Universal Drive were estimated by generating and assigning trips for the nine (9) homes that are accessed via Universal Drive. It was estimated that there will be 8 AM trips: 2 enter 6 exit and 10 PM trips: 7 enter 3 exit. The trips were distributed to the north and south along Jonesville Road the same as site trips. Through traffic volumes were balanced from the Mitchell Mill Road/Jonesville Road intersection.

Weekday AM and PM traffic volumes were balanced between study intersections, where appropriate. Refer to Figure 4 for 2022 existing weekday AM and PM peak hour traffic volumes. A copy of the count data is located in Appendix B of this report.

### 2.2. Analysis of $\mathbf{2 0 2 2}$ Existing Peak Hour Traffic Conditions

The 2022 existing weekday AM and PM peak hour traffic volumes were analyzed to determine the current levels of service at the study intersections under existing roadway conditions. The results of the analysis are presented in Section 7 of this report.


## 3. 2027 NO-BUILD PEAK HOUR CONDITIONS

In order to account for growth of traffic and subsequent traffic conditions at a future year, nobuild traffic projections are needed. No-build traffic is the component of traffic due to the growth of the community and surrounding area that is anticipated to occur regardless of whether or not the proposed development is constructed. No-build traffic is comprised of existing traffic growth within the study area and additional traffic created as a result of adjacent approved developments.

### 3.1. Ambient Traffic Growth

Through coordination with NCDOT and the Town, it was determined that an annual growth rate of $0 \%$ would be used to generate 2027 projected weekday AM and PM peak hour traffic volumes. A growth rate of $0 \%$ was used due to the number of developments included in the background traffic and the proximity of some of these developments to the proposed development. Refer to Figure 5 for 2027 projected peak hour traffic.

### 3.2. Adjacent Development Traffic

Through coordination with NCDOT and the Town, the following adjacent developments were identified to be included in this study:

- Cobblestone Crossing Mixed-Use (Cobblestone)
- Young Street PUD (The Point)
- Wheeler Tract (Rolesville Crossing)
- Louisbury Road Assemblage
- Kalas / Watkins Family Property (Kalas Falls)
- 5109 Mitchell Mill
- Hills at Harris Creek

Table 2, on the following page, provides a summary of the adjacent developments. Adjacent development trips are shown in Figure 6. Adjacent development information can be found in Appendix C.

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Table 2: Adjacent Development Information

| Development Name | Location | BuildOut Year | Land Use / Intensity | TIA <br> Performed |
| :---: | :---: | :---: | :---: | :---: |
| Cobblestone Crossing MixedUse | Northwest quadrant of the intersection of Main Street and Young Street | 2023 | 180 multi-family homes 18,200 sq. ft. municipal flex space 50,000 sq. ft. general retail | March 2021 by RKA |
| Young Street PUD | Along both sides of US 401 Bypass west of Young Street | 2025 | 96 single-family homes 525 single-family homes 320 multi-family homes 122,800 sq. ft. general retail | June 2019 <br> by Kimley <br> Horn |
| Wheeler Tract | Northeast quadrant of the intersection of Rolesville Road and Mitchell Mill Road | 2026 | 233 single-family homes 125 multi-family homes | June 2019 <br> by RKA |
| Louisbury Road Assemblage | West of Louisbury Road and south of Stells Road | 2025 | 152 single-family homes | May 2020 by RKA |
| Kalas / Watkins Family Property | Along the west side of Rolesville Road, north of Mitchell Mill Road | 2025 | 439 single-family homes 96 multi-family homes | August 2019 by Stantec |
| $\begin{aligned} & 5109 \text { Mitchell } \\ & \text { Mill } \end{aligned}$ | Along both sides of Jonesville Road north of Mitchell Mill Road | 2028 | 69 single-family homes 195 single-family homes 129 multi-family homes 50,000 sq. ft. shopping center | August 2022 by RKA |
| Hills at Harris Creek | North of Mitchell Mill Road, west of Manly Farm Road and east of Gro Peg Lane | 2027 | 211 single-family homes 109 multi-family homes 25,400 sq. ft. general retail | May 2022 by RKA |

### 3.3. Future Roadway Improvements

Based on coordination with NCDOT and the Town, it was determined there were two previously approved TIA's that recommended roadway improvements that were considered under future conditions with this study. Both developments are to construct improvements at the intersection of Jonesville Road and Mitchell Mill Road. An exclusive eastbound leftturn lane was identified in the 5109 Mitchell Mill Road TIA. An exclusive westbound rightturn lane was identified in the Hills at Harris Creek TIA. In both the 5109 Mitchell Mill Road TIA and the Hills at Harris Creek TIA an exclusive southbound left-turn lane improvement was identified. It should be noted that per the Rolesville Community Transportation Plan (dated May 2022), the ultimate cross-section of Jonesville Road is identified as a 2-lane roadway with a center two-way-left-turn-lane (TWLTL) and Mitchell Mill Road is identified as a 4-lane median-divided roadway.

### 3.4. 2027 No-Build Peak Hour Traffic Volumes

The 2027 no-build traffic volumes were determined by projecting the 2022 existing peak hour traffic to the year 2027 and adding the adjacent development trips. Refer to Figure 7 for an illustration of the 2027 no-build peak hour traffic volumes at the study intersections.

### 3.5. Analysis of $\mathbf{2 0 2 7}$ No-Build Peak Hour Traffic Conditions

The 2027 no-build AM and PM peak hour traffic volumes at the study intersections were analyzed with existing geometric roadway conditions and traffic control. The analysis results are presented in Section 7 of this report.




## 4. SITE TRIP GENERATION AND DISTRIBUTION

### 4.1. Trip Generation

The proposed development is assumed to consist of 68 single-family homes and 81 townhomes. Average weekday daily, AM peak hour, and PM peak hour trips for the proposed development were estimated using methodology contained within the ITE Trip Generation Manual, 11th Edition. Table 3 provides a summary of the trip generation potential for the site.

Table 3: Trip Generation Summary

| Land Use (ITE Code) | Intensity | Daily Traffic (vpd) | Weekday AM Peak Hour Trips (vph) |  |  | Weekday PM Peak Hour Trips (vph) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Enter | Exit | Total | Enter | Exit | Total |
| Single-Family Home (210) | 68 DU | 708 | 13 | 39 | 52 | 44 | 25 | 69 |
| Single Family Attached (215) | 81 DU | 568 | 9 | 27 | 36 | 26 | 19 | 45 |
| Total Primary Trips |  | 1,276 | 22 | 66 | 88 | 70 | 44 | 114 |

It is estimated that the proposed development will generate approximately 1,276 total site trips on the roadway network during a typical 24 -hour weekday period. Of the daily traffic volume, it is anticipated that 88 trips ( 22 entering and 66 exiting) will occur during the weekday AM peak hour and 114 trips ( 70 entering and 44 exiting) will occur during the weekday PM peak hour.

### 4.2. Site Trip Distribution and Assignment

Trip distribution percentages used in assigning site trips for this development were approved during the scoping process and were estimated based on a combination of existing traffic patterns, population centers adjacent to the study area, and engineering judgment.

It is estimated that the residential site trips will be regionally distributed as follows:

- $35 \%$ to/from the west via Mitchell Mill Road
- $30 \%$ to/from the west via US 401 Bypass
- $15 \%$ to/from the east via US 401 Bypass
- $10 \%$ to/from the south via Peebles Road
- $10 \%$ to/from the east via Mitchell Mill Road

The site trip distribution is shown in Figure 8 and the peak hour site trip assignment is shown in Figure 9.



## 5. 2027 BUILD TRAFFIC CONDITIONS

### 5.1. 2027 Build Peak Hour Traffic Volumes

To estimate traffic conditions with the site fully built-out, the total site trips were added to the 2027 no-build traffic volumes to determine the 2027 build traffic volumes. Refer to Figure 10 for an illustration of the 2027 build peak hour traffic volumes with the proposed site fully developed.

### 5.2. Analysis of 2027 Build Peak Hour Traffic Conditions

Study intersections were analyzed with the 2027 build traffic volumes using the same methodology previously discussed for existing and no-build traffic conditions. Intersections were analyzed with improvements necessary to accommodate future traffic volumes. The results of the capacity analysis for each intersection are presented in Section 7 of this report.


## 6. TRAFFIC ANALYSIS PROCEDURE

Study intersections were analyzed using the methodology outlined in the Highway Capacity Manual (HCM), $6^{\text {th }}$ Edition published by the Transportation Research Board. Capacity and level of service are the design criteria for this traffic study. A computer software package, Synchro (Version 11), was used to complete the analyses for most of the study area intersections. Please note that the unsignalized capacity analysis does not provide an overall level of service for an intersection; only delay for an approach with a conflicting movement.

The HCM defines capacity as "the maximum hourly rate at which persons or vehicles can reasonably be expected to traverse a point or uniform section of a lane or roadway during a given time period under prevailing roadway, traffic, and control conditions." Level of service (LOS) is a term used to represent different driving conditions, and is defined as a "qualitative measure describing operational conditions within a traffic stream, and their perception by motorists and/or passengers." Level of service varies from Level "A" representing free flow, to Level "F" where breakdown conditions are evident. Refer to Table 4 for HCM levels of service and related average control delay per vehicle for both signalized and unsignalized intersections. Control delay as defined by the HCM includes "initial deceleration delay, queue move-up time, stopped delay, and final acceleration delay." An average control delay of 50 seconds at a signalized intersection results in LOS "D" operation at the intersection.

## Table 4: Highway Capacity Manual - Levels-of-Service and Delay

| UNSIGNALIZED INTERSECTION |  | SIGNALIZED INTERSECTION |  |
| :---: | :---: | :---: | :---: |
| LEVEL | AVERAGE |  | AVERAGE |
| OF | CONTROL DELAY | LEVEL OF | CONTROL DELAY |
| SERVICE | PER VEHICLE | SERVICE | PER VEHICLE |
|  | (SECONDS) |  | (SECONDS) |
| A | $0-10$ | A | $0-10$ |
| B | $10-15$ | B | $10-20$ |
| C | $15-25$ | C | $20-35$ |
| D | $25-35$ | D | $35-55$ |
| E | $35-50$ | E | $55-80$ |
| F | $>50$ | F | $>80$ |

### 6.1. Adjustments to Analysis Guidelines

Capacity analysis at all study intersections was completed according to Town LDO and NCDOT Congestions Management Guidelines.

## 7. CAPACITY ANALYSIS

### 7.1. US 401 Bypass and Jonesville Road

The existing unsignalized intersection of US 401 Bypass Road and Jonesville Road was analyzed under 2022 existing, 2027 no-build, and 2027 build traffic conditions with the lane configurations and traffic control shown in Table 5. Refer to Table 5 for a summary of the analysis results. Refer to Appendix D for the Synchro capacity analysis reports.

Table 5: Analysis Summary of US 401 Bypass and Jonesville Road

| ANALYSIS SCENARIO | $\begin{aligned} & \hline \mathbf{A} \\ & \mathbf{P} \\ & \mathbf{P} \\ & \mathbf{R} \\ & \mathbf{O} \\ & \mathbf{A} \\ & \mathbf{C} \\ & \mathbf{H} \\ & \hline \end{aligned}$ | LANE CONFIGURATIONS | WEEKDAY AM PEAK HOUR LEVEL OF SERVICE |  | WEEKDAY PM PEAK HOUR LEVEL OF SERVICE |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Approach | Overall (seconds) | Approach | Overall (seconds) |
| 2022 Existing | $\begin{gathered} \text { EB } \\ \text { WB } \\ \text { NB } \end{gathered}$ | $\begin{gathered} 2 \mathrm{TH}, 1 \mathrm{RT} \\ 1 \mathrm{LT} \\ 1 \mathrm{RT} \end{gathered}$ | $\begin{aligned} & -- \\ & \mathrm{C}^{1} \\ & \mathrm{~B}^{2} \end{aligned}$ | N/A | $\mathrm{E}^{1}$ $\mathrm{C}^{2}$ | N/A |
|  | $\begin{aligned} & \hline \mathrm{EB}^{* *} \\ & \text { WB } \\ & \text { SB } \\ & \hline \end{aligned}$ | $\begin{gathered} 1 \mathrm{LT} \\ 2 \mathrm{TH}, 1 \mathrm{RT} \\ 1 \mathrm{RT} \\ \hline \end{gathered}$ | $\begin{aligned} & \mathrm{F}^{1} \\ & -- \\ & \mathrm{E}^{2} \\ & \hline \end{aligned}$ | N/A | $\begin{aligned} & \hline \mathrm{C}^{1} \\ & -- \\ & \mathrm{B}^{2} \\ & \hline \end{aligned}$ | N/A |
| 2027 No-Build | $\begin{gathered} \text { EB } \\ \text { WB* } \\ \text { NB } \end{gathered}$ | $\begin{gathered} \hline 2 \mathrm{TH}, 1 \mathrm{RT} \\ 1 \mathrm{LT} \\ 1 \mathrm{RT} \end{gathered}$ | $\begin{aligned} & -- \\ & \mathrm{D}^{1} \\ & \mathrm{D}^{2} \\ & \hline \end{aligned}$ | N/A | $\begin{aligned} & -- \\ & \mathrm{F}^{1} \\ & \mathrm{~F}^{2} \end{aligned}$ | N/A |
|  | $\begin{aligned} & \hline \mathrm{EB}^{* *} \\ & \text { WB } \\ & \text { SB } \end{aligned}$ | 1 LT 2 TH, 1 RT 1 RT | $\begin{aligned} & \hline F^{1} \\ & -- \\ & F^{2} \\ & \hline \end{aligned}$ | N/A | $\begin{gathered} \hline \mathrm{E}^{1} \\ - \\ \mathrm{B}^{2} \\ \hline \end{gathered}$ | N/A |
| 2027 Build | $\begin{gathered} \hline \text { EB } \\ \text { WB } \\ \text { NB } \end{gathered}$ | $\begin{gathered} \hline 2 \mathrm{TH}, 1 \mathrm{RT} \\ 1 \mathrm{LT} \\ 1 \mathrm{RT} \end{gathered}$ | $\begin{aligned} & -- \\ & \mathrm{D}^{1} \\ & \mathrm{D}^{2} \end{aligned}$ | N/A | $\begin{aligned} & -- \\ & \mathrm{F}^{1} \\ & \mathrm{~F}^{2} \end{aligned}$ | N/A |
|  | $\begin{aligned} & \text { EB** } \\ & \text { WB } \\ & \text { SB } \end{aligned}$ | 1 LT $2 \mathrm{TH}, 1$ RT 1 RT | $\begin{aligned} & \hline F^{1} \\ & -- \\ & F^{2} \end{aligned}$ | N/A | $\begin{gathered} \hline \mathrm{E}^{1} \\ -- \\ \mathrm{B}^{2} \end{gathered}$ | N/A |
| 2027 BuildImproved | $\begin{gathered} \text { EB } \\ \text { WB } \\ \text { NB } \end{gathered}$ | $\begin{gathered} 2 \mathrm{TH}, 1 \mathrm{RT} \\ 1 \mathrm{LT} \\ 1 \mathrm{RT} \end{gathered}$ | $\begin{aligned} & \text { B } \\ & \text { B } \\ & \text { B } \end{aligned}$ | $\begin{gathered} \text { B } \\ (16) \end{gathered}$ | $\begin{aligned} & \text { B } \\ & \text { D } \\ & \text { C } \end{aligned}$ | $\begin{gathered} \text { C } \\ (23) \end{gathered}$ |
|  | $\begin{aligned} & \hline \text { EB** } \\ & \text { WB } \\ & \text { SB } \end{aligned}$ | $\begin{gathered} \hline 1 \mathrm{LT} \\ 2 \mathrm{TH}, 1 \mathrm{RT} \\ 1 \mathrm{RT} \end{gathered}$ | $\begin{aligned} & \hline F^{1} \\ & -- \\ & F^{2} \end{aligned}$ | N/A | $\begin{gathered} \hline \mathrm{E}^{1} \\ -- \\ \mathrm{B}^{2} \end{gathered}$ | N/A |

*Synchro analyzed the WB left-turns as SB through movements due to the nature of the superstreet and synchro limitations.
**Synchro analyzed the EB left-turns as NB through movements due to the nature of the superstreet and synchro limitations.

1. Level of service for major-street left-turn movement.
2. Level of service for minor-street approach.

Capacity analysis of 2022 existing traffic conditions indicates that the major-street left-turn movements and minor-street approaches are expected to operate at LOS D or better with the exception of the eastbound left-turn movement during the weekday AM peak hour (LOS F), the westbound left-turn movement during the weekday PM peak hour (LOS E), and the southbound minor-street approach during the weekday AM peak hour (LOS E).

Under 2027 no-build and 2027 build traffic conditions, the major-street left-turn movements are expected to operate at LOS E/F during the weekday AM and PM peak hours with the exception of the westbound left-turn movement during the weekday AM peak hour (LOS D) under 2027 no-build and 2027 build traffic conditions. The minor-street approaches are expected to operate at LOS E/F during the weekday AM and PM peak hours with the exception of the northbound approach during the weekday AM peak hour (LOS D) and the southbound approach during the weekday PM peak hour (LOS B) under 2027 no-build and 2027 build traffic conditions. It should be noted that the proposed development is expected to account for approximately $2 \%$ of the overall traffic at this intersection during the weekday AM and PM peak hours. The proposed development is expected to account for $8 \%$ and $6 \%$ of the northbound right movements during the AM and PM peak hours, respectively.

Due to the poor levels-of-service expected at this intersection, a traffic signal was considered under 2027 build traffic conditions to achieve acceptable levels of service. Weekday AM and PM peak hour traffic volumes were utilized in evaluating the potential need for signalization based on the guidelines contained within the Manual on Uniform Traffic Control Devices (MUTCD) and within the Guidelines for Signalization of Intersections with Two or Three Approaches Final Report, published by ITRE. Based on a review of the peak hour signal warrant at this intersection, the intersection is expected to meet the peak hour warrant for both the weekday AM and PM peak hours under 2027 no-build and 2027 build traffic conditions. It is not expected that this intersection would satisfy the MUTCD 8-hour (warrant 1) or 4-hour (warrant 2) warrants, which NCDOT favors for installation of a traffic signal. These longer period warrants are not typically met for residential areas due to the distinct peak traffic periods for these types of development. Based on a review of ITRE 95th percentile queue length calculations, the northbound right-turn movement demand is expected to be over $85 \%$
capacity during the weekday AM peak hour and exceed capacity during the weekday PM peak hour under 2027 no-build and 2027 build traffic conditions. Refer to Appendix J for a copy of the MUTCD warrants and the ITRE $95^{\text {th }}$ percentile queue length calculations.

Based on the Town's LDO, improvements must be identified to maintain no-build levels-ofservice under build traffic conditions or to limit the degradation to less than a five percent increase in total delay on any approach for those operating at failing levels-of-service under no-build traffic conditions. Therefore, additional turn-lanes were considered for the northbound right-turn and westbound left-turn movements at this intersection to achieve acceptable operation per the Town's LDO. However, additional turn-lanes are not a realistic or practical improvement at an unsignalized intersection operating with superstreet configurations.

Based on the Town's LDO, it is recommended that this intersection be monitored for signalization and a full signal warrant analysis be conducted prior to the full build-out of the proposed development and install a traffic signal if warranted and approved by the Town and NCDOT. With signalization, it is expected that this intersection will operate at acceptable levels-of-service during the weekday AM and PM peak hours.

### 7.2. US 401 Bypass and Eastern U-Turn Location

The existing unsignalized intersection of US 401 Bypass and Eastern U-Turn Location was analyzed under 2022 existing, 2027 no-build, and 2027 build traffic conditions with the lane configurations and traffic control shown in Table 6. Refer to Table 6 for a summary of the analysis results. Refer to Appendix E for the Synchro capacity analysis reports.

Table 6: Analysis Summary of US 401 Bypass and Eastern U-Turn Location

| ANALYSIS SCENARIO | $\begin{aligned} & \hline \mathbf{A} \\ & \mathbf{P} \\ & \mathbf{P} \\ & \mathbf{R} \\ & \mathbf{O} \\ & \mathbf{A} \\ & \mathbf{C} \\ & \mathbf{H} \end{aligned}$ | LANE <br> CONFIGURATIONS | WEEKDAY AM PEAK HOUR LEVEL OF SERVICE |  | WEEKDAY PM PEAK HOUR LEVEL OF SERVICE |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Approach | Overall (seconds) | Approach | Overall (seconds) |
| 2022 Existing | $\begin{aligned} & \text { EB* } \\ & \text { WB } \end{aligned}$ | $\begin{aligned} & \hline 1 \mathrm{UT} \\ & 2 \mathrm{TH} \end{aligned}$ | $\overline{C^{1}}$ | N/A | B1 | N/A |
| 2027 No-Build | $\begin{aligned} & \text { EB* } \\ & \text { WB } \end{aligned}$ | $\begin{aligned} & 1 \mathrm{UT} \\ & 2 \mathrm{TH} \end{aligned}$ | F -- | N/A | $\mathrm{C}^{1}$ | N/A |
| 2027 Build | $\begin{aligned} & \text { EB }^{*} \\ & \text { WB } \end{aligned}$ | $\begin{aligned} & 1 \mathrm{UT} \\ & 2 \mathrm{TH} \end{aligned}$ | F ${ }^{1}$ | N/A | $\mathrm{C}^{1}$ | N/A |
| 2027 Build Improved | $\begin{aligned} & \text { EB }{ }^{*} \\ & \text { WB } \end{aligned}$ | $\begin{aligned} & \hline 1 \mathrm{UT} \\ & 2 \mathrm{TH} \end{aligned}$ | $\begin{aligned} & \hline \mathrm{D} \\ & \mathrm{~B} \end{aligned}$ | $\begin{gathered} \hline \text { C } \\ (21) \end{gathered}$ | $\begin{aligned} & \hline \text { B } \\ & \text { A } \end{aligned}$ | $\begin{gathered} \hline \text { B } \\ (11) \end{gathered}$ |

*Synchro analyzed the EB u-turn as a NB left-turn movement due to the nature of the superstreet and synchro limitations.

1. Level of service for major-street u-turn movement.

Capacity analysis of 2022 existing and 2027 no-build traffic conditions indicates that the major-street u-turn movement is expected to operate at LOS C or better during the weekday AM and PM peak hours, with the exception of the weekday AM peak hour under 2027 nobuild conditions (LOS F).

Under 2027 build traffic conditions, the major-street u-turn movement is expected to operate at LOS F during the weekday AM peak hour and at LOS C during the weekday PM peak hour. It should be noted that the proposed development is expected to account for approximately $1 \%$ of the overall traffic at this intersection during the weekday AM and PM peak hours. The proposed development is expected to account for approximately $8 \%$ and $7 \%$
of the overall eastbound u-turn movements at this intersection during the weekday AM and PM peak hours, respectively.

Due to the poor levels-of-service expected at this intersection, a traffic signal was considered under 2027 build traffic conditions to achieve acceptable levels of service. Weekday AM and PM peak hour traffic volumes were utilized in evaluating the potential need for signalization based on the guidelines contained within the Manual on Uniform Traffic Control Devices (MUTCD) and within the Guidelines for Signalization of Intersections with Two or Three Approaches Final Report, published by ITRE. Based on a review of signal warrants at this intersection, the peak hour warrant (warrant 3) from the MUTCD is expected to be met for the weekday AM peak hour under 2027 no-build and build traffic conditions. It is not expected that this intersection would satisfy the MUTCD 8-hour (warrant 1) or 4-hour (warrant 2) warrants, which NCDOT favors for installation of a traffic signal. These longer period warrants are not typically met for residential areas due to the distinct peak traffic periods for these types of development. Based on a review of ITRE $95^{\text {th }}$ percentile queue length calculations, the eastbound u-turn movement demand is expected to exceed capacity during the weekday AM peak hour under 2027 no-build and 2027 build traffic conditions. Refer to Appendix J for a copy of the MUTCD warrants and the ITRE 95th percentile queue length calculations.

Based on the Town's LDO, improvements must be identified to maintain no-build levels-ofservice under build traffic conditions or to limit the degradation to less than a five percent increase in total delay on any approach for those operating at failing levels-of-service under no-build traffic conditions. Therefore, additional turn-lanes were considered for the eastbound u-turn movement at this intersection to achieve acceptable operation per the Town's LDO. However, additional turn-lanes are not a realistic or practical improvement at an unsignalized intersection operating with superstreet configurations.

Based on the Town's LDO, it is recommended that this intersection be monitored for signalization and a full signal warrant analysis be conducted prior to the full build-out of the proposed development and install a traffic signal if warranted and approved by the Town
and NCDOT. With signalization, it is expected that this intersection will operate at acceptable levels-of-service during the weekday AM and PM peak hours.

### 7.3. Mitchell Mill Road and Jonesville Road / Peebles Road

The existing unsignalized four-way stop intersection of Mitchell Mill Road and Jonesville Road / Peebles Road was analyzed under 2022 existing, 2027 no-build, and 2027 build traffic conditions with the lane configurations and traffic control shown in Table 7. Refer to Table 7 for a summary of the analysis results. Refer to Appendix F for the Synchro capacity analysis reports.

## Table 7: Analysis Summary of Mitchell Mill Road and Jonesville Road / <br> Peebles Road

| ANALYSIS SCENARIO | $\mathbf{A}$$\mathbf{P}$$\mathbf{P}$$\mathbf{R}$$\mathbf{O}$$\mathbf{A}$$\mathbf{C}$$\mathbf{H}$ | LANE CONFIGURATIONS | WEEKDAY AM PEAK HOUR LEVEL OF SERVICE |  | WEEKDAY PM PEAK HOUR LEVEL OF SERVICE |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Approach | Overall (seconds) | Approach | Overall (seconds) |
| 2022 Existing | $\begin{array}{\|c\|} \hline \text { EB } \\ \text { WB } \\ \text { NB } \\ \text { SB } \\ \hline \end{array}$ | $\begin{aligned} & \hline 1 \text { LT-TH-RT } \\ & \text { 1 LT-TH-RT } \\ & \text { 1 LT-TH-RT } \\ & \text { 1 LT-TH-RT } \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline \mathrm{B}^{1} \\ & \mathrm{~B}^{1} \\ & \mathrm{~B}^{1} \\ & \mathrm{~B}^{1} \\ & \hline \end{aligned}$ | $\begin{gathered} \text { B } \\ (13) \end{gathered}$ | $\begin{aligned} & \hline \mathrm{B}^{1} \\ & \mathrm{~A}^{1} \\ & \mathrm{~A}^{1} \\ & \mathrm{~A}^{1} \\ & \hline \end{aligned}$ | $\begin{gathered} \text { B } \\ (11) \end{gathered}$ |
| 2027 No-Build | $\begin{aligned} & \text { EB } \\ & \text { WB } \\ & \text { NB } \\ & \text { SB } \end{aligned}$ | 1 LT, 1 TH-RT <br> 1 LT-TH, 1 RT <br> 1 LT-TH-RT <br> 1 LT, 1 TH-RT | $\begin{aligned} & \mathrm{C}^{1} \\ & \mathrm{~F}^{1} \\ & \mathrm{C}^{1} \\ & \mathrm{C}^{1} \end{aligned}$ | $\begin{gathered} \text { F } \\ (95) \end{gathered}$ | $\begin{aligned} & \mathrm{F}^{1} \\ & \mathrm{E}^{1} \\ & \mathrm{C}^{1} \\ & \mathrm{C}^{1} \end{aligned}$ | $\begin{gathered} F \\ (57) \end{gathered}$ |
| 2027 Build | $\begin{aligned} & \text { EB } \\ & \text { WB } \\ & \text { NB } \\ & \text { SB } \end{aligned}$ | 1 LT, 1 TH-RT <br> 1 LT-TH, 1 RT <br> 1 LT-TH-RT <br> 1 LT, 1 TH-RT | $\begin{aligned} & \mathrm{C}^{1} \\ & \mathrm{~F}^{1} \\ & \mathrm{C}^{1} \\ & \mathrm{C}^{1} \end{aligned}$ | $\begin{gathered} \text { F } \\ (104) \end{gathered}$ | $\begin{aligned} & \mathrm{F}^{1} \\ & \mathrm{~F}^{1} \\ & \mathrm{C}^{1} \\ & \mathrm{C}^{1} \end{aligned}$ | $\begin{gathered} F \\ (61) \end{gathered}$ |
| 2027 Build Improved | $\begin{aligned} & \text { EB } \\ & \text { WB } \\ & \text { NB } \\ & \text { SB } \end{aligned}$ | 1 LT, 1 TH-RT <br> 1 LT-TH, 1 RT <br> 1 LT-TH-RT <br> $1 \mathrm{LT}, 1 \mathrm{TH}-\mathrm{RT}$ | $\begin{aligned} & \text { A } \\ & \text { B } \\ & \text { B } \\ & \text { C } \end{aligned}$ | $\begin{gathered} \text { B } \\ (14) \end{gathered}$ | $\begin{aligned} & \text { B } \\ & \text { B } \\ & \text { B } \\ & \text { B } \end{aligned}$ | $\begin{gathered} \text { B } \\ (13) \end{gathered}$ |

1. Level of service for all-way stop controlled approach.

Capacity analysis of 2022 existing indicates that the intersection is expected to operate at an overall LOS B or better during the weekday AM and PM peak hours. Under 2027 no-build and 2027 build traffic conditions, this intersection is expected to operate at an overall LOS F during the weekday AM and PM peak hours. It should be noted that the proposed development is expected to account for approximately $3 \%$ and $4 \%$ of the overall traffic at this
intersection during the weekday AM and PM peak hours, respectively. The proposed development is expected to account for approximately $11 \%$ and $17 \%$ of the eastbound left movement and $17 \%$ and $7 \%$ of the westbound right movements during the weekday AM and PM peak hours, respectively.

Several turn lanes expected to be constructed by adjacent developments were included in the 2027 no-build and 2027 build scenarios. An exclusive eastbound left-turn lane was identified in the 5109 Mitchell Mill Road TIA. An exclusive westbound right-turn lane was identified in the Hills at Harris Creek TIA. In both the 5109 Mitchell Mill Road TIA and the Hills at Harris Creek TIA an exclusive southbound left-turn lane improvement was identified.

Due to the poor levels-of-service expected at this intersection, a traffic signal was considered under 2027 build traffic conditions to achieve acceptable levels-of-service. The peak hour warrant (warrant 3) from the Manual on Uniform Traffic Control Devices (MUTCD) was considered. Based on a review of the peak hour signal warrant at this intersection, the intersection is expected to meet the peak hour warrant for both the weekday AM and PM peak hours under 2027 no-build and 2027 build traffic conditions. It is not expected that this intersection would satisfy the MUTCD 8-hour (warrant 1) or 4-hour (warrant 2) warrants, which NCDOT favors for installation of a traffic signal. These longer period warrants are not typically met for residential areas due to the distinct peak traffic periods for these types of development. Refer to Appendix J for a copy of the MUTCD warrants.

Based on the Town's LDO, it is recommended that this intersection be monitored for signalization and a full signal warrant analysis be conducted prior to the full build-out of the proposed development and install a traffic signal if warranted and approved by the Town and NCDOT. With signalization, it is expected that this intersection will operate at acceptable levels-of-service during the weekday AM and PM peak hours.

### 7.4. Jonesville Road and Universal Drive

The existing unsignalized intersection of Jonesville Road and Universal Drive was analyzed under 2027 build traffic conditions with the lane configurations and traffic control shown in Table 8. Refer to Table 8 for a summary of the analysis results. Refer to Appendix G for the synchro capacity analysis reports.

Table 8: Analysis Summary of Jonesville Road and Universal Drive

| ANALYSIS SCENARIO | $\begin{aligned} & \hline \mathbf{A} \\ & \mathbf{P} \\ & \mathbf{P} \\ & \mathbf{R} \\ & \mathbf{O} \\ & \mathbf{A} \\ & \mathbf{C} \\ & \mathbf{H} \\ & \hline \end{aligned}$ | LANE CONFIGURATIONS | WEEKDAY AM PEAK HOUR LEVEL OF SERVICE |  | WEEKDAY PM PEAK HOUR LEVEL OF SERVICE |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Approach | Overall (seconds) | Approach | Overall (seconds) |
| 2022 Existing | $\begin{aligned} & \text { EB } \\ & \text { NB } \\ & \text { SB } \end{aligned}$ | $\begin{aligned} & 1 \text { LT-RT } \\ & 1 \text { LT-TH } \\ & 1 \text { TH-RT } \end{aligned}$ | $\begin{aligned} & \mathrm{A}^{2} \\ & \mathrm{~A}^{1} \end{aligned}$ | N/A | $\begin{aligned} & \mathrm{A}^{2} \\ & \mathrm{~A}^{1} \end{aligned}$ | N/A |
| 2027 No-Build | $\begin{aligned} & \text { EB } \\ & \text { NB } \\ & \text { SB } \end{aligned}$ | $\begin{aligned} & 1 \text { LT-RT } \\ & 1 \text { LT-TH } \\ & 1 \text { TH-RT } \end{aligned}$ | $B^{2}$ A $^{1}$ -- | N/A | $\begin{aligned} & \mathrm{B}^{2} \\ & \mathrm{~A}^{1} \end{aligned}$ | N/A |
| 2027 Build | $\begin{aligned} & \text { EB } \\ & \text { NB } \\ & \text { SB } \end{aligned}$ | $\begin{aligned} & 1 \text { LT-RT } \\ & 1 \text { LT-TH } \\ & 1 \text { TH-RT } \end{aligned}$ | $B^{2}$ A -- | N/A | $\begin{aligned} & \mathrm{B}^{2} \\ & \mathrm{~A}^{1} \end{aligned}$ | N/A |

1. Level of service for major-street left-turn movement.
2. Level of service for minor-street approach.

Capacity analysis of 2027 build traffic conditions indicates that the major-street left-turn movement is expected to operate at LOS A during the weekday AM and PM peak hours. The minor-street approach is expected to operate at LOS B or better during the weekday AM and PM peak hours.

Right and left-turn lanes were considered based on the NCDOT Policy on Street and Driveway Access to North Carolina Highways. Based on the estimated low volume of right-turn and leftturn movements into the proposed development at this intersection, exclusive right-turn and left-turn lanes are not recommended. Refer to Appendix I for a copy of the turn lane warrants. No improvements are recommended by the developer.

### 7.5. Jonesville Road and Site Drive

The proposed intersection of Jonesville Road and Site Drive was analyzed under 2027 build traffic conditions with the lane configurations and traffic control shown in Table 9. Refer to Table 9 for a summary of the analysis results. Refer to Appendix H for the synchro capacity analysis reports.

Table 9: Analysis Summary of Jonesville Road and Site Drive

| ANALYSIS SCENARIO | $\begin{aligned} & \hline \mathbf{A} \\ & \mathbf{P} \\ & \mathbf{P} \\ & \mathbf{R} \\ & \mathbf{O} \\ & \mathbf{A} \\ & \mathbf{C} \\ & \mathbf{H} \end{aligned}$ | LANE CONFIGURATIONS | WEEKDAY AM PEAK HOUR LEVEL OF SERVICE |  | WEEKDAY PM PEAK HOUR LEVEL OF SERVICE |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Approach | Overall (seconds) | Approach | Overall (seconds) |
| 2027 Build | EB NB SB | $\begin{aligned} & \hline 1 \text { LT-RT } \\ & 1 \text { LT-TH } \\ & 1 \text { TH-RT } \end{aligned}$ | $\begin{aligned} & \hline \mathrm{B}^{2} \\ & \mathrm{~A}^{1} \end{aligned}$ | N/ A | $\begin{aligned} & \mathrm{B}^{2} \\ & \mathrm{~A}^{1} \\ & - \end{aligned}$ | N/A |

1. Level of service for major-street left-turn movement.
2. Level of service for minor-street approach.

Capacity analysis of 2027 build traffic conditions indicates that the major-street left-turn movement is expected to operate at LOS A during the weekday AM and PM peak hours. The minor-street approach is expected to operate at LOS B or better during the weekday AM and PM peak hours.

Right and left-turn lanes were considered based on the NCDOT Policy on Street and Driveway Access to North Carolina Highways. Based on the estimated low volume of right-turn and leftturn movements into the proposed development at this intersection, exclusive right-turn and left-turn lanes are not recommended. Refer to Appendix I for a copy of the turn lane warrants. No improvements are recommended by the developer.

## 8. CONCLUSIONS

This Traffic Impact Analysis was conducted to determine the potential traffic impacts of the proposed Harris Creek Farm development to be located on the west side of Jonesville Road near Universal Drive in Rolesville, North Carolina. The development is expected to consist of 68 single-family homes and 81 townhomes and to be built-out in 2027. Site access is proposed via two (2) full-movement driveway connections: one on Universal Drive and one on Jonesville Road approximately 700 feet south of Universal Drive.

The study analyzes traffic conditions during the weekday AM and PM peak hours for the following scenarios:

- 2022 Existing Traffic Conditions
- 2027 No-Build Traffic Conditions
- 2027 Build Traffic Conditions


## Trip Generation

It is estimated that the proposed development will generate approximately 1,276 site trips on the roadway network during a typical 24-hour weekday period. Of the daily traffic volume, it is anticipated that 88 trips ( 22 entering and 66 exiting) will occur during the weekday AM peak hour and 114 trips ( 70 entering and 44 exiting) will occur during the weekday PM peak hour.

## Adjustments to Analysis Guidelines

Capacity analysis at all study intersections was completed according to NCDOT Congestion Management Guidelines. Refer to section 6.1 of this report for a detailed description of any adjustments to these guidelines made throughout the analysis.

## Intersection Capacity Analysis Summary

All the study area intersections (including the proposed site driveways) are expected to operate at acceptable levels-of-service under existing and future year conditions with the exception of those identified in Section 7 of this report.

## 9. RECOMMENDATIONS

Based on the findings of this study, specific geometric improvements have been identified and are recommended to accommodate future traffic conditions. See a more detailed description of the recommended improvements below. Refer to Figure 11 for an illustration of the recommended lane configurations for the proposed development.

## Recommended Improvements by Developer

## US 401 Bypass and Jonesville Road

- Conduct a full signal warrant analysis prior to full build-out of the proposed development and install a traffic signal if warranted and approved by the Town and NCDOT.


## US 401 Bypass and Eastern U-Turn Location

- Conduct a full signal warrant analysis prior to full build-out of the proposed development and install a traffic signal if warranted and approved by the Town and NCDOT.


## Mitchell Mill Road and Jonesville Road / Peebles Road

- Construct a southbound (Jonesville Road) left-turn lane with at least 100 feet of storage and appropriate decel and taper.
- It should be noted that this improvement was also identified by the 5109 Mitchell Mill Road TIA and Hills at Harris Creek TIA
- Construct a westbound (Mitchell Mill Road) right-turn lane with at least 100 feet of storage and appropriate decel and taper.
- It should be noted that this improvement was also identified by the Hills at Harris Creek TIA
- Construct an eastbound (Mitchell Mill Road) left-turn lane with at least 100 feet of storage and appropriate decel and taper.
- It should be noted that this improvement was also identified by the 5109 Mitchell Mill Road TIA
- Conduct a full signal warrant analysis prior to full build-out of the proposed development and install a traffic signal if warranted and approved by the Town and NCDOT.

Jonesville Road and Site Drive

- Construct the eastbound approach (Site Drive) with one ingress lane and one egress lane.
- Provide stop-control for the eastbound approach (Site Drive).



## TECHNICAL APPENDIX

## APPENDIX A

## SCOPING DOCUMENTATION

March 17, 2023

Jeremy L. Warren, PE<br>NCDOT District 1 Engineer<br>4009 District Drive<br>Raleigh, NC 27507<br>jlwarren@ncdot.gov

[Sent via Email]
Reference: Harris Creek Farm
Rolesville, North Carolina
Subject: Memorandum of Understanding for TIA Report

Dear Mr. Warren:

The following is a Memorandum of Understanding (MOU) outlining the proposed scope of work and assumptions related to the Traffic Impact Analysis (TIA) for the proposed Harris Creek Farm development in Rolesville, North Carolina. The proposed development is to be located on the west side of Jonesville Road near Universal Drive in Rolesville, NC. The development is expected to consist of 68 single-family homes and 81 townhomes and is anticipated to be built out by 2027. Refer to the attached site location map. Site access to the proposed development is expected to be provided via two (2) full-movement driveway connections: one on Jonesville Road and one on Universal Drive. Refer to the attachments for a copy of the preliminary site plan.

## Study Area

The study area is proposed to consist of the following intersections:

- Mitchell Mill Road \& Jonesville Road / Peebles Road (unsignalized)
- US 401 Bypass and Jonesville Road (unsignalized)
- US 401 Bypass and Eastern U-Turn Location (unsignalized)
- Jonesville Road and Universal Drive (unsignalized)
- Jonesville Road and Site Driveway (unsignalized)


## Existing Traffic Volumes

Existing peak hour traffic volumes will be determined based on previously collected traffic counts at the study intersections below, in November 2021 during typical weekday AM (7:00 AM - 9:00 AM) and PM (4:00 PM - 6:00 PM) peak periods, while schools were in session for in-person learning:

- Mitchell Mill Road \& Jonesville Road / Peebles Road
- US 401 Bypass and Jonesville Road
- US 401 Bypass and Eastern U-Turn Location

These previously collected counts will be projected to the year 2022 using a compounded annual growth rate of $2 \%$.

Existing peak hour turning movement volumes at the intersection of Jonesville Road and Universal Drive will be estimated by generating and assigning trips for the nine (9) homes that are accessed via Universal Drive (AM trips: 2 enter 6 exit and PM trips: 7 enter 3 exit, distributed to the north and south al ong Jonesville Road the same as site trips). Through traffic volumes will be balanced from the Mitchell Mill Road/ Jonesville Road intersection.

Refer to the attachments for an illustration of 2022 existing peak hour traffic volumes.

## Background Traffic Volumes

Background traffic volumes will be determined by projecting 2022 existing traffic volumes to the year 2027 using a $0 \%$ annual growth rate. A growth rate of $0 \%$ will be used due to the number of devel opments included in the background traffic and the proximity of some of these developments to the proposed development. It is assumed that the following adjacent developments are to be included in this study:

- Cobblestone Crossing Mixed-Use (Cobblestone)
- Young Street PUD (The Point)
- Wheeler Tract (Rolesville Crossing)
- Louisbury Road Assemblage
- Kalas / Watkins Family Property (Kalas Falls)
- 5109 Mitchell Mill
- Hills at Harris Creek


## Future Roadway Improvements

There are no future roadway improvements within the study area to consider under future traffic conditions.

## Trip Generation

Average weekday daily, AM peak hour, and PM peak hour trips for the proposed development were estimated using methodology contained within the ITE Trip Generation Manual, 11 ${ }^{\text {th }}$ Edition. Refer to Table 1, on the following page, for a summary of the proposed site trip generation for full buildout of the proposed development.

Table 1: Trip Generation Summary

| Land Use (ITE Code) | Intensity | Daily Traffic (vpd) | Weekday AM Peak Hour Trips (vph) |  |  | Weekday PM Peak Hour Trips (vph) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Enter | Exit | Total | Enter | Exit | Total |
| SingleFamily Home <br> (210) | 68 DU | 710 | 13 | 39 | 52 | 44 | 25 | 69 |
| Multi-Family Home (Low-Rise) (220) | 81 DU | 568 | 9 | 27 | 36 | 26 | 19 | 45 |
| Total Trips |  | 1,268 | 22 | 66 | 88 | 70 | 44 | 114 |

It is estimated that the proposed development will generate approximately 1,268 site trips on the roadway network during a typical 24 -hour weekday period. Of the daily traffic volume, it is anticipated that 88 trips ( 22 entering and 66 exiting) will occur during the weekday AM peak hour and 114 trips ( 70 entering and 44 exiting) will occur during the weekday PM peak hour.

## Trip Distribution and Assignment

Site trips are distributed based on the locations of existing traffic patterns, population centers adjacent to the study area, and engineering judgment. A summary of the overall distributions is below.

## Residential

- $30 \%$ to/ from the west via US 401 Bypass
- $15 \%$ to/ from the east via US 401 Bypass
- $10 \%$ to/ from the south via Peebles Road
- $35 \%$ to/ from the west via Mitchell Mill Road
- $10 \%$ to/ from the east via Mitchell Mill Road

Refer to the attached site trip distribution figure.

## Analysis Scenarios

All capacity analyses will be performed utilizing Synchro (Version 11). All study intersections will be analyzed during the weekday AM and PM peak hours under the following proposed traffic scenarios:

- 2022 Existing Traffic Conditions
- 2027 N o-Build Traffic Conditions
- 2027 Build Traffic Conditions


## Report

The TIA report will be prepared based on theTown and NCDOT requirements.
If you find this memorandum of understanding acceptable, please let me know so that we may include it in the TIA report. If you have any questions or concerns, please do not hesitate to contact me.

Sincerely,
Ramey Kemp Associates,

J. Andrew Eagle, PE, PTOE

Senior Traffic Engineering Project Manager
Attachments: Site Location Map Site Plan
2022 Existing Traffic Volumes Figure
Proposed SiteTrip Distribution Figure
cc: Matthew J. Nolfo, NCDOT
Holt Willis, NCDOT
Clarence Bunting, NCDOT
Nicholas Lineberger, NCDOT
Daniel Collins, NCDOT
Meredith Gruber, Town of Rolesville
Michael Elabarger, Town of Rolesville


Harris Creek Farm
Rolesville, NC

Site Location Map

## REZONING AND ANNEXATION

## JONESVILLE ROAD

ROLESVILLE, NORTH CAROLINA


| Sheet List Table |  |  |  |
| :---: | :---: | :---: | :---: |
| Sheet Number | Sheet Title | Date | Revised Date |
| co.0 | COVER - REZONNG | 8/12022 | 9/30/2022 |
| co. 1 | ExITTMG Convitions | 81/2022 | 9/3012022 |
| ${ }^{6} 1.0$ | OYERALL SITE PLAN | 81/2022 | 9/3012022 |
| ${ }^{\text {c.1. }}$ | SIE PLAN - SHEET OF 6 | 8/012022 | 9/30/2022 |
| ${ }^{0} 12$ | SIIE PLAN - SHEET 2 OF 6 | 8/12022 | 9/30/2022 |
| ${ }^{1} 13$ | SITE PLAN - SHEET 3 OF 6 | 8/12022 | 9/30/2022 |
| ${ }^{\text {c. }} 1$ | SITE PLAN - SHEET 4 OF 6 | 8/12022 | 9/3012022 |
| ${ }^{1.5}$ | SITE PLAN - SHEET 5 OF 6 | 8/12022 | 9/3012022 |
| ${ }^{1.6}$ | SIIE PLAN - SHEET 6 OF 6 | 8/12022 | 9/30/2022 |
| ${ }^{6} 1.7$ | OVERALL ZONING PLAN | 8/12022 | 9/30/2022 |






PROJECT TEAM

```
M
```

```
M
```







Harris Creek Farm
Rolesville, NC

| 2022 Existing <br> Peak Hour Traffic |  |
| :---: | :--- |
| cale: Not to Scale |  | Figure 4



## APPENDIX B

## TRAFFIC COUNTS



## TRAFFIC DATA COLLECTION

File Name : Rolesville(US 401 and Jonesville)AM Peak Site Code :
Start Date : 11/9/2021
Page No : 1

|  | Jonesville Road Southbound |  |  |  | US 401 Westbound |  |  |  | Jonesville Road Northbound |  |  |  | US 401 <br> Eastbound |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Int. Total |
| 07:00 AM | 63 | 0 | 0 | 63 | 24 | 380 | 21 | 425 | 23 | 0 | 0 | 23 | 18 | 182 | 3 | 203 | 714 |
| 07:15 AM | 42 | 0 | 0 | 42 | 39 | 362 | 24 | 425 | 37 | 0 | 0 | 37 | 11 | 125 | 7 | 143 | 647 |
| 07:30 AM | 51 | 0 | 0 | 51 | 80 | 318 | 23 | 421 | 48 | 0 | 0 | 48 | 24 | 136 | 15 | 175 | 695 |
| 07:45 AM | 65 | 0 | 0 | 65 | 38 | 249 | 16 | 303 | 25 | 0 | 0 | 25 | 25 | 135 | 10 | 170 | 563 |
| Total | 221 | 0 | 0 | 221 | 181 | 1309 | 84 | 1574 | 133 | 0 | 0 | 133 | 78 | 578 | 35 | 691 | 2619 |
| 08:00 AM | 61 | 0 | 0 | 61 | 26 | 236 | 13 | 275 | 23 | 0 | 0 | 23 | 30 | 120 | 10 | 160 | 519 |
| 08:15 AM | 36 | 0 | 0 | 36 | 12 | 233 | 9 | 254 | 16 | 0 | 0 | 16 | 13 | 94 | 9 | 116 | 422 |
| 08:30 AM | 24 | 0 | 0 | 24 | 10 | 213 | 5 | 228 | 9 | 0 | 0 | 9 | 6 | 91 | 3 | 100 | 361 |
| 08:45 AM | 28 | 0 | 0 | 28 | 9 | 145 | 5 | 159 | 10 | 0 | 0 | 10 | 11 | 85 | 2 | 98 | 295 |
| Total | 149 | 0 | 0 | 149 | 57 | 827 | 32 | 916 | 58 | 0 | 0 | 58 | 60 | 390 | 24 | 474 | 1597 |
| Grand Total | 370 | 0 | 0 | 370 | 238 | 2136 | 116 | 2490 | 191 | 0 | 0 | 191 | 138 | 968 | 59 | 1165 | 4216 |
| Apprch \% | 100 | 0 | 0 |  | 9.6 | 85.8 | 4.7 |  | 100 | 0 | 0 |  | 11.8 | 83.1 | 5.1 |  |  |
| Total \% | 8.8 | 0 | 0 | 8.8 | 5.6 | 50.7 | 2.8 | 59.1 | 4.5 | 0 | 0 | 4.5 | 3.3 | 23 | 1.4 | 27.6 |  |
| Cars + | 366 | 0 | 0 | 366 | 233 | 2094 | 114 | 2441 | 188 | 0 | 0 | 188 | 135 | 916 | 57 | 1108 | 4103 |
| \% Cars + | 98.9 | 0 | 0 | 98.9 | 97.9 | 98 | 98.3 | 98 | 98.4 | 0 | 0 | 98.4 | 97.8 | 94.6 | 96.6 | 95.1 | 97.3 |
| Trucks | 4 | 0 | 0 | 4 | 5 | 42 | 2 | 49 | 3 | 0 | 0 | 3 | 3 | 52 | 2 | 57 | 113 |
| \% Trucks | 1.1 | 0 | 0 | 1.1 | 2.1 | 2 | 1.7 | 2 | 1.6 | 0 | 0 | 1.6 | 2.2 | 5.4 | 3.4 | 4.9 | 2.7 |



TRAFFIC DATA COLLECTION
File Name : Rolesville(US 401 and Jonesville)AM Peak Site Code :
Start Date : 11/9/2021
Page No : 2

|  | Jonesville Road Southbound |  |  |  | US 401 Westbound |  |  |  | Jonesville Road Northbound |  |  |  | US 401 Fastbound |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Int. Total |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour for Entire Intersection Begins at 07:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 07:00 AM | 63 | 0 | 0 | 63 | 24 | 380 | 21 | 425 | 23 | 0 | 0 | 23 | 18 | 182 | 3 | 203 | 714 |
| 07:15 AM | 42 | 0 | 0 | 42 | 39 | 362 | 24 | 425 | 37 | 0 | 0 | 37 | 11 | 125 | 7 | 143 | 647 |
| 07:30 AM | 51 | 0 | 0 | 51 | 80 | 318 | 23 | 421 | 48 | 0 | 0 | 48 | 24 | 136 | 15 | 175 | 695 |
| 07:45 AM | 65 | 0 | 0 | 65 | 38 | 249 | 16 | 303 | 25 | 0 | 0 | 25 | 25 | 135 | 10 | 170 | 563 |
| Total Volume | 221 | 0 | 0 | 221 | 181 | 1309 | 84 | 1574 | 133 | 0 | 0 | 133 | 78 | 578 | 35 | 691 | 2619 |
| \% App. Total | 100 | 0 | 0 |  | 11.5 | 83.2 | 5.3 |  | 100 | 0 | 0 |  | 11.3 | 83.6 | 5.1 |  |  |
| PHF | . 850 | . 000 | . 000 | 850 | . 566 | . 861 | . 875 | 926 | 693 | 000 | . 000 | 693 | 780 | . 794 | . 583 | 851 | 917 |




## TRAFFIC DATA COLLECTION

File Name : Rolesville(US 401 and Jonesville)PM Peak Site Code :
Start Date : 11/9/2021
Page No : 1

|  | Jonesville Road Southbound |  |  |  | US 401 Westbound |  |  |  | Jonesville Road Northbound |  |  |  | US 401 Eastbound |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Int. Total |
| 04:00 PM | 47 | 0 | 0 | 47 | 13 | 124 | 6 | 143 | 21 | 0 | 0 | 21 | 37 | 217 | 22 | 276 | 487 |
| 04:15 PM | 34 | 0 | 0 | 34 | 13 | 119 | 6 | 138 | 26 | 0 | 0 | 26 | 15 | 231 | 20 | 266 | 464 |
| 04:30 PM | 30 | 0 | 0 | 30 | 19 | 118 | 12 | 149 | 32 | 0 | 0 | 32 | 12 | 291 | 28 | 331 | 542 |
| 04:45 PM | 15 | 0 | 0 | 15 | 22 | 137 | 6 | 165 | 32 | 0 | 0 | 32 | 8 | 303 | 30 | 341 | 553 |
| Total | 126 | 0 | 0 | 126 | 67 | 498 | 30 | 595 | 111 | 0 | 0 | 111 | 72 | 1042 | 100 | 1214 | 2046 |
| 05:00 PM | 37 | 0 | 0 | 37 | 10 | 143 | 7 | 160 | 23 | 0 | 0 | 23 | 23 | 322 | 30 | 375 | 595 |
| 05:15 PM | 30 | 0 | 0 | 30 | 22 | 146 | 11 | 179 | 36 | 0 | 0 | 36 | 15 | 257 | 26 | 298 | 543 |
| 05:30 PM | 39 | 0 | 0 | 39 | 20 | 145 | 3 | 168 | 34 | 0 | 0 | 34 | 23 | 262 | 14 | 299 | 540 |
| 05:45 PM | 24 | 0 | 0 | 24 | 10 | 112 | 9 | 131 | 22 | 0 | 0 | 22 | 11 | 227 | 21 | 259 | 436 |
| Total | 130 | 0 | 0 | 130 | 62 | 546 | 30 | 638 | 115 | 0 | 0 | 115 | 72 | 1068 | 91 | 1231 | 2114 |
| Grand Total | 256 | 0 | 0 | 256 | 129 | 1044 | 60 | 1233 | 226 | 0 | 0 | 226 | 144 | 2110 | 191 | 2445 | 4160 |
| Apprch \% | 100 | 0 | 0 |  | 10.5 | 84.7 | 4.9 |  | 100 | 0 | 0 |  | 5.9 | 86.3 | 7.8 |  |  |
| Total \% | 6.2 | 0 | 0 | 6.2 | 3.1 | 25.1 | 1.4 | 29.6 | 5.4 | 0 | 0 | 5.4 | 3.5 | 50.7 | 4.6 | 58.8 |  |
| Cars + | 252 | 0 | 0 | 252 | 127 | 1020 | 60 | 1207 | 223 | 0 | 0 | 223 | 142 | 2051 | 191 | 2384 | 4066 |
| \% Cars + | 98.4 | 0 | 0 | 98.4 | 98.4 | 97.7 | 100 | 97.9 | 98.7 | 0 | 0 | 98.7 | 98.6 | 97.2 | 100 | 97.5 | 97.7 |
| Trucks | 4 | 0 | 0 | 4 | 2 | 24 | 0 | 26 | 3 | 0 | 0 | 3 | 2 | 59 | 0 | 61 | 94 |
| \% Trucks | 1.6 | 0 | 0 | 1.6 | 1.6 | 2.3 | 0 | 2.1 | 1.3 | 0 | 0 | 1.3 | 1.4 | 2.8 | 0 | 2.5 | 2.3 |



## TRAFFIC DATA COLLECTION

File Name: Rolesville(US 401 and Jonesville)PM Peak Site Code :
Start Date :11/9/2021
Page No : 2

|  | Jonesville Road Southbound |  |  |  | US 401 Westbound |  |  |  | Jonesville Road Northbound |  |  |  | US 401 <br> Eastbound |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Int. Total |
| Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1 Peak Hour for Entire Intersection Begins at 04:30 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 04:30 PM | 30 | 0 | 0 | 30 | 19 | 118 | 12 | 149 | 32 | 0 | 0 | 32 | 12 | 291 | 28 | 331 | 542 |
| 04:45 PM | 15 | 0 | 0 | 15 | 22 | 137 | 6 | 165 | 32 | 0 | 0 | 32 | 8 | 303 | 30 | 341 | 553 |
| 05:00 PM | 37 | 0 | 0 | 37 | 10 | 143 | 7 | 160 | 23 | 0 | 0 | 23 | 23 | 322 | 30 | 375 | 595 |
| 05:15 PM | 30 | 0 | 0 | 30 | 22 | 146 | 11 | 179 | 36 | 0 | 0 | 36 | 15 | 257 | 26 | 298 | 543 |
| Total Volume | 112 | 0 | 0 | 112 | 73 | 544 | 36 | 653 | 123 | 0 | 0 | 123 | 58 | 1173 | 114 | 1345 | 2233 |
| \% App. Total | 100 | 0 | 0 |  | 11.2 | 83.3 | 5.5 |  | 100 | 0 | 0 |  | 4.3 | 87.2 | 8.5 |  |  |
| PHF | . 757 | . 000 | . 000 | . 757 | . 830 | . 932 | . 750 | . 912 | . 854 | . 000 | . 000 | . 854 | . 630 | . 911 | . 950 | . 897 | . 938 |




## TRAFFIC DATA COLLECTION

File Name : Rolesville(US 401 and Eastern U Turn)AM Peak Site Code :
Start Date : 11/9/2021
Page No :1

| Groups Printed- Cars + - Trucks |  |  |  |  |  |  | Int Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | US 401 Westbound |  |  | US 401 Eastbound |  |  |  |
| Start Time | Thru | UTrn | App. Total | Thru | UTrn | App. Total |  |
| 07:00 AM | 421 | 0 | 421 | 198 | 12 | 210 | 631 |
| 07:15 AM | 410 | 0 | 410 | 136 | 24 | 160 | 570 |
| 07:30 AM | 392 | 0 | 392 | 149 | 36 | 185 | 577 |
| 07:45 AM | 279 | 0 | 279 | 137 | 17 | 154 | 433 |
| Total | 1502 | 0 | 1502 | 620 | 89 | 709 | 2211 |
| 08:00 AM | 253 | 0 | 253 | 130 | 20 | 150 | 403 |
| 08:15 AM | 243 | 0 | 243 | 98 | 13 | 111 | 354 |
| 08:30 AM | 223 | 0 | 223 | 94 | 7 | 101 | 324 |
| 08:45 AM | 147 | 0 | 147 | 85 | 9 | 94 | 241 |
| Total | 866 | 0 | 866 | 407 | 49 | 456 | 1322 |
| Grand Total | 2368 | 0 | 2368 | 1027 | 138 | 1165 | 3533 |
| Apprch \% | 100 | 0 |  | 88.2 | 11.8 |  |  |
| Total \% | 67 | 0 | 67 | 29.1 | 3.9 | 33 |  |
| Cars + | 2318 | 0 | 2318 | 973 | 136 | 1109 | 3427 |
| \% Cars + | 97.9 | 0 | 97.9 | 94.7 | 98.6 | 95.2 | 97 |
| Trucks | 50 | 0 | 50 | 54 | 2 | 56 | 106 |
| \% Trucks | 2.1 | 0 | 2.1 | 5.3 | 1.4 | 4.8 | 3 |



## TRAFFIC DATA COLLECTION

File Name : Rolesville(US 401 and Eastern U Turn)AM Peak
Site Code :
Start Date : 11/9/2021
Page No : 2

|  | US 401 Westbound |  |  | US 401 Eastbound |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Thru | UTrn | App. Total | Thru | UTrn | App. Total | Int. Total |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 Peak Hour for Entire Intersection Begins at 07:00 AM |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
| 07:00 AM | 421 | 0 | 421 | 198 | 12 | 210 | 631 |
| 07:15 AM | 410 | 0 | 410 | 136 | 24 | 160 | 570 |
| 07:30 AM | 392 | 0 | 392 | 149 | 36 | 185 | 577 |
| 07:45 AM | 279 | 0 | 279 | 137 | 17 | 154 | 433 |
| Total Volume | 1502 | 0 | 1502 | 620 | 89 | 709 | 2211 |
| \% App. Total | 100 | 0 |  | 87.4 | 12.6 |  |  |
| PHF | . 892 | . 000 | . 892 | . 783 | . 618 | . 844 | . 876 |




## TRAFFIC DATA COLLECTION

File Name : Rolesville(US 401 and Eastern U Turn)PM Peak Site Code :
Start Date : 11/9/2021
Page No :1

| Groups Printed- Cars + - Trucks |  |  |  |  |  |  | Int. Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | US 401 <br> Westbound |  |  | US 401 Eastbound |  |  |  |
| Start Time | Thru | UTrn | App. Total | Thru | UTrn | App. Total |  |
| 04:00 PM | 130 | 0 | 130 | 240 | 12 | 252 | 382 |
| 04:15 PM | 128 | 0 | 128 | 237 | 15 | 252 | 380 |
| 04:30 PM | 129 | 0 | 129 | 311 | 19 | 330 | 459 |
| 04:45 PM | 149 | 0 | 149 | 317 | 19 | 336 | 485 |
| Total | 536 | 0 | 536 | 1105 | 65 | 1170 | 1706 |
| 05:00 PM | 149 | 0 | 149 | 342 | 8 | 350 | 499 |
| 05:15 PM | 160 | 0 | 160 | 284 | 19 | 303 | 463 |
| 05:30 PM | 161 | 0 | 161 | 273 | 22 | 295 | 456 |
| 05:45 PM | 120 | 0 | 120 | 235 | 12 | 247 | 367 |
| Total | 590 | 0 | 590 | 1134 | 61 | 1195 | 1785 |
| Grand Total | 1126 | 0 | 1126 | 2239 | 126 | 2365 | 3491 |
| Apprch \% | 100 | 0 |  | 94.7 | 5.3 |  |  |
| Total \% | 32.3 | 0 | 32.3 | 64.1 | 3.6 | 67.7 |  |
| Cars + | 1101 | 0 | 1101 | 2175 | 125 | 2300 | 3401 |
| \% Cars + | 97.8 | 0 | 97.8 | 97.1 | 99.2 | 97.3 | 97.4 |
| Trucks | 25 | 0 | 25 | 64 | 1 | 65 | 90 |
| \% Trucks | 2.2 | 0 | 2.2 | 2.9 | 0.8 | 2.7 | 2.6 |



## TRAFFIC DATA COLLECTION

File Name : Rolesville(US 401 and Eastern U Turn)PM Peak
Site Code :
Start Date : 11/9/2021
Page No : 2

|  | US 401 Westbound |  |  | US 401 Eastbound |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Thru | UTrn | App. Total | Thru | UTrn | App. Total | Int. Total |
| Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1 Peak Hour for Entire Intersection Begins at 04:30 PM |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
| 04:30 PM | 129 | 0 | 129 | 311 | 19 | 330 | 459 |
| 04:45 PM | 149 | 0 | 149 | 317 | 19 | 336 | 485 |
| 05:00 PM | 149 | 0 | 149 | 342 | 8 | 350 | 499 |
| 05:15 PM | 160 | 0 | 160 | 284 | 19 | 303 | 463 |
| Total Volume | 587 | 0 | 587 | 1254 | 65 | 1319 | 1906 |
| \% App. Total | 100 | 0 |  | 95.1 | 4.9 |  |  |
| PHF | . 917 | . 000 | . 917 | . 917 | . 855 | . 942 | . 955 |




## TRAFFIC DATA COLLECTION

File Name : Rolesville(Jonesville and Mitchell Mill)AM Peak Site Code :
Start Date : 11/30/2021
Page No : 1

Groups Printed- Cars + - Trucks

|  | Peebles Road Southbound |  |  |  | Mitchell Mill Westbound |  |  |  | Peebles Road Northbound |  |  |  | Mitchell Mill Eastbound |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Int. Total |
| 07:00 AM | 4 | 17 | 13 | 34 | 8 | 73 | 5 | 86 | 6 | 11 | 3 | 20 | 0 | 74 | 1 | 75 | 215 |
| 07:15 AM | 4 | 36 | 7 | 47 | 8 | 101 | 2 | 111 | 3 | 26 | 1 | 30 | 0 | 32 | 1 | 33 | 221 |
| 07:30 AM | 6 | 34 | 5 | 45 | 16 | 87 | 3 | 106 | 0 | 24 | 0 | 24 | 1 | 33 | 1 | 35 | 210 |
| 07:45 AM | 2 | 43 | 6 | 51 | 8 | 49 | 1 | 58 | 2 | 15 | 0 | 17 | 1 | 24 | 4 | 29 | 155 |
| Total | 16 | 130 | 31 | 177 | 40 | 310 | 11 | 361 | 11 | 76 | 4 | 91 | 2 | 163 | 7 | 172 | 801 |
| 08:00 AM | 7 | 31 | 12 | 50 | 4 | 53 | 1 | 58 | 1 | 8 | 2 | 11 | 0 | 28 | 3 | 31 | 150 |
| 08:15 AM | 12 | 17 | 3 | 32 | 1 | 37 | 1 | 39 | 1 | 7 | 0 | 8 | 1 | 24 | 1 | 26 | 105 |
| 08:30 AM | 6 | 4 | 2 | 12 | 3 | 49 | 2 | 54 | 1 | 4 | 2 | 7 | 0 | 19 | 0 | 19 | 92 |
| 08:45 AM | 1 | 13 | 3 | 17 | 4 | 32 | 1 | 37 | 1 | 3 | 1 | 5 | 1 | 18 | 2 | 21 | 80 |
| Total | 26 | 65 | 20 | 111 | 12 | 171 | 5 | 188 | 4 | 22 | 5 | 31 | 2 | 89 | 6 | 97 | 427 |
| Grand Total | 42 | 195 | 51 | 288 | 52 | 481 | 16 | 549 | 15 | 98 | 9 | 122 | 4 | 252 | 13 | 269 | 1228 |
| Apprch \% | 14.6 | 67.7 | 17.7 |  | 9.5 | 87.6 | 2.9 |  | 12.3 | 80.3 | 7.4 |  | 1.5 | 93.7 | 4.8 |  |  |
| Total \% | 3.4 | 15.9 | 4.2 | 23.5 | 4.2 | 39.2 | 1.3 | 44.7 | 1.2 | 8 | 0.7 | 9.9 | 0.3 | 20.5 | 1.1 | 21.9 |  |
| Cars + | 42 | 195 | 50 | 287 | 52 | 479 | 16 | 547 | 15 | 98 | 9 | 122 | 4 | 249 | 13 | 266 | 1222 |
| \% Cars + | 100 | 100 | 98 | 99.7 | 100 | 99.6 | 100 | 99.6 | 100 | 100 | 100 | 100 | 100 | 98.8 | 100 | 98.9 | 99.5 |
| Trucks | 0 | 0 | 1 | 1 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 3 | 6 |
| \% Trucks | 0 | 0 | 2 | 0.3 | 0 | 0.4 | 0 | 0.4 | 0 | 0 | 0 | 0 | 0 | 1.2 | 0 | 1.1 | 0.5 |



## TRAFFIC DATA COLLECTION

File Name : Rolesville(Jonesville and Mitchell Mill)AM Peak Site Code :
Start Date : 11/30/2021
Page No : 2

|  | Peebles Road Southbound |  |  |  | Mitchell Mill Westbound |  |  |  | Peebles Road Northbound |  |  |  | Mitchell Mill Eastbound |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Int. Total |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 07:00 AM | 4 | 17 | 13 | 34 | 8 | 73 | 5 | 86 | 6 | 11 | 3 | 20 | 0 | 74 | 1 | 75 | 215 |
| 07:15 AM | 4 | 36 | 7 | 47 | 8 | 101 | 2 | 111 | 3 | 26 | 1 | 30 | 0 | 32 | 1 | 33 | 221 |
| 07:30 AM | 6 | 34 | 5 | 45 | 16 | 87 | 3 | 106 | 0 | 24 | 0 | 24 | 1 | 33 | 1 | 35 | 210 |
| 07:45 AM | 2 | 43 | 6 | 51 | 8 | 49 | 1 | 58 | 2 | 15 | 0 | 17 | 1 | 24 | 4 | 29 | 155 |
| Total Volume | 16 | 130 | 31 | 177 | 40 | 310 | 11 | 361 | 11 | 76 | 4 | 91 | 2 | 163 | 7 | 172 | 801 |
| \% App. Total | 9 | 73.4 | 17.5 |  | 11.1 | 85.9 | 3 |  | 12.1 | 83.5 | 4.4 |  | 1.2 | 94.8 | 4.1 |  |  |
| PHF | . 667 | . 756 | . 596 | . 868 | . 625 | . 767 | . 550 | . 813 | 458 | . 731 | . 333 | . 758 | . 500 | . 551 | . 438 | . 573 | . 906 |




## TRAFFIC DATA COLLECTION

File Name : Rolesville(Jonesville and Mitchell Mill)PM Peak Site Code :
Start Date : 11/30/2021
Page No : 1

Groups Printed- Cars + - Trucks

|  | Peebles Road Southbound |  |  |  | Mitchell Mill Westbound |  |  |  | Peebles Road Northbound |  |  |  | Mitchell Mill Eastbound |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Int. Total |
| 04:00 PM | 7 | 11 | 13 | 31 | 6 | 25 | 1 | 32 | 1 | 14 | 1 | 16 | 2 | 44 | 6 | 52 | 131 |
| 04:15 PM | 6 | 11 | 4 | 21 | 2 | 27 | 2 | 31 | 1 | 17 | 3 | 21 | 1 | 62 | 4 | 67 | 140 |
| 04:30 PM | 3 | 13 | 3 | 19 | 4 | 30 | 2 | 36 | 0 | 27 | 1 | 28 | 3 | 64 | 3 | 70 | 153 |
| 04:45 PM | 2 | 8 | 5 | 15 | 4 | 37 | 0 | 41 | 3 | 18 | 0 | 21 | 3 | 71 | 3 | 77 | 154 |
| Total | 18 | 43 | 25 | 86 | 16 | 119 | 5 | 140 | 5 | 76 | 5 | 86 | 9 | 241 | 16 | 266 | 578 |
| 05:00 PM | 1 | 15 | 6 | 22 | 5 | 31 | 0 | 36 | 3 | 19 | 2 | 24 | 1 | 78 | 5 | 84 | 166 |
| 05:15 PM | 3 | 15 | 6 | 24 | 4 | 23 | 0 | 27 | 3 | 26 | 1 | 30 | 4 | 89 | 7 | 100 | 181 |
| 05:30 PM | 5 | 11 | 9 | 25 | 8 | 36 | 0 | 44 | 1 | 27 | 2 | 30 | 5 | 62 | 3 | 70 | 169 |
| 05:45 PM | 1 | 7 | 4 | 12 | 2 | 21 | 1 | 24 | 2 | 13 | 2 | 17 | 4 | 55 | 6 | 65 | 118 |
| Total | 10 | 48 | 25 | 83 | 19 | 111 | 1 | 131 | 9 | 85 | 7 | 101 | 14 | 284 | 21 | 319 | 634 |
| Grand Total | 28 | 91 | 50 | 169 | 35 | 230 | 6 | 271 | 14 | 161 | 12 | 187 | 23 | 525 | 37 | 585 | 1212 |
| Apprch \% | 16.6 | 53.8 | 29.6 |  | 12.9 | 84.9 | 2.2 |  | 7.5 | 86.1 | 6.4 |  | 3.9 | 89.7 | 6.3 |  |  |
| Total \% | 2.3 | 7.5 | 4.1 | 13.9 | 2.9 | 19 | 0.5 | 22.4 | 1.2 | 13.3 | 1 | 15.4 | 1.9 | 43.3 | 3.1 | 48.3 |  |
| Cars + | 28 | 91 | 50 | 169 | 35 | 229 | 6 | 270 | 14 | 161 | 12 | 187 | 23 | 524 | 37 | 584 | 1210 |
| \% Cars + | 100 | 100 | 100 | 100 | 100 | 99.6 | 100 | 99.6 | 100 | 100 | 100 | 100 | 100 | 99.8 | 100 | 99.8 | 99.8 |
| Trucks | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 2 |
| \% Trucks | 0 | 0 | 0 | 0 | 0 | 0.4 | 0 | 0.4 | 0 | 0 | 0 | 0 | 0 | 0.2 | 0 | 0.2 | 0.2 |



## TRAFFIC DATA COLLECTION

File Name : Rolesville(Jonesville and Mitchell Mill)PM Peak Site Code :
Start Date : 11/30/2021
Page No : 2

|  | Peebles Road Southbound |  |  |  | Mitchell Mill Westbound |  |  |  | Peebles Road Northbound |  |  |  | Mitchell Mill Eastbound |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Int. Total |
| Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 04:45 PM | 2 | 8 | 5 | 15 | 4 | 37 | 0 | 41 | 3 | 18 | 0 | 21 | 3 | 71 | 3 | 77 | 154 |
| 05:00 PM | 1 | 15 | 6 | 22 | 5 | 31 | 0 | 36 | 3 | 19 | 2 | 24 | 1 | 78 | 5 | 84 | 166 |
| 05:15 PM | 3 | 15 | 6 | 24 | 4 | 23 | 0 | 27 | 3 | 26 | 1 | 30 | 4 | 89 | 7 | 100 | 181 |
| 05:30 PM | 5 | 11 | 9 | 25 | 8 | 36 | 0 | 44 | 1 | 27 | 2 | 30 | 5 | 62 | 3 | 70 | 169 |
| Total Volume | 11 | 49 | 26 | 86 | 21 | 127 | 0 | 148 | 10 | 90 | 5 | 105 | 13 | 300 | 18 | 331 | 670 |
| \% App. Total | 12.8 | 57 | 30.2 |  | 14.2 | 85.8 | 0 |  | 9.5 | 85.7 | 4.8 |  | 3.9 | 90.6 | 5.4 |  |  |
| PHF | . 550 | . 817 | . 722 | . 860 | . 656 | . 858 | . 000 | . 841 | 833 | . 833 | . 625 | . 875 | . 650 | . 843 | . 643 | 828 | . 925 |



## APPENDIX C

## ADJACENT DEVELOPMENT <br> INFORMATION

# TRAFFIC IMPACT ANALYSIS 

FOR

# COBBLESTONE CROSSING MIXED-USE 

## LOCATED

IN

## ROLESVILLE, NORTH CAROLINA

Prepared For:
Town of Rolesville
502 Southtown Circle
Rolesville, NC 27571

Prepared By:
Ramey Kemp \& Associates, Inc. 5808 Faringdon Place, Suite 100

Raleigh, NC 27609


License \#C-0910

MARCH 2021



## 9. RECOMMENDATIONS

Based on the findings of this study, specific geometric improvements have been identified and are recommended to accommodate future traffic conditions. See a more detailed description of the recommended improvements below. Refer to Figure 14 for an illustration of the recommended lane configuration for the proposed development.

## Improvements by STIP U-6241

STIP U-6241 is expected to realign Burlington Mills Road and install a traffic signal at the relocated intersection on Main Street. STIP U-6241 is also expected to provide improvements to the pedestrian and bike facilities along Main Street and add a concrete median island along Main Street west of Rogers Road. These improvements associated with STIP U-6241 will alter the existing lane configurations at the study intersections along Main Street.

## Recommended Improvements by Developer

## Main Street and Site Drive 1

- Construct the southbound approach with one ingress and two egress lanes.
- Provide stop control for the southbound approach.
- Install an eastbound left-turn lane with at least 125 feet of storage and appropriate decel and taper.


## Young Street and Site Drive 2

- Construct the eastbound approach with one ingress and egress lane.
- Provide stop control for the eastbound approach.



# Revised Traffic Impact Analysis for Young Street PUD 

Rolesville, North Carolina

Prepared for:<br>Ashton Woods<br>Raleigh, North Carolina

Prepared by:
Kimley-Horn and Associates, Inc.
NC License \#F-0102
421 Fayetteville Street, Suite 600
Raleigh, NC 27601
(919) 677-2000

June 2019
015956012



## Kimley») Horn

| YOUNG STREET PUD |
| :---: |
| ROLESVILLE, VC |
| TRAFFIC IMPACT' ANALYSIS |

$\square$



## Kimley»Horn

### 7.0 Recommendations

## Residential Build-out

The following improvements are recommended to be performed to accommodate projected site traffic volumes at build-out of the residential portion of the development:

## US 401 Bypass:

- Coordinate the traffic signals at the intersections of US 401 at Young Street and the Superstreet U-turns


## Young Street at Quarry Road/North Site Driveway:

- Construct a northbound left-turn lane on Young Street with 100 feet of storage and appropriate tapers
- Construct a southbound right-turn lane on Young Street with 100 feet of storage and appropriate tapers
- Restripe the existing westbound left-turn lane on Quarry Road to a shared left/through lane
- Provide an exclusive left-turn lane with 275 feet of storage and appropriate tapers and a shared through/right lane on the North Site Driveway
- Install a traffic signal when warranted


## Young Street at Central Site Driveway:

- Construct a northbound left-turn lane on Young Street with 100 feet of storage and appropriate tapers
- Construct a southbound right-turn lane on Young Street with 100 feet of storage and appropriate tapers
- Provide exclusive left and right-turn lanes on the Central Site Driveway with 125 feet of storage and appropriate tapers for the left-turn lane


## Young Street at Rolesville High School Driveway/South Site Driveway:

- Construct a northbound left-turn lane on Young Street with 50 feet of storage and appropriate tapers
- Provide one egress lane on the South Site Driveway

Rolesville Road at Mitchell Mill Road:

- Install a traffic signal when warranted

Analyses indicate that with the recommended improvements in place, all of the study intersections except for Young Street at Century Farm Road and Young Street at Rolesville High School Driveway/South Site Driveway are expected to operate at an acceptable LOS at build-out of the residential-only phase of the development.

Analyses indicate that the intersection of Young Street at Century Farm Road is expected to operate with long delays on the minor street approach (Century Farm Road) in the AM peak hour at project build-out. However, it is typical for stop sign controlled side streets and driveways intersecting major streets to experience long delays during peak hours while the majority of the traffic moving through the intersection on the major street experiences little or no delay. SimTraffic traffic simulations indicate that no queuing issues are expected at this intersection.

Analyses indicate that the intersection of Young Street at the Rolesville High School Driveway/South Site Driveway is expected to operate with long delays on the minor street approach (Rolesville High School Driveway) in the AM peak hour and school PM peak hour with or without the proposed project in place in the study year 2025. SimTraffic traffic simulations also indicate the possibility of long queues on the westbound left-turn movement at this intersection in the AM peak hour and school PM peak hour. However, it is typical for stop sign controlled side streets and driveways intersecting major streets to experience long delays during peak hours, while the majority of the traffic moving through the intersection on the major street experiences little or no delay. This intersection is not expected to meet 4-hour or 8-hour MUTCD traffic signal warrants.

## Commercial Build-out

The following additional improvements are recommended to be performed in addition to those recommended above for the residential phase to accommodate projected site traffic volumes when the retail portion of the site is developed:

## US 401 Bypass Eastbound at Young Street:

- Extend the storage of the existing eastbound right-turn lane on US 401 Bypass by approximately 175 feet to provide 400 feet of storage and appropriate tapers


## Young Street at Quarry Road/North Site Driveway:

- Construct a northbound right-turn lane on Young Street with 100 feet of storage and appropriate tapers
- Modify the traffic signal to accommodate the additional laneage

Analyses indicate that with the recommended improvements in place, all of the study intersections except for Young Street at Century Farm Road, Young Street at the Central Site Driveway, and Young Street at Rolesville High School Driveway/South Site Driveway are expected to operate at acceptable LOS at commercial build-out of the development.

Analyses indicate that the intersection of Young Street at Century Farm Road is expected to operate with long delays on the minor street approach (Century Farm Road) in the AM peak hour at project build-out. It is typical for stop sign controlled side streets and driveways intersecting major streets to experience long delays during peak hours, while the majority of the traffic moving through the intersection on the major street experiences little or no delay. SimTraffic

## Kimley»Horn

traffic simulations indicate that short queues are likely on the minor street approach in the AM peak hour at commercial build-out.

Analyses indicate that the intersection of Young Street at the Central Site Driveway is expected to operate with long delays on the minor street approach (Central Site Driveway) in the AM peak hour in the commercial build-out traffic condition. It is typical for stop sign controlled side streets and driveways intersecting major streets to experience long delays during peak hours, while the majority of the traffic moving through the intersection on the major street experiences little or no delay. SimTraffic traffic simulations indicate the possibility of long queues on the eastbound leftturn movement at this intersection in the AM peak hour in the commercial build-out condition.

Analyses indicate that the intersection of Young Street at the Rolesville High School Driveway/South Site Driveway is expected to operate with long delays on the minor street approach (Rolesville High School Driveway) in the AM peak hour and school PM peak hour with or without the proposed project in place in the study year 2025. SimTraffic traffic simulations also indicate the possibility of long queues on the westbound left-turn movement at this intersection in the AM peak hour and school PM peak hour. However, it is typical for stop sign controlled side streets and driveways intersecting major streets to experience long delays during peak hours, while the majority of the traffic moving through the intersection on the major street experiences little or no delay. This intersection is not expected to meet 4-hour or 8-hour MUTCD traffic signal warrants.

As shown in the analysis, the impact of site traffic associated with the commercial build-out of this proposed PUD is generally consistent with the currently-approved PUD for the site. The proposed PUD is expected to generate no more than 50 additional peak hour trips in each of the studied peak hours compared to the approved PUD, and delays at commercial build-out of both plans are generally consistent at each of the study intersections.

The recommended laneage for the development is shown on Figure 17.


# TRAFFIC IMPACT ANALYSIS 

## FOR

## WHEELER TRACT

LOCATED<br>IN<br>ROLESVILLE，NC

Prepared For：<br>Hopper Communities<br>173 Paraggi Court<br>Clayton，NC 27527

Prepared By：
Ramey Kemp \＆Associates，Inc． 5808 Faringdon Place，Suite 100

Raleigh，NC 27609
License \＃C－0910

June 2019


6－18－19



## 9. RECOMMENDATIONS

Based on the findings of this study, specific geometric improvements have been identified and are recommended to accommodate future traffic conditions. See a more detailed description of the recommended improvements below. Refer to Figure 11 for an illustration of the recommended lane configuration for the proposed development.

## Recommended Improvements by Developer

Rolesville Road and Mitchell Mill Road

- Monitor intersection for signalization.


## Rolesville Road and Site Drive 1

- Provide site access via a full movement intersection with one ingress lane and one egress lane.
- Provide stop control for westbound Site Drive 1 approach.
- Provide a designated southbound left-turn lane with at least 100 feet of storage and appropriate deceleration and taper.

Mitchell Mill Road and Site Drive 2

- Provide site access via a full movement intersection with one ingress lane and one egress lane.
- Provide stop control for southbound Site Drive 2 approach.



# TRAFFIC IMPACT ANALYSIS 

## FOR <br> LOUISBURY ROAD ASSEMBLAGE

## LOCATED

## IN

## RALEIGH, NC

Prepared For: McAdam Company
2905 Meridian Parkway
Durham, NC 27713

Prepared By:
Ramey Kemp \& Associates, Inc.
5808 Faringdon Place, Suite 100
Raleigh, NC 27609
License \#C-0910


5/8/2020

May 2020


| Moving forward. | Louisbury Road Assemblage |
| :--- | :--- | :--- | :--- |
| Raleigh, NC |  |

## LEGEND

O Unsignalized Intersection
Signalized Intersection
$\mathrm{X} / \mathrm{Y} \rightarrow$ Weekday AM / PM Peak Hour Site Trips


| Moving forward. | Souisbury Road Assemblage |
| :--- | :--- | :--- | :--- |
| Raleigh, NC |  |

## 12. RECOMMENDATIONS

Based on the findings of this study, specific geometric improvements have been identified and are recommended to accommodate future traffic conditions. See a more detailed description of the recommended improvements below. Refer to Figure 9 for an illustration of the recommended lane configuration for the proposed development.

## Recommended Improvements by Developer

Mitchell Mill Road and Louisbury Road

- Monitor for signalization after site is constructed.


## US 401 and Louisbury Road

- Per NCDOT, extend northbound left turn lane to $\mathbf{1 7 5}^{\prime}$ of storage.
- Monitor for signalization after site is constructed.


## Louisbury Road and Site Drive 1

- Provide site access via full movement intersection with one (1) ingress lane and one (1) egress lane.
- Per NCDOT, provide northbound left turn lane with $100^{\prime}$ of storage.
- Provide stop control for eastbound approach.


## Louisbury Road and Site Drive 2

- Provide site access via full movement intersection with one (1) ingress lane and one (1) egress lane.
- Provide stop control for eastbound approach.


*Based on NCDOT Review


| Moving forward. <br> RAMEY KEMP ASSOCIATES | Louisbury Road Assemblage Raleigh, NC | Recommended Lane Configurations |  |
| :---: | :---: | :---: | :---: |
|  |  | Scale: Not to Scale | Figure 9 |

# Stantec 

## Kalas / Watkins Family Property Traffic Impact Analysis

Rolesville Road, Rolesville, North Carolina

August 24, 2019

Prepared for:
Mitchell Mill Road Investors LLC
PO Box 3557
Cary, NC 27519
Prepared by:
Stantec Consulting Services Inc.
801 Jones Franklin Road
Suite 300
Raleigh, NC 27606

## Sign-off Sheet

This document entitled Kalas / Watkins Family Property Traffic Impact Analysis was prepared by Stantec Consulting Services Inc. ("Stantec") for the account of Mitchell Mill Road Investors LLC (the "Client"). Any reliance on this document by any third party is strictly prohibited. The material in it reflects Stantec's professional judgment in light of the scope, schedule and other limitations stated in the document and in the contract between Stantec and the Client. The opinions in the document are based on conditions and information existing at the time the document was published and do not take into account any subsequent changes. In preparing the document, Stantec did not verify information supplied to it by others. Any use which a third party makes of this document is the responsibility of such third party. Such third party agrees that Stantec shall not be responsible for costs or damages of any kind, if any, suffered by it or any other third party as a result of decisions made or actions taken based on this document.

Prepared by

(signature)
Maggie Rogers
Reviewed by

(signature)

(signature)

## Christa Greene, PE



## KALAS / WATKINS FAMILY PROPERTY TRAFFIC IMPACT ANALYSIS

Introduction
August 24, 2019

### 1.0 INTRODUCTION

The purpose of this report is to evaluate the transportation impacts of the proposed Kalas / Watkins Family Property development located on the west side of Rolesville Road just north of Mitchell Mill Road in Rolesville, NC. The project location is shown below in Figure 1

Figure 1: Site Location


Trip Generation and Distribution
August 24, 2019
Figure 6: Site Trip Assignment


Traffic Analysis
August 24, 2019

### 5.42025 BUILD WITH IMPROVEMENTS

Geometric improvements such as the installation of turn-lanes are recommended and therefore analyzed in this scenario. These items are listed below as well as in the recommendations section.

## Rolesville Road at Site Driveway A

- Construct Driveway A as a full-movement access point onto Rolesville Road with one ingress lane and one egress lane.
- Construct an exclusive eastbound right-turn lane with 100 feet of full-width storage and appropriate taper on Driveway A.
- Construct an exclusive northbound left-turn lane with 100 feet of full-width storage and appropriate taper on Rolesville Road.
- Construct an exclusive southbound right-turn lane with 100 feet of full-width storage and appropriate taper on Rolesville Road.


## Rolesville Road at Site Driveway B / Wheeler Tract Driveway

- Construct Driveway B as a full-movement access point onto Rolesville Road with one ingress lane and one egress lane.
- Construct an exclusive northbound left-turn lane with 100 feet of full-width storage and appropriate taper on Rolesville Road.
- Construct an exclusive southbound right-turn lane with 50 feet of full-width storage and appropriate taper on Rolesville Road.


## Rolesville Road at Site Driveway C

- Construct Driveway $C$ as a full-movement access point onto Rolesville Road with one ingress lane and one egress lane.
- Construct an exclusive eastbound right-turn lane with 100 feet of full-width storage and appropriate taper on Driveway C.
- Construct an exclusive northbound left-turn lane with 100 feet of full-width storage and appropriate taper on Rolesville Road.
- Construct an exclusive southbound right-turn lane with 100 feet of full-width storage and appropriate taper on Rolesville Road.

Accordingly, all study area intersections and approaches operate at acceptable levels of service with the following exceptions:

- The east and westbound approaches to the intersection of Rolesville Road at Rolesville High School Driveway / Young Street PUD Southern Driveway operates at LOS F in the AM peak hour. This causes high overall delays at the intersection. Furthermore, the eastbound approach operates at LOS F and westbound approach operates at LOS E in the PM peak hour.
- The east and westbound approaches at the intersection of Rolesville Road at Site Driveway B / Wheeler Tract Driveway operate at LOS E in the AM peak hour.

The east and westbound approaches to the intersection of Rolesville Road at Rolesville High School Driveway / Young Street PUD Southern Driveway performs unacceptably across analysis scenarios. These delays can be

## KALAS / WATKINS FAMILY PROPERTY TRAFFIC IMPACT ANALYSIS

Traffic Analysis
August 24, 2019
attributed to both the Young Street PUD and High School traffic on the side street approaches. The Kalas / Watkins development is projected to only add through volumes to the intersection and are anticipated to have a minimal impact on overall delays at this intersection.

Delays on the eastbound approach of Site Driveway B at Rolesville Road can be attributed to high thru volumes on Rolesville Road during the AM peak hour. Traffic volumes using this approach are anticipated to be minor (i.e. 15 vehicles in the AM peak hour and 10 vehicles in the PM peak hour) and side street delays should dissipate after High School Traffic passes through the network. Table 8 lists the results of the capacity analysis under the 2025 buildimproved traffic conditions. The recommended improvements are illustrated in figure 14.

Figure 14: Recommended Improvements


# TRAFFIC IMPACT ANALYSIS 

FOR

## 5109 MITCHELL MILL ROAD

## LOCATED

IN

## ROLESVILLE, NORTH CAROLINA

Prepared For:<br>Town of Rolesville<br>502 Southtown Circle<br>Rolesville, NC 27571

Prepared By: Infrastructure Consulting Services, Inc. $d b a$ Ramey Kemp Associates

5808 Faringdon Place
Raleigh, NC 27609
License \#F-1489

AUGUST 2022


## LEGEND

-     - $\quad$ Proposed Site Location

O Study Intersection
こー・ Study Area

|  | 5109 Mitchell Mill Road <br> Rolesville, NC | Site Location Map |  |
| :---: | :---: | :--- | :--- |



## 9. RECOMMENDATIONS

Based on the findings of this study, specific geometric improvements have been identified and are recommended to accommodate future traffic conditions. See a more detailed description of the recommended improvements below. Refer to Figure 14 for an illustration of the recommended lane configurations for the proposed development.

## Recommended Improvements by Developer

Required Frontage Improvements per Rolesville Community Transportation Plan

- Widen Jonesville Road along the site frontage between Site Access 1 and Mitchell Mill Road to this roadway's ultimate section (2-lane w/ TWLTL).
- Widen one-half section of Mitchell Mill Road along the site frontage to this roadway's ultimate section (4-lane median divided).


## US 401 Bypass and Jonesville Road

- Conduct a full signal warrant analysis prior to full build-out of the proposed development and install a traffic signal if warranted and approved by the Town and NCDOT.


## US 401 Bypass and Eastern U-Turn Location

- Conduct a full signal warrant analysis prior to full build-out of the proposed development and install a traffic signal if warranted and approved by the Town and NCDOT.


## Mitchell Mill Road and Jonesville Road / Peebles Road

- Construct a southbound (Jonesville Road) left-turn lane with at least 100 feet of storage and appropriate decel and taper.
- Construct an eastbound (Mitchell Mill Road) left-turn lane with at least 100 feet of storage and appropriate decel and taper.
- Conduct a full signal warrant analysis prior to full build-out of the proposed development and install a traffic signal if warranted and approved by the Town and NCDOT.


## Jonesville Road and Site Access 1

- Construct the westbound approach (Site Access 1) with one ingress lane and one egress lane.
- Provide stop-control for the westbound approach (Site Access 1).
- Construct a southbound (Jonesville Road) left-turn lane with at least 100 feet of storage and appropriate decel and taper.


## Jonesville Road and Site Access 2

- Construct the westbound approach (Site Access 2) with one ingress lane and one egress lane.
- Provide stop-control for the westbound approach (Site Access 2).
- Construct a northbound (Jonesville Road) right-turn lane with at least 100 feet of storage and appropriate decel and taper.
- Construct a southbound (Jonesville Road) left-turn lane with at least 100 feet of storage and appropriate decel and taper.


## Jonesville Road and Site Access 3

- Construct the eastbound and westbound approaches (Site Access 3) with one ingress lane and one egress lane.
- Provide stop-control for the eastbound and westbound approaches (Site Access 3).
- Construct a northbound (Jonesville Road) left-turn lane with at least 100 feet of storage and appropriate decel and taper.
- Construct a northbound (Jonesville Road) right-turn lane with at least 100 feet of storage and appropriate decel and taper.
- Construct a southbound (Jonesville Road) left-turn lane with at least 100 feet of storage and appropriate decel and taper.
- Construct a southbound (Jonesville Road) right-turn lane with at least 100 feet of storage and appropriate decel and taper.


## Jonesville Road and Site Access 4

- Construct the eastbound approach (Site Access 4) with one ingress lane and one egress lane.
- Provide stop-control for the eastbound approach (Site Access 4).
- Construct a northbound (Jonesville Road) left-turn lane with at least 100 feet of storage and appropriate decel and taper.
- Construct a southbound (Jonesville Road) right-turn lane with at least 100 feet of storage and appropriate decel and taper.


## Mitchell Mill Road and Site Access 5

- Construct the southbound approach (Site Access 5) with one ingress lane and one egress lane striped as an exclusive right-turn lane.
- Provide stop-control for the southbound approach (Site Access 5). This proposed intersection will be restricted to right-in/right-out operations.
- Construct an exclusive westbound (Mitchell Mill Road) right-turn lane with at least 100 feet of storage and appropriate decel and taper.


## Mitchell Mill Road and Site Access 6

- Construct the southbound approach (Site Access 6) with one ingress lane and one egress lane striped as an exclusive right-turn lane.
- Provide stop-control for the southbound approach (Site Access 6). This proposed intersection will be restricted to right-in/right-out operations.
- Construct an exclusive westbound (Mitchell Mill Road) right-turn lane with at least 100 feet of storage and appropriate decel and taper.


## Mitchell Mill Road and Site Access 7

- Construct the southbound approach (Site Access 7) with one ingress lane and one egress lane.
- Provide stop-control for the southbound approach (Site Access 7)
- Construct an exclusive eastbound (Mitchell Mill Road) left-turn lane with at least 100 feet of storage and appropriate decel and taper.


## Mitchell Mill Road and Site Access 8

- Construct the southbound approach (Site Access 8 ) with one ingress lane and one egress lane striped as an exclusive right-turn lane.
- Provide stop-control for the southbound approach (Site Access 8). This proposed intersection will be restricted to right-in/right-out operations.
- Construct an exclusive westbound (Mitchell Mill Road) right-turn lane with at least 100 feet of storage and appropriate decel and taper.



# TRAFFIC IMPACT <br> ANALYSIS 

FOR

## HILLS AT HARIS CREEK

## LOCATED

IN

## ROLESVILLE, NORTH CAROLINA

Prepared For:<br>Town of Rolesville 502 Southtown Circle Rolesville, NC 27571<br>Prepared By:<br>Ramey Kemp \& Associates, Inc. 5808 Faringdon Place, Suite 100<br>Raleigh, NC 27609<br>License \#C-0910



MAY 2022


## LEGEND

- = I Proposed Site Location
$\bigcirc$ Study Intersection
= = I Study Area

|  | Hills at Harris Creek <br> Rolesville, NC | Site Location Map |  |
| :---: | :---: | :--- | :--- |
| Ramey kemp associates |  |  |  |



## 9. RECOMMENDATIONS

Based on the findings of this study, specific geometric improvements have been identified and are recommended to accommodate future traffic conditions. See a more detailed description of the recommended improvements below. Refer to Figure 14 for an illustration of the recommended lane configurations for the proposed development.

## Recommended Improvements by Developer

Required Frontage Improvements per Rolesville Community Transportation Plan

- Widen one-half section of Mitchell Mill Road along the site frontage to this roadway's ultimate section (4-lane median divided).


## US 401 Bypass and Jonesville Road

- Conduct a full signal warrant analysis prior to full build-out of the proposed development and install a traffic signal if warranted and approved by the Town and NCDOT.


## US 401 Bypass and Eastern U-Turn Location

- Conduct a full signal warrant analysis prior to full build-out of the proposed development and install a traffic signal if warranted and approved by the Town and NCDOT.


## Mitchell Mill Road and Jonesville Road / Peebles Road

- Construct a southbound (Jonesville Road) left-turn lane with at least 100 feet of storage and appropriate decel and taper.
- It should be noted that this improvement was also identified by the 5109 Mitchell Mill Road TIA.
- Construct a westbound (Mitchell Mill Road) right-turn lane with at least 100 feet of storage and appropriate decel and taper.
- Conduct a full signal warrant analysis prior to full build-out of the proposed development and install a traffic signal if warranted and approved by the Town and NCDOT.


## Mitchell Mill Road and Site Access 1

- Construct the southbound approach (Site Access 1) with one ingress lane and one egress lane.
- Provide stop-control for the southbound approach (Site Access 1).
- Construct an eastbound (Mitchell Mill Road) left-turn lane with at least 100 feet of storage and appropriate decel and taper.


## Mitchell Mill Road and Site Access 2

- Construct the southbound approach (Site Access 2) with one ingress lane and one egress lane.
- Provide stop-control for the southbound approach (Site Access 2).
- Construct an eastbound (Mitchell Mill Road) left-turn lane with at least 150 feet of storage and appropriate decel and taper.
- Construct a westbound (Mitchell Mill Road) right-turn lane with at least 100 feet of storage and appropriate decel and taper.

**Refer to Section 9 of the report for more information



## APPENDIX D

## CAPACITY ANALYSIS CALCULATIONS US 401 BYPASS <br> \& <br> JONESVILLE ROAD




Platoon blocked, \%

| Mov Cap-1 Maneuver | - | - | - | - | - | 668 | - | 384 | - |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | - | 384 | - |
| Stage 1 | - | - | - | - | - | - | - | - | - |

Stage 2 - - - - - - 460

| Approach | EB | NB | SB |
| :--- | :---: | :---: | ---: |
| HCM Control Delay, s | 0 | 12 | 17.5 |
| HCM LOS | B | C |  |


| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR SBLn1 |
| :--- | ---: | ---: | ---: |
| Capacity (veh/h) | 668 | - | -384 |
| HCM Lane V/C Ratio | 0.226 | - | -0.249 |
| HCM Control Delay (s) | 12 | - | -17.5 |
| HCM Lane LOS | B | - | - |
| HCM 95th \%tile Q(veh) | 0.9 | - | - |
| C | 1 |  |  |



| Major/Minor | Major1 | Minor1 |  |  |  |  |  |  | Minor2 |  |  |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | - | 0 | 0 | - | - | 678 | - | 1356 | - |  |  |  |  |  |  |
| Stage 1 | - | - | - | - | - | - | - | 0 | - |  |  |  |  |  |  |
| Stage 2 | - | - | - | - | - | - | - | 1356 | - |  |  |  |  |  |  |
| Critical Hdwy | - | - | - | - | - | 6.94 | - | 6.54 | - |  |  |  |  |  |  |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | - | - | - |  |  |  |  |  |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | - | 5.54 | - |  |  |  |  |  |  |
| Follow-up Hdwy | - | - | - | - | - | 3.32 | - | 4.02 | - |  |  |  |  |  |  |
| Pot Cap-1 Maneuver | 0 | - | - | 0 | 0 | 395 | 0 | 148 | 0 |  |  |  |  |  |  |
| Stage 1 | 0 | - | - | 0 | 0 | - | 0 | - | 0 |  |  |  |  |  |  |
| Stage 2 | 0 | - | - | 0 | 0 | - | 0 | 216 | 0 |  |  |  |  |  |  |

Platoon blocked, \%

| Mov Cap-1 Maneuver | - | - | - | - | - | 395 | - | 148 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | - | 148 |
| Stage 1 | - | - | - | - | - | - | - | - |

Stage 2 - $\quad$ - $\quad$ - $\quad-\quad$ - 216

| Approach | EB | NB | SB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 0 | 19 | 38.4 |
| HCM LOS |  | C | E |


| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR SBLn1 |
| :--- | ---: | ---: | ---: |
| Capacity (veh/h) | 395 | - | -148 |
| HCM Lane V/C Ratio | 0.352 | - | -0.278 |
| HCM Control Delay (s) | 19 | - | -38.4 |
| HCM Lane LOS | C | - | - |
| HCM 95th \%tile Q(veh) | 1.6 | - | - |



| Major/Minor | Major1 | Minor1 |  |  |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Conflicting Flow All | - | 0 | 0 | - | - | 451 | - | 902 |

Platoon blocked, \%

| Mov Cap-1 Maneuver | - | - | - | - | - | 556 | - | 276 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | - | 276 |
| Stage 1 | - | - | - | - | - | - | - | - |

Stage 2 - $\quad$ - $\quad$ - $\quad-\quad$ - 355

| Approach | EB | NB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0 | 25.2 | 31.1 |
| HCM LOS |  | D | D |


| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR SBLn1 |
| :--- | ---: | ---: | ---: |
| Capacity (veh/h) | 556 | - | -276 |
| HCM Lane V/C Ratio | 0.699 | - | -0.515 |
| HCM Control Delay (s) | 25.2 | - | -31.1 |
| HCM Lane LOS | $D$ | - | - |
| HCM 95th \%tile Q(veh) | 5.5 | - | - |



| Major/Minor | Major1 | Minor1 |  |  |  |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Conflicting Flow All | - | 0 | 0 | - | - | 949 | - | 1898 | - |
| Stage 1 | - | - | - | - | - | - | - | 0 | - |
| Stage 2 | - | - | - | - | - | - | -1898 | - |  |
| Critical Hdwy | - | - | - | - | - | 6.94 | - | 6.54 | - |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | - | 5.54 | - |
| Follow-up Hdwy | - | - | - | - | - | 3.32 | - | 4.02 | - |
| Pot Cap-1 Maneuver | 0 | - | - | 0 | 0 | $\sim 261$ | 0 | $\sim 69$ | 0 |
| Stage 1 | 0 | - | - | 0 | 0 | - | 0 | - | 0 |
| Stage 2 | 0 | - | - | 0 | 0 | - | 0 | $\sim 116$ | 0 |

Platoon blocked, \%

| Mov Cap-1 Maneuver | - | - | - | - | - | $\sim 261$ | - | $\sim 69$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | - | $\sim 69$ |
| Stage 1 | - | - | - | - | - | - | - | - |

Stage 2 - $\quad$ - $\quad$ - $\quad-\quad$ - 116

| Approach | EB | NB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0 | 180.2 | $\$ 579.5$ |
| HCM LOS | F | F |  |


| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR SBLn1 |
| :--- | ---: | ---: | ---: |
| Capacity (veh/h) | 261 | - | -69 |
| HCM Lane V/C Ratio | 1.252 | - | -1.965 |
| HCM Control Delay (s) | 180.2 | - | $-\$ 579.5$ |
| HCM Lane LOS | F | - | - |
| HCM 95th \%tile Q(veh) | 15.9 | - | -12.4 |

## Notes

~: Volume exceeds capacity $\$$ : Delay exceeds 300s $\quad+$ : Computation Not Defined *: All major volume in platoon


| Major/Minor | Major1 | Minor1 |  |  |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Conflicting Flow All | - | 0 | 0 | - | - | 451 | - | 902 |

Platoon blocked, \%

| Mov Cap-1 Maneuver | - | - | - | - | - | 556 | - | 276 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | - | 276 |
| Stage 1 | - | - | - | - | - | - | - | - |



| Approach | EB | NB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0 | 29.1 | 31.7 |
| HCM LOS | D | D |  |


| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR SBLn1 |
| :--- | ---: | ---: | ---: |
| Capacity (veh/h) | 556 | - | -276 |
| HCM Lane V/C Ratio | 0.759 | - | -0.527 |
| HCM Control Delay (s) | 29.1 | - | -31.7 |
| HCM Lane LOS | D | - | - |
| HCM 95th \%tile Q(veh) | 6.7 | - | - |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 64.2 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 14 | $7^{7}$ |  |  |  |  |  | F |  | $\uparrow$ |  |
| Traffic Vol, veh/h | 0 | 1708 | 242 | 0 | 0 | 0 | 0 | 0 | 314 | 0 | 133 | 0 |
| Future Vol, veh/h | 0 | 1708 | 242 | 0 | 0 | 0 | 0 | 0 | 314 | 0 | 133 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control F | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | Yield | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | 125 | - | - | - | - | - | 0 | - | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | - | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 1898 | 269 | 0 | 0 | 0 | 0 | 0 | 349 | 0 | 148 | 0 |


| Major/Minor | Major1 | Minor1 |  |  |  |  |  |  |  |
| :--- | :---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Conflicting Flow All | - | 0 | 0 | - | - | 949 | -1898 | - |  |
| Stage 1 | - | - | - | - | - | - | - | 0 | - |
| Stage 2 | - | - | - | - | - | - | - | 1898 | - |
| Critical Hdwy | - | - | - | - | - | 6.94 | - | 6.54 | - |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | - | 5.54 | - |
| Follow-up Hdwy | - | - | - | - | - | 3.32 | - | 4.02 | - |
| Pot Cap-1 Maneuver | 0 | - | - | 0 | 0 | $\sim 261$ | 0 | $\sim 69$ | 0 |
| Stage 1 | 0 | - | - | 0 | 0 | - | 0 | - | 0 |
| Stage 2 | 0 | - | - | 0 | 0 | - | 0 | $\sim 116$ | 0 |

Platoon blocked, \%

| Mov Cap-1 Maneuver | - | - | - | - | $-\sim 261$ | - | $\sim 69$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | - |

Stage 2 - $\quad$ - $\quad$ - $\quad-\quad$ - 116

| Approach | EB | NB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0 | 213 | $\$ 655$ |
| HCM LOS |  | $F$ | $F$ |


| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR SBLn1 |
| :--- | ---: | ---: | ---: |
| Capacity (veh/h) | 261 | - | - |
| HCM Lane V/C Ratio | 1.337 | - | -2.142 |
| HCM Control Delay (s) | 213 | - | $-\$ 655$ |
| HCM Lane LOS | F | - | - |
| HCM 95th \%tile Q(veh) | 18.2 | - | -13.8 |

## Notes

~: Volume exceeds capacity $\$$ : Delay exceeds 300s $\quad+$ : Computation Not Defined *: All major volume in platoon

|  | $\checkmark$ |  |  |  |  |  |  | $\uparrow$ |  |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ¢个 | 7 |  |  |  |  |  | 7 |  | $\uparrow$ |  |
| Trafic Volume (vph) | 0 | 812 | 161 | 0 | 0 | 0 | 0 | 0 | 380 | 0 | 131 | 0 |
| Future Volume (vph) | 0 | 812 | 161 | 0 | 0 | 0 | 0 | 0 | 380 | 0 | 131 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 0 |  | 125 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 0 |  | 1 | 0 |  | 0 | 0 |  | 1 | 0 |  | 0 |
| Taper Length (ft) | 100 |  |  | 100 |  |  | 100 |  |  | 100 |  |  |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  |  | 0.850 |  |  |  |  |  | 0.865 |  |  |  |
| Flt Protected |  |  |  |  |  |  |  |  |  |  |  |  |
| Satd. Flow (prot) | 0 | 3539 | 1583 | 0 | 0 | 0 | 0 | 0 | 1611 | 0 | 1863 | 0 |
| Flt Permitted |  |  |  |  |  |  |  |  |  |  |  |  |
| Satd. Flow (perm) | 0 | 3539 | 1583 | 0 | 0 | 0 | 0 | 0 | 1611 | 0 | 1863 | 0 |
| Right Turn on Red |  |  | No |  |  | No |  |  | No | No |  | No |
| Satd. Flow (RTOR) |  |  |  |  |  |  |  |  |  |  |  |  |
| Link Speed (mph) |  | 55 |  |  | 55 |  |  | 35 |  |  | 45 |  |
| Link Distance (ft) |  | 278 |  |  | 727 |  |  | 1295 |  |  | 275 |  |
| Travel Time (s) |  | 3.4 |  |  | 9.0 |  |  | 25.2 |  |  | 4.2 |  |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 0 | 902 | 179 | 0 | 0 | 0 | 0 | 0 | 422 | 0 | 146 | 0 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 902 | 179 | 0 | 0 | 0 | 0 | 0 | 422 | 0 | 146 | 0 |
| Turn Type |  | NA | Perm |  |  |  |  |  | Prot |  | NA |  |
| Protected Phases |  | 2 |  |  |  |  |  |  | 4 |  | 4 |  |
| Permitted Phases |  |  | 2 |  |  |  |  |  |  |  |  |  |
| Detector Phase |  | 2 | 2 |  |  |  |  |  | 4 |  | 4 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial ( s ) |  | 14.0 | 14.0 |  |  |  |  |  | 7.0 |  | 7.0 |  |
| Minimum Split (s) |  | 21.0 | 21.0 |  |  |  |  |  | 14.0 |  | 14.0 |  |
| Total Split (s) |  | 28.0 | 28.0 |  |  |  |  |  | 32.0 |  | 32.0 |  |
| Total Split (\%) |  | 46.7\% | 46.7\% |  |  |  |  |  | 53.3\% |  | 53.3\% |  |
| Maximum Green (s) |  | 21.0 | 21.0 |  |  |  |  |  | 25.0 |  | 25.0 |  |
| Yellow Time (s) |  | 5.0 | 5.0 |  |  |  |  |  | 5.0 |  | 5.0 |  |
| All-Red Time (s) |  | 2.0 | 2.0 |  |  |  |  |  | 2.0 |  | 2.0 |  |
| Lost Time Adjust (s) |  | -2.0 | -2.0 |  |  |  |  |  | -2.0 |  | -2.0 |  |
| Total Lost Time (s) |  | 5.0 | 5.0 |  |  |  |  |  | 5.0 |  | 5.0 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) |  | 3.0 | 3.0 |  |  |  |  |  | 3.0 |  | 3.0 |  |
| Recall Mode |  | None | None |  |  |  |  |  | Min |  | Min |  |
| Act Effct Green (s) |  | 20.8 | 20.8 |  |  |  |  |  | 20.4 |  | 20.4 |  |
| Actuated g/C Ratio |  | 0.40 | 0.40 |  |  |  |  |  | 0.40 |  | 0.40 |  |
| $\mathrm{v} / \mathrm{c}$ Ratio |  | 0.63 | 0.28 |  |  |  |  |  | 0.66 |  | 0.20 |  |
| Control Delay |  | 15.5 | 13.2 |  |  |  |  |  | 18.6 |  | 11.0 |  |
| Queue Delay |  | 0.0 | 0.0 |  |  |  |  |  | 0.0 |  | 0.0 |  |
| Total Delay |  | 15.5 | 13.2 |  |  |  |  |  | 18.6 |  | 11.0 |  |
| LOS |  | B | B |  |  |  |  |  | B |  | B |  |
| Approach Delay |  | 15.1 |  |  |  |  |  | 18.6 |  |  | 11.0 |  |
| Approach LOS |  | B |  |  |  |  |  | B |  |  | B |  |


|  | $y$ | $\rightarrow$ |  | $\checkmark$ |  |  |  | $\uparrow$ | $p$ |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Queue Length 50th (ft) |  | 114 | 36 |  |  |  |  |  | 107 |  | 30 |  |
| Queue Length 95th (ft) |  | 194 | 84 |  |  |  |  |  | 187 |  | 59 |  |
| Internal Link Dist (ft) |  | 198 |  |  | 647 |  |  | 1215 |  |  | 195 |  |
| Turn Bay Length (ft) |  |  | 125 |  |  |  |  |  |  |  |  |  |
| Base Capacity (vph) |  | 1629 | 728 |  |  |  |  |  | 870 |  | 1006 |  |
| Starvation Cap Reductn |  | 0 | 0 |  |  |  |  |  | 0 |  | 0 |  |
| Spillback Cap Reductn |  | 0 | 0 |  |  |  |  |  | 0 |  | 0 |  |
| Storage Cap Reductn |  | 0 | 0 |  |  |  |  |  | 0 |  | 0 |  |
| Reduced v/c Ratio |  | 0.55 | 0.25 |  |  |  |  |  | 0.49 |  | 0.15 |  |

## Intersection Summary

Area Type: Other

Cycle Length: 60
Actuated Cycle Length: 51.4
Natural Cycle: 40
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 0.66

| Intersection Signal Delay: 15.6 | Intersection LOS: B |
| :--- | :--- |
| Intersection Capacity Utilization $58.7 \%$ | ICU Level of Service B |
| Analysis Period $(\min ) 15$ |  |

Splits and Phases: 1: Jonesville Road/WB Left-Over \& US 401 Bypass EB


|  | $\checkmark$ |  |  |  |  |  |  | $\uparrow$ |  |  |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 个个 | ${ }^{7}$ |  |  |  |  |  | ${ }^{7}$ |  | $\uparrow$ |  |
| Trafic Volume (vph) | 0 | 1708 | 242 | 0 | 0 | 0 | 0 | 0 | 314 | 0 | 133 | 0 |
| Future Volume (vph) | 0 | 1708 | 242 | 0 | 0 | 0 | 0 | 0 | 314 | 0 | 133 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 0 |  | 125 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 0 |  | 1 | 0 |  | 0 | 0 |  | 1 | 0 |  | 0 |
| Taper Length (ft) | 100 |  |  | 100 |  |  | 100 |  |  | 100 |  |  |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  |  | 0.850 |  |  |  |  |  | 0.865 |  |  |  |
| Flt Protected |  |  |  |  |  |  |  |  |  |  |  |  |
| Satd. Flow (prot) | 0 | 3539 | 1583 | 0 | 0 | 0 | 0 | 0 | 1611 | 0 | 1863 | 0 |
| Flt Permitted |  |  |  |  |  |  |  |  |  |  |  |  |
| Satd. Flow (perm) | 0 | 3539 | 1583 | 0 | 0 | 0 | 0 | 0 | 1611 | 0 | 1863 | 0 |
| Right Turn on Red |  |  | No |  |  | No |  |  | No | No |  | No |
| Satd. Flow (RTOR) |  |  |  |  |  |  |  |  |  |  |  |  |
| Link Speed (mph) |  | 55 |  |  | 55 |  |  | 35 |  |  | 45 |  |
| Link Distance (ft) |  | 278 |  |  | 727 |  |  | 1295 |  |  | 275 |  |
| Travel Time (s) |  | 3.4 |  |  | 9.0 |  |  | 25.2 |  |  | 4.2 |  |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 0 | 1898 | 269 | 0 | 0 | 0 | 0 | 0 | 349 | 0 | 148 | 0 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 1898 | 269 | 0 | 0 | 0 | 0 | 0 | 349 | 0 | 148 | 0 |
| Turn Type |  | NA | Perm |  |  |  |  |  | Prot |  | NA |  |
| Protected Phases |  | 2 |  |  |  |  |  |  | 4 |  | 4 |  |
| Permitted Phases |  |  | 2 |  |  |  |  |  |  |  |  |  |
| Detector Phase |  | 2 | 2 |  |  |  |  |  | 4 |  | 4 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial ( s ) |  | 14.0 | 14.0 |  |  |  |  |  | 7.0 |  | 7.0 |  |
| Minimum Split (s) |  | 21.0 | 21.0 |  |  |  |  |  | 14.0 |  | 14.0 |  |
| Total Split (s) |  | 40.0 | 40.0 |  |  |  |  |  | 20.0 |  | 20.0 |  |
| Total Split (\%) |  | 66.7\% | 66.7\% |  |  |  |  |  | 33.3\% |  | 33.3\% |  |
| Maximum Green (s) |  | 33.0 | 33.0 |  |  |  |  |  | 13.0 |  | 13.0 |  |
| Yellow Time (s) |  | 5.0 | 5.0 |  |  |  |  |  | 5.0 |  | 5.0 |  |
| All-Red Time (s) |  | 2.0 | 2.0 |  |  |  |  |  | 2.0 |  | 2.0 |  |
| Lost Time Adjust (s) |  | -2.0 | -2.0 |  |  |  |  |  | -2.0 |  | -2.0 |  |
| Total Lost Time (s) |  | 5.0 | 5.0 |  |  |  |  |  | 5.0 |  | 5.0 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) |  | 3.0 | 3.0 |  |  |  |  |  | 3.0 |  | 3.0 |  |
| Recall Mode |  | None | None |  |  |  |  |  | Min |  | Min |  |
| Act Effct Green (s) |  | 35.0 | 35.0 |  |  |  |  |  | 15.0 |  | 15.0 |  |
| Actuated g/C Ratio |  | 0.58 | 0.58 |  |  |  |  |  | 0.25 |  | 0.25 |  |
| $\mathrm{v} / \mathrm{c}$ Ratio |  | 0.92 | 0.29 |  |  |  |  |  | 0.87 |  | 0.32 |  |
| Control Delay |  | 20.8 | 7.3 |  |  |  |  |  | 46.6 |  | 20.6 |  |
| Queue Delay |  | 0.0 | 0.0 |  |  |  |  |  | 0.0 |  | 0.0 |  |
| Total Delay |  | 20.8 | 7.3 |  |  |  |  |  | 46.6 |  | 20.6 |  |
| LOS |  | C | A |  |  |  |  |  | D |  | C |  |
| Approach Delay |  | 19.1 |  |  |  |  |  | 46.6 |  |  | 20.6 |  |
| Approach LOS |  | B |  |  |  |  |  | D |  |  | C |  |


| $y$ |  |  |  |  |  |  | $\uparrow$ | $p$ |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Queue Length 50th (ft) | 285 | 43 |  |  |  |  |  | 121 |  | 44 |  |
| Queue Length 95th (ft) | \#481 | 78 |  |  |  |  |  | \#254 |  | 87 |  |
| Internal Link Dist (ft) | 198 |  |  | 647 |  |  | 1215 |  |  | 195 |  |
| Turn Bay Length (ft) |  | 125 |  |  |  |  |  |  |  |  |  |
| Base Capacity (vph) | 2064 | 923 |  |  |  |  |  | 402 |  | 465 |  |
| Starvation Cap Reductn | 0 | 0 |  |  |  |  |  | 0 |  | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  |  |  |  |  | 0 |  | 0 |  |
| Storage Cap Reductn | 0 | 0 |  |  |  |  |  | 0 |  | 0 |  |
| Reduced v/c Ratio | 0.92 | 0.29 |  |  |  |  |  | 0.87 |  | 0.32 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other | Other |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 60 |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 60 |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 60 |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Uncoordinated |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.92 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 22.8 |  |  | Intersection LOS: C |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 75.0\% |  |  | ICU Level of Service D |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer.Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 1: Jonesville Road/WB Left-Over \& US 401 Bypass EB


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 6 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  | 个1 | T |  | $\uparrow$ |  |  |  | $\overline{7}$ |
| Traffic Vol, veh/h | 0 | 0 | 0 | 0 | 1352 | 185 | 0 | 36 | 0 | 0 | 0 | 225 |
| Future Vol, veh/h | 0 | 0 | 0 | 0 | 1352 | 185 | 0 | 36 | 0 | 0 | 0 | 225 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control Stop | Stop | Stop | Stop | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | , | None |
| Storage Length | - | - | - | - | - | 150 | - | - | - | - | - | 0 |
| Veh in Median Storage, \# | \# | 1 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 0 | 0 | 0 | 1502 | 206 | 0 | 40 | 0 | 0 | 0 | 250 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 4.3 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |  |
| Lane Configurations |  |  |  |  | 14 | 7 |  | $\uparrow$ |  |  |  | F |  |
| Traffic Vol, veh/h | 0 | 0 | 0 | 0 | 555 | 74 | 0 | 116 | 0 | 0 | 0 | 114 |  |
| Future Vol, veh/h | 0 | 0 | 0 | 0 | 555 | 74 | 0 | 116 | 0 | 0 | 0 | 114 |  |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Sign Control Stop | Stop | Stop | Stop | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |  |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |  |
| Storage Length | - | - | - | - | - | 150 | - | - | - | - | - | 0 |  |
| Veh in Median Storage, \# | \# | 1 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |  |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |  |
| Mvmt Flow | 0 | 0 | 0 | 0 | 617 | 82 | 0 | 129 | 0 | 0 | 0 | 127 |  |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 15.1 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  | 个1 | F |  | $\uparrow$ |  |  |  | F |
| Traffic Vol, veh/h | 0 | 0 | 0 | 0 | 1797 | 185 | 0 | 36 | 0 | 0 | 0 | 225 |
| Future Vol, veh/h | 0 | 0 | 0 | 0 | 1797 | 185 | 0 | 36 | 0 | 0 | 0 | 225 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control S | Stop | Stop | Stop | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | 150 | - | - | - | - | - | 0 |
| Veh in Median Storage, \# | \# | 1 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 0 | 0 | 0 | 1997 | 206 | 0 | 40 | 0 | 0 | 0 | 250 |


| Major/Minor |  |  | Major2 |  |  |  |  | Minor1 |  |  | Minor2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All |  |  | - |  | - |  | 0 | - | 2203 | - | - | - | 999 |  |
| Stage 1 |  |  | - |  | - | - | - | - | 0 | - | - | - | - |  |
| Stage 2 |  |  | - |  | - |  | - | - | 2203 | - | - | - | - |  |
| Critical Hdwy |  |  | - |  | - |  | - | - | 6.54 | - | - | - | 6.94 |  |
| Critical Hdwy Stg 1 |  |  |  |  | - | - | - | - | - | - | - | - | - |  |
| Critical Hdwy Stg 2 |  |  | - |  | - |  | - | - | 5.54 | - | - | - | - |  |
| Follow-up Hdwy |  |  | - |  | - | - | - | - | 4.02 | - | - | - | 3.32 |  |
| Pot Cap-1 Maneuver |  |  | 0 |  | - |  | - | 0 | 44 | 0 | 0 | 0 | $\sim 242$ |  |
| Stage 1 |  |  | 0 |  | - | - | - | 0 | - | 0 | 0 | 0 | - |  |
| Stage 2 |  |  | 0 |  | - | - | - | 0 | 81 | 0 | 0 | 0 | - |  |
| Platoon blocked, \% |  |  |  |  | - | - | - |  |  |  |  |  |  |  |
| Mov Cap-1 Maneuver |  |  | - |  | - |  | - | - | 44 | - | - | - | ~ 242 |  |
| Mov Cap-2 Maneuver |  |  | - |  | - |  | - | - | 44 | - | - | - | - |  |
| Stage 1 |  |  | - |  | - | - | - | - | - | - | - | - | - |  |
| Stage 2 |  |  |  | - |  | - | - | - | 81 | - | - | - | - |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Approach |  |  | WB |  |  |  |  | NB |  |  | SB |  |  |  |
| HCM Control Delay, s |  |  | 0 | 0 |  |  |  | 250.5 |  |  | 110.8 |  |  |  |
| HCM LOS |  |  |  |  |  |  |  | F |  |  | F |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt | NBLn1 | WBT | WBR | SB | Ln1 |  |  |  |  |  |  |  |  |  |
| Capacity (veh/h) | 44 | - | - | - | 242 |  |  |  |  |  |  |  |  |  |
| HCM Lane V/C Ratio | 0.909 | - | - | - 1. | . 033 |  |  |  |  |  |  |  |  |  |
| HCM Control Delay (s) | 250.5 | - |  |  | 10.8 |  |  |  |  |  |  |  |  |  |
| HCM Lane LOS | F | - | - | - | F |  |  |  |  |  |  |  |  |  |
| HCM 95th \%tile Q(veh) | 3.6 | - | - | - | 10.2 |  |  |  |  |  |  |  |  |  |
| Notes |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $\sim$ : Volume exceeds capacity | \$: Delay exceeds 300s |  |  |  |  | +: Computation Not Defined |  |  |  |  | *: All major volume in platoon |  |  |  |

[^0]Synchro 11 Report



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 15.8 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  |  | 个4 | F |  | $\uparrow$ |  |  |  | T |
| Traffic Vol, veh/h | 0 | 0 | 0 | 0 | 1817 | 185 | 0 | 36 | 0 | 0 | 0 | 225 |
| Future Vol, veh/h | 0 | 0 | 0 | 0 | 1817 | 185 | 0 | 36 | 0 | 0 | 0 | 225 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | 150 | - | - | - | - | - | 0 |
| Veh in Median Storage, \# | \# 147 | 45600 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 0 | 0 | 0 | 2019 | 206 | 0 | 40 | 0 | 0 | 0 | 250 |


| Major/Minor | Major2 |  | Minor1 |  |  | Minor2 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | - | - | 0 | - | 2225 | - | - | - | 1010 |  |
| Stage 1 | - | - | - | - | 0 | - | - | - | - |  |
| Stage 2 | - | - | - | - | 2225 | - | - | - | - |  |
| Critical Hdwy | - | - | - | - | 6.54 | - | - | - | 6.94 |  |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | - | - | - |  |
| Critical Hdwy Stg 2 | - | - | - | - | 5.54 | - | - | - | - |  |
| Follow-up Hdwy | - | - | - | - | 4.02 | - | - | - | 3.32 |  |
| Pot Cap-1 Maneuver | 0 | - | - | 0 | 43 | 0 | 0 | 0 | $\sim 238$ |  |
| Stage 1 | 0 | - | - | 0 | - | 0 | 0 | 0 | ~ |  |
| Stage 2 | 0 | - | - | 0 | 79 | 0 | 0 | 0 | - |  |
| Platoon blocked, \% |  | - | - |  |  |  |  |  |  |  |
| Mov Cap-1 Maneuver | - | - | - | - | 43 | - | - | - | ~ 238 |  |
| Mov Cap-2 Maneuver | - | - | - | - | 43 | - | - | - | - |  |
| Stage 1 | - | - | - | - | - | - | - | - | - |  |
| Stage 2 | - | - | - | - | 79 | - | - | - | - |  |


| Approach | WB | NB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0 | 260.9 | 116.8 |
| HCM LOS |  | F | F |


| Minor Lane/Major Mvmt | NBLn1 | WBT | WBR SBLn1 |  |
| :--- | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 43 | - | -238 |  |
| HCM Lane V/C Ratio | 0.93 | - | -1.05 |  |
| HCM Control Delay (s) | 260.9 | - | -116.8 |  |
| HCM Lane LOS | F | - | - | F |
| HCM 95th \%tile Q(veh) | 3.7 | - | -10.5 |  |

## Notes

~: Volume exceeds capacity $\$$ : Delay exceeds 300s $\quad+$ : Computation Not Defined *: All major volume in platoon



## APPENDIX E

## CAPACITY ANALYSIS CALCULATIONS US 401 BYPASS <br> \&

EASTERN U-TURN LOCATION

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.3 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations |  |  |  | 个个 | T |  |
| Traffic Vol, veh/h | 0 | 0 | 0 | 1532 | 91 | 0 |
| Future Vol, veh/h | 0 | 0 | 0 | 1532 | 91 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 2 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 0 | 0 | 1702 | 101 | 0 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.1 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations |  |  |  | 个个 | F |  |
| Traffic Vol, veh/h | 0 | 0 | 0 | 600 | 66 | 0 |
| Future Vol, veh/h | 0 | 0 | 0 | 600 | 66 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 2 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 0 | 0 | 667 | 73 | 0 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 16.8 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations |  |  |  | 个个 | T |  |
| Traffic Vol, veh/h | 0 | 0 | 0 | 1877 | 233 | 0 |
| Future Vol, veh/h | 0 | 0 | 0 | 1877 | 233 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 2 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 0 | 0 | 2086 | 259 | 0 |


| Major/Minor | Major2 | Minor1 |  |
| :--- | ---: | ---: | :--- |
| Conflicting Flow All | - | - | 1043 |
| $\quad$ Stage 1 | - | - | - |
| $\quad$ Stage 2 | - | -1043 | - |
| Critical Hdwy | - | - | 6.84 |
| Critical Hdwy Stg 1 | - | - | - |
| Critical Hdwy Stg 2 | - | - | - |
| Follow-up Hdwy | - | - | - |
| Pot Cap-1 Maneuver | 0 | - | - |
| $\quad$ Stage 1 | 0 | - | - |
| $\quad$ Stage 2 | 0 | - | - |
| Platoon blocked, \% |  | - | 0 |
| Mov Cap-1 Maneuver | - | $-\sim 225$ | - |
| Mov Cap-2 Maneuver | - | $-\sim 225$ | - |
| $\quad$ Stage 1 | - | - | - |
| Stage 2 | - | - | - |
|  |  |  |  |


| Approach | WB | NB |
| :--- | ---: | ---: |
| HCM Control Delay, s | 0 | 152 |
| HCM LOS |  | F |


| Minor Lane/Major Mvmt | NBLn1 | WBT |
| :--- | ---: | :--- |
| Capacity (veh/h) | 225 | - |
| HCM Lane V/C Ratio | 1.151 | - |
| HCM Control Delay (s) | 152 | - |
| HCM Lane LOS | F | - |
| HCM 95th \%tile Q(veh) | 12.2 | - |

## Notes

~: Volume exceeds capacity $\$$ : Delay exceeds 300s $\quad+$ : Computation Not Defined $\quad$ : All major volume in platoon

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.7 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations |  |  |  | 个个 | T |  |
| Traffic Vol, veh/h | 0 | 0 | 0 | 915 | 175 | 0 |
| Future Vol, veh/h | 0 | 0 | 0 | 915 | 175 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 2 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 0 | 0 | 1017 | 194 | 0 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 22.5 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations |  |  |  | 个个 | T |  |
| Traffic Vol, veh/h | 0 | 0 | 0 | 1880 | 253 | 0 |
| Future Vol, veh/h | 0 | 0 | 0 | 1880 | 253 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 0 | 0 | 2089 | 281 | 0 |



[^1]Synchro 11 Report

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 3 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations |  |  |  | 个T | T |  |
| Traffic Vol, veh/h | 0 | 0 | 0 | 926 | 188 | 0 |
| Future Vol, veh/h | 0 | 0 | 0 | 926 | 188 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 0 | 0 | 1029 | 209 | 0 |





Splits and Phases: 2: Eastern U-Turn \& US 401 Bypass WB


|  | $\rightarrow$ |  |  |  | 4 | $p$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations |  |  |  | 个4 | \% |  |
| Traffic Volume (vph) | 0 | 0 | 0 | 926 | 188 | 0 |
| Future Volume (vph) | 0 | 0 | 0 | 926 | 188 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Frt |  |  |  |  |  |  |
| Flt Protected |  |  |  |  | 0.950 |  |
| Satd. Flow (prot) | 0 | 0 | 0 | 3539 | 1770 | 0 |
| Flt Permitted |  |  |  |  | 0.950 |  |
| Satd. Flow (perm) | 0 | 0 | 0 | 3539 | 1770 | 0 |
| Right Turn on Red |  | No |  |  | No | No |
| Satd. Flow (RTOR) |  |  |  |  |  |  |
| Link Speed (mph) | 55 |  |  | 55 | 45 |  |
| Link Distance (ft) | 520 |  |  | 1076 | 100 |  |
| Travel Time (s) | 6.4 |  |  | 13.3 | 1.5 |  |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 0 | 0 | 0 | 1029 | 209 | 0 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 0 | 0 | 1029 | 209 | 0 |
| Turn Type |  |  |  | NA | Prot |  |
| Protected Phases |  |  |  | 6 | 8 |  |
| Permitted Phases |  |  |  |  |  |  |
| Detector Phase |  |  |  | 6 | 8 |  |
| Switch Phase |  |  |  |  |  |  |
| Minimum Initial (s) |  |  |  | 14.0 | 7.0 |  |
| Minimum Split (s) |  |  |  | 21.0 | 14.0 |  |
| Total Split (s) |  |  |  | 38.0 | 22.0 |  |
| Total Split (\%) |  |  |  | 63.3\% | 36.7\% |  |
| Maximum Green (s) |  |  |  | 31.0 | 15.0 |  |
| Yellow Time (s) |  |  |  | 5.0 | 5.0 |  |
| All-Red Time (s) |  |  |  | 2.0 | 2.0 |  |
| Lost Time Adjust (s) |  |  |  | -2.0 | -2.0 |  |
| Total Lost Time (s) |  |  |  | 5.0 | 5.0 |  |
| Lead/Lag |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |
| Vehicle Extension (s) |  |  |  | 3.0 | 3.0 |  |
| Recall Mode |  |  |  | None | Min |  |
| Act Effct Green (s) |  |  |  | 22.7 | 12.7 |  |
| Actuated g/C Ratio |  |  |  | 0.50 | 0.28 |  |
| v/c Ratio |  |  |  | 0.59 | 0.42 |  |
| Control Delay |  |  |  | 9.9 | 17.9 |  |
| Queue Delay |  |  |  | 0.0 | 0.0 |  |
| Total Delay |  |  |  | 9.9 | 17.9 |  |
| LOS |  |  |  | A | B |  |
| Approach Delay |  |  |  | 9.9 | 17.9 |  |
| Approach LOS |  |  |  | A | B |  |
| Queue Length 50th (ft) |  |  |  | 87 | 43 |  |
| Queue Length 95th (ft) |  |  |  | 157 | 111 |  |
| Internal Link Dist (ft) | 440 |  |  | 996 | 20 |  |



Splits and Phases: 2: Eastern U-Turn \& US 401 Bypass WB


## APPENDIX F

## CAPACITY ANALYSIS CALCULATIONS MITCHELL MILL ROAD <br> \&

JONESVILLE ROAD / PEEBLES ROAD

| Intersection |  |
| :--- | ---: | :--- |
| Intersection Delay, s/veh | 12.7 |
| Intersection LOS | B |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | 4 |  |  | * |  |  | \& |  |  | * |  |
| Traffic Vol, veh/h | 7 | 166 | 2 | 11 | 316 | 41 | 4 | 78 | 11 | 32 | 133 | 16 |
| Future Vol, veh/h | 7 | 166 | 2 | 11 | 316 | 41 | 4 | 78 | 11 | 32 | 133 | 16 |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 8 | 184 | 2 | 12 | 351 | 46 | 4 | 87 | 12 | 36 | 148 | 18 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 10.8 |  |  | 14.8 |  |  | 10.1 |  |  | 11.4 |  |  |
| HCM LOS | B |  |  | B |  |  | B |  |  | B |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $4 \%$ | $4 \%$ | $3 \%$ | $18 \%$ |
| Vol Thru, \% | $84 \%$ | $95 \%$ | $86 \%$ | $73 \%$ |
| Vol Right, \% | $12 \%$ | $1 \%$ | $11 \%$ | $9 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 93 | 175 | 368 | 181 |
| LT Vol | 4 | 7 | 11 | 32 |
| Through Vol | 78 | 166 | 316 | 133 |
| RT Vol | 11 | 2 | 41 | 16 |
| Lane Flow Rate | 103 | 194 | 409 | 201 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.168 | 0.294 | 0.576 | 0.318 |
| Departure Headway (Hd) | 5.843 | 5.438 | 5.074 | 5.691 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 612 | 659 | 711 | 631 |
| Service Time | 3.897 | 3.483 | 3.111 | 3.736 |
| HCM Lane V/C Ratio | 0.168 | 0.294 | 0.575 | 0.319 |
| HCM Control Delay | 10.1 | 10.8 | 14.8 | 11.4 |
| HCM Lane LOS | B | B | B | B |
| HCM 95th-tile Q | 0.6 | 1.2 | 3.7 | 1.4 |


| Intersection |  |
| :--- | ---: | :--- |
| Intersection Delay, s/veh | 10.8 |
| Intersection LOS | B |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | \& |  |  | * |  |  | \& |  |  | * |  |
| Traffic Vol, veh/h | 18 | 306 | 13 | 0 | 130 | 21 | 5 | 92 | 10 | 27 | 50 | 11 |
| Future Vol, veh/h | 18 | 306 | 13 | 0 | 130 | 21 | 5 | 92 | 10 | 27 | 50 | 11 |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 20 | 340 | 14 | 0 | 144 | 23 | 6 | 102 | 11 | 30 | 56 | 12 |
| Number of Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Approach | EB |  |  |  | WB |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  |  | EB |  | SB |  |  | NB |  |  |
| Opposing Lanes | 1 |  |  |  | 1 |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  |  | NB |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 1 |  |  |  | 1 |  | 1 |  |  | 1 |  |  |
| Conflicting Approach Right | NB |  |  |  | SB |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  |  | 1 |  | 1 |  |  | 1 |  |  |
| HCM Control Delay | 12.2 |  |  |  | 9.4 |  | 9.5 |  |  | 9.4 |  |  |
| HCM LOS | B |  |  |  | A |  | A |  |  | A |  |  |


| Lane | NBLn1 | EBLn1 | WBLn1 | SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $5 \%$ | $5 \%$ | $0 \%$ | $31 \%$ |
| Vol Thru, \% | $86 \%$ | $91 \%$ | $86 \%$ | $57 \%$ |
| Vol Right, \% | $9 \%$ | $4 \%$ | $14 \%$ | $12 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 107 | 337 | 151 | 88 |
| LT Vol | 5 | 18 | 0 | 27 |
| Through Vol | 92 | 306 | 130 | 50 |
| RT Vol | 10 | 13 | 21 | 11 |
| Lane Flow Rate | 119 | 374 | 168 | 98 |
| Geometry Grp | 1 | 1 | 1 | 1 |
| Degree of Util (X) | 0.175 | 0.488 | 0.227 | 0.146 |
| Departure Headway (Hd) | 5.3 | 4.694 | 4.868 | 5.368 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 669 | 760 | 730 | 660 |
| Service Time | 3.395 | 2.76 | 2.948 | 3.464 |
| HCM Lane V/C Ratio | 0.178 | 0.492 | 0.23 | 0.148 |
| HCM Control Delay | 9.5 | 12.2 | 9.4 | 9.4 |
| HCM Lane LOS | A | B | A | A |
| HCM 95th-tile Q | 0.6 | 2.7 | 0.9 | 0.5 |


| Intersection |  |
| :--- | :---: |
| Intersection Delay, s/veh | 95.4 |
| Intersection LOS | F |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ | $\uparrow$ |  |  | 4 | F |  | 4 |  | \% | $\uparrow$ |  |
| Traffic Vol, veh/h | 63 | 253 | 12 | 29 | 607 | 119 | 12 | 86 | 20 | 84 | 149 | 54 |
| Future Vol, veh/h | 63 | 253 | 12 | 29 | 607 | 119 | 12 | 86 | 20 | 84 | 149 | 54 |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 70 | 281 | 13 | 32 | 674 | 132 | 13 | 96 | 22 | 93 | 166 | 60 |
| Number of Lanes | 1 | 1 | 0 | 0 | 1 | 1 | 0 | 1 | 0 | 1 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 2 |  |  | 2 |  |  | 2 |  |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 2 |  |  | 1 |  |  | 2 |  |  | 2 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 2 |  |  | 2 |  |  | 2 |  |  |
| HCM Control Delay | 19.9 |  |  | 170.3 |  |  | 16.1 |  |  | 17.2 |  |  |
| HCM LOS | C |  |  | F |  |  | C |  |  | C |  |  |


| Lane | NBLn1 | EBLn1 | EBLn2 | WBLn1 | WBLn2 | SBLn1 | SBLn2 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $10 \%$ | $100 \%$ | $0 \%$ | $5 \%$ | $0 \%$ | $100 \%$ | $0 \%$ |
| Vol Thru, \% | $73 \%$ | $0 \%$ | $95 \%$ | $95 \%$ | $0 \%$ | $0 \%$ | $73 \%$ |
| Vol Right, \% | $17 \%$ | $0 \%$ | $5 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $27 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 118 | 63 | 265 | 636 | 119 | 84 | 203 |
| LT Vol | 12 | 63 | 0 | 29 | 0 | 84 | 0 |
| Through Vol | 86 | 0 | 253 | 607 | 0 | 0 | 149 |
| RT Vol | 20 | 0 | 12 | 0 | 119 | 0 | 54 |
| Lane Flow Rate | 131 | 70 | 294 | 707 | 132 | 93 | 226 |
| Geometry Grp | 6 | 7 | 7 | 7 | 7 | 7 | 7 |
| Degree of Util (X) | 0.302 | 0.152 | 0.597 | 1.372 | 0.229 | 0.215 | 0.476 |
| Departure Headway (Hd) | 9.162 | 8.438 | 7.887 | 6.988 | 6.248 | 9.036 | 8.326 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 395 | 428 | 462 | 516 | 570 | 399 | 435 |
| Service Time | 7.162 | 6.138 | 5.587 | 4.777 | 4.036 | 6.736 | 6.026 |
| HCM Lane V/C Ratio | 0.332 | 0.164 | 0.636 | 1.37 | 0.232 | 0.233 | 0.52 |
| HCM Control Delay | 16.1 | 12.6 | 21.6 | 200.1 | 10.9 | 14.2 | 18.4 |
| HCM Lane LOS | C | B | C | F | B | B | C |
| HCM 95th-tile Q | 1.3 | 0.5 | 3.8 | 31.9 | 0.9 | 0.8 | 2.5 |


| Intersection |  |
| :--- | ---: | :--- |
| Intersection Delay, s/veh | 57.2 |
| Intersection LOS | F |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | $\uparrow$ |  |  | 4 | 7 |  | 4 |  | F | $\dagger$ |  |
| Traffic Vol, veh/h | 114 | 459 | 19 | 14 | 387 | 95 | 19 | 106 | 31 | 159 | 65 | 33 |
| Future Vol, veh/h | 114 | 459 | 19 | 14 | 387 | 95 | 19 | 106 | 31 | 159 | 65 | 33 |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 127 | 510 | 21 | 16 | 430 | 106 | 21 | 118 | 34 | 177 | 72 | 37 |
| Number of Lanes | 1 | 1 | 0 | 0 | 1 | 1 | 0 | 1 | 0 | 1 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 2 |  |  | 2 |  |  | 2 |  |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 2 |  |  | 1 |  |  | 2 |  |  | 2 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 2 |  |  | 2 |  |  | 2 |  |  |
| HCM Control Delay | 90.6 |  |  | 50 |  |  | 19.2 |  |  | 17.4 |  |  |
| HCM LOS | F |  |  | E |  |  | C |  |  | C |  |  |


| Lane | NBLn1 | EBLn1 | EBLn2 | WBLn1 | WBLn2 | SBLn1 | SBLn2 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $12 \%$ | $100 \%$ | $0 \%$ | $3 \%$ | $0 \%$ | $100 \%$ | $0 \%$ |
| Vol Thru, \% | $68 \%$ | $0 \%$ | $96 \%$ | $97 \%$ | $0 \%$ | $0 \%$ | $66 \%$ |
| Vol Right, \% | $20 \%$ | $0 \%$ | $4 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $34 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 156 | 114 | 478 | 401 | 95 | 159 | 98 |
| LT Vol | 19 | 114 | 0 | 14 | 0 | 159 | 0 |
| Through Vol | 106 | 0 | 459 | 387 | 0 | 0 | 65 |
| RT Vol | 31 | 0 | 19 | 0 | 95 | 0 | 33 |
| Lane Flow Rate | 173 | 127 | 531 | 446 | 106 | 177 | 109 |
| Geometry Grp | 6 | 7 | 7 | 7 | 7 | 7 | 7 |
| Degree of Util (X) | 0.429 | 0.289 | 1.13 | 0.95 | 0.204 | 0.443 | 0.251 |
| Departure Headway (Hd) | 9.353 | 8.206 | 7.661 | 7.994 | 7.251 | 9.428 | 8.662 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 388 | 438 | 473 | 459 | 498 | 385 | 417 |
| Service Time | 7.353 | 5.959 | 5.414 | 5.694 | 4.951 | 7.128 | 6.362 |
| HCM Lane V/C Ratio | 0.446 | 0.29 | 1.123 | 0.972 | 0.213 | 0.46 | 0.261 |
| HCM Control Delay | 19.2 | 14.3 | 108.8 | 59 | 11.8 | 19.4 | 14.2 |
| HCM Lane LOS | C | B | F | F | B | C | B |
| HCM 95th-tile Q | 2.1 | 1.2 | 18.4 | 11.3 | 0.8 | 2.2 | 1 |


| Intersection |  |
| :--- | :---: |
| Intersection Delay, s/veh $\quad 104$ |  |
| Intersection LOS | F |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | $\dagger$ |  |  | \$ | T |  | 4 |  | \% | $\dagger$ |  |
| Traffic Vol, veh/h | 71 | 253 | 12 | 29 | 607 | 121 | 12 | 88 | 20 | 91 | 156 | 76 |
| Future Vol, veh/h | 71 | 253 | 12 | 29 | 607 | 121 | 12 | 88 | 20 | 91 | 156 | 76 |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 79 | 281 | 13 | 32 | 674 | 134 | 13 | 98 | 22 | 101 | 173 | 84 |
| Number of Lanes | 1 | 1 | 0 | 0 | 1 | 1 | 0 | 1 | 0 | 1 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 2 |  |  | 2 |  |  | 2 |  |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 2 |  |  | 1 |  |  | 2 |  |  | 2 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 2 |  |  | 2 |  |  | 2 |  |  |
| HCM Control Delay | 20.8 |  |  | 191.1 |  |  | 16.7 |  |  | 19 |  |  |
| HCM LOS | C |  |  | F |  |  | C |  |  | C |  |  |


| Lane | NBLn1 | EBLn1 | EBLn2 | WBLn1 | WBLn2 | SBLn1 | SBLn2 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $10 \%$ | $100 \%$ | $0 \%$ | $5 \%$ | $0 \%$ | $100 \%$ | $0 \%$ |
| Vol Thru, \% | $73 \%$ | $0 \%$ | $95 \%$ | $95 \%$ | $0 \%$ | $0 \%$ | $67 \%$ |
| Vol Right, \% | $17 \%$ | $0 \%$ | $5 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $33 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 120 | 71 | 265 | 636 | 121 | 91 | 232 |
| LT Vol | 12 | 71 | 0 | 29 | 0 | 91 | 0 |
| Through Vol | 88 | 0 | 253 | 607 | 0 | 0 | 156 |
| RT Vol | 20 | 0 | 12 | 0 | 121 | 0 | 76 |
| Lane Flow Rate | 133 | 79 | 294 | 707 | 134 | 101 | 258 |
| Geometry Grp | 6 | 7 | 7 | 7 | 7 | 7 | 7 |
| Degree of Util (X) | 0.313 | 0.176 | 0.611 | 1.43 | 0.244 | 0.234 | 0.545 |
| Departure Headway (Hd) | 9.455 | 8.699 | 8.147 | 7.283 | 6.541 | 9.17 | 8.414 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 383 | 415 | 448 | 502 | 553 | 394 | 430 |
| Service Time | 7.455 | 6.399 | 5.847 | 4.983 | 4.241 | 6.87 | 6.114 |
| HCM Lane V/C Ratio | 0.347 | 0.19 | 0.656 | 1.408 | 0.242 | 0.256 | 0.6 |
| HCM Control Delay | 16.7 | 13.2 | 22.8 | 225.3 | 11.3 | 14.6 | 20.7 |
| HCM Lane LOS | C | B | C | F | B | B | C |
| HCM 95th-tile Q | 1.3 | 0.6 | 4 | 34.3 | 1 | 0.9 | 3.2 |


| Intersection |  |
| :--- | ---: |
| Intersection Delay, s/veh | 60.9 |
| Intersection LOS | F |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | 7 | $\dagger$ |  |  | $\uparrow$ | T |  | \& |  | F | $\dagger$ |  |
| Traffic Vol, veh/h | 138 | 459 | 19 | 14 | 387 | 102 | 19 | 113 | 31 | 163 | 69 | 49 |
| Future Vol, veh/h | 138 | 459 | 19 | 14 | 387 | 102 | 19 | 113 | 31 | 163 | 69 | 49 |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 153 | 510 | 21 | 16 | 430 | 113 | 21 | 126 | 34 | 181 | 77 | 54 |
| Number of Lanes | 1 | 1 | 0 | 0 | 1 | 1 | 0 | 1 | 0 | 1 | 1 | 0 |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| Opposing Approach | WB |  |  | EB |  |  | SB |  |  | NB |  |  |
| Opposing Lanes | 2 |  |  | 2 |  |  | 2 |  |  | 1 |  |  |
| Conflicting Approach Left | SB |  |  | NB |  |  | EB |  |  | WB |  |  |
| Conflicting Lanes Left | 2 |  |  | 1 |  |  | 2 |  |  | 2 |  |  |
| Conflicting Approach Right | NB |  |  | SB |  |  | WB |  |  | EB |  |  |
| Conflicting Lanes Right | 1 |  |  | 2 |  |  | 2 |  |  | 2 |  |  |
| HCM Control Delay | 96.6 |  |  | 54.4 |  |  | 20.2 |  |  | 18 |  |  |
| HCM LOS | F |  |  | F |  |  | C |  |  | C |  |  |


| Lane | NBLn1 | EBLn1 | EBLn2 | WBLn1 | WBLn2 | SBLn1 | SBLn2 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $12 \%$ | $100 \%$ | $0 \%$ | $3 \%$ | $0 \%$ | $100 \%$ | $0 \%$ |
| Vol Thru, \% | $69 \%$ | $0 \%$ | $96 \%$ | $97 \%$ | $0 \%$ | $0 \%$ | $58 \%$ |
| Vol Right, \% | $19 \%$ | $0 \%$ | $4 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $42 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 163 | 138 | 478 | 401 | 102 | 163 | 118 |
| LT Vol | 19 | 138 | 0 | 14 | 0 | 163 | 0 |
| Through Vol | 113 | 0 | 459 | 387 | 0 | 0 | 69 |
| RT Vol | 31 | 0 | 19 | 0 | 102 | 0 | 49 |
| Lane Flow Rate | 181 | 153 | 531 | 446 | 113 | 181 | 131 |
| Geometry Grp | 6 | 7 | 7 | 7 | 7 | 7 | 7 |
| Degree of Util (X) | 0.455 | 0.358 | 1.159 | 0.973 | 0.225 | 0.459 | 0.304 |
| Departure Headway (Hd) | 9.533 | 8.403 | 7.857 | 8.211 | 7.466 | 9.559 | 8.735 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 380 | 428 | 462 | 446 | 484 | 379 | 414 |
| Service Time | 7.533 | 6.158 | 5.612 | 5.911 | 5.166 | 7.259 | 6.435 |
| HCM Lane V/C Ratio | 0.476 | 0.357 | 1.149 | 1 | 0.233 | 0.478 | 0.316 |
| HCM Control Delay | 20.2 | 15.8 | 119.9 | 65.1 | 12.3 | 20.1 | 15.2 |
| HCM Lane LOS | C | C | F | F | B | C | C |
| HCM 95th-tile Q | 2.3 | 1.6 | 19.3 | 11.9 | 0.9 | 2.3 | 1.3 |


|  | $\checkmark$ | $\rightarrow$ |  |  |  |  | 4 | $\uparrow$ | $p$ |  | $\downarrow$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | t |  |  | 4 | F |  | 4 |  | 7 | F |  |
| Traffic Volume (vph) | 71 | 253 | 12 | 29 | 607 | 121 | 12 | 88 | 20 | 91 | 156 | 76 |
| Future Volume (vph) | 71 | 253 | 12 | 29 | 607 | 121 | 12 | 88 | 20 | 91 | 156 | 76 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 100 |  | 0 | 0 |  | 100 | 0 |  | 0 | 100 |  | 0 |
| Storage Lanes | 1 |  | 0 | 0 |  | 1 | 0 |  | 0 | 1 |  | 0 |
| Taper Length (ft) | 100 |  |  | 100 |  |  | 100 |  |  | 100 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  | 0.993 |  |  |  | 0.850 |  | 0.978 |  |  | 0.951 |  |
| Flt Protected | 0.950 |  |  |  | 0.998 |  |  | 0.995 |  | 0.950 |  |  |
| Satd. Flow (prot) | 1770 | 1850 | 0 | 0 | 1859 | 1583 | 0 | 1813 | 0 | 1770 | 1771 | 0 |
| Flt Permitted | 0.247 |  |  |  | 0.976 |  |  | 0.946 |  | 0.785 |  |  |
| Satd. Flow (perm) | 460 | 1850 | 0 | 0 | 1818 | 1583 | 0 | 1723 | 0 | 1462 | 1771 | 0 |
| Right Turn on Red |  |  | No |  |  | No |  |  | No |  |  | No |
| Satd. Flow (RTOR) |  |  |  |  |  |  |  |  |  |  |  |  |
| Link Speed (mph) |  | 45 |  |  | 45 |  |  | 45 |  |  | 45 |  |
| Link Distance (ft) |  | 1536 |  |  | 1126 |  |  | 1017 |  |  | 1092 |  |
| Travel Time (s) |  | 23.3 |  |  | 17.1 |  |  | 15.4 |  |  | 16.5 |  |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 79 | 281 | 13 | 32 | 674 | 134 | 13 | 98 | 22 | 101 | 173 | 84 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 79 | 294 | 0 | 0 | 706 | 134 | 0 | 133 | 0 | 101 | 257 | 0 |
| Turn Type | Perm | NA |  | Perm | NA | Perm | Perm | NA |  | Perm | NA |  |
| Protected Phases |  | 2 |  |  | 6 |  |  | 8 |  |  | 4 |  |
| Permitted Phases | 2 |  |  | 6 |  | 6 | 8 |  |  | 4 |  |  |
| Detector Phase | 2 | 2 |  | 6 | 6 | 6 | 8 | 8 |  | 4 | 4 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 12.0 | 12.0 |  | 12.0 | 12.0 | 12.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |  |
| Minimum Split (s) | 19.0 | 19.0 |  | 19.0 | 19.0 | 19.0 | 14.0 | 14.0 |  | 14.0 | 14.0 |  |
| Total Split (s) | 40.0 | 40.0 |  | 40.0 | 40.0 | 40.0 | 20.0 | 20.0 |  | 20.0 | 20.0 |  |
| Total Split (\%) | 66.7\% | 66.7\% |  | 66.7\% | 66.7\% | 66.7\% | 33.3\% | 33.3\% |  | 33.3\% | 33.3\% |  |
| Maximum Green (s) | 33.0 | 33.0 |  | 33.0 | 33.0 | 33.0 | 13.0 | 13.0 |  | 13.0 | 13.0 |  |
| Yellow Time (s) | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| All-Red Time (s) | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 |  |
| Lost Time Adjust (s) | -2.0 | -2.0 |  |  | -2.0 | -2.0 |  | -2.0 |  | -2.0 | -2.0 |  |
| Total Lost Time (s) | 5.0 | 5.0 |  |  | 5.0 | 5.0 |  | 5.0 |  | 5.0 | 5.0 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None | None | Min | Min |  | Min | Min |  |
| Act Effct Green (s) | 26.5 | 26.5 |  |  | 26.5 | 26.5 |  | 13.3 |  | 13.3 | 13.3 |  |
| Actuated g/C Ratio | 0.53 | 0.53 |  |  | 0.53 | 0.53 |  | 0.26 |  | 0.26 | 0.26 |  |
| v/c Ratio | 0.33 | 0.30 |  |  | 0.74 | 0.16 |  | 0.29 |  | 0.26 | 0.55 |  |
| Control Delay | 10.9 | 7.4 |  |  | 14.4 | 6.5 |  | 19.1 |  | 19.1 | 23.0 |  |
| Queue Delay | 0.0 | 0.0 |  |  | 0.0 | 0.0 |  | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 10.9 | 7.4 |  |  | 14.4 | 6.5 |  | 19.1 |  | 19.1 | 23.0 |  |
| LOS | B | A |  |  | B | A |  | B |  | B | C |  |
| Approach Delay |  | 8.2 |  |  | 13.2 |  |  | 19.1 |  |  | 21.9 |  |
| Approach LOS |  | A |  |  | B |  |  | B |  |  | C |  |



Splits and Phases: 3: Peebles Road/Jonesville Road \& Mitchell Mill Road


|  | 4 | $\rightarrow$ | $\checkmark$ | $\checkmark$ |  |  | 4 | $\uparrow$ | $p$ | $\downarrow$ | $\downarrow$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | $\dagger$ |  |  | $\uparrow$ | T |  | \& |  | 7 | $\dagger$ |  |
| Traffic Volume (vph) | 138 | 459 | 19 | 14 | 387 | 102 | 19 | 113 | 31 | 163 | 69 | 49 |
| Future Volume (vph) | 138 | 459 | 19 | 14 | 387 | 102 | 19 | 113 | 31 | 163 | 69 | 49 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 100 |  | 0 | 0 |  | 100 | 0 |  | 0 | 100 |  | 0 |
| Storage Lanes | 1 |  | 0 | 0 |  | 1 | 0 |  | 0 | 1 |  | 0 |
| Taper Length (ft) | 100 |  |  | 100 |  |  | 100 |  |  | 100 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  | 0.994 |  |  |  | 0.850 |  | 0.975 |  |  | 0.938 |  |
| Flt Protected | 0.950 |  |  |  | 0.998 |  |  | 0.994 |  | 0.950 |  |  |
| Satd. Flow (prot) | 1770 | 1852 | 0 | 0 | 1859 | 1583 | 0 | 1805 | 0 | 1770 | 1747 | 0 |
| Flt Permitted | 0.436 |  |  |  | 0.973 |  |  | 0.951 |  | 0.728 |  |  |
| Satd. Flow (perm) | 812 | 1852 | 0 | 0 | 1812 | 1583 | 0 | 1727 | 0 | 1356 | 1747 | 0 |
| Right Turn on Red |  |  | No |  |  | No |  |  | No |  |  | No |
| Satd. Flow (RTOR) |  |  |  |  |  |  |  |  |  |  |  |  |
| Link Speed (mph) |  | 45 |  |  | 45 |  |  | 45 |  |  | 45 |  |
| Link Distance (ft) |  | 1536 |  |  | 1126 |  |  | 1017 |  |  | 1092 |  |
| Travel Time (s) |  | 23.3 |  |  | 17.1 |  |  | 15.4 |  |  | 16.5 |  |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 153 | 510 | 21 | 16 | 430 | 113 | 21 | 126 | 34 | 181 | 77 | 54 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 153 | 531 | 0 | 0 | 446 | 113 | 0 | 181 | 0 | 181 | 131 | 0 |
| Turn Type | Perm | NA |  | Perm | NA | Perm | Perm | NA |  | Perm | NA |  |
| Protected Phases |  | 2 |  |  | 6 |  |  | 8 |  |  | 4 |  |
| Permitted Phases | 2 |  |  | 6 |  | 6 | 8 |  |  | 4 |  |  |
| Detector Phase | 2 | 2 |  | 6 | 6 | 6 | 8 | 8 |  | 4 | 4 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 12.0 | 12.0 |  | 12.0 | 12.0 | 12.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |  |
| Minimum Split (s) | 19.0 | 19.0 |  | 19.0 | 19.0 | 19.0 | 14.0 | 14.0 |  | 14.0 | 14.0 |  |
| Total Split (s) | 36.0 | 36.0 |  | 36.0 | 36.0 | 36.0 | 24.0 | 24.0 |  | 24.0 | 24.0 |  |
| Total Split (\%) | 60.0\% | 60.0\% |  | 60.0\% | 60.0\% | 60.0\% | 40.0\% | 40.0\% |  | 40.0\% | 40.0\% |  |
| Maximum Green (s) | 29.0 | 29.0 |  | 29.0 | 29.0 | 29.0 | 17.0 | 17.0 |  | 17.0 | 17.0 |  |
| Yellow Time (s) | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| All-Red Time (s) | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 |  |
| Lost Time Adjust (s) | -2.0 | -2.0 |  |  | -2.0 | -2.0 |  | -2.0 |  | -2.0 | -2.0 |  |
| Total Lost Time (s) | 5.0 | 5.0 |  |  | 5.0 | 5.0 |  | 5.0 |  | 5.0 | 5.0 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None | None | Min | Min |  | Min | Min |  |
| Act Effct Green (s) | 21.1 | 21.1 |  |  | 21.1 | 21.1 |  | 13.9 |  | 13.9 | 13.9 |  |
| Actuated g/C Ratio | 0.46 | 0.46 |  |  | 0.46 | 0.46 |  | 0.31 |  | 0.31 | 0.31 |  |
| v/c Ratio | 0.41 | 0.62 |  |  | 0.53 | 0.15 |  | 0.34 |  | 0.44 | 0.25 |  |
| Control Delay | 12.4 | 13.1 |  |  | 11.6 | 8.0 |  | 15.8 |  | 18.1 | 14.8 |  |
| Queue Delay | 0.0 | 0.0 |  |  | 0.0 | 0.0 |  | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 12.4 | 13.1 |  |  | 11.6 | 8.0 |  | 15.8 |  | 18.1 | 14.8 |  |
| LOS | B | B |  |  | B | A |  | B |  | B | B |  |
| Approach Delay |  | 12.9 |  |  | 10.9 |  |  | 15.8 |  |  | 16.7 |  |
| Approach LOS |  | B |  |  | B |  |  | B |  |  | B |  |


|  | $y$ |  |  |  |  |  |  | $\uparrow$ | $p$ |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Queue Length 50th ( t ) | 23 | 92 |  |  | 73 | 15 |  | 34 |  | 35 | 24 |  |
| Queue Length 95th (ft) | 68 | 198 |  |  | 160 | 41 |  | 95 |  | 101 | 71 |  |
| Internal Link Dist (ft) |  | 1456 |  |  | 1046 |  |  | 937 |  |  | 1012 |  |
| Turn Bay Length (ft) | 100 |  |  |  |  | 100 |  |  |  | 100 |  |  |
| Base Capacity (vph) | 581 | 1326 |  |  | 1297 | 1133 |  | 758 |  | 595 | 766 |  |
| Starvation Cap Reductn | 0 | 0 |  |  | 0 | 0 |  | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  |  | 0 | 0 |  | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  |  | 0 | 0 |  | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.26 | 0.40 |  |  | 0.34 | 0.10 |  | 0.24 |  | 0.30 | 0.17 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: | her |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 60 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 45.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 40 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Uncoordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.62 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 13.2 |  |  |  | Intersection LOS: B |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 81.0\% |  |  |  | ICU Level of Service D |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 3: Peebles Road/Jonesville Road \& Mitchell Mill Road


## APPENDIX G

## CAPACITY ANALYSIS CALCULATIONS Jonesville Road <br> \& <br> Universal Drive

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |


| Major/Minor | Minor2 | Major1 | Major2 |  |  |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Conflicting Flow All | 707 | 328 | 328 | 0 | - |
| $\quad$ Stage 1 | 328 | - | - | - | - |
| $\quad$ Stage 2 | 379 | - | - | - |  |
| Critical Hdwy | 6.42 | 6.22 | 4.12 | - | - |

HCM LOS B

| Minor Lane/Major Mvmt | NBL | NBT EBLn1 | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1232 | -514 | - | - |  |
| HCM Lane V/C Ratio | 0.001 | -0.013 | - | - |  |
| HCM Control Delay (s) | 7.9 | 0 | 12.1 | - | - |
| HCM Lane LOS | A | A | B | - | - |
| HCM 95th \%tile Q(veh) | 0 | - | 0 | - | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.4 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | M |  |  | - | l |  |
| Traffic Vol, veh/h | 16 | 6 | 2 | 356 | 300 | 5 |
| Future Vol, veh/h | 16 | 6 | 2 | 356 | 300 | 5 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 18 | 7 | 2 | 396 | 333 | 6 |


| Major/Minor | Minor2 |  | Major1 |  | ajor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 736 | 336 | 339 | 0 | - | 0 |
| Stage 1 | 336 | - | - | - | - | - |
| Stage 2 | 400 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | 4.12 | - | - | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | 2.218 | - | - | - |
| Pot Cap-1 Maneuver | 386 | 706 | 1220 | - | - | - |
| Stage 1 | 724 | - | - | - | - | - |
| Stage 2 | 677 | - | - | - | - | - |
| Platoon blocked, \% |  |  |  | - | - | - |
| Mov Cap-1 Maneuver | 385 | 706 | 1220 | - | - | - |
| Mov Cap-2 Maneuver | 385 | - | - | - | - | - |
| Stage 1 | 723 | - | - | - | - | - |
| Stage 2 | 677 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | NB |  | SB |  |
| HCM Control Delay, s | 13.7 |  | 0 |  | 0 |  |
| HCM LOS | B |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBL | NBT EBLn1 |  | SBT | SBR |
| Capacity (veh/h) |  | 1220 | - | 439 | - | - |
| HCM Lane V/C Ratio |  | 0.002 | - | 0.056 | - | - |
| HCM Control Delay (s) |  | 8 | 0 | 13.7 | - | - |
| HCM Lane LOS |  | A | A | B | - | - |
| HCM 95th \%tile Q(veh) |  | 0 | - | 0.2 | - | - |




## APPENDIX H

## CAPACITY ANALYSIS CALCULATIONS Jonesville Road \&

Site Drive

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | 1 |  | 1 | $\uparrow$ | $\mathbf{h}$ |  |
| Traffic Vol, veh/h | 17 | 33 | 11 | 335 | 306 | 6 |
| Future Vol, veh/h | 17 | 33 | 11 | 335 | 306 | 6 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | 50 | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 19 | 37 | 12 | 372 | 340 | 7 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | 1 |  | 1 | $\uparrow$ | $\mathbf{h}$ |  |
| Traffic Vol, veh/h | 11 | 22 | 34 | 308 | 335 | 18 |
| Future Vol, veh/h | 11 | 22 | 34 | 308 | 335 | 18 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | 50 | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 12 | 24 | 38 | 342 | 372 | 20 |



## APPENDIX I

## TURN LANE WARRANTS




Jonesville Road and Site Drive

| 2027 Build |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Peak Hour | Approach | Right Turn <br> Volume | Approach <br> Volume | Warranted? |  |
| AM | Southbound | 6 | 312 | No |  |
| PM | Southbound | 18 | 353 | No |  |



Jonesville Road and Universal Drive

| 2027 Build |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Peak Hour | Approach | Right Turn <br> Volume | Approach <br> Volume | Warranted? |  |
| AM | Southbound | 5 | 305 | No |  |
| PM | Southbound | 17 | 371 | No |  |

## RIGHT TURN LANE WARRANTS



# APPENDIX J 

## MUTCD / ITRE

 SIGNAL WARRANT ANALYSIS
# Traffic Signal Warrant Analysis 

Warrants 1-3 (Volume Warrants)

| Project Name | Harris Creek Farm |
| :--- | :---: |
| Project/ File \# | 20498-09 |
| Scenario | 2027 No-Build |


| Intersection Intormation |  |  |  |
| :--- | :---: | :--- | :---: |
| M ajor Street (E/W Road) | US 401 Bypass | Minor Street (N/SRoad) | Jonesville Road / WB Left-Over |
| Analyzed with | 2 or more approach lanes | Analyzed with | 1 Approach Lane |
| Total Approach Volume | 2895 vehicles | Total Approach Volume | 894 vehicles |
| Total Ped/Bike Volume | 0 crossings | Total Ped/Bike Volume | 0 crossings |
| Right turn reduction of | 0 percent applied | Right turn reduction of | 100 percent applied |

No high speed or isolated community reduction applied to the Volume Warrant thresholds.

| Warrant 1 , Elght Four venicular volume |  |  |  |
| :---: | :---: | :---: | :---: |
|  | Condition A | Condition B | Condition A+B* |
| Condition Satisfied? | Not Satisfied | Not Satisfied | Not Satisfied |
| Required values reached for | 2 hours | 2 hours | 2 (Cond. A) \& 2 (Cond. B) |
| Criteria - M ajor Street (veh/hr) | 420 | 630 | 336 (Cond. A) \& 504 (Cond. B) |
| Criteria - M inor Street (veh/hr) | 105 | 53 | 84 (Cond. A) \& 42 (Cond. B) |

* Should be applied only after an adequate trial of other alternatives that could cause less delay and inconvenience to traffic has failed to solve the traffic problems.

| Warrant 2 , rour hour venicular volume |  |  |
| :---: | :---: | :---: |
|  |  |  |
| Condition Satisfied? | Not Satisfied |  |
| Required values reached for | 2 hours |  |
| Criteria | See Figure Below |  |
|  |  |  |
| Warrant 5, peak four venicular volume |  |  |
|  | Condition A | Condition B |
| Condition Satisfied? | Not Satisfied | Satisfied |
| Required values reached for | 2051 total, 122 minor, 0 delay | 2 hours |
| Criteria - Total Approach Volume (veh in one hour) | 800 | See Figure Below |
| Criteria - M inor Street High Side Volume (veh in one hour) | 100 |  |
| Criteria - M inor Street High Side Delay (veh-hrs) | 4 |  |

Figure 4C-2 (Warrant 2-70\% Factor) \& Figure 4C-4 (Warrant 3-70\% Factor)


# Traffic Signal Warrant Analysis 

Warrants 1-3 (Volume Warrants)

| Project Name | Harris Creek Farm |
| :--- | :---: |
| Project/ File \# | 20498-09 |
| Scenario | 2027 Build |


| Intersection |  |  |  |
| :--- | :---: | :--- | :---: |
| M ajor Street (E/W Road) | US 401 Bypass | Minor Street (N/SRoad) | Jonesville Road / WB Left-Over |
| Analyzed with | 2 or more approach lanes | Analyzed with | 1 Approach Lane |
| Total Approach Volume | 2923 vehicles | Total Approach Volume | 958 vehicles |
| Total Ped/Bike Volume | 0 crossings | Total Ped/Bike Volume | 0 crossings |
| Right turn reduction of | 0 percent applied | Right turn reduction of | 100 percent applied |

No high speed or isolated community reduction applied to the Volume Warrant thresholds.

| Warrant I, agnt Four venicular volume |  |  |  |
| :---: | :---: | :---: | :---: |
|  | Condition A | Condition B | Condition A+B* |
| Condition Satisfied? | Not Satisfied | Not Satisfied | Not Satisfied |
| Required values reached for | 2 hours | 2 hours | 2 (Cond. A) \& 2 (Cond. B) |
| Criteria - M ajor Street (veh/hr) | 420 | 630 | 336 (Cond. A) \& 504 (Cond. B) |
| Criteria - M inor Street (veh/hr) | 105 | 53 | 84 (Cond. A) \& 42 (Cond. B) |

* Should be applied only after an adequate trial of other alternatives that could cause less delay and inconvenience to traffic has failed to solve the traffic problems.

| Warrant 2 , rour hour venicular volume |  |  |
| :---: | :---: | :---: |
|  |  |  |
| Condition Satisfied? | Not Satisfied |  |
| Required values reached for | 2 hours |  |
| Criteria | See Figure Below |  |
|  |  |  |
| Warrant 5, peak four venicular volume |  |  |
|  | Condition A | Condition B |
| Condition Satisfied? | Not Satisfied | Satisfied |
| Required values reached for | 2083 total, 133 minor, 0 delay | 2 hours |
| Criteria - Total Approach Volume (veh in one hour) | 800 | See Figure Below |
| Criteria - M inor Street High Side Volume (veh in one hour) | 100 |  |
| Criteria - M inor Street High Side Delay (veh-hrs) | 4 |  |

Figure 4C-2 (Warrant 2-70\% Factor) \& Figure 4C-4 (Warrant 3-70\% Factor)


# Traffic Signal Warrant Analysis 

Warrants 1-3 (Volume Warrants)

| Project Name | Harris Creek Farm |
| :--- | :---: |
| Project/File \# | $20498-09$ |
| Scenario | 2022 Existing |


| Intersection InTormation |  |  |  |
| :--- | :---: | :--- | :---: |
| M ajor Street (E/W Road) | US 401 Bypass | Minor Street (N/SRoad) | Eastern U-Turn Location |
| Analyzed with | 2 or more approach lanes | Analyzed with | 1 Approach Lane |
| Total Approach Volume | 2132 vehicles | Total Approach Volume | 157 vehicles |
| Total Ped/Bike Volume | 0 crossings | Total Ped/Bike Volume | 0 crossings |
| Right turn reduction of | 0 percent applied | Right turn reduction of | 0 percent applied |

No high speed or isolated community reduction applied to the Volume Warrant thresholds.

| Warrant , Eignt nour venicular volume |  |  |  |
| :---: | :---: | :---: | :---: |
|  | Condition A | Condition B | Condition A+B* |
| Condition Satisfied? | Not Satisfied | Not Satisfied | Not Satisfied |
| Required values reached for | 0 hours | 1 hour | 1 (Cond. A) \& 2 (Cond. B) |
| Criteria - Major Street (veh/hr) | 420 | 630 | 336 (Cond. A) \& 504 (Cond. B) |
| Criteria - Minor Street (veh/hr) | 105 | 53 | 84 (Cond. A) \& 42 (Cond. B) |

* Should be appried only after an adequate trial of other alternatives that could cause less delay and inconvenience to traffic has failed to solve the traffic problems.

| Walrant 2, Four inour venicular volume |  |  |
| ---: | ---: | :---: |
| Condition Satisfied? |  |  |
| Required values reached for | Not Satisfied |  |
| Criteria | 1 hour |  |
| Ree Figure Below |  |  |


|  | Condition A | Condition B |
| :---: | :---: | :---: |
| Condition Satisfied? | Not Satisfied | Satisfied |
| Required values reached for | 1623 total, 91 minor, 0 delay | 1 hour |
| Criteria - Total Approach Volume (veh in one hour) | 650 | See Figure Below |
| Criteria - M inor Street High Side Volume (veh in one hour) | 100 |  |
| Criteria - M inor Street High Side Delay (veh-hrs) | 4 |  |

Figure 4C-2 (Warrant $2-70 \%$ Factor) \& Fiqure 4C-4 (Warrant $3-70 \%$ Factor)


# Traffic Signal Warrant Analysis 

Warrants 1-3 (Volume Warrants)

| Project Name | Harris Creek Farm |
| :--- | :---: |
| Project/ File \# | 20498-09 |
| Scenario | 2027 No-Build |


| Intersection Intormation |  |  |  |
| :--- | :---: | :--- | :---: |
| M ajor Street (E/W Road) | US 401 Bypass | Minor Street (N/S Road) | Eastern U-Turn Location |
| Analyzed with | 2 or more approach lanes | Analyzed with | 1 Approach Lane |
| Total Approach Volume | 2792 vehicles | Total Approach Volume | 408 vehicles |
| Total Ped/Bike Volume | 0 crossings | Total Ped/Bike Volume | 0 crossings |
| Right turn reduction of | 0 percent applied | Right turn reduction of | 0 percent applied |

No high speed or isolated community reduction applied to the Volume Warrant thresholds.

| Warrant 1, agnt Four venicular volume |  |  |  |
| :---: | :---: | :---: | :---: |
|  | Condition A | Condition B | Condition A+B* |
| Condition Satisfied? | Not Satisfied | Not Satisfied | Not Satisfied |
| Required values reached for | 2 hours | 2 hours | 2 (Cond. A) \& 2 (Cond. B) |
| Criteria - M ajor Street (veh/hr) | 420 | 630 | 336 (Cond. A) \& 504 (Cond. B) |
| Criteria - M inor Street (veh/hr) | 105 | 53 | 84 (Cond. A) \& 42 (Cond. B) |

* Should be applied only after an adequate trial of other alternatives that could cause less delay and inconvenience to traffic has failed to solve the traffic problems.

| Warrant 2, Four hour venicular volume |  |  |
| :---: | :---: | :---: |
|  | Not Satisfied |  |
| Condition Satisfied? |  |  |
| Required values reached for | 2 hours |  |
| Criteria | See Figure Below |  |
|  |  |  |
| Warrant 5 , peak four venicular volume |  |  |
|  | Condition A | Condition B |
| Condition Satisfied? | Not Satisfied | Satisfied |
| Required values reached for | 2110 total, 233 minor, 0 delay | 2 hours |
| Criteria - Total Approach Volume (veh in one hour) | 650 | See Figure Below |
| Criteria - M inor Street High Side Volume (veh in one hour) | 100 |  |
| Criteria - M inor Street High Side Delay (veh-hrs) | 4 |  |

Figure 4C-2 (Warrant 2-70\% Factor) \& Figure 4C-4 (Warrant 3-70\% Factor)


# Traffic Signal Warrant Analysis 

Warrants 1-3 (Volume Warrants)

| Project Name | Harris Creek Farm |
| :--- | :---: |
| Project/ File \# | $20498-09$ |
| Scenario | 2027 Build |


| Intersection Intormation |  |  |  |
| :--- | :---: | :--- | :---: |
| M ajor Street (E/W Road) | US 401 Bypass | Minor Street (N/S Road) | Eastern U-Turn Location |
| Analyzed with | 2 or more approach lanes | Analyzed with | 1 Approach Lane |
| Total Approach Volume | 2806 vehicles | Total Approach Volume | 441 vehicles |
| Total Ped/Bike Volume | 0 crossings | Total Ped/Bike Volume | 0 crossings |
| Right turn reduction of | 0 percent applied | Right turn reduction of | 0 percent applied |

No high speed or isolated community reduction applied to the Volume Warrant thresholds.

| Warrant 1, agnt Four venicular volume |  |  |  |
| :---: | :---: | :---: | :---: |
|  | Condition A | Condition B | Condition A+B* |
| Condition Satisfied? | Not Satisfied | Not Satisfied | Not Satisfied |
| Required values reached for | 2 hours | 2 hours | 2 (Cond. A) \& 2 (Cond. B) |
| Criteria - M ajor Street (veh/hr) | 420 | 630 | 336 (Cond. A) \& 504 (Cond. B) |
| Criteria - M inor Street (veh/hr) | 105 | 53 | 84 (Cond. A) \& 42 (Cond. B) |

* Should be applied only after an adequate trial of other alternatives that could cause less delay and inconvenience to traffic has failed to solve the traffic problems.

| Walrant 2, rour fiour venicular volume |  |  |
| ---: | ---: | :---: |
|  |  |  |
| Condition Satisfied? | Not Satisfied |  |
| Required values reached for | 2 hours |  |
| Criteria | See Figure Below |  |


| Walrant 5, Peak Four venicular volume |  |  |  |
| ---: | :---: | :---: | :---: |
| Condition Satisfied? | Condition A | Condition B |  |
| Required values reached for | 2133 total, 253 minor, 0 delay | Satisfied |  |
| Criteria - Total Approach Volume (veh in one hour) | 650 | 2 hours |  |
| Criteria - Minor Street High Side Volume (veh in one hour) | 100 | See Figure Below |  |
| Criteria - M inor Street High Side Delay (veh-hrs) | 4 |  |  |

Figure 4C-2 (Warrant 2-70\% Factor) \& Figure 4C-4 (Warrant 3-70\% Factor)


# Traffic Signal Warrant Analysis 

Warrants 1-3 (Volume Warrants)

| Project Name | Harris Creek Farm |
| :--- | :---: |
| Project/File \# | 20498-09 |
| Scenario | 2022 Existing |


| Intersection Iniormation |  |  |  |
| :--- | :---: | :--- | :---: |
| Major Street (E/W Road) | M itchell Mill Road | Minor Street (N/SRoad) | Jonesville Road |
| Analyzed with | 1 approach lane | Analyzed with | 1 Approach Lane |
| Total Approach Volume | 1031 vehicles | Total Approach Volume | 469 vehicles |
| Total Ped/Bike Volume | 0 crossings | Total Ped/Bike Volume | 0 crossings |
| Right turn reduction of | 0 percent applied | Right turn reduction of | 0 percent applied |

No high speed or isolated community reduction applied to the Volume Warrant thresholds.

| Warrant , Eignt nour venicular volume |  |  |  |
| :---: | :---: | :---: | :---: |
|  | Condition A | Condition B | Condition A+B* |
| Condition Satisfied? | Not Satisfied | Not Satisfied | Not Satisfied |
| Required values reached for | 2 hours | 1 hour | 2 (Cond. A) \& 2 (Cond. B) |
| Criteria - Major Street (veh/hr) | 350 | 525 | 280 (Cond. A) \& 420 (Cond. B) |
| Criteria - Minor Street (veh/hr) | 105 | 53 | 84 (Cond. A) \& 42 (Cond. B) |

${ }^{*}$ Should be appried only after an adequate trial of other alternatives that could cause less delay and inconvenience to traffic has failed to solve the traffic problems.

| Walrant 2, Four inour venicular volume |  |  |
| ---: | ---: | :---: |
| Condition Satisfied? |  |  |
| Required values reached for | Not Satisfied |  |
| Criteria | 1 hour |  |
| Ree Figure Below |  |  |


|  | Condition A | Condition B |
| :---: | :---: | :---: |
| Condition Satisfied? | Not Satisfied | Not Satisfied |
| Required values reached for | 817 total, 181 minor, 0 delay | 0 hours |
| Criteria - Total Approach Volume (veh in one hour) | 800 | See Figure Below |
| Criteria - M inor Street High Side Volume (veh in one hour) | 100 |  |
| Criteria - M inor Street High Side Delay (veh-hrs) | 4 |  |

Figure 4C-2 (Warrant $2-70 \%$ Factor) \& Fiqure 4C-4 (Warrant $3-70 \%$ Factor)


# Traffic Signal Warrant Analysis 

Warrants 1-3 (Volume Warrants)

| Project Name | Harris Creek Farm |
| :--- | :---: |
| Project/ File \# | 20498-09 |
| Scenario | 2027 No-Build |


| Intersection Intormation |  |  |  |
| :--- | :---: | :--- | :---: |
| M ajor Street (E/W Road) | Mitchell M ill Road | Minor Street (N/SRoad) | Jonesville Road |
| Analyzed with | 1 approach lane | Analyzed with | 1 Approach Lane |
| Total Approach Volume | 2171 vehicles | Total Approach Volume | 818 vehicles |
| Total Ped/Bike Volume | 0 crossings | Total Ped/Bike Volume | 0 crossings |
| Right turn reduction of | 0 percent applied | Right turn reduction of | 0 percent applied |

No high speed or isolated community reduction applied to the Volume Warrant thresholds.

| Warrant 1 , Elght Four venicular volume |  |  |  |
| :---: | :---: | :---: | :---: |
|  | Condition A | Condition B | Condition A+B* |
| Condition Satisfied? | Not Satisfied | Not Satisfied | Not Satisfied |
| Required values reached for | 2 hours | 2 hours | 2 (Cond. A) \& 2 (Cond. B) |
| Criteria - M ajor Street (veh/hr) | 350 | 525 | 280 (Cond. A) \& 420 (Cond. B) |
| Criteria - M inor Street (veh/hr) | 105 | 53 | 84 (Cond. A) \& 42 (Cond. B) |

* Should be applied only after an adequate trial of other alternatives that could cause less delay and inconvenience to traffic has failed to solve the traffic problems.

| Warrant 2 , Four hour venicular volume |  |  |
| :---: | :---: | :---: |
|  |  |  |
| Condition Satisfied? | Not Satisfied |  |
| Required values reached for | 2 hours |  |
| Criteria | See Figure Below |  |
|  |  |  |
| Warrant 5 , peak four venicular volume |  |  |
|  | Condition A | Condition B |
| Condition Satisfied? | Not Satisfied | Satisfied |
| Required values reached for | 1488 total, 287 minor, 0 delay | 2 hours |
| Criteria - Total Approach Volume (veh in one hour) | 800 | See Figure Below |
| Criteria - M inor Street High Side Volume (veh in one hour) | 100 |  |
| Criteria - M inor Street High Side Delay (veh-hrs) | 4 |  |

Figure 4C-2 (Warrant 2-70\% Factor) \& Figure 4C-4 (Warrant 3-70\% Factor)


# Traffic Signal Warrant Analysis 

Warrants 1-3 (Volume Warrants)

| Project Name | Harris Creek Farm |
| :--- | :---: |
| Project/ Fle \# | 20498-09 |
| Scenario | 2027 Build |


| Intersection Intormation |  |  |  |
| :--- | :---: | :--- | :---: |
| M ajor Street (E/W Road) | Mitchell M ill Road | Minor Street (N/SRoad) | Jonesville Road |
| Analyzed with | 1 approach lane | Analyzed with | 1 Approach Lane |
| Total Approach Volume | 2212 vehicles | Total Approach Volume | 887 vehicles |
| Total Ped/Bike Volume | 0 crossings | Total Ped/Bike Volume | 0 crossings |
| Right turn reduction of | 0 percent applied | Right turn reduction of | 0 percent applied |

No high speed or isolated community reduction applied to the Volume Warrant thresholds.

| Warrant 1 , Elght Four venicular volume |  |  |  |
| :---: | :---: | :---: | :---: |
|  | Condition A | Condition B | Condition A+B* |
| Condition Satisfied? | Not Satisfied | Not Satisfied | Not Satisfied |
| Required values reached for | 2 hours | 2 hours | 2 (Cond. A) \& 2 (Cond. B) |
| Criteria - M ajor Street (veh/hr) | 350 | 525 | 280 (Cond. A) \& 420 (Cond. B) |
| Criteria - M inor Street (veh/hr) | 105 | 53 | 84 (Cond. A) \& 42 (Cond. B) |

* Should be applied only after an adequate trial of other alternatives that could cause less delay and inconvenience to traffic has failed to solve the traffic problems.

| Warrant 2 , Four hour venicular volume |  |  |
| :---: | :---: | :---: |
|  |  |  |
| Condition Satisfied? | Not Satisfied |  |
| Required values reached for | 2 hours |  |
| Criteria | See Figure Below |  |
|  |  |  |
| Warrant 5 , peak four venicular volume |  |  |
|  | Condition A | Condition B |
| Condition Satisfied? | Not Satisfied | Satisfied |
| Required values reached for | 1536 total, 323 minor, 0 delay | 2 hours |
| Criteria - Total Approach Volume (veh in one hour) | 800 | See Figure Below |
| Criteria - M inor Street High Side Volume (veh in one hour) | 100 |  |
| Criteria - M inor Street High Side Delay (veh-hrs) | 4 |  |

Figure 4C-2 (Warrant 2-70\% Factor) \& Figure 4C-4 (Warrant 3-70\% Factor)


## US 401 Bypass \& Jonesville Road [Minor-Street Right-Turn] [No-Build]

| AM Peak Hour |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| vph | $\mathrm{g} / \mathrm{c}$ | a | b | C |
| 720 | 0.7 | 0.00004 | 0.0108 | 0.2587 |
| 812 | 0.7 | 3.5E-05 | 0.010033 | 0.310936 |
| 900 | 0.7 | 0.00003 | 0.0093 | 0.3609 |


| PM Peak Hour |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| vph | $\mathrm{g} / \mathrm{c}$ | a | b | c |  |  |
| 1620 | 0.7 | 0.00004 | 0.0108 | 0.2587 |  |  |
| 1708 | 0.7 | $3.5 \mathrm{E}-05$ | 0.010067 | 0.308664 |  |  |
| 1800 | 0.7 | 0.00003 | 0.0093 | 0.3609 |  |  |


| CVAF | 1 |
| :---: | :---: |
| Conflicting Volume (vph) | 812 |
| Adjusted Conflicting (vph) | 812 |
| Turning Volume (vph) | 350 |


| CVAF | 1 |
| :---: | :---: |
| Conflicting Volume (vph) | 1708 |
| Adjusted Conflicting (vph) | 1708 |
| Turning Volume (vph) | 294 |


| Distance to Upstream Signal | 8800 | ft |
| :---: | :---: | :---: |
| Posted Speed Limit | 55 | mph |
| Travel Time | 109.09 | s |



## US 401 Bypass \& Jonesville Road [Minor-Street Right-Turn] [Build]

| AM Peak Hour |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| vph | $\mathrm{g} / \mathrm{c}$ | a | b | C |
| 720 | 0.7 | 0.00004 | 0.0108 | 0.2587 |
| 812 | 0.7 | 3.5E-05 | 0.010033 | 0.310936 |
| 900 | 0.7 | 0.00003 | 0.0093 | 0.3609 |


| PM Peak Hour |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| vph | $\mathrm{g} / \mathrm{c}$ | a | b | c |  |  |
| 1620 | 0.7 | 0.00004 | 0.0108 | 0.2587 |  |  |
| 1708 | 0.7 | $3.5 \mathrm{E}-05$ | 0.010067 | 0.308664 |  |  |
| 1800 | 0.7 | 0.00003 | 0.0093 | 0.3609 |  |  |



| Distance to Upstream Signal | 8800 | ft |
| :---: | :---: | :---: |
| Posted Speed Limit | 55 | mph |
| Travel Time | 109.09 | s |


| CVAF | 1 |
| :---: | :---: |
| Conflicting Volume (vph) | 812 |
| Adjusted Conflicting (vph) | 812 |
| Turning Volume (vph) | 380 |


| CVAF | 1 |
| :---: | :---: |
| Conflicting Volume (vph) | 1708 |
| Adjusted Conflicting (vph) | 1708 |
| Turning Volume (vph) | 314 |



## US 401 Bypass \& Jonesville Road [Major-Street Left-Turn] [No-Build]

| AM Peak Hour |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| vph | g/c | a | b | c |  |  |
| 900 | 0.7 | 0.00004 | 0.0097 | 0.4284 |  |  |
| 966 | 0.7 | $4.0 \mathrm{E}-05$ | 0.00915 | 0.46261 |  |  |
| 1080 | 0.7 | 0.00004 | 0.0082 | 0.5217 |  |  |


| PM Peak Hour |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| vph | $\mathrm{g} / \mathrm{c}$ | a | b | c |  |  |
| 1800 | 0.7 | 0.00004 | 0.0097 | 0.4284 |  |  |
| 1929 | 0.7 | $4.0 \mathrm{E}-05$ | 0.008625 | 0.495265 |  |  |
| 1980 | 0.7 | 0.00004 | 0.0082 | 0.5217 |  |  |


| CVAF | 1 |
| :---: | :---: |
| Conflicting Volume (vph) | 966 |
| Adjusted Conflicting (vph) | 966 |
| Turning Volume (vph) | 128 |


| Distance to Upstream Signal | 8800 | ft |
| :---: | :---: | :---: |
| Posted Speed Limit | 55 | mph |
| Travel Time | 109.09 | s |


| CVAF | 1 |
| :---: | :---: |
| Conflicting Volume (vph) | 1929 |
| Adjusted Conflicting (vph) | 1929 |
| Turning Volume (vph) | 122 |



| AM Peak Hour |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| vph | g/c | a | b | c |  |  |
| 900 | 0.7 | 0.00004 | 0.0097 | 0.4284 |  |  |
| 973 | 0.7 | $4.0 \mathrm{E}-05$ | 0.009092 | 0.466238 |  |  |
| 1080 | 0.7 | 0.00004 | 0.0082 | 0.5217 |  |  |


| CVAF | 1 |
| :---: | :---: |
| Conflicting Volume (vph) | 973 |
| Adjusted Conflicting (vph) | 973 |
| Turning Volume (vph) | 131 |


| PM Peak Hour |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| vph | $\mathrm{g} / \mathrm{c}$ | a | b | c |  |  |
| 1800 | 0.7 | 0.00004 | 0.0097 | 0.4284 |  |  |
| 1950 | 0.7 | $4.0 \mathrm{E}-05$ | 0.00845 | 0.50615 |  |  |
| 1980 | 0.7 | 0.00004 | 0.0082 | 0.5217 |  |  |


| CVAF | 1 |
| :---: | :---: |
| Conflicting Volume (vph) | 1950 |
| Adjusted Conflicting (vph) | 1950 |
| Turning Volume (vph) | 133 |



| Distance to Upstream Signal | 8800 | ft |
| :---: | :---: | :---: |
| Posted Speed Limit | 55 | mph |
| Travel Time | 109.09 | s |

Left Turn -95\% Queue Length


## US 401 Bypass \& Eastern U-Turn Location [Major-Street U-Turn] [No-Build]

| AM Peak Hour |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| vph | $\mathrm{g} / \mathrm{c}$ | a | b | c |  |  |
| 1800 | 0.7 | 0.00003 | 0.0072 | 0.5106 |  |  |
| 1877 | 0.7 | $3.0 \mathrm{E}-05$ | 0.007114 | 0.522064 |  |  |
| 1980 | 0.7 | 0.00003 | 0.007 | 0.5374 |  |  |


| CVAF | 1 |
| :---: | :---: |
| Conflicting Volume (vph) | 1877 |
| Adjusted Conflicting (vph) | 1877 |
| Turning Volume (vph) | 233 |


| PM Peak Hour |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| vph | $\mathrm{g} / \mathrm{c}$ | a | b | c |  |  |
| 900 | 0.7 | 0.00003 | 0.0072 | 0.5106 |  |  |
| 915 | 0.7 | $3.0 \mathrm{E}-05$ | 0.007183 | 0.512833 |  |  |
| 1080 | 0.7 | 0.00003 | 0.007 | 0.5374 |  |  |


| CVAF | 1 |
| :---: | :---: |
| Conflicting Volume (vph) | 915 |
| Adjusted Conflicting (vph) | 915 |
| Turning Volume (vph) | 175 |


| Distance to Upstream Signal | 10000 | ft |
| :---: | :---: | :---: |
| Posted Speed Limit | 55 | mph |
| Travel Time | 123.97 | s |



## US 401 Bypass \& Eastern U-Turn Location [Major-Street U-Turn] [Build]

| AM Peak Hour |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| vph | g/c | a | b | c |  |  |
| 1800 | 0.7 | 0.00003 | 0.0072 | 0.5106 |  |  |
| 1880 | 0.7 | $3.0 \mathrm{E}-05$ | 0.007111 | 0.522511 |  |  |
| 1980 | 0.7 | 0.00003 | 0.007 | 0.5374 |  |  |


| PM Peak Hour |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| vph | $\mathrm{g} / \mathrm{c}$ | a | b | c |  |  |
| 900 | 0.7 | 0.00003 | 0.0072 | 0.5106 |  |  |
| 926 | 0.7 | $3.0 \mathrm{E}-05$ | 0.007171 | 0.514471 |  |  |
| 1080 | 0.7 | 0.00003 | 0.007 | 0.5374 |  |  |


| CVAF | 1 |
| :---: | :---: |
| Conflicting Volume (vph) | 926 |
| Adjusted Conflicting (vph) | 926 |
| Turning Volume (vph) | 188 |


253/188 $939 / 1834 \rightarrow$

| Distance to Upstream Signal | 10000 | ft |
| :---: | :---: | :---: |
| Posted Speed Limit | 55 | mph |
| Travel Time | 123.97 | s |




[^0]:    2027 No-Build AM Harris Creek Farm - Rolesville, NC 11:04 am 04/14/2023 2027 No-Build RKA

[^1]:    2027 Build AM Harris Creek Farm - Rolesville, NC 11:36 am 01/05/2023 2027 Build RKA

