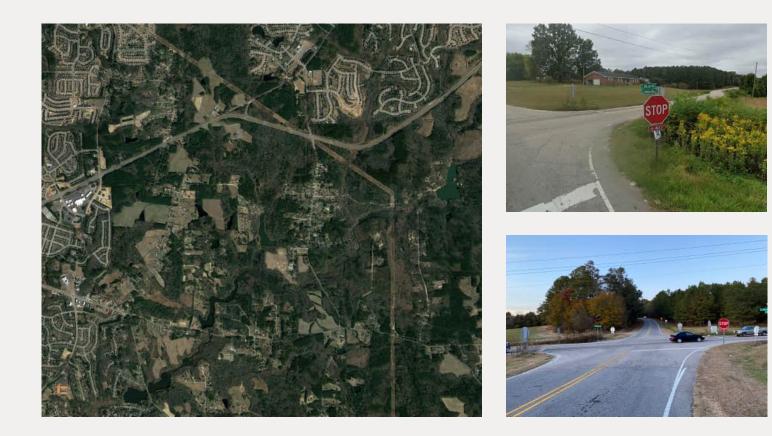
Rcvd 06-23-2023 from RKA

RAMEY KEMP ASSOCIATES

TOGETHER WE ARE LIMITLESS



Hills at Harris Creek Traffic Impact Analysis Rolesville, North Carolina



rameykemp.com

TRAFFIC IMPACT ANALYSIS

FOR

HILLS AT HARIS CREEK

LOCATED

IN

ROLESVILLE, NORTH CAROLINA

Prepared For: Town of Rolesville 502 Southtown Circle Rolesville, NC 27571

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JUNE 2023

Prepared By: DAR

RKA Project No. 20498 - 005

Reviewed By: <u>JAE</u>

TRAFFIC IMPACT ANALYSIS HILLS AT HARRIS CREEK ROLESVILLE, NORTH CAROLINA

EXECUTIVE SUMMARY

1. Development Overview

A Traffic Impact Analysis (TIA) was conducted for the proposed Hills at Harris Creek development in accordance with the Town of Rolesville (Town) Land Development Ordinance (LDO) and North Carolina Department of Transportation (NCDOT) capacity analysis guidelines. The proposed development is to be located north of Mitchell Mill Road, west of Manly Farm Road, and east of Gro Peg Lane in Rolesville, North Carolina. This TIA is an update to the approved TIA that was sealed on May 19, 2022. This updated study reflects changes to the proposed land use types and densities and a change to the site access at the westernmost driveway from full-movement to right-in/right-out. No other scope changes were made from the previous TIA.

The proposed development is anticipated to be completed in 2027 and is expected to consist of 155 single-family homes, 115 townhomes, and a 12,000 sq. ft. day care center. Site access is proposed via one (1) full-movement and one (1) right-in/right-out (RIRO) driveway connection along Mitchell Mill Road.

The study analyzes traffic conditions during the weekday AM and PM peak hours for the following scenarios:

- 2022 Existing Traffic Conditions
- 2027 No-Build Traffic Conditions
- 2027 Build Traffic Conditions



2. Existing Traffic Conditions

The study area for the TIA was determined through coordination with NCDOT and the Town and consists of the following existing intersections:

- US 401 Bypass and Jonesville Road
- US 401 Bypass and Eastern U-Turn Location
- Mitchell Mill Road and Jonesville Road / Peebles Road

Existing peak hour traffic volumes were determined based on traffic counts conducted at the study intersection listed above, in November of 2021 during typical weekday AM (7:00 AM – 9:00 AM) and PM (4:00 PM – 6:00 PM) peak periods, while schools were in session for in-person learning.

Previously collected counts from the year 2021 were projected to the 2022 existing analysis year using a compounded annual growth rate of 2%. Weekday AM and PM traffic volumes were balanced between study intersections, where appropriate.

3. Site Trip Generation

The proposed development is assumed to consist of 155 single-family homes, 115 townhomes, and a 12,000 sq. ft. day care center. Average weekday daily, AM peak hour, and PM peak hour trips for the proposed development were estimated using methodology contained within the ITE *Trip Generation Manual*, 11th Edition. Table E-1 provides a summary of the trip generation potential for the site.



Land Use (ITE Code)	Intensity Tra	Daily Traffic (vpd)	Weekday AM Peak Hour Trips (vph)			Weekday PM Peak Hour Trips (vph)		
		(vpu)	Enter	Exit	Total	Enter	Exit	Total
Single-Family Home (210)	155 DU	1,510	28	83	111	95	55	150
Single-Family Attached Housing (220)	115 DU	812	14	45	59	44	26	70
Day Care Center (565)	12 KSF	572	70	62	132	63	70	133
Total Trips 2,894		112	190	302	202	151	353	
Pass-By Trips: Day Care Center (44% PM)			-	-	-	-30	-30	-60
Total Primary Trips			112	190	302	172	121	293

Table E-1: Site Trip Generation

4. Future Traffic Conditions

Through coordination with NCDOT and the Town, it was determined that an annual growth rate of 2% would be used to generate 2027 projected weekday AM and PM peak hour traffic volumes. The following adjacent developments were identified to be considered under future conditions:

- Cobblestone Crossing Mixed-Use
- Young Street PUD
- Wheeler Tract
- Louisbury Road Assemblage
- Kalas / Watkins Family Property

5. Capacity Analysis Summary

The analysis considered weekday AM and PM peak hour traffic for 2022 existing, 2027 no-build, and 2027 build conditions. Refer to Section 7 of the TIA for the capacity analysis summary performed at each study intersection.



6. Recommendations

Based on the findings of this study, specific geometric and traffic control improvements have been identified at study intersections. The improvements are summarized below and are illustrated in Figure E-1.

Recommended Improvements by Developer

Required Frontage Improvements per Rolesville Community Transportation Plan

• Widen one-half section of Mitchell Mill Road along the site frontage to this roadway's ultimate section (4-lane median divided).

US 401 Bypass and Jonesville Road

Conduct a full signal warrant analysis prior to full build-out of the proposed development and install a traffic signal if warranted and approved by NCDOT and the Town.

US 401 Bypass and Eastern U-Turn Location

Conduct a full signal warrant analysis prior to full build-out of the proposed development and install a traffic signal if warranted and approved by NCDOT and the Town.

Mitchell Mill Road and Jonesville Road / Peebles Road

- Construct a southbound (Jonesville Road) left-turn lane with at least 100 feet of • storage and appropriate decel and taper.
 - o It should be noted that this improvement was also identified by the 5109 Mitchell Mill Road TIA.
- Construct a westbound (Mitchell Mill Road) right-turn lane with at least 100 feet of storage and appropriate decel and taper.
- Conduct a full signal warrant analysis prior to full build-out of the proposed development and install a traffic signal if warranted and approved by NCDOT and the Town.



Mitchell Mill Road and Site Access 1

- Construct the southbound approach (Site Access 1) as a right-in/right-out with one ingress lane and one egress lane.
- Provide stop-control for the southbound approach (Site Access 1).
- Construct a concrete median on Mitchell Mill Road that restricts access to rightin/right-out.

Mitchell Mill Road and Site Access 2

- Construct the southbound approach (Site Access 2) with one ingress lane and one egress lane.
- Provide stop-control for the southbound approach (Site Access 2).
- Construct an eastbound (Mitchell Mill Road) left-turn lane with at least 150 feet of storage and appropriate decel and taper.
- Construct a westbound (Mitchell Mill Road) right-turn lane with at least 100 feet of storage and appropriate decel and taper.



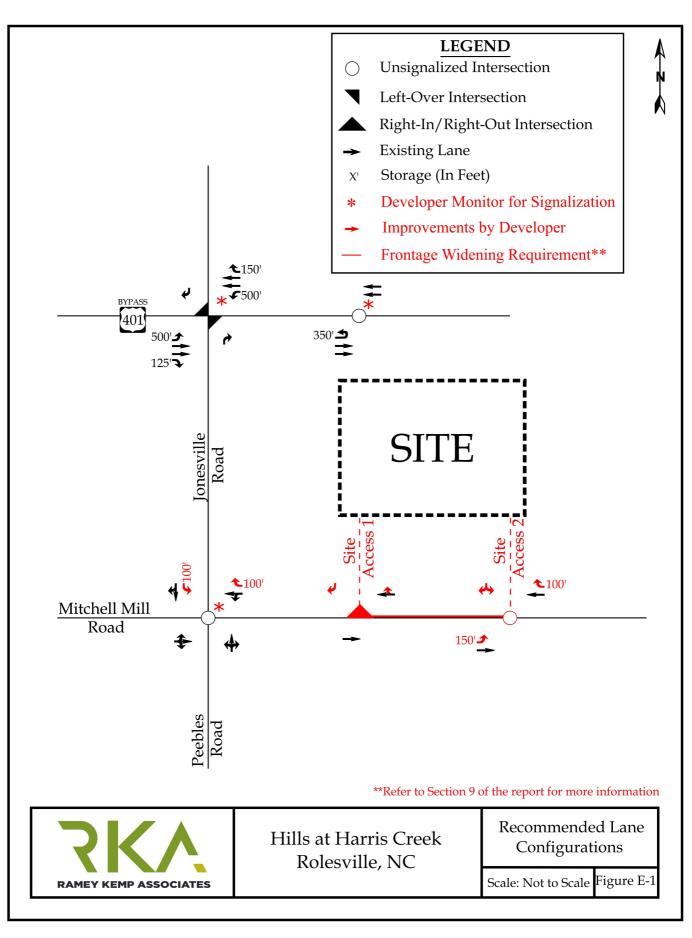


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- Appendix A: Scoping Documentation
- Appendix B: Traffic Counts
- Appendix C: Adjacent Development Information
- Appendix D: Capacity Calculations US 401 Bypass & Jonesville Road
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- Appendix G: Capacity Calculations Mitchell Mill Road & Site Access 1
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- Appendix I: Turn Lane Warrants
- Appendix J: MUTCD / ITRE Signal Warrant Analysis



TRAFFIC IMPACT ANALYSIS HILLS AT HARRIS CREEK ROLESVILLE, NORTH CAROLINA

1. INTRODUCTION

The contents of this report present the findings of the Traffic Impact Analysis (TIA) conducted for the proposed Hills at Harris Creek development in Rolesville, North Carolina. The proposed development, anticipated to be completed in 2027, is located north of Mitchell Mill Road, west of Manly Farm Road, and east of Gro Peg Lane in Rolesville, North Carolina. The purpose of this study is to determine the potential impacts to the surrounding transportation system created by traffic generated by the proposed development, as well as recommend improvements to mitigate the impacts.

This TIA is an update to the approved TIA that was sealed on May 19, 2022. This updated study reflects changes to the proposed land use types and densities and a change to the site access at the westernmost driveway from full-movement to right-in/right-out. No other scope changes were made from the previous TIA.

The proposed development is expected to consist of 155 single-family homes, 115 townhomes, and a 12,000 sq. ft. day care center.

The study analyzes traffic conditions during the weekday AM and PM peak hours for the following scenarios:

- 2022 Existing Traffic Conditions
- 2027 No-Build Traffic Conditions
- 2027 Build Traffic Conditions



1.1. Site Location and Study Area

The proposed development is located north of Mitchell Mill Road, west of Manly Farm Road, and east of Gro Peg Lane in Rolesville, North Carolina. Refer to Figure 1 for the site location map. The study area for the TIA was determined through coordination with the North Carolina Department of Transportation (NCDOT) and the Town of Rolesville (Town) and consists of the following existing intersections:

- US 401 Bypass and Jonesville Road
- US 401 Bypass and Eastern U-Turn Location
- Mitchell Mill Road and Jonesville Road / Peebles Road

Refer to Appendix A for the approved scoping documentation.

1.2. Proposed Land Use and Site Access

The site is to be located north of Mitchell Mill Road, west of Manly Farm Road, and east of Gro Peg Lane. The proposed development, anticipated to be completed in 2027, is assumed to consist of the following uses:

- 155 single-family homes
- 115 townhomes
- 12,000 sq. ft. day care center

Site access is proposed via one (1) full-movement and one (1) right-in/right-out (RIRO) driveway connection along Mitchell Mill Road. Refer to Figure 2 for a copy of the preliminary site plan.

1.3. Adjacent Land Uses

The proposed development is located in an area consisting primarily of undeveloped land and residential development.



1.4. Existing Roadways

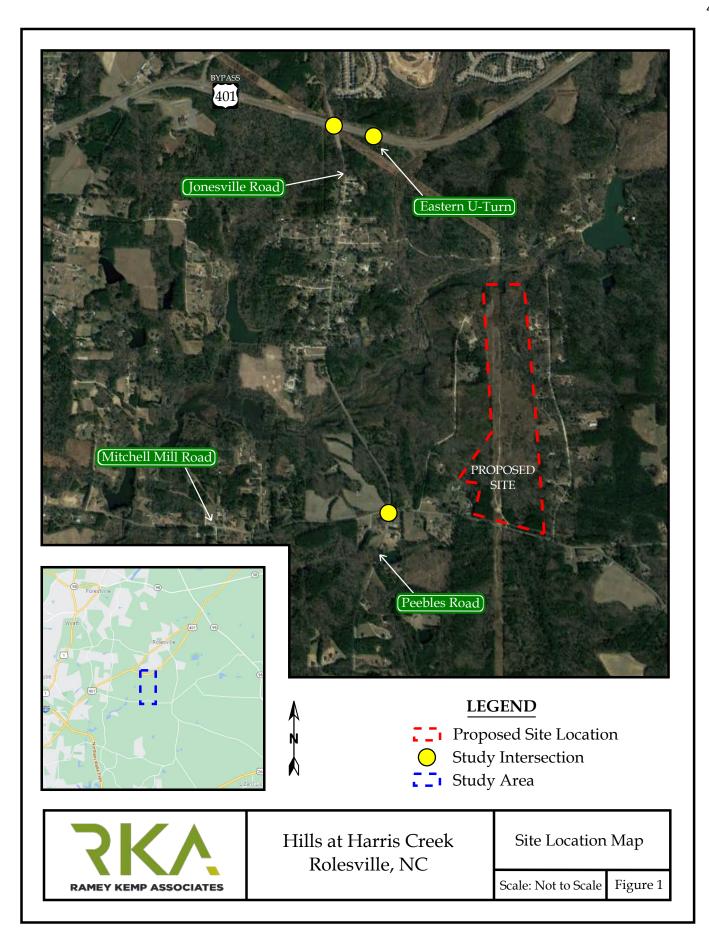
Existing lane configurations (number of traffic lanes on each intersection approach), storage capacities, and other intersection and roadway information within the study area are shown in Figure 3. Table 1 provides a summary of this information, as well.

Road Name	Route Number	Typical Cross- Section	Speed Limit	Maintained By	2019 AADT (vpd)	
US 401 Bypass 4-lane divided			55 mph	NCDOT	17,500	
Jonesville Road	SR 2226	2-lane undivided	35 mph / 45 mph	NCDOT	2,210*	
Mitchell Mill Road	SR 2224	2-lane undivided	45 mph	NCDOT	4,000	
Peebles Road	SR 2929	2-lane undivided	45 mph	NCDOT	1,700*	

Table 1: Existing Roadway Inventory

*ADT based on 2022 existing traffic volumes and assuming the weekday PM peak hour volume is 10% of the average daily traffic.







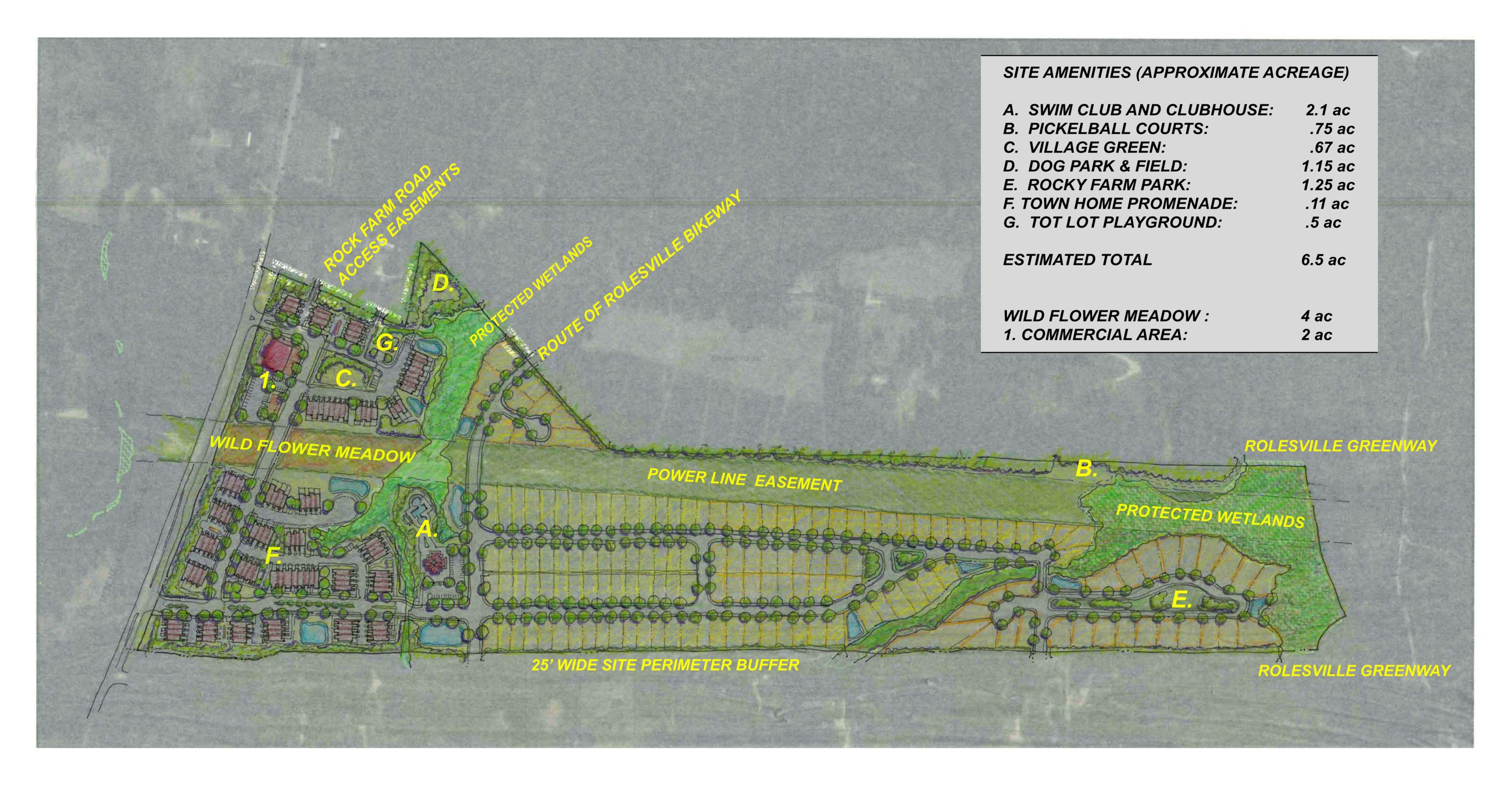
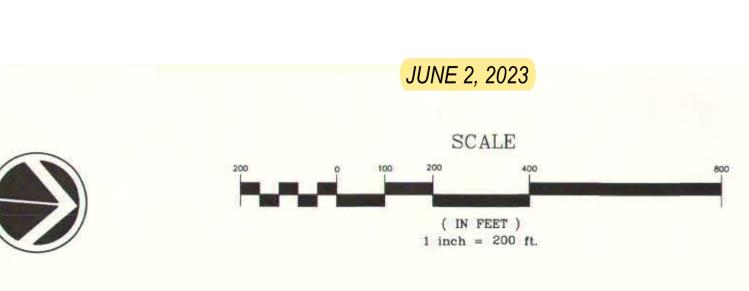


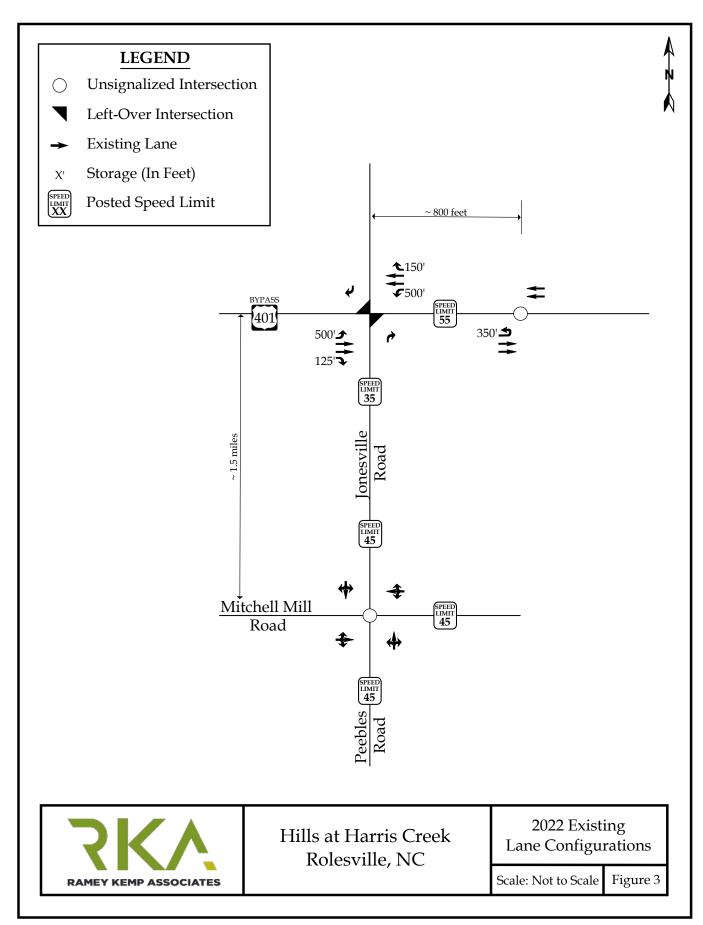




EXHIBIT ONE: CONCEPT PLAN (SKETCH PLAN)

N RE N \mathbf{N} S 1 03





2. 2022 EXISTING PEAK HOUR CONDITIONS

2.1. 2022 Existing Peak Hour Traffic Volumes

Existing peak hour traffic volumes were determined based on previously collected traffic counts conducted at the study intersections listed below, in November of 2021 during typical weekday AM (7:00 AM – 9:00 AM) and PM (4:00 PM – 6:00 PM) peak periods, while schools were in session for in-person learning:

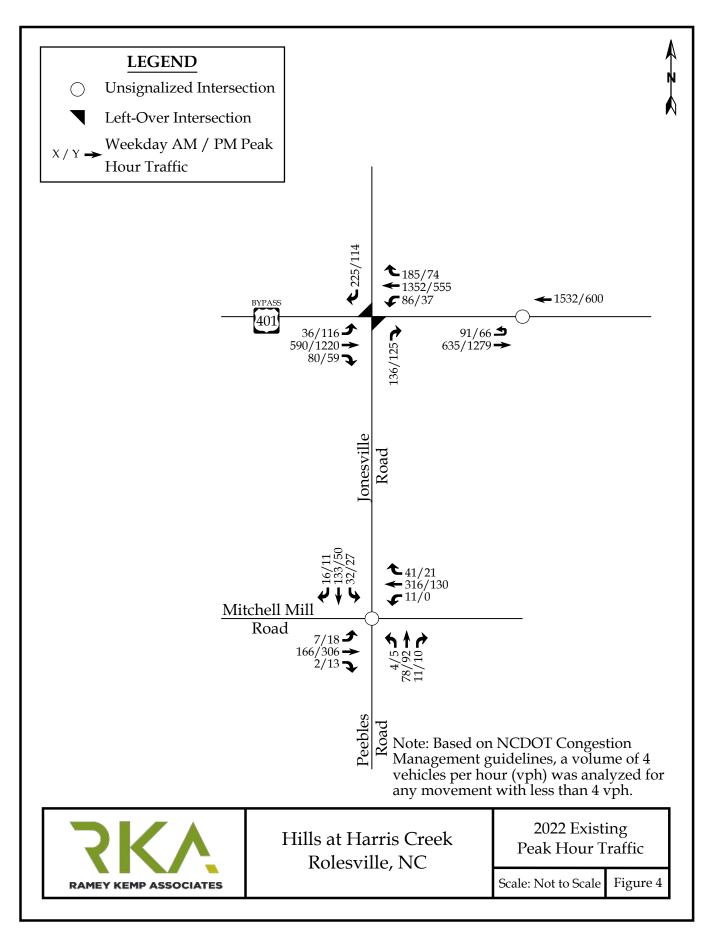
- US 401 Bypass and Jonesville Road
- US 401 Bypass and Eastern U-Turn Location
- Mitchell Mill Road and Jonesville Road / Peebles Road

Previously collected counts from the year 2021 were projected to the 2022 existing analysis year using a compounded annual growth rate of 2%. Weekday AM and PM traffic volumes were balanced between study intersections, where appropriate. Refer to Figure 4 for 2022 existing weekday AM and PM peak hour traffic volumes. A copy of the count data is located in Appendix B of this report.

2.2. Analysis of 2022 Existing Peak Hour Traffic Conditions

The 2022 existing weekday AM and PM peak hour traffic volumes were analyzed to determine the current levels of service at the study intersections under existing roadway conditions. The results of the analysis are presented in Section 7 of this report.





3. 2027 NO-BUILD PEAK HOUR CONDITIONS

In order to account for the growth of traffic and subsequent traffic conditions at a future year, no-build traffic projections are needed. No-build traffic is the component of traffic due to the growth of the community and surrounding area that is anticipated to occur regardless of whether the proposed development is constructed. No-build traffic is comprised of existing traffic growth within the study area and additional traffic created as a result of adjacent approved developments.

3.1. Ambient Traffic Growth

Through coordination with NCDOT and the Town, it was determined that an annual growth rate of 2% would be used to generate 2027 projected weekday AM and PM peak hour traffic volumes. Refer to Figure 5 for 2027 projected peak hour traffic.

3.2. Adjacent Development Traffic

Through coordination with NCDOT and the Town, the following adjacent developments were identified to be included as an approved adjacent development in this study:

- Cobblestone Crossing Mixed-Use
- Young Street PUD
- Wheeler Tract
- Louisbury Road Assemblage
- Kalas / Watkins Family Property

Table 2, on the following page, provides a summary of the adjacent developments.



Development Name	Location	Build- Out Year	Land Use / Intensity	TIA Performed	
Cobblestone Crossing Mixed- Use	Northwest quadrant of the intersection of Main Street and Young Street180 multi-family homes 18,200 sq. ft. municipal flex space 50,000 sq. ft. general retail		March 2021 by RKA		
Young Street PUD	Along both sides of US 401 Bypass west of Young Street		96 single-family homes 525 single-family homes 320 multi-family homes 122,800 sq. ft. general retail	June 2019 by Kimley Horn	
Wheeler Tract	Northeast quadrant of the intersection of Rolesville Road and Mitchell Mill Road	2026	233 single-family homes 125 multi-family homes	June 2019 by RKA	
Louisbury Road Assemblage	F KOAG ANG SOUTH OF		152 single-family homes	May 2020 by RKA	
Kalas / WatkinsAlong the west sideFamily Propertyof Rolesville Road,North of Mitchell MillRoad		2025	439 single-family homes 96 multi-family homes	August 2019 by Stantec	

Table 2: Adjacent Development Information

Adjacent development trips are shown in Figure 6. Adjacent development information can be found in Appendix C.

3.3. Future Roadway Improvements

Based on coordination with the NCDOT and the Town, it was determined there were no future roadway improvements to consider under future conditions with this study. It should be noted that per the Rolesville Community Transportation Plan (dated May 2022), the ultimate cross-section of Jonesville Road is identified as a 2-lane roadway with a center two-way-left-turn-lane (TWLTL) and Mitchell Mill Road is identified as a 4-lane median-divided roadway.



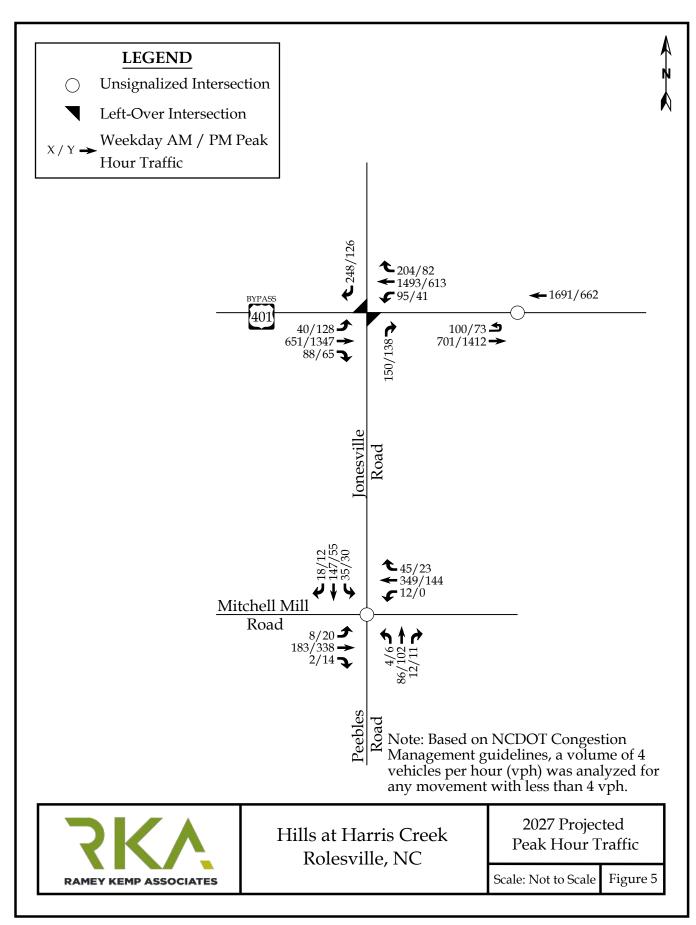
3.4. 2027 No-Build Peak Hour Traffic Volumes

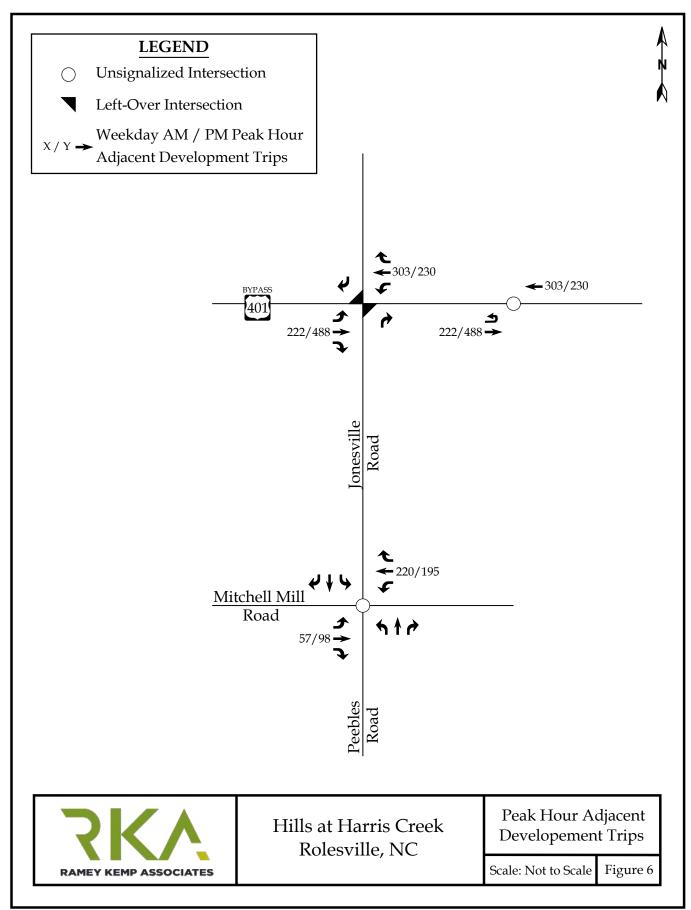
The 2027 no-build traffic volumes were determined by projecting the 2022 existing peak hour traffic to the year 2027 and adding the adjacent development trips. Refer to Figure 7 for an illustration of the 2027 no-build peak hour traffic volumes at the study intersections.

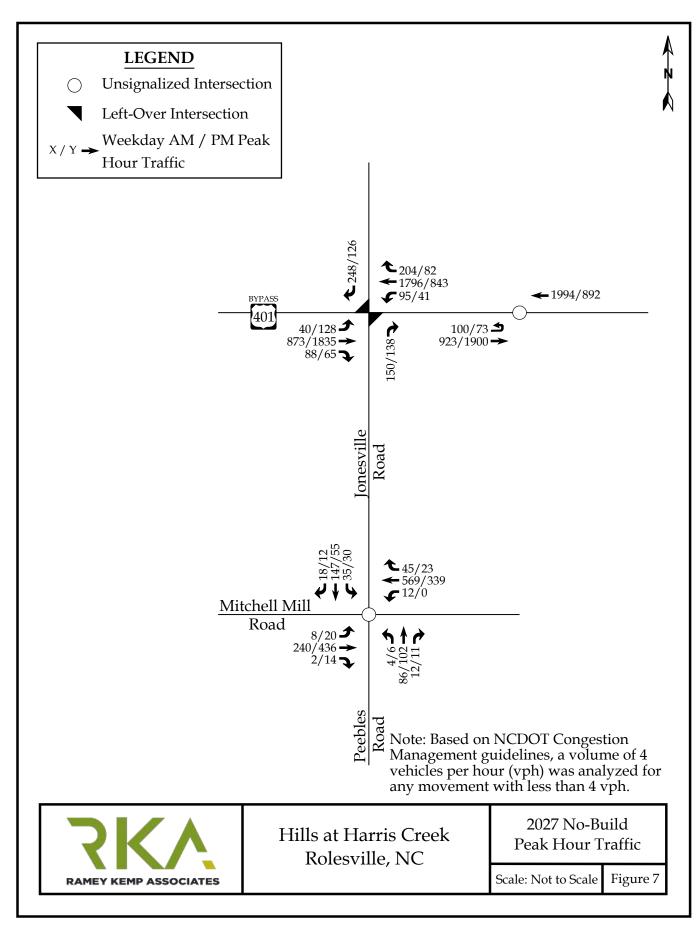
3.5. Analysis of 2027 No-Build Peak Hour Traffic Conditions

The 2027 no-build AM and PM peak hour traffic volumes at the study intersections were analyzed with existing geometric roadway conditions and traffic control. The analysis results are presented in Section 7 of this report.









4. SITE TRIP GENERATION AND DISTRIBUTION

4.1. Trip Generation

The proposed development is assumed to consist of 155 single-family homes, 115 townhomes, and a 12,000 sq. ft. day care center. Average weekday daily, AM peak hour, and PM peak hour trips for the proposed development were estimated using methodology contained within the ITE *Trip Generation Manual*, 11th Edition. Table 3 provides a summary of the trip generation potential for the site.

Land Use (ITE Code)	Intensity	(vpd) 1,510 812 572	Weekday AM Peak Hour Trips (vph)			Weekday PM Peak Hour Trips (vph)		
			Enter	Exit	Total	Enter	Exit	Total
Single-Family Home (210)	155 DU	1,510	28	83	111	95	55	150
Single-Family Attached Housing (220)	115 DU	812	14	45	59	44	26	70
Day Care Center (565)	12 KSF	572	70	62	132	63	70	133
Total Trips		2,894	112	190	302	202	151	353
Pass-By Trips: Day Care Center (44% PM)		-	-	-	-30	-30	-60	
Total Primary Trips		112	190	302	172	121	293	

Table 3: Trip Generation Summary

It is estimated that the proposed development will generate approximately 2,894 total site trips on the roadway network during a typical 24-hour weekday period. Of the daily traffic volume, it is anticipated that 302 trips (112 entering and 190 exiting) will occur during the weekday AM peak hour and 353 trips (202 entering and 151 exiting) will occur during the weekday PM peak hour.

Pass-by trips were also taken into consideration in this study. Pass-by trips are made by the traffic already using the adjacent roadway, entering the site as an intermediate stop on their way to another destination. Pass-by trips are expected to account for approximately 60 trips (30 entering and 30 exiting) during the weekday PM peak hour. It should be noted that the



pass-by trips were balanced, as it is likely that these trips would enter and exit in the same hour.

The total primary site trips are the calculated site trips after the reduction for pass-by trips. There are anticipated to be approximately 302 primary site trips (112 entering and 190 exiting) during the weekday AM peak hour and 293 primary site trips (172 entering and 121 exiting) during the weekday PM peak hour.

4.2. Site Trip Distribution and Assignment

Trip distribution percentages used in assigning site traffic for this development were estimated based on a combination of existing traffic patterns, population centers adjacent to the study area, and engineering judgment.

It is estimated that site trips will be regionally distributed as follows:

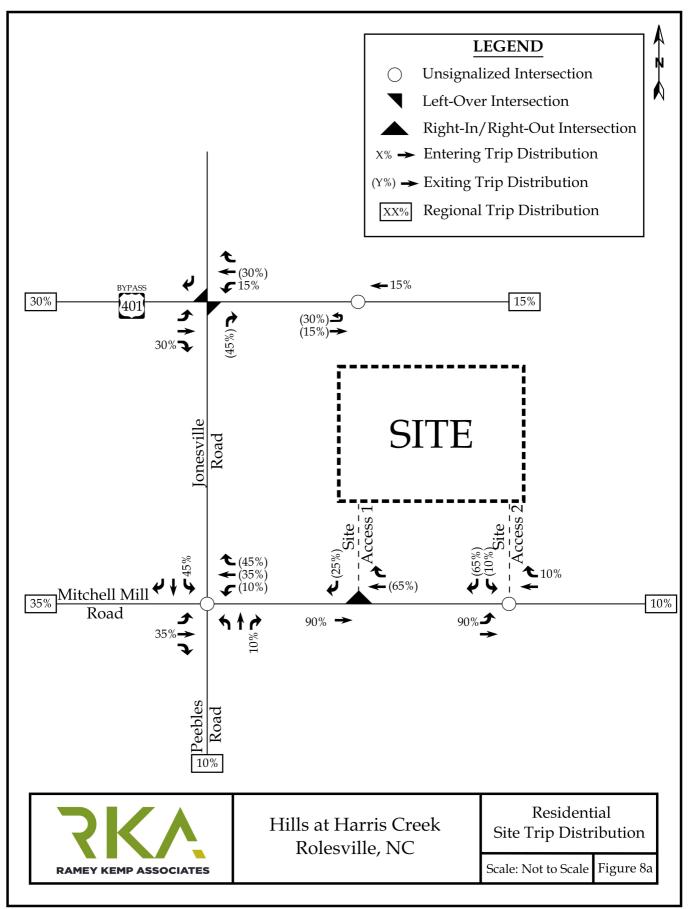
- 30% to/from the west via US 401 Bypass
- 15% to/from the east via US 401 Bypass
- 10% to/from the south via Peebles Road
- 35% to/from the west via Mitchell Mill Road
- 10% to/from the east via Mitchell Mill Road

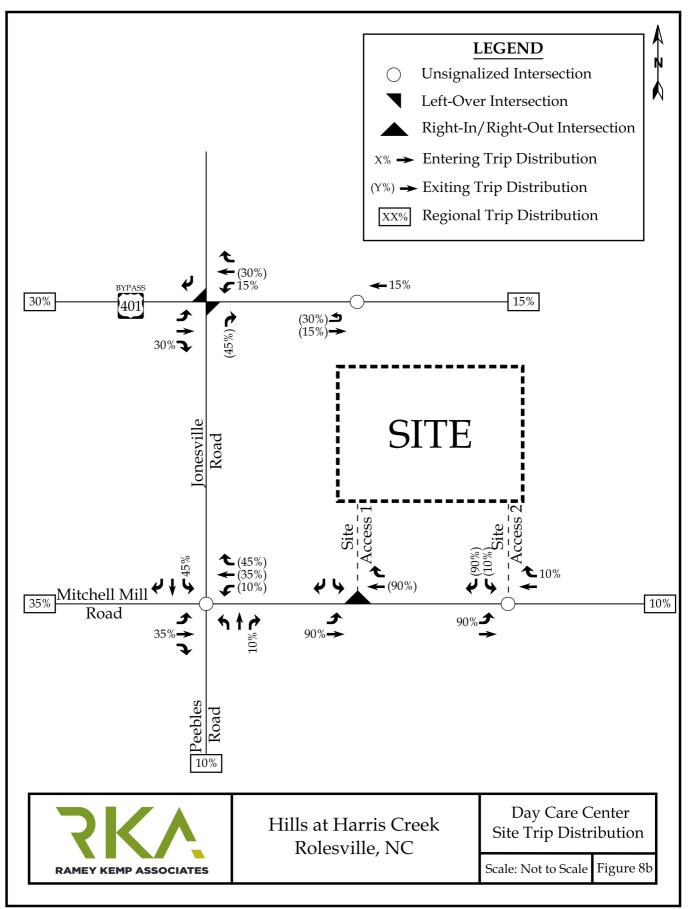
The residential site trip distribution is shown in Figure 8a and the day care center site trip distribution is shown in Figure 8b. Refer to Figures 9a and 9b for the residential site trip assignment and day care center site trip assignment, respectively.

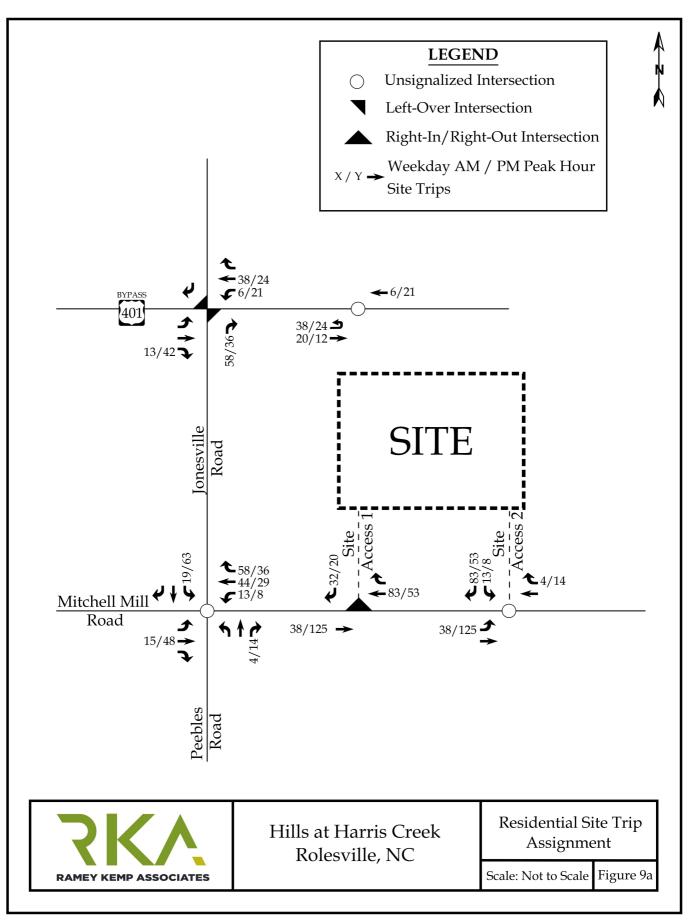
The pass-by site trips were distributed based on existing traffic patterns with consideration given to the proposed driveway access and site layout. Refer to Figure 10 for the pass-by site trip distribution. Pass-by site trips are shown in Figure 11.

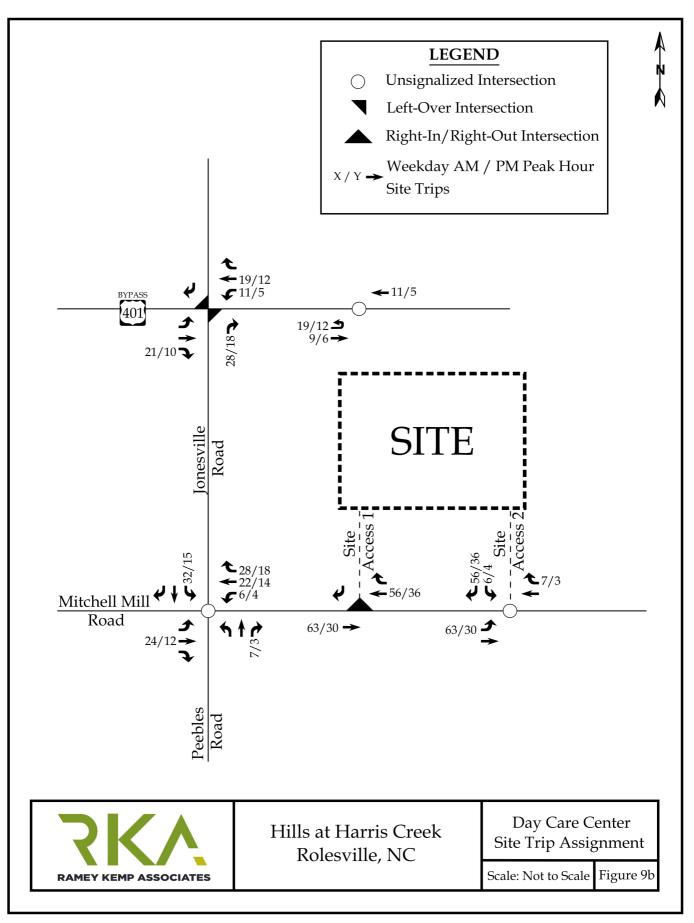
The total site trips were determined by adding the primary site trips and the pass-by site trips. Refer to Figure 12 for the total peak hour site trips at the study intersections.

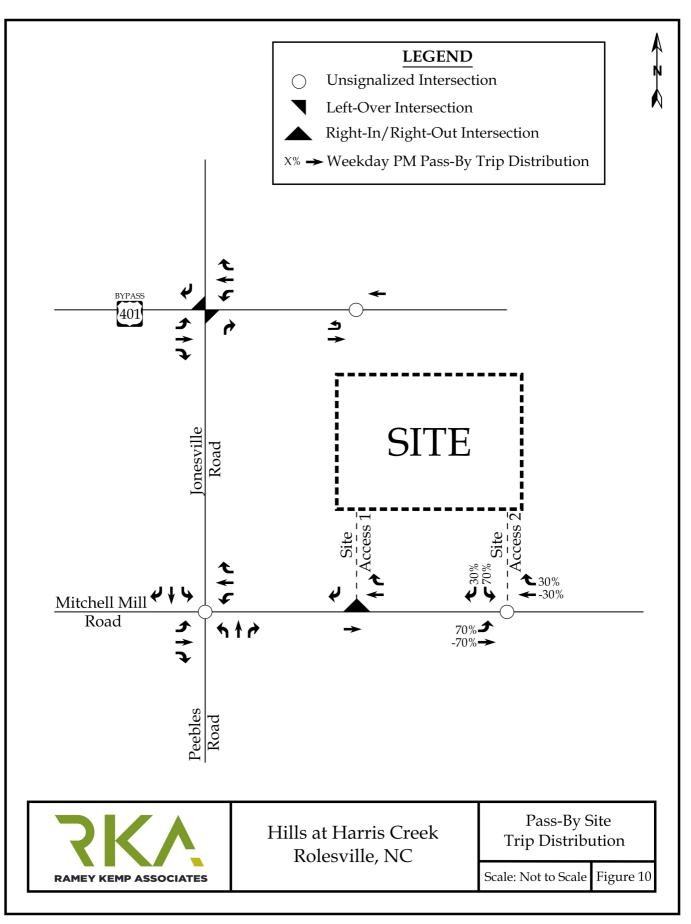


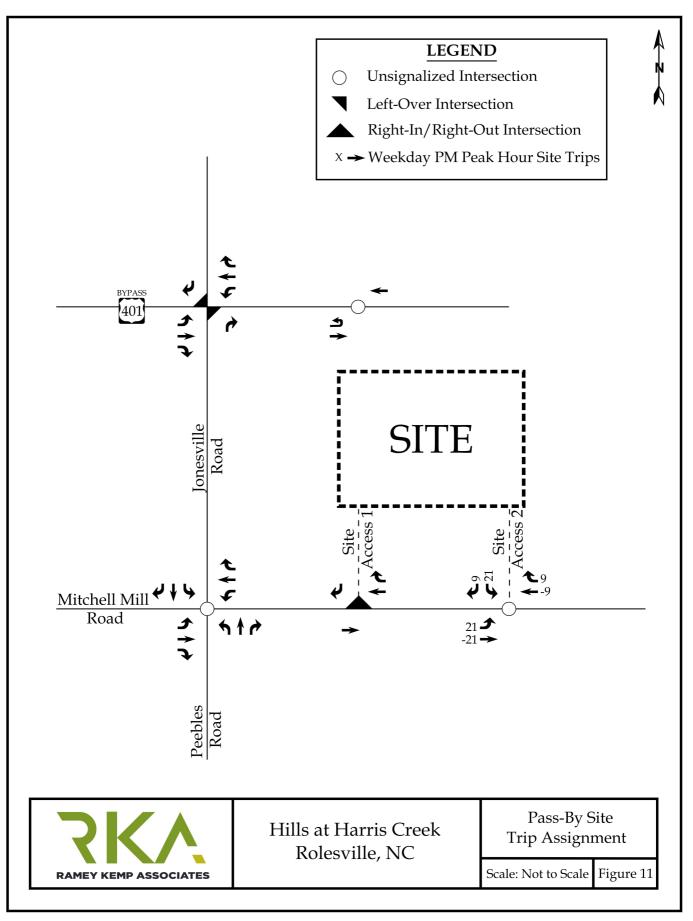


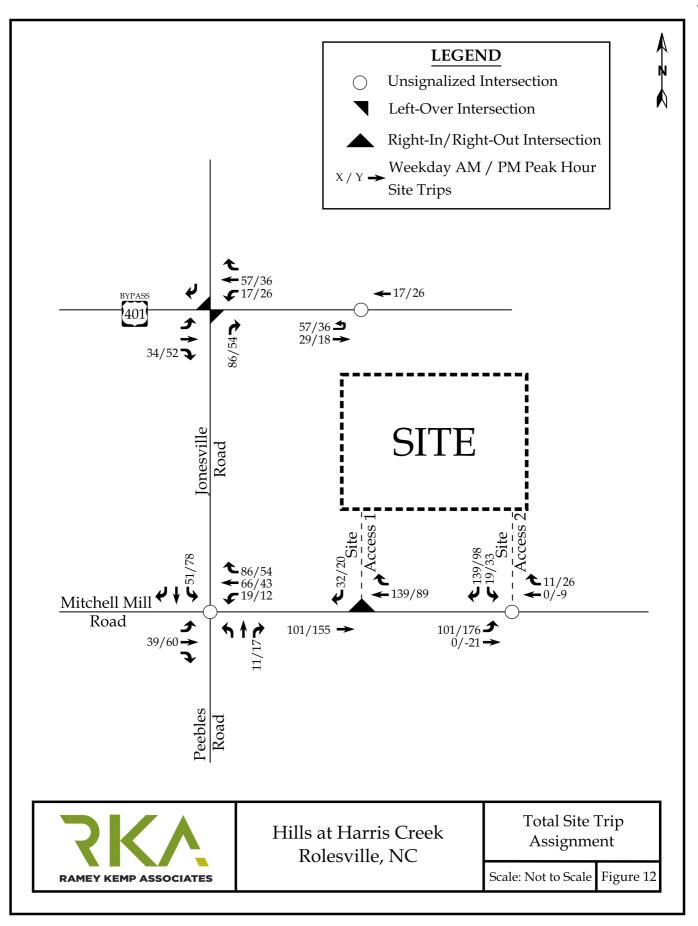












5. **2027 BUILD TRAFFIC CONDITIONS**

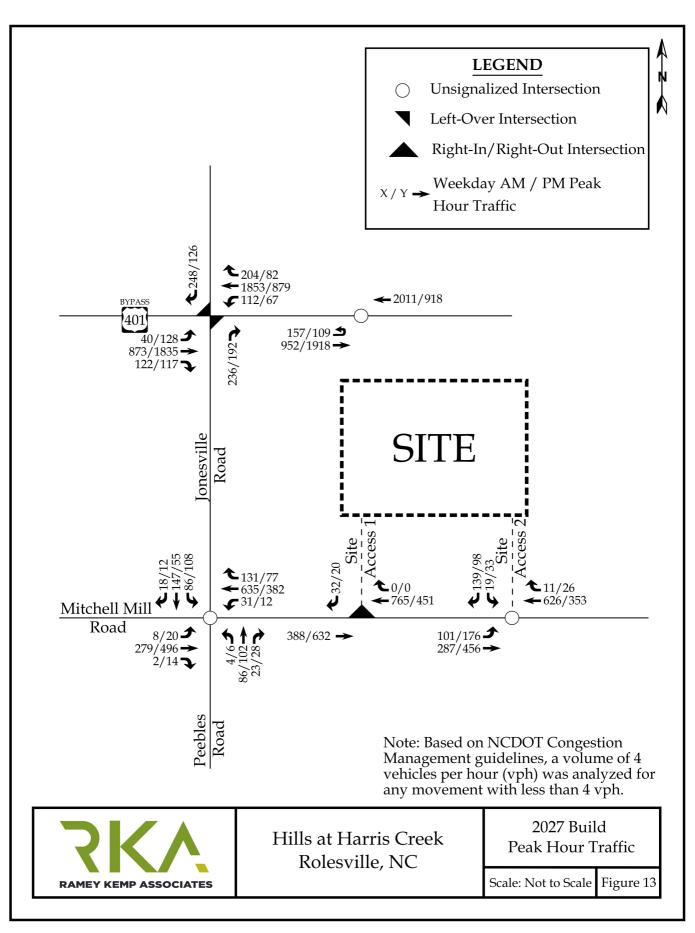
5.1. 2027 Build Peak Hour Traffic Volumes

To estimate traffic conditions with the site fully built-out, the total site trips were added to the 2027 no-build traffic volumes to determine the 2027 build traffic volumes. Refer to Figure 13 for an illustration of the 2027 build peak hour traffic volumes with the proposed site fully developed.

5.2. Analysis of 2027 Build Peak Hour Traffic Conditions

Study intersections were analyzed with the 2027 build traffic volumes using the same methodology previously discussed for existing and no-build traffic conditions. Intersections were analyzed with improvements necessary to accommodate future traffic volumes. The results of the capacity analysis for each intersection are presented in Section 7 of this report.





6. TRAFFIC ANALYSIS PROCEDURE

Study intersections were analyzed using the methodology outlined in the *Highway Capacity Manual* (HCM), 6th Edition published by the Transportation Research Board. Capacity and level of service are the design criteria for this traffic study. A computer software package, Synchro (Version 11), was used to complete the analyses for most of the study area intersections. Please note that the unsignalized capacity analysis does not provide an overall level of service for an intersection; only delay for an approach with a conflicting movement.

The HCM defines capacity as "the maximum hourly rate at which persons or vehicles can reasonably be expected to traverse a point or uniform section of a lane or roadway during a given time period under prevailing roadway, traffic, and control conditions." Level of service (LOS) is a term used to represent different driving conditions and is defined as a "qualitative measure describing operational conditions within a traffic stream, and their perception by motorists and/or passengers." Level of service varies from Level "A" representing free flow, to Level "F" where breakdown conditions are evident. Refer to Table 4 for HCM levels of service and related average control delay per vehicle for both signalized and unsignalized intersections. Control delay as defined by the HCM includes "initial deceleration delay, queue move-up time, stopped delay, and final acceleration delay". An average control delay of 50 seconds at a signalized intersection results in LOS "D" operation at the intersection.

UNSIGN	ALIZED INTERSECTION	SIGNALIZED INTERSECTION				
LEVEL OF SERVICE	OF CONTROL DELAY SERVICE PER VEHICLE (SECONDS)		AVERAGE CONTROL DELAY PER VEHICLE (SECONDS)			
А	0-10	А	0-10			
В	10-15	В	10-20			
С	15-25	С	20-35			
D	25-35	D	35-55			
Е	35-50	E	55-80			
F	>50	F	>80			

Table 4: Highway Capacity Manual – Levels-of-Service and Delay

6.1. Adjustments to Analysis Guidelines

Capacity analysis at all study intersections was completed according to Town LDO and NCDOT Congestions Management Guidelines.



7. CAPACITY ANALYSIS

7.1. US 401 Bypass and Jonesville Road

The existing unsignalized intersection of US 401 Bypass Road and Jonesville Road was analyzed under 2022 existing, 2027 no-build, and 2027 build traffic conditions with the lane configurations and traffic control shown in Table 5. Refer to Table 5 for a summary of the analysis results. Refer to Appendix D for the Synchro capacity analysis reports.

ANALYSIS SCENARIO	A P P R	LANE	PEAK	DAY AM HOUR F SERVICE	WEEKDAY PM PEAK HOUR LEVEL OF SERVICE		
	O A C H	CONFIGURATIONS	Approach	Overall (seconds)	Approach	Overall (seconds)	
	EB	2 TH, 1 RT					
	WB*	1 LT	C^1	N/A	E^1	N/A	
2022 Existing	NB	1 RT	B2		C ²		
2022 Existing	EB**	1 LT	F^1		C1		
	WB	2 TH, 1 RT		N/A		N/A	
	SB	1 RT	E ²		B ²		
	EB 2 TH, 1 RT						
	WB*	1 LT	D^1	N/A	F^1	N/A	
2027 No-Build	NB	1 RT	B2	-	E ²	-	
2027 NO-Dullu	EB**	1 LT	F ¹		E1		
	WB	2 TH, 1 RT		N/A		N/A	
	SB	1 RT	F ²		B2		
	EB	2 TH, 1 RT					
	WB*	1 LT	D^1	N/A	F^1	N/A	
2027 Build	NB	1 RT	C ²	,	F^2	,	
2027 Dullu	EB**	1 LT	F1		E1		
	WB	2 TH, 1 RT		N/A		N/A	
	SB	1 RT	F ²	-	B ²	,	

Table 5: Analysis Summary of US 401 Bypass and Jonesville Road

*Synchro analyzed the WB left-turns as SB through movements due to the nature of the superstreet and synchro limitations.

**Synchro analyzed the EB left-turns as NB through movements due to the nature of the superstreet and synchro limitations.

1. Level of service for major-street left-turn movement.

2. Level of service for minor-street approach.

Capacity analysis of 2022 existing traffic conditions indicates that the major-street left-turn movements and minor-street approaches are expected to operate at LOS D or better with the exception of the eastbound left-turn movement during the weekday AM peak hour (LOS F),



the westbound left-turn movement during the weekday PM peak hour (LOS E), and the southbound minor-street approach during the weekday AM peak hour (LOS E).

Under 2027 no-build and 2027 build traffic conditions, the major-street left-turn movements are expected to operate at LOS E/F during the weekday AM and PM peak hours with the exception of the westbound left-turn movement during the weekday AM peak hour (LOS D) under 2027 no-build and 2027 build traffic conditions. The minor-street approaches are expected to operate at LOS E/F during the weekday AM and PM peak hours with the exception of the northbound approach during the weekday AM peak hour (LOS B/C) and the southbound approach during the weekday PM peak hour (LOS B) under 2027 no-build and 2027 build traffic conditions. It should be noted that the proposed development is expected to account for approximately 5% of the total traffic at this intersection during both the weekday AM and PM peak hours. The proposed development is expected to account for approximately 36% and 28% of the overall northbound approach traffic at this intersection during the weekday AM and PM peak hours, respectively.

Due to the poor levels-of-service expected at this intersection, a traffic signal was considered under 2027 build traffic conditions to achieve acceptable levels of service. Weekday AM and PM peak hour traffic volumes were utilized in evaluating the potential need for signalization based on the guidelines contained within the *Manual on Uniform Traffic Control Devices* (MUTCD) and within the *Guidelines for Signalization of Intersections with Two or Three Approaches Final Report,* published by ITRE. Based on a review of signal warrants at this intersection, the peak hour warrant (warrant 3) from the MUTCD is expected to be met for both the weekday AM and PM peak hours under 2027 no-build and build traffic conditions. It is not expected that this intersection would satisfy the MUTCD 8-hour (warrant 1) or 4-hour (warrant 2) warrants, which NCDOT favors for installation of a traffic signal. These longer period warrants are not typically met for residential areas due to the distinct peak traffic periods for these types of development. Based on a review of ITRE 95th percentile queue length calculations, the northbound right-turn movement demand is expected to exceed capacity during the weekday PM peak hour under 2027 no-build and 2027 build traffic



conditions. Refer to Appendix J for a copy of the MUTCD warrants and the ITRE 95th percentile queue length calculations.

Based on the Town's LDO, improvements must be identified to maintain no-build levels-ofservice under build traffic conditions or to limit the degradation to less than a five percent increase in total delay on any approach for those operating at failing levels-of-service under no-build traffic conditions. Therefore, additional turn-lanes were considered for the northbound right-turn and westbound left-turn movements at this intersection to achieve acceptable operation per the Town's LDO. However, additional turn-lanes are not a realistic or practical improvement at an unsignalized intersection operating with superstreet configurations.

Based on the Town's LDO, it is recommended that this intersection be monitored for signalization and a full signal warrant analysis be conducted prior to the full build-out of the proposed development and install a traffic signal if warranted and approved by the Town and NCDOT. With signalization, it is expected that this intersection will operate at acceptable levels-of-service during the weekday AM and PM peak hours.



7.2. US 401 Bypass and Eastern U-Turn Location

The existing unsignalized intersection of US 401 Bypass and Eastern U-Turn Location was analyzed under 2022 existing, 2027 no-build, and 2027 build traffic conditions with the lane configurations and traffic control shown in Table 6. Refer to Table 6 for a summary of the analysis results. Refer to Appendix E for the Synchro capacity analysis reports.

ANALYSIS	A P P R	LANE	PEAK	DAY AM HOUR SERVICE	PEAK	DAY PM (HOUR F SERVICE
SCENARIO		CONFIGURATIONS	Approach	Overall (seconds)	Approach	Overall (seconds)
2022 Existing	EB* WB	1 UT 2 TH	C1	N/A	B1 	N/A
2027 No-Build	EB* WB	1 UT 2 TH	E1	N/A	B1 	N/A
2027 Build	EB* WB	1 UT 2 TH	F ¹	N/A	B1 	N/A

Table 6: Analysis Summary of US 401 Bypass and Eastern U-TurnLocation

*Synchro analyzed the EB u-turn as a NB left-turn movement due to the nature of the superstreet and synchro limitations.

1. Level of service for major-street u-turn movement.

Capacity analysis of 2022 existing and 2027 no-build traffic conditions indicates that the major-street u-turn movement is expected to operate at LOS C or better during the weekday AM and PM peak hours, with the exception of the weekday AM peak hour under 2027 no-build conditions (LOS E).

Under 2027 build traffic conditions, the major-street u-turn movement is expected to operate at LOS F during the weekday AM peak hour and at LOS B during the weekday PM peak hour. It should be noted that the proposed development is expected to account for approximately 3% of the total traffic at this intersection during the weekday AM and PM peak hours. The proposed development is expected to account for approximately 36% and 33% of the overall northbound approach traffic at this intersection during the weekday AM and PM peak hours, respectively.



RAMEY KEMP ASSOCIATES

Due to the poor levels-of-service expected at this intersection, a traffic signal was considered under 2027 build traffic conditions to achieve acceptable levels of service. Weekday AM and PM peak hour traffic volumes were utilized in evaluating the potential need for signalization based on the guidelines contained within the Manual on Uniform Traffic Control Devices (MUTCD) and within the Guidelines for Signalization of Intersections with Two or Three Approaches Final Report, published by ITRE. Based on a review of signal warrants at this intersection, the peak hour warrant (warrant 3) from the MUTCD is expected to be met for the weekday AM peak hour under 2027 no-build and 2027 build traffic conditions. It is not expected that this intersection would satisfy the MUTCD 8-hour (warrant 1) or 4-hour (warrant 2) warrants, which NCDOT favors for installation of a traffic signal. These longer period warrants are not typically met for residential areas due to the distinct peak traffic periods for these types of development. Based on a review of ITRE 95th percentile queue length calculations, the eastbound u-turn movement demand is expected to exceed capacity during the weekday AM peak hour under 2027 no-build and 2027 build traffic conditions. Refer to Appendix J for a copy of the MUTCD warrants and the ITRE 95th percentile queue length calculations.

Based on the Town's LDO, improvements must be identified to maintain no-build levels-ofservice under build traffic conditions or to limit the degradation to less than a five percent increase in total delay on any approach for those operating at failing levels-of-service under no-build traffic conditions. Therefore, additional turn-lanes were considered for the eastbound u-turn movement at this intersection to achieve acceptable operation per the Town's LDO. However, additional turn-lanes are not a realistic or practical improvement at an unsignalized intersection operating with superstreet configurations.

Based on the Town's LDO, it is recommended that this intersection be monitored for signalization and a full signal warrant analysis be conducted prior to the full build-out of the proposed development and install a traffic signal if warranted and approved by the Town and NCDOT. With signalization, it is expected that this intersection will operate at acceptable levels-of-service during the weekday AM and PM peak hours.



7.3. Mitchell Mill Road and Jonesville Road / Peebles Road

The existing unsignalized intersection of Mitchell Mill Road and Jonesville Road / Peebles Road was analyzed under 2022 existing, 2027 no-build, and 2027 build traffic conditions with the lane configurations and traffic control shown in Table 7. Refer to Table 7 for a summary of the analysis results. Refer to Appendix F for the Synchro capacity analysis reports.

ANALYSIS	A P P R	LANE	WEEKI PEAK LEVEL OF	WEEKDAY PM PEAK HOUR LEVEL OF SERVICE		
SCENARIO		Approach	Overall (seconds)	Approach	Overall (seconds)	
2022 Existing	EB WB NB SB	1 LT-TH-RT 1 LT-TH-RT 1 LT-TH-RT 1 LT-TH-RT	$egin{array}{c} B^1 \ B^1 \ B^1 \ B^1 \ B^1 \end{array}$	B (13)	$\begin{array}{c} B^1 \\ A^1 \\ A^1 \\ A^1 \end{array}$	B (11)
2027 No-Build	EB WB NB SB	1 LT-TH-RT 1 LT-TH-RT 1 LT-TH-RT 1 LT-TH-RT 1 LT-TH-RT	$\begin{array}{c} C^1 \\ F^1 \\ B^1 \\ B^1 \end{array}$	F (51)	$\begin{array}{c} C^1\\ C^1\\ B^1\\ B^1\end{array}$	C (19)
2027 Build	EB WB NB SB	1 LT-TH-RT 1 LT-TH-RT 1 LT-TH-RT 1 LT-TH-RT 1 LT-TH-RT	$\begin{array}{c} C^1 \\ F^1 \\ B^1 \\ C^1 \end{array}$	F (142)	$\begin{matrix} F^1 \\ E^1 \\ C^1 \\ C^1 \end{matrix}$	F (53)
2027 Build - Improved	EB WB NB SB	1 LT-TH-RT 1 LT-TH, 1 RT 1 LT-TH-RT 1 LT , 1 TH-RT	$\begin{array}{c} C^1 \\ F^1 \\ C^1 \\ C^1 \end{array}$	F (103)	$F^1 \\ D^1 \\ C^1 \\ B^1$	F (61)

Table 7: Analysis Summary of Mitchell Mill Road and Jonesville Road / Peebles Road

Improvements by the developer are shown in bold.

1. Level of service for all-way stop controlled approach.

Capacity analysis of 2022 existing and 2027 no-build traffic conditions indicates that the intersection is expected to operate at an overall LOS C or better during the weekday AM and PM peak hours, with the exception of the weekday AM peak hour under 2027 no-build traffic conditions (LOS F). Under 2027 build traffic conditions, this intersection is expected to operate at an overall LOS F during the weekday AM and PM peak hours. It should be noted that the



proposed development is expected to account for approximately 19% and 20% of the total traffic at this intersection during the weekday AM and PM peak hours, respectively. The proposed development is expected to account for approximately 13% and 11% of the overall eastbound approach traffic and 21% and 23% of the overall westbound approach at this intersection during the weekday AM and PM peak hours, respectively.

Turn lanes were considered at this intersection in order to mitigate the proportional impact that the proposed site traffic is expected to have at this intersection and to improve overall operations. An exclusive left-turn lane on the southbound approach (Jonesville Road) and right-turn lane on the westbound approach (Mitchell Mill Road) are recommended by the developer. It should be noted that an exclusive southbound left-turn lane was also identified in the 5109 Mitchell Mill Road TIA. With these improvements, the intersection is expected to continue operating at an overall LOS F during the weekday AM and PM peak hours.

It should be noted that the overall intersection delay is expected to increase during the weekday PM peak hour as a result of the recommended improvements to the southbound and westbound approaches. This increase in delay is attributable to minor increases in delays for all approaches caused by adding additional lanes to an all-way stop-controlled intersection. No feasible improvements other than signalization would be expected to decrease delays further at this intersection.

Due to the poor levels-of-service expected at this intersection, a traffic signal was considered under 2027 build traffic conditions to achieve acceptable levels-of-service. The peak hour warrant (warrant 3) from the *Manual on Uniform Traffic Control Devices* (MUTCD) was considered. Based on a review of the peak hour signal warrant at this intersection, the intersection is expected to meet the peak hour warrant for the weekday AM peak hour under 2027 no-build traffic conditions and both the weekday AM and PM peak hours under 2027 build traffic conditions. It is not expected that this intersection would satisfy the MUTCD 8hour (warrant 1) or 4-hour (warrant 2) warrants, which NCDOT favors for installation of a traffic signal. These longer period warrants are not typically met for residential areas due to



the distinct peak traffic periods for these types of development. Refer to Appendix J for a copy of the MUTCD warrants.

Based on the Town's LDO, it is recommended that this intersection be monitored for signalization and a full signal warrant analysis be conducted prior to the full build-out of the proposed development and install a traffic signal if warranted and approved by the Town and NCDOT. With signalization, it is expected that this intersection will operate at acceptable levels-of-service during the weekday AM and PM peak hours.



7.4. Mitchell Mill Road and Site Access 1

The proposed intersection of Mitchell Mill Road and Site Access 1 was analyzed under 2027 build traffic conditions with the lane configurations and traffic control shown in Table 8. Refer to Table 8 for a summary of the analysis results. Refer to Appendix G for the synchro capacity analysis reports.

Table 8: Analysis Summary of Mitchell Mill Road and Site Access 1

ANALYSIS	A P P R LANE		PEAK	DAY AM HOUR SERVICE	WEEKDAY PM PEAK HOUR LEVEL OF SERVICE		
SCENARIO	O A C H	CONFIGURATIONS	Approach	Overall (seconds)	Approach	Overall (seconds)	
2027 Build	EB WB SB	1 TH 1 TH -RT 1 RT	 C ²	N/A	 B ²	N/A	

Improvements to lane configurations by the developer are shown in bold.

1. Level of service for major-street left-turn movement.

2. Level of service for minor-street approach.

Capacity analysis of 2027 build traffic conditions indicates that the minor-street approach is expected to operate at LOS C or better during the weekday AM and PM peak hours.

Based on the estimated low volume of right-turn movements into the proposed development at this intersection, an exclusive right-turn lane is not recommended.



7.5. Mitchell Mill Road and Site Access 2

The proposed intersection of Mitchell Mill Road and Site Access 2 was analyzed under 2027 build traffic conditions with the lane configurations and traffic control shown in Table 9. Refer to Table 9 for a summary of the analysis results. Refer to Appendix H for the synchro capacity analysis reports.

Α WEEKDAY AM WEEKDAY PM Ρ PEAK HOUR PEAK HOUR Ρ LEVEL OF SERVICE LEVEL OF SERVICE ANALYSIS R LANE **SCENARIO** 0 CONFIGURATIONS Overall Α Overall Approach Approach С (seconds) (seconds) н EB **1 LT**, 1 TH \mathbf{A}^1 \mathbf{A}^1 2027 Build N/A N/A WB 1 TH, 1 RT C^2 C^2 SB 1 LT-RT

Table 9: Analysis Summary of Mitchell Mill Road and Site Access 2

Improvements to lane configurations by the developer are shown in bold.

1. Level of service for major-street left-turn movement.

2. Level of service for minor-street approach.

Capacity analysis of 2027 build traffic conditions indicates that the major-street left-turn movement is expected to operate at LOS A during the weekday AM and PM peak hours. The minor-street approach is expected to operate at LOS C during the weekday AM and PM peak hours.

Right and left-turn lanes were considered based on the NCDOT *Policy on Street and Driveway Access to North Carolina Highways*. The policy states that turn lanes should be considered on roads that carry at least 4,000 vehicles per day. Mitchell Mill Road is expected to carry more than 4,000 vehicles per day. Based on previous coordination with NCDOT, an eastbound left turn lane and a westbound right turn lane is recommended to be constructed by the developer on Mitchell Mill Road at Site Access 2. Refer to Appendix I for a copy of the turn lane warrants.



8. CONCLUSIONS

This Traffic Impact Analysis was conducted to determine the potential traffic impacts of the proposed Hills at Harris Creek development located north of Mitchell Mill Road, west of Manly Farm Road, and east of Gro Peg Lane in Rolesville, North Carolina. The development is expected to consist of 155 single-family homes, 115 townhomes, and a 12,000 sq. ft. day care center and to be built-out in 2027. Site access is proposed via one (1) full-movement and one (1) right-in/right-out driveway connection along Mitchell Mill Road.

The study analyzes traffic conditions during the weekday AM and PM peak hours for the following scenarios:

- 2022 Existing Traffic Conditions
- 2027 No-Build Traffic Conditions
- 2027 Build Traffic Conditions

Trip Generation

It is estimated that the proposed development will generate approximately 302 primary trips (112 entering and 190 exiting) during the weekday AM peak hour and 293 primary trips (172 entering and 121 exiting) during the weekday PM peak hour.

Rolesville Community Transportation Plan

Per the Rolesville Community Transportation Plan (CTP), the ultimate cross-section of Mitchell Mill Road is identified as a 4-lane median-divided roadway. It is recommended that the proposed development widen one-half section of Mitchell Mill Road along the site frontage in accordance with the Town's CTP.



Adjustments to Analysis Guidelines

Capacity analysis at all study intersections was completed according to NCDOT Congestion Management Guidelines. Refer to section 6.1 of this report for a detailed description of any adjustments to these guidelines made throughout the analysis.

Intersection Capacity Analysis Summary

All the study area intersections (including the proposed site driveways) are expected to operate at acceptable levels-of-service under existing and future year conditions with the exception of those identified in Section 7 of this report.



9. **RECOMMENDATIONS**

Based on the findings of this study, specific geometric improvements have been identified and are recommended to accommodate future traffic conditions. See a more detailed description of the recommended improvements below. Refer to Figure 14 for an illustration of the recommended lane configurations for the proposed development.

Recommended Improvements by Developer

Required Frontage Improvements per Rolesville Community Transportation Plan

• Widen one-half section of Mitchell Mill Road along the site frontage to this roadway's ultimate section (4-lane median divided).

US 401 Bypass and Jonesville Road

• Conduct a full signal warrant analysis prior to full build-out of the proposed development and install a traffic signal if warranted and approved by NCDOT and the Town.

US 401 Bypass and Eastern U-Turn Location

• Conduct a full signal warrant analysis prior to full build-out of the proposed development and install a traffic signal if warranted and approved by NCDOT and the Town.

Mitchell Mill Road and Jonesville Road / Peebles Road

- Construct a southbound (Jonesville Road) left-turn lane with at least 100 feet of storage and appropriate decel and taper.
 - It should be noted that this improvement was also identified by the 5109
 Mitchell Mill Road TIA.
- Construct a westbound (Mitchell Mill Road) right-turn lane with at least 100 feet of storage and appropriate decel and taper.
- Conduct a full signal warrant analysis prior to full build-out of the proposed development and install a traffic signal if warranted and approved by NCDOT and the Town.



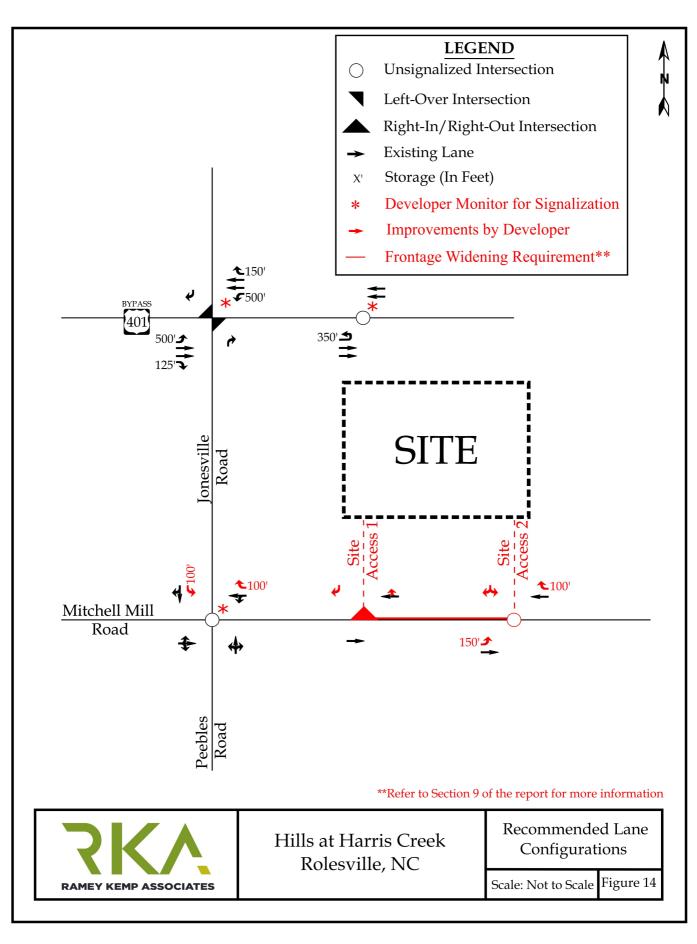
Mitchell Mill Road and Site Access 1

- Construct the southbound approach (Site Access 1) as a right-in/right-out with one ingress lane and one egress lane.
- Provide stop-control for the southbound approach (Site Access 1).
- Construct a concrete median on Mitchell Mill Road that restricts access to rightin/right-out.

Mitchell Mill Road and Site Access 2

- Construct the southbound approach (Site Access 2) with one ingress lane and one egress lane.
- Provide stop-control for the southbound approach (Site Access 2).
- Construct an eastbound (Mitchell Mill Road) left-turn lane with at least 150 feet of storage and appropriate decel and taper.
- Construct a westbound (Mitchell Mill Road) right-turn lane with at least 100 feet of storage and appropriate decel and taper.





APPENDIX A

SCOPING DOCUMENTATION

Andrew Eagle

From:	Warren, Jeremy L <jlwarren@ncdot.gov></jlwarren@ncdot.gov>
Sent:	Tuesday, May 23, 2023 12:17 PM
То:	Andrew Eagle; Nolfo, Matthew J
Cc:	Jessica McClure; Daniel Reisfeld; Elabarger, Michael S; Gruber, Meredith; Jason Pfister;
	Lineberger, Nicholas C; Darnell, Trevor S
Subject:	RE: [External] RE: Hills at Harris Creek

Andrew, We would prefer to see an updated TIA with the new volumes and the RIRO. Thanks,

Jeremy Warren, P.E. Assistant Division Maintenance Engineer Division 5 North Carolina Department of Transportation

jlwarren@ncdot.gov

4009 District Drive Raleigh, NC 27607



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From: Andrew Eagle <AEagle@rameykemp.com>
Sent: Monday, May 22, 2023 9:34 AM
To: Warren, Jeremy L <jlwarren@ncdot.gov>; Nolfo, Matthew J <mjnolfo@ncdot.gov>
Cc: Jessica McClure <jmcclure@rameykemp.com>; Daniel Reisfeld <dreisfeld@rameykemp.com>; Elabarger, Michael S
<michael.elabarger@rolesville.nc.gov>; Gruber, Meredith <meredith.gruber@rolesville.nc.gov>; Jason Pfister
<jason@ellisdevgroup.com>
Subject: RE: [External] RE: Hills at Harris Creek

CAUTION: External email. Do not click links or open attachments unless verified. Report suspicious emails with the Report Message button located on your Outlook menu bar on the Home tab.

Jeremy/Matt,

It's my understanding NCDOT prefers Access A to be RIRO. We can update the TIA to match this configuration. Also, the developer now plans the commercial area to be 12,000 square feet of Day Care instead of 14,000 square feet of retail. This results in 30 more entering trips and 20 more exiting trips during the AM peak hour when compared to the original TIA. During the PM peak hour the Day Care scenario results in 11 fewer entering trips and 4 more exiting trips.

Does NCDOT want the TIA updated to reflect the Day Care trip generation as well as the RIRO?

Andrew Eagle, PE, PTOE Senior Traffic Engineering Project Manager D 704 220 6847 | C 704 467 0325



From: Andrew Eagle
Sent: Monday, May 8, 2023 2:59 PM
To: Warren, Jeremy L <jlwarren@ncdot.gov>; Nolfo, Matthew J <mjnolfo@ncdot.gov>
Cc: Jessica McClure <JMCClure@rameykemp.com>; Daniel Reisfeld <dreisfeld@rameykemp.com>; Elabarger, Michael S
<michael.elabarger@rolesville.nc.gov>; Gruber, Meredith <meredith.gruber@rolesville.nc.gov>; Jason Pfister
<jason@ellisdevgroup.com>
Subject: RE: [External] RE: Hills at Harris Creek

The link below can be used to download the TIA, site plan, and Synchro files. Please review and let me know if you have any questions/comments. Thank you!

20498-0005 - Hills at Harris Creek - 05-08-2023

Andrew Eagle, PE, PTOE Senior Traffic Engineering Project Manager D 704 220 6847 | C 704 467 0325



From: Warren, Jeremy L <<u>jlwarren@ncdot.gov</u>>
Sent: Friday, April 14, 2023 8:53 AM
To: Andrew Eagle <<u>AEagle@rameykemp.com</u>>; Nolfo, Matthew J <<u>mjnolfo@ncdot.gov</u>>
Cc: Jessica McClure <<u>JMCClure@rameykemp.com</u>>; Daniel Reisfeld <<u>dreisfeld@rameykemp.com</u>>
Subject: RE: [External] RE: Hills at Harris Creek

The study area should be the same so an updated TIA with an explanation should suffice.

Jeremy Warren, P.E. Assistant Division Maintenance Engineer Division 5 North Carolina Department of Transportation

jlwarren@ncdot.gov

4009 District Drive Raleigh, NC 27607



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From: Andrew Eagle <<u>AEagle@rameykemp.com</u>>
Sent: Friday, April 14, 2023 8:37 AM
To: Warren, Jeremy L <<u>jlwarren@ncdot.gov</u>>; Nolfo, Matthew J <<u>mjnolfo@ncdot.gov</u>>
Cc: Jessica McClure <<u>jmcclure@rameykemp.com</u>>; Daniel Reisfeld <<u>dreisfeld@rameykemp.com</u>>
Subject: [External] RE: Hills at Harris Creek

CAUTION: External email. Do not click links or open attachments unless you verify. Send all suspicious email as an attachment to <u>Report Spam.</u>

Jeremy,

NCDOT approved the Hills at Harris Creek TIA in June of last year. The site plan has been changed, resulting in less density and fewer trips. The Town of Rolesville wants the TIA updated to match the latest site plan. Do you want an updated MOU, or can we revise the TIA and submit it via email with an explanation of the changes?

...and a heads up due to the similar names, this is a different project from Harris Creek Farm. NCDOT recently approved the MOU for that one on April 3.

Thanks,

Andrew Eagle, PE, PTOE Senior Traffic Engineering Project Manager D 704 220 6847 | C 704 467 0325



From: Warren, Jeremy L <<u>jlwarren@ncdot.gov</u>>
Sent: Friday, June 17, 2022 1:47 PM
To: Tucker Fulle <<u>tfulle@rameykemp.com</u>>
Cc: Nolfo, Matthew J <<u>mjnolfo@ncdot.gov</u>>; Brennan, Sean P <<u>spbrennan@ncdot.gov</u>>
Subject: FW: Hills at Harris Creek

Please see congestions comments.

Jeremy Warren, P.E. District Engineer Division 5, District 1 North Carolina Department of Transportation

919 733 3213 office jlwarren@ncdot.gov

4009 District Drive Raleigh, NC 27607



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From: Walker, Braden M <<u>bmwalker1@ncdot.gov</u>>
Sent: Thursday, June 16, 2022 9:32 AM
To: Warren, Jeremy L <<u>jlwarren@ncdot.gov</u>>
Cc: Lacy, Kevin <<u>jklacy1@ncdot.gov</u>>; Brennan, Sean P <<u>spbrennan@ncdot.gov</u>>; Grant, John H <<u>jhgrant@ncdot.gov</u>>; Keilson, David P <<u>dpkeilson@ncdot.gov</u>>; Ishak, Doumit Y <<u>dishak@ncdot.gov</u>>; Bunting, Clarence B
<<u>cbunting@ncdot.gov</u>>; Jones, Brandon H <<u>bhjones@ncdot.gov</u>>; Parrott, Tracy N <<u>tnparrott@ncdot.gov</u>>; Holmes, Benjamin W <<u>bwholmes@ncdot.gov</u>>; Mcneal, Douglas R <<u>dmcneal@ncdot.gov</u>>; Nolfo, Matthew J
<<u>mjnolfo@ncdot.gov</u>>
Subject: Hills at Harris Creek

Attached is a PDF copy of our final review letter for Hills at Harris Creek. This letter is only being distributed electronically and should be considered as the official documentation. If you have any questions, please contact me or Clarence Bunting.

Thank you,

Braden M. Walker, PE. Congestion Management Project Design Engineer Traffic Management Unit North Carolina Department of Transportation

919 814 5078 office bmwalker1@ncdot.gov

750 N. Greenfield Parkway Garner, NC 27529



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RAMEY KEMP ASSOCIATES

TOGETHER WE ARE LIMITLESS

T 919 872 5115 5808 Faringdon Pl, Raleigh, NC 27609

March 24, 2022

Meredith Gruber, PLA, AICP Town of Rolesville - Planning Director PO Box 250 502 Southtown Circle Rolesville, NC 27571 <u>meredith.gruber@rolesville.nc.gov</u> [Sent via Email]

Reference:	Hills at Harris Creek
	Rolesville, North Carolina

Subject: Memorandum of Understanding for TIA Report

Dear Ms. Gruber:

The following is a Memorandum of Understanding (MOU) outlining the proposed scope of work and assumptions related to the Traffic Impact Analysis (TIA) for the proposed Hills at Harris Creek development in Rolesville, North Carolina. The proposed development is to be located north of Mitchell Mill Road, west of Manly Farm Road, and east of Gro Peg Lane in Rolesville, NC. The development is expected to consist of 211 single-family homes, 109 townhomes, and 3.626 acres of commercial development. This MOU reflects the assumptions outlined during the initial coordination between Ramey Kemp Associates (RKA), the Town of Rolesville (Town), and the North Carolina Department of Transportation (NCDOT). Refer to the attached site location map. Site access to the proposed development is expected to be provided via two (2) full-movement driveway connections along Mitchell Mill Road. Refer to the attachments for a copy of the preliminary site plan.

The proposed development, anticipated to be completed in 2027, is expected to consist of 211 singlefamily homes, 109 townhomes, and 3.626 acres of commercial development. It should be noted that the commercial development land use(s) and intensity are not known at this time. Therefore, 7,000 square feet (sq. ft.) of general retail space per acre of land [approximately 25,400 sq. ft.] was assumed for the commercial development in this study. The proposed development is assumed to consist of the following land uses:

- 211 single-family homes
- 109 townhomes
- 25,400 sq. ft. of general retail



Study Area

Based on a coordination with NCDOT and Town staff, the study area is proposed to consist of the following intersections:

- Mitchell Mill Road & Jonesville Road / Peebles Road (unsignalized)
- US 401 Bypass and Jonesville Road (unsignalized)
- US 401 Bypass and Eastern U-Turn Location (unsignalized)
- Mitchell Mill Road and Site Driveways (2)

Existing Traffic Volumes

Existing peak hour traffic volumes will be determined based on previously collected traffic counts at the study intersections below, in November 2021 during typical weekday AM (7:00 AM – 9:00 AM) and PM (4:00 PM – 6:00 PM) peak periods, while schools were in session for in-person learning:

- Mitchell Mill Road & Jonesville Road / Peebles Road
- US 401 Bypass and Jonesville Road
- US 401 Bypass and Eastern U-Turn Location

These previously collected counts will be projected to the year 2022 using a compounded annual growth rate of 2%. Refer to the attachments for an illustration of 2022 existing peak hour traffic volumes.

Background Traffic Volumes

Based on coordination with NCDOT and the Town, background traffic volumes will be determined by projecting 2022 existing traffic volumes to the year 2027 using a 2% annual growth rate. Additionally, it was determined that the following adjacent developments are to be included in this study:

- Cobblestone Crossing Mixed-Use
- Young Street PUD
- Wheeler Tract
- Louisbury Road Assemblage
- Kalas / Watkins Family Property

Future Roadway Improvements

Based on coordination with the Town and NCDOT, it was determined that there are no future roadway improvements within the study area to consider under future traffic conditions.

Trip Generation

Average weekday daily, AM peak hour, and PM peak hour trips for the proposed development were estimated using methodology contained within the ITE *Trip Generation Manual*, 11th Edition. Refer to



Table 1, on the following page, for a summary of the proposed site trip generation for full buildout of the proposed development.

	Table 1: Trip Generation Summary												
Land Use (ITE Code)	Intensity			ntensity Traffic AM Peak Hour Trips				Weekday PM Peak Hour Trips (vph)					
		(vpd)	Enter	Exit	Total	Enter	Exit	Total					
Single-Family Home (210)	211 DU	2,010	38	109	147	126	74	200					
Multi-Family Home (Low-Rise) (220)	109 DU	770	14	43	57	42	25	67					
Retail (<40 KSF) (822)	25.4* KSF	1,300	32	21	53	75	76	151					
Total Trips	•	4,080	84	173	257	243	175	418					
Internal Captu (2% AM, 1% PN			-2	-3	-5	-5	-3	-8					
Total External Trips			82	170	252	238	172	410					
Pass-By Trips: Shoppi (34% PM)	-	-	-	-25	-25	-50							
Total Primary T	Total Primary Trips					213	147	360					

T-1.1. 1. T...

*Since the commercial development is unknown at this time, 7,000 SF of general retail space per acre of land [3.626 acres in total] was assumed for this land use.

**Utilizing methodology contained in the NCHRP Report 684.

It is estimated that the proposed development will generate approximately 4,080 site trips on the roadway network during a typical 24-hour weekday period. Of the daily traffic volume, it is anticipated that 257 trips (84 entering and 173 exiting) will occur during the weekday AM peak hour and 418 trips (243 entering and 175 exiting) will occur during the weekday PM peak hour.

Internal capture of trips between the retail and residential land uses was considered in this study. Internal capture is the consideration for trips that will be made within the site between different land uses, so the vehicle technically never leaves the internal site but can still be considered as a trip to that specific land use. Based on NCHRP Report 684 methodology, weekday AM and PM peak hour internal capture rates of 2% and 1%, respectively, were applied to the trips generated from the development. The internal capture reductions are expected to account for approximately 5 trips (2 entering and 3 exiting) during the weekday AM peak hour and 8 trips (5 entering and 3 exiting) during the weekday PM peak hour. Refer to the attached NCHRP internal capture reports for reference.

Pass-by trips will also be taken into consideration in this study. Pass-by trips are made by the traffic already using the adjacent roadway, entering the site as an intermediate stop on their way to another destination. Pass-by percentages are applied to site trips after adjustments for internal capture. Passby trips are expected to account for approximately 50 trips (25 entering and 25 exiting) during the



weekday PM peak hour. It should be noted that the pass-by trips were balanced, as it is likely that these trips would enter and exit in the same hour.

The total primary trips are the calculated site trips after the reduction for internal capture and pass-by trips. Primary site traffic is expected to generate approximately 252 trips (82 entering and 170 exiting) during the weekday AM peak hour, and 360 trips (213 entering and 147 exiting) during the weekday PM peak hour.

Trip Distribution and Assignment

Site trips are distributed based on the locations of existing traffic patterns, population centers adjacent to the study area, and engineering judgment. A summary of the overall distributions is below.

Residential

- 30% to/from the west via US 401 Bypass
- 15% to/from the east via US 401 Bypass
- 10% to/from the south via Peebles Road
- 35% to/from the west via Mitchell Mill Road
- 10% to/from the east via Mitchell Mill Road

Commercial

- 25% to/from the west via US 401 Bypass
- 15% to/from the east via US 401 Bypass
- 10% to/from the south via Peebles Road
- 40% to/from the west via Mitchell Mill Road
- 10% to/from the east via Mitchell Mill Road

Refer to the attached site trip distribution figures.

Analysis Scenarios

All capacity analyses will be performed utilizing Synchro (Version 10.3). All study intersections will be analyzed during the weekday AM and PM peak hours under the following proposed traffic scenarios:

- 2022 Existing Traffic Conditions
- 2027 No-Build Traffic Conditions
- 2027 Build Traffic Conditions



<u>Report</u>

The TIA report will be prepared based on the Town and NCDOT requirements.

If you find this memorandum of understanding acceptable, please let me know so that we may include it in the TIA report. If you have any questions or concerns, please do not hesitate to contact me.

Sincerely, *Ramey Kemp Associates*,

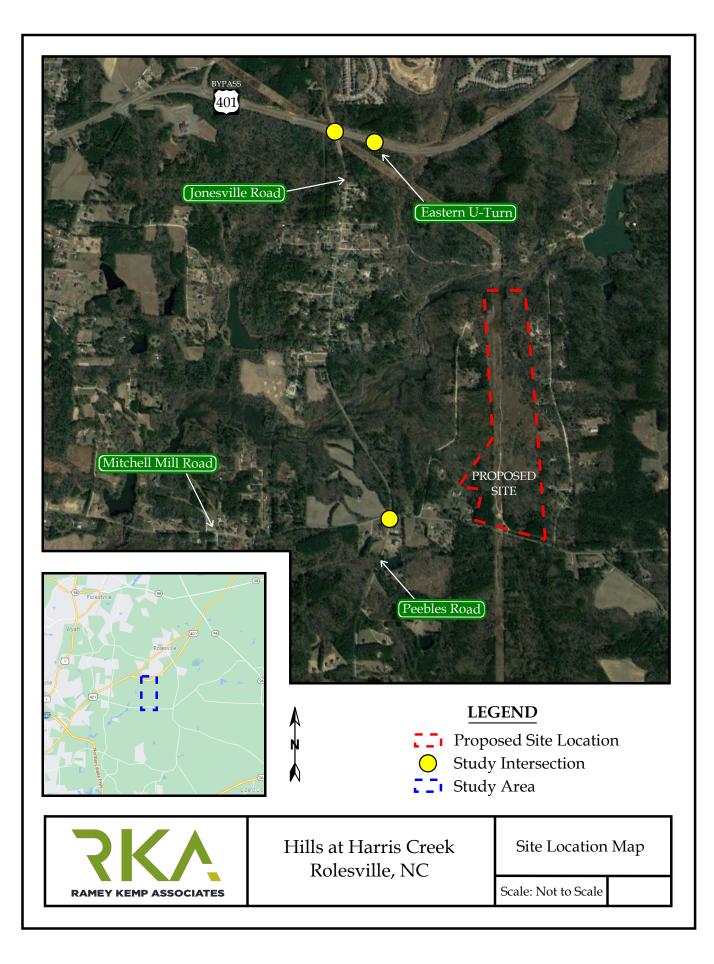
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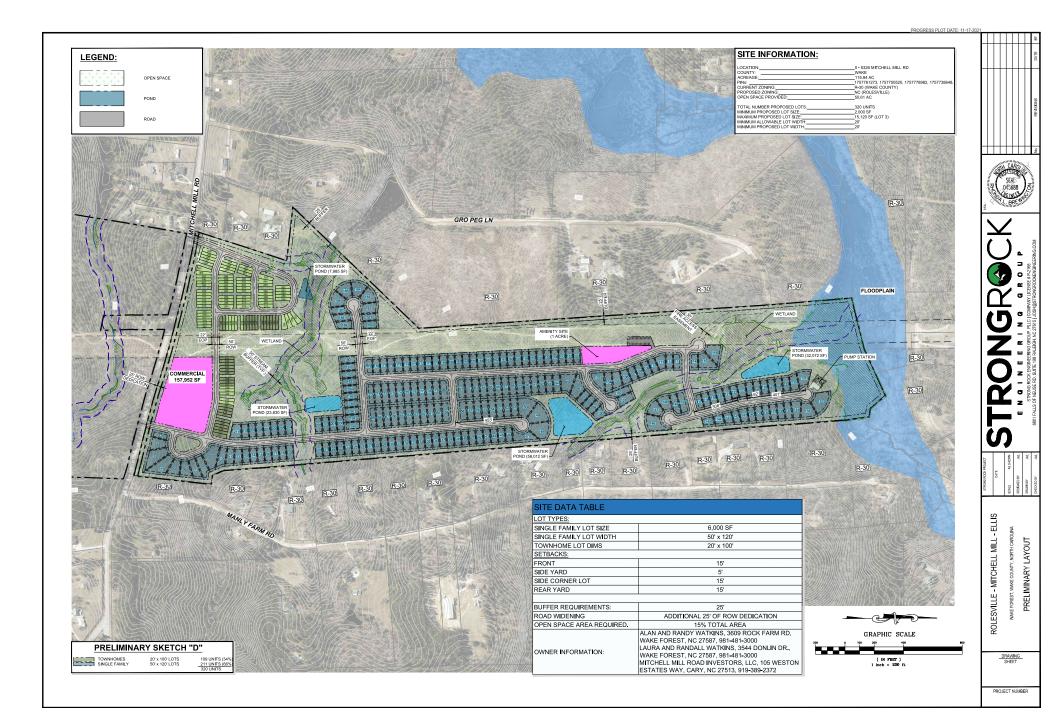
Michael Karpkinski, P.E. Traffic Engineering Project Manager

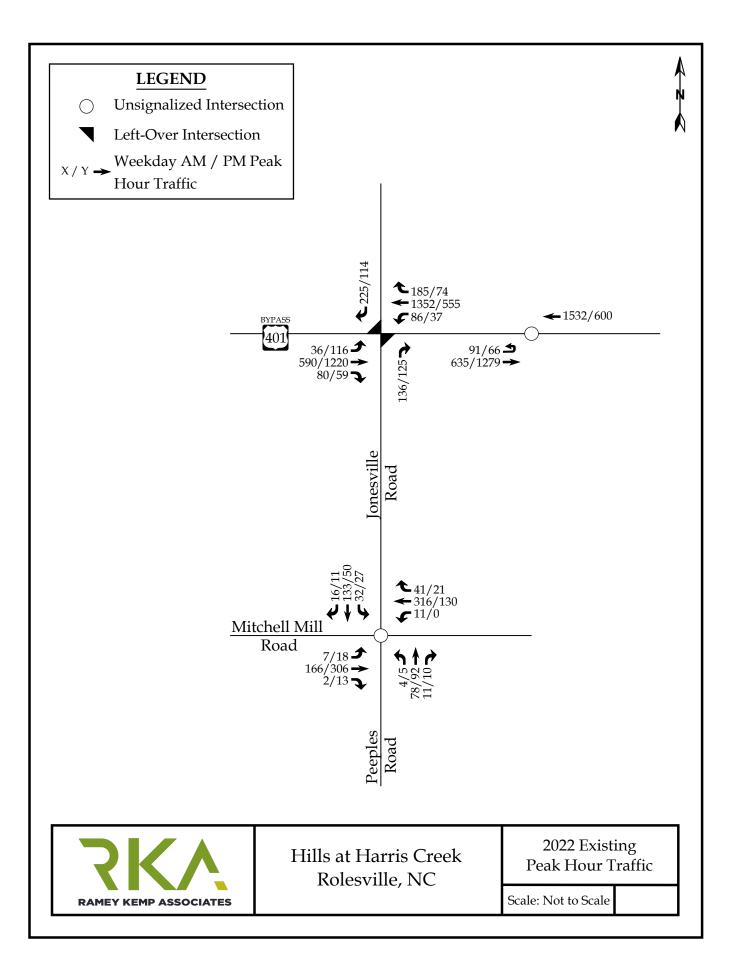
Attachments:

Site Location Map Site Plan 2022 Existing Traffic Volumes Figure NCHRP 684 Internal Capture Reports Proposed Site Trip Distribution Figures









	NCHRP 684 Internal Trip Capture Estimation Tool										
Project Name:	Hills at Harris Creek	Ramey Kemp & Associates									
Project Location:	Rolesville, NC		Performed By:	TF							
Scenario Description:	AM Street Peak Hour		Date:	3/18/2022							
Analysis Year:	20xx Build		Checked By:								
Analysis Period:	AM Street Peak Hour		Date:								

Table 1-A: Base Vehicle-Trip Generation Estimates (Single-Use Site Estimate)

Land Use	Development Data (For Information Only)				Estimated Vehicle-Trips ³				
Lanu Use	ITE LUCs ¹	Quantity	Units		Total	Entering	Exiting		
Office									
Retail	822	25,400	sq.ft.			32	21		
Restaurant									
Cinema/Entertainment									
Residential	210,220	211,109	units			52	152		
Hotel									
All Other Land Uses ²									
					0	84	173		

Table 2-A: Mode Split and Vehicle Occupancy Estimates												
Land Use		Entering Trip	os		Exiting Trips							
	Veh. Occ.4	% Transit	% Non-Motorized		Veh. Occ. ⁴	% Transit	% Non-Motorized					
Office	1.10	0%	0%		1.10	0%	0%					
Retail	1.10	0%	0%		1.10	0%	0%					
Restaurant	1.10	0%	0%		1.10	0%	0%					
Cinema/Entertainment	1.10	0%	0%		1.10	0%	0%					
Residential	1.10	0%	0%		1.10	0%	0%					
Hotel	1.10	0%	0%		1.10	0%	0%					
All Other Land Uses ²	1.10	0%	0%		1.10	0%	0%					

Table 3-A: Average Land Use Interchange Distances (Feet Walking Distance)												
Origin (From)		Destination (To)										
	Office	Retail	Restaurant	Cinema/Entertainment	Residential	Hotel						
Office												
Retail												
Restaurant												
Cinema/Entertainment												
Residential												
Hotel												

	Table 4-A: Internal Person-Trip Origin-Destination Matrix*									
Origin (From)	Destination (To)									
Oligili (Fioliti)	Office	Retail	Restaurant	Cinema/Entertainment	Residential	Hotel				
Office		0	0	0	0	0				
Retail	0		0	0	1	0				
Restaurant	0	0		0	0	0				
Cinema/Entertainment	0	0	0		0	0				
Residential	0	2	0	0		0				
Hotel	0	0	0	0	0					

Table 5-A:	Table 5-A: Computations Summary				Table 6-A: Internal Trip Capture Percentages by Land Use			
	Total	Entering	Exiting	Land Use	Entering Trips	Exiting Trips		
All Person-Trips	282	92	190	Office	N/A	N/A		
Internal Capture Percentage	2%	3%	2%	Retail	6%	4%		
				Restaurant	N/A	N/A		
External Vehicle-Trips ⁵	251	81	170	Cinema/Entertainment	N/A	N/A		
External Transit-Trips ⁶	0	0	0	Residential	2%	1%		
External Non-Motorized Trips ⁶	0	0	0	Hotel	N/A	N/A		

¹Land Use Codes (LUCs) from *Trip Generation Manual*, published by the Institute of Transportation Engineers.

²Total estimate for all other land uses at mixed-use development site is not subject to internal trip capture computations in this estimator.

³Enter trips assuming no transit or non-motorized trips (as assumed in ITE *Trip Generation Manual*).

⁴Enter vehicle occupancy assumed in Table 1-A vehicle trips. If vehicle occupancy changes for proposed mixed-use project, manual adjustments must be made to Tables 5-A, 9-A (O and D). Enter transit, non-motorized percentages that will result with proposed mixed-use project complete.

⁵Vehicle-trips computed using the mode split and vehicle occupancy values provided in Table 2-A.

⁶Person-Trips

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*Indicates computation that has been rounded to the nearest whole number.

Estimation Tool Developed by the Texas A&M Transportation Institute - Version 2013.1

Project Name:	Hills at Harris Creek
Analysis Period:	AM Street Peak Hour

Table 7-A: Conversion of Vehicle-Trip Ends to Person-Trip Ends								
Land Use	Tab	le 7-A (D): Enter	ring Trips		-	Table 7-A (O): Exiting Trips		
Lanu Ose	Veh. Occ.	Vehicle-Trips	Person-Trips*		Veh. Occ.	Vehicle-Trips	Person-Trips*	
Office	1.10	0	0		1.10	0	0	
Retail	1.10	32	35		1.10	21	23	
Restaurant	1.10	0	0]	1.10	0	0	
Cinema/Entertainment	1.10	0	0	1	1.10	0	0	
Residential	1.10	52	57]	1.10	152	167	
Hotel	1.10	0	0	1	1.10	0	0	

	Table 8-A (O): Internal Person-Trip Origin-Destination Matrix (Computed at Origin)									
Origin (From)	Destination (To)									
Oligin (FIBIN)	Office	Retail	Restaurant	Cinema/Entertainment	Residential	Hotel				
Office		0	0	0	0	0				
Retail	7		3	0	3	0				
Restaurant	0	0		0	0	0				
Cinema/Entertainment	0	0	0		0	0				
Residential	3	2	33	0		0				
Hotel	0	0	0	0	0					

Table 8-A (D): Internal Person-Trip Origin-Destination Matrix (Computed at Destination)											
Origin (From)		Destination (To)									
Origin (From)	Office	Retail	Restaurant	Cinema/Entertainment	Residential	Hotel					
Office		11	0	0	0	0					
Retail	0		0	0	1	0					
Restaurant	0	3		0	3	0					
Cinema/Entertainment	0	0	0		0	0					
Residential	0	6	0	0		0					
Hotel	0	1	0	0	0						

	Т	able 9-A (D): Int	ernal and External	Tri	ips Summary (Entering	Trips)		
Destination Land Use		Person-Trip Esti	mates		External Trips by Mode*			
Destination Land Ose	Internal	External	Total	1	Vehicles ¹	Transit ²	Non-Motorized ²	
Office	0	0	0	1	0	0	0	
Retail	2	33	35	1	30	0	0	
Restaurant	0	0	0	1	0	0	0	
Cinema/Entertainment	0	0	0	1	0	0	0	
Residential	1	56	57	1	51	0	0	
Hotel	0	0	0	1	0	0	0	
All Other Land Uses ³	0	0	0	1	0	0	0	

	٦	fable 9-A (O): In	ternal and Externation	al Ti	rips Summary (Exiting 1	rips)		
Origin Land Use		Person-Trip Esti	mates		External Trips by Mode*			
Origin Land Ose	Internal	External	Total	1	Vehicles ¹	Transit ²	Non-Motorized ²	
Office	0	0	0	1	0	0	0	
Retail	1	22	23	1	20	0	0	
Restaurant	0	0	0	1	0	0	0	
Cinema/Entertainment	0	0	0	1	0	0	0	
Residential	2	165	167	1	150	0	0	
Hotel	0	0	0	1	0	0	0	
All Other Land Uses ³	0	0	0	1	0	0	0	

¹Vehicle-trips computed using the mode split and vehicle occupancy values provided in Table 2-A

²Person-Trips

³Total estimate for all other land uses at mixed-use development site is not subject to internal trip capture computations in this estimator *Indicates computation that has been rounded to the nearest whole number.

	NCHRP 684 Internal Trip Capture Estimation Tool							
Project Name:	Ramey Kemp & Associates							
Project Location:	Rolesville, NC		Performed By:	TF				
Scenario Description:	AM Street Peak Hour		Date:	3/18/2022				
Analysis Year:	20xx Build		Checked By:					
Analysis Period:	PM Street Peak Hour		Date:					

	Table 1	-P: Base Vehic	le-Trip Generatio	ı Es	timates (Single-Use Site	e Estimate)		
Land Use	Developm	ent Data (For Inf	formation Only)		Estimated Vehicle-Trips ³			
	ITE LUCs ¹	Quantity	Units	1	Total	Entering	Exiting	
Office				1				
Retail	822	25,400	sq.ft.	1		75	76	
Restaurant				1				
Cinema/Entertainment				1				
Residential	210,220	211,109	units			168	99	
Hotel								
All Other Land Uses ²]				
					0	243	175	

	Table 2-P: Mode Split and Vehicle Occupancy Estimates								
Land Use		Entering Trip	os			Exiting Trips			
Land Use	Veh. Occ.4	% Transit	% Non-Motorized		Veh. Occ. ⁴	% Transit	% Non-Motorized		
Office	1.10	0%	0%		1.10	0%	0%		
Retail	1.10	0%	0%		1.10	0%	0%		
Restaurant	1.10	0%	0%		1.10	0%	0%		
Cinema/Entertainment	1.10	0%	0%		1.10	0%	0%		
Residential	1.10	0%	0%		1.10	0%	0%		
Hotel	1.10	0%	0%		1.10	0%	0%		
All Other Land Uses ²	1.10	0%	0%		1.10	0%	0%		

Table 3-P: Average Land Use Interchange Distances (Feet Walking Distance)										
Origin (From)		Destination (To)								
	Office	Retail	Restaurant	Cinema/Entertainment	Residential	Hotel				
Office		4000	4000		4000					
Retail					4000					
Restaurant					4000					
Cinema/Entertainment					4000					
Residential		4000	4000							
Hotel					4000					

Table 4-P: Internal Person-Trip Origin-Destination Matrix*											
Origin (From)		Destination (To)									
	Office	Retail	Restaurant	Cinema/Entertainment	Residential	Hotel					
Office		0	0	0	0	0					
Retail	0		0	0	2	0					
Restaurant	0	0		0	0	0					
Cinema/Entertainment	0	0	0		0	0					
Residential	0	1	0	0		0					
Hotel	0	0	0	0	0						

Table 5-P	: Computatio	ns Summary	Table 6-P: Internal Trip Capture Percentages by Land Use			
Total Entering Exiting		Land Use	Entering Trips	Exiting Trips		
All Person-Trips	461	268	193	Office	N/A	N/A
Internal Capture Percentage	1%	1%	2%	Retail	1%	2%
				Restaurant	N/A	N/A
External Vehicle-Trips ⁵	414	241	173	Cinema/Entertainment	N/A	N/A
External Transit-Trips ⁶	0	0	0	Residential	1%	1%
External Non-Motorized Trips ⁶	0	0	0	Hotel	N/A	N/A

¹Land Use Codes (LUCs) from *Trip Generation Manual*, published by the Institute of Transportation Engineers.

²Total estimate for all other land uses at mixed-use development site is not subject to internal trip capture computations in this estimator.

³Enter trips assuming no transit or non-motorized trips (as assumed in ITE *Trip Generation Manual*).

⁴Enter vehicle occupancy assumed in Table 1-P vehicle trips. If vehicle occupancy changes for proposed mixed-use project, manual adjustments must be made ⁵Vehicle-trips computed using the mode split and vehicle occupancy values provided in Table 2-P.

⁶Person-Trips

*Indicates computation that has been rounded to the nearest whole number.

Estimation Tool Developed by the Texas A&M Transportation Institute - Version 2013.1

Project Name:	Hills at Harris Creek
Analysis Period:	PM Street Peak Hour

Table 7-P: Conversion of Vehicle-Trip Ends to Person-Trip Ends									
Land Use	Table	Table 7-P (D): Entering Trips				Table 7-P (O): Exiting Trips			
	Veh. Occ.	Vehicle-Trips	Person-Trips*	1	Veh. Occ.	Vehicle-Trips	Person-Trips*		
Office	1.10	0	0	1	1.10	0	0		
Retail	1.10	75	83		1.10	76	84		
Restaurant	1.10	0	0		1.10	0	0		
Cinema/Entertainment	1.10	0	0	1	1.10	0	0		
Residential	1.10	168	185		1.10	99	109		
Hotel	1.10	0	0	1	1.10	0	0		

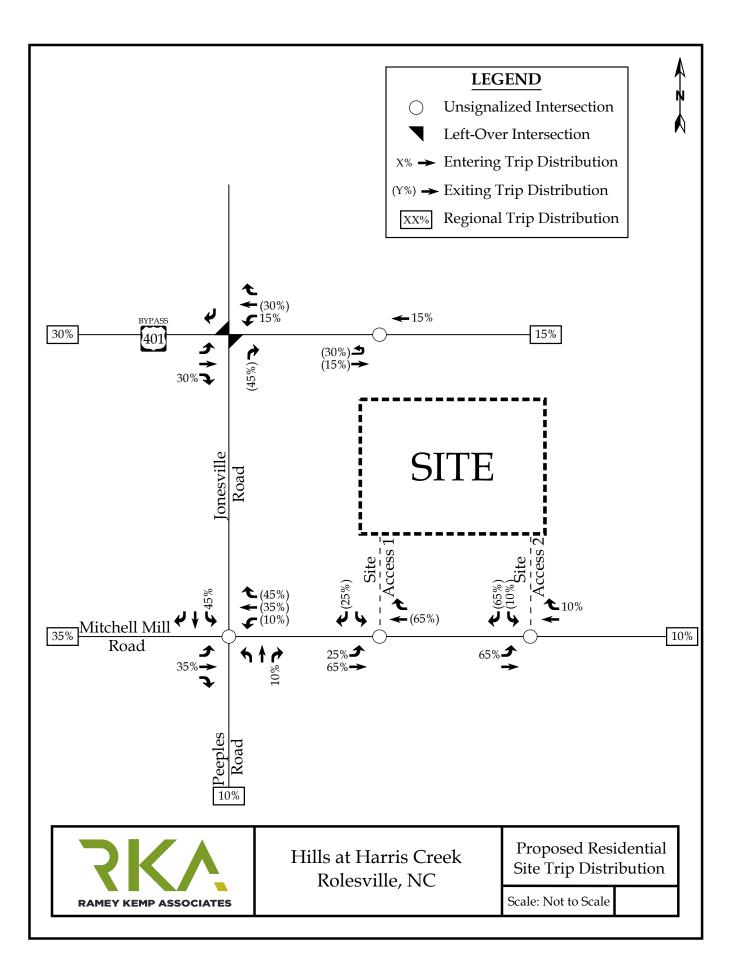
Table 8-P (O): Internal Person-Trip Origin-Destination Matrix (Computed at Origin)									
Origin (From)	Destination (To)								
	Office	Retail	Restaurant	Cinema/Entertainment	Residential	Hotel			
Office		0	0	0	0	0			
Retail	2		24	3	2	4			
Restaurant	0	0		0	0	0			
Cinema/Entertainment	0	0	0		0	0			
Residential	4	5	2	0		3			
Hotel	0	0	0	0	0				

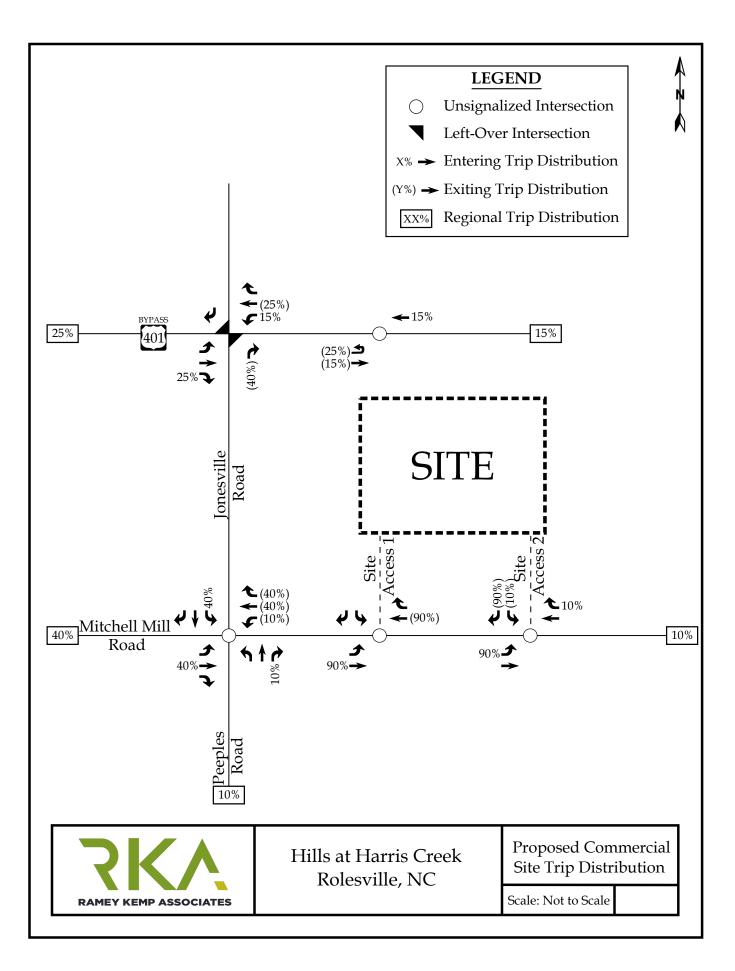
Table 8-P (D): Internal Person-Trip Origin-Destination Matrix (Computed at Destination)									
Origin (From)	Destination (To)								
	Office	Retail	Restaurant	Cinema/Entertainment	Residential	Hotel			
Office		1	0	0	7	0			
Retail	0		0	0	85	0			
Restaurant	0	42		0	30	0			
Cinema/Entertainment	0	3	0		7	0			
Residential	0	1	0	0		0			
Hotel	0	2	0	0	0				

Table 9-P (D): Internal and External Trips Summary (Entering Trips)								
Destination Land Use	Person-Trip Estimates				External Trips by Mode*			
Destination Land Ose	Internal	External	Total		Vehicles ¹	Transit ²	Non-Motorized ²	
Office	0	0	0		0	0	0	
Retail	1	82	83		75	0	0	
Restaurant	0	0	0		0	0	0	
Cinema/Entertainment	0	0	0		0	0	0	
Residential	2	183	185		166	0	0	
Hotel	0	0	0		0	0	0	
All Other Land Uses ³	0	0	0		0	0	0	

	Ta	ble 9-P (O): Inter	rnal and External	Trips	s Summary (Exiting Tr	ips)		
Origin Land Use	Person-Trip Estimates				External Trips by Mode*			
	Internal	External	Total	1 [Vehicles ¹	Transit ²	Non-Motorized ²	
Office	0	0	0	1 [0	0	0	
Retail	2	82	84	1 [75	0	0	
Restaurant	0	0	0	1 [0	0	0	
Cinema/Entertainment	0	0	0	1 [0	0	0	
Residential	1	108	109	1 [98	0	0	
Hotel	0	0	0	1 [0	0	0	
All Other Land Uses ³	0	0	0	1 [0	0	0	

¹Vehicle-trips computed using the mode split and vehicle occupancy values provided in Table 2-P ²Person-Trips ³Total estimate for all other land uses at mixed-use development site is not subject to internal trip capture computations in this estimator *Indicates computation that has been rounded to the nearest whole number.





APPENDIX B

TRAFFIC COUNTS



File Name : Rolesville(US 401 and Jonesville)AM Peak Site Code : Start Date : 11/9/2021 Page No : 1

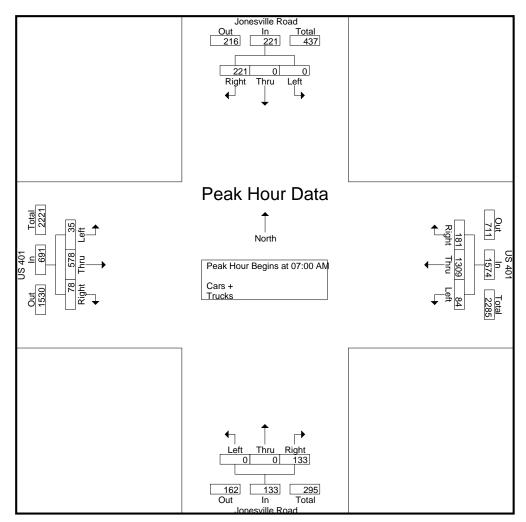
Grou	ps Pri	nted-	Cars	+ -	Trucks	

		Jonesvil		d		US	401			Jonesvil		d		US	401		
		South	bound			West	bound			North	<u>oound</u>			East	bound		
Start Time	Right	Thru	Left	App. Total	Right	Thru	Left	App. Total	Right	Thru	Left	App. Total	Right	Thru	Left	App. Total	Int. Total
07:00 AM	63	0	0	63	24	380	21	425	23	0	0	23	18	182	3	203	714
07:15 AM	42	0	0	42	39	362	24	425	37	0	0	37	11	125	7	143	647
07:30 AM	51	0	0	51	80	318	23	421	48	0	0	48	24	136	15	175	695
07:45 AM	65	0	0	65	38	249	16	303	25	0	0	25	25	135	10	170	563
Total	221	0	0	221	181	1309	84	1574	133	0	0	133	78	578	35	691	2619
00.00 414	01	0	0	64		220	10	075	22	0	0	22	20	100	10	100	540
08:00 AM	61	0	0	61	26	236	13	275	23	0	0	23	30	120	10	160	519
08:15 AM	36	0	0	36	12	233	9	254	16	0	0	16	13	94	9	116	422
08:30 AM	24	0	0	24	10	213	5	228	9	0	0	9	6	91	3	100	361
08:45 AM	28	0	0	28	9	145	5	159	10	0	0	10	11	85	2	98	295
Total	149	0	0	149	57	827	32	916	58	0	0	58	60	390	24	474	1597
Grand Total	370	0	0	370	238	2136	116	2490	191	0	0	191	138	968	59	1165	4216
Apprch %	100	Ő	õ	010	9.6	85.8	4.7	2100	100	Ő	Ő	101	11.8	83.1	5.1	1100	1210
Total %	8.8	Õ	Õ	8.8	5.6	50.7	2.8	59.1	4.5	0	Ő	4.5	3.3	23	1.4	27.6	
Cars +	366	0	0	366	233	2094	114	2441	188	0	0	188	135	916	57	1108	4103
% Cars +	98.9	Ō	Ō	98.9	97.9	98	98.3	98	98.4	Ō	Ō	98.4	97.8	94.6	96.6	95.1	97.3
Trucks	4	0	0	4	5	42	2	49	3	0	0	3	3	52	2	57	113
% Trucks	1.1	0	0	1.1	2.1	2	1.7	2	1.6	0	0	1.6	2.2	5.4	3.4	4.9	2.7



File Name : Rolesville(US 401 and Jonesville)AM Peak Site Code : Start Date : 11/9/2021 Page No : 2

		Jonesvi	lle Roa	d		US	401			Jonesvi	lle Roa	d		US	401]
		South	bound			West	bound			North	bound			East	bound		
Start Time	Right	Thru	Left	App. Total	Right	Thru	Left	App. Total	Right	Thru	Left	App. Total	Right	Thru	Left	App. Total	Int. Total
Peak Hour Ana	alysis Fro	om 07:0	0 AM t	o 08:45 A	M - Pea	ak 1 of 1			-				-				
Peak Hour for	Entire In	tersection	on Beg	ins at 07:	00 AM												
07:00 AM	63	0	0	63	24	380	21	425	23	0	0	23	18	182	3	203	714
07:15 AM	42	0	0	42	39	362	24	425	37	0	0	37	11	125	7	143	647
07:30 AM	51	0	0	51	80	318	23	421	48	0	0	48	24	136	15	175	695
07:45 AM	65	0	0	65	38	249	16	303	25	0	0	25	25	135	10	170	563
Total Volume	221	0	0	221	181	1309	84	1574	133	0	0	133	78	578	35	691	2619
% App. Total	100	0	0		11.5	83.2	5.3		100	0	0		11.3	83.6	5.1		
PHF	.850	.000	.000	.850	.566	.861	.875	.926	.693	.000	.000	.693	.780	.794	.583	.851	.917





File Name : Rolesville(US 401 and Jonesville)PM Peak Site Code : Start Date : 11/9/2021 Page No : 1

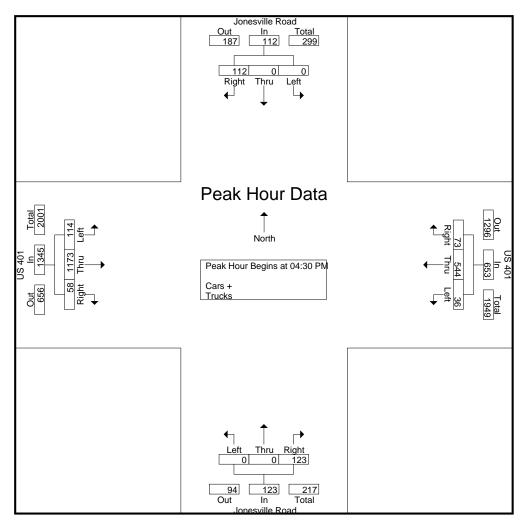
Groups Printed- Cars + - Trucks

		Jonesvil		d		US	401	Inited O		Jonesvi		d			401		
		South	bound			West	bound			North	bound			East	ound		
Start Time	Right	Thru	Left	App. Total	Right	Thru	Left	App. Total	Right	Thru	Left	App. Total	Right	Thru	Left	App. Total	Int. Total
04:00 PM	47	0	0	47	13	124	6	143	21	0	0	21	37	217	22	276	487
04:15 PM	34	0	0	34	13	119	6	138	26	0	0	26	15	231	20	266	464
04:30 PM	30	0	0	30	19	118	12	149	32	0	0	32	12	291	28	331	542
04:45 PM	15	0	0	15	22	137	6	165	32	0	0	32	8	303	30	341	553
Total	126	0	0	126	67	498	30	595	111	0	0	111	72	1042	100	1214	2046
	07	•	•	07	10	4.40	-	400		0	0			000		075	505
05:00 PM	37	0	0	37	10	143	7	160	23	0	0	23	23	322	30	375	595
05:15 PM	30	0	0	30	22	146	11	179	36	0	0	36	15	257	26	298	543
05:30 PM	39	0	0	39	20	145	3	168	34	0	0	34	23	262	14	299	540
05:45 PM	24	0	0	24	10	112	9	131	22	0	0	22	11	227	21	259	436
Total	130	0	0	130	62	546	30	638	115	0	0	115	72	1068	91	1231	2114
Grand Total	256	0	0	256	129	1044	60	1233	226	0	0	226	144	2110	191	2445	4160
			-	250	-	-		1255	-	0	0	220		-	-	2445	4100
Apprch %	100	0	0		10.5	84.7	4.9		100	0	0		5.9	86.3	7.8		
Total %	6.2	0	0	6.2	3.1	25.1	1.4	29.6	5.4	0	0	5.4	3.5	50.7	4.6	58.8	
Cars +	252	0	0	252	127	1020	60	1207	223	0	0	223	142	2051	191	2384	4066
% Cars +	98.4	0	0	98.4	98.4	97.7	100	97.9	98.7	0	0	98.7	98.6	97.2	100	97.5	97.7
Trucks	4	0	0	4	2	24	0	26	3	0	0	3	2	59	0	61	94
% Trucks	1.6	0	0	1.6	1.6	2.3	0	2.1	1.3	0	0	1.3	1.4	2.8	0	2.5	2.3



File Name : Rolesville(US 401 and Jonesville)PM Peak Site Code : Start Date : 11/9/2021 Page No : 2

		Jonesvi	lle Roa	d		US	401			Jonesvi	ille Roa	d		US	401]
		South	bound			West	bound			North	bound			Eastl	bound		
Start Time	Right	Thru	Left	App. Total	Right	Thru	Left	App. Total	Right	Thru	Left	App. Total	Right	Thru	Left	App. Total	Int. Total
Peak Hour Ana	ilysis Fro	om 04:0	0 PM t	o 05:45 P	M - Pea	ak 1 of 1			-				-				
Peak Hour for	Entire In	tersection	on Beg	ins at 04:	30 PM												
04:30 PM	30	0	0	30	19	118	12	149	32	0	0	32	12	291	28	331	542
04:45 PM	15	0	0	15	22	137	6	165	32	0	0	32	8	303	30	341	553
05:00 PM	37	0	0	37	10	143	7	160	23	0	0	23	23	322	30	375	595
05:15 PM	30	0	0	30	22	146	11	179	36	0	0	36	15	257	26	298	543
Total Volume	112	0	0	112	73	544	36	653	123	0	0	123	58	1173	114	1345	2233
% App. Total	100	0	0		11.2	83.3	5.5		100	0	0		4.3	87.2	8.5		
PHF	.757	.000	.000	.757	.830	.932	.750	.912	.854	.000	.000	.854	.630	.911	.950	.897	.938





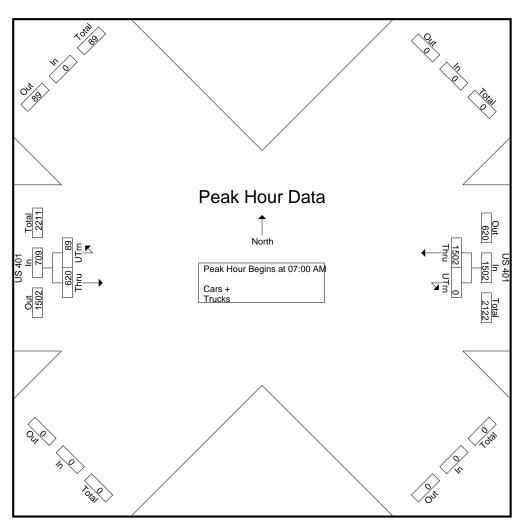
File Name : Rolesville(US 401 and Eastern U Turn)AM Peak Site Code : Start Date : 11/9/2021 Page No : 1

			Trucks	s Printed- Cars + -	Group		
		US 401			US 401		
		Eastbound			Westbound	1	
Int. Tota	App. Total	UTrn	Thru	App. Total	UTrn	Thru	Start Time
63	210	12	198	421	0	421	07:00 AM
57	160	24	136	410	0	410	07:15 AM
57	185	36	149	392	0	392	07:30 AM
43	154	17	137	279	0	279	07:45 AM
221	709	89	620	1502	0	1502	Total
40	150	20	130	253	0	253	08:00 AM
35	111	13	98	243	0	243	08:15 AM
32	101	7	94	223	0	223	08:30 AM
24	94	9	85	147	0	147	08:45 AM
132	456	49	407	866	0	866	Total
353	1165	138	1027	2368	0	2368	Grand Total
		11.8	88.2		0	100	Apprch %
	33	3.9	29.1	67	0	67	Total %
342	1109	136	973	2318	0	2318	Cars +
9	95.2	98.6	94.7	97.9	0	97.9	% Cars +
10	56	2	54	50	0	50	Trucks
	4.8	1.4	5.3	2.1	0	2.1	% Trucks



File Name : Rolesville(US 401 and Eastern U Turn)AM Peak Site Code : Start Date : 11/9/2021 Page No : 2

		US 401			US 401		
		Westbound			Eastbound		
Start Time	Thru	UTrn	App. Total	Thru	UTrn	App. Total	Int. Total
Peak Hour Analysis From 07:00	0 AM to 08:45 AM	- Peak 1 of 1					
Peak Hour for Entire Intersection	on Begins at 07:00	AM					
07:00 AM	421	0	421	198	12	210	631
07:15 AM	410	0	410	136	24	160	570
07:30 AM	392	0	392	149	36	185	577
07:45 AM	279	0	279	137	17	154	433
Total Volume	1502	0	1502	620	89	709	2211
% App. Total	100	0		87.4	12.6		
PHF	.892	.000	.892	.783	.618	.844	.876





File Name : Rolesville(US 401 and Eastern U Turn)PM Peak Site Code : Start Date : 11/9/2021 Page No : 1

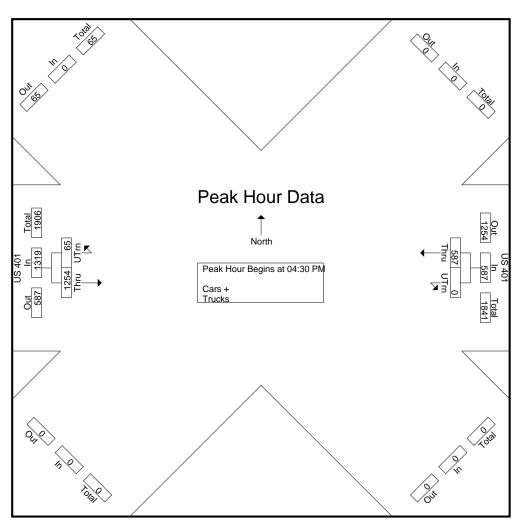
Groups Printed- Cars + - Trucks

		US 401		THUNKS	US 401		
		Westbound			Eastbound		
Start Time	Thru	UTrn	App. Total	Thru	UTrn	App. Total	Int. Total
04:00 PM	130	0	130	240	12	252	382
04:15 PM	128	0	128	237	15	252	380
04:30 PM	129	0	129	311	19	330	459
04:45 PM	149	0	149	317	19	336	485
Total	536	0	536	1105	65	1170	1706
05:00 PM	149	0	149	342	8	350	499
05:15 PM	160	0	160	284	19	303	463
05:30 PM	161	0	161	273	22	295	456
05:45 PM	120	0	120	235	12	247	367
Total	590	0	590	1134	61	1195	1785
Grand Total	1126	0	1126	2239	126	2365	3491
Apprch %	100	0		94.7	5.3		
Total %	32.3	0	32.3	64.1	3.6	67.7	
Cars +	1101	0	1101	2175	125	2300	3401
% Cars +	97.8	0	97.8	97.1	99.2	97.3	97.4
Trucks	25	0	25	64	1	65	90
% Trucks	2.2	0	2.2	2.9	0.8	2.7	2.6



File Name : Rolesville(US 401 and Eastern U Turn)PM Peak Site Code : Start Date : 11/9/2021 Page No : 2

		US 401			US 401		
		Westbound			Eastbound		
Start Time	Thru	UTrn	App. Total	Thru	UTrn	App. Total	Int. Total
Peak Hour Analysis From 04:00	OPM to 05:45 PM	Peak 1 of 1					
Peak Hour for Entire Intersection	on Begins at 04:30	PM					
04:30 PM	129	0	129	311	19	330	459
04:45 PM	149	0	149	317	19	336	485
05:00 PM	149	0	149	342	8	350	499
05:15 PM	160	0	160	284	19	303	463
Total Volume	587	0	587	1254	65	1319	1906
% App. Total	100	0		95.1	4.9		
PHF	.917	.000	.917	.917	.855	.942	.955





File Name : Rolesville(Jonesville and Mitchell Mill)AM Peak Site Code : Start Date : 11/30/2021 Page No : 1

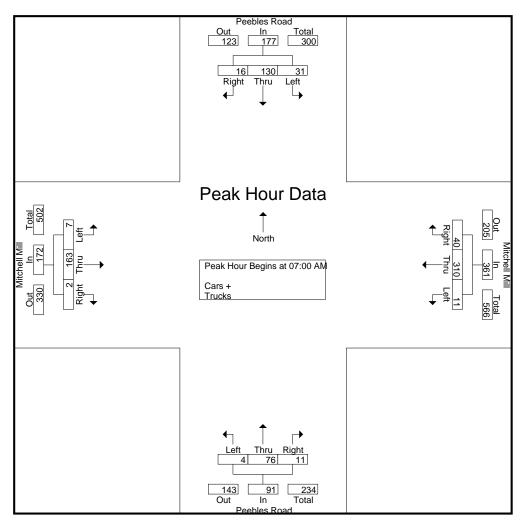
Groups Printed- Cars + - Trucks

		Peeble	s Road	4			ell Mill			Peeble	s Road	4		Mitch	ell Mill		
			bound				bound				bound				bound		
Start Time	Right	Thru	Left	App. Total	Right	Thru	Left	App. Total	Right	Thru	Left	App. Total	Right	Thru	Left	App. Total	Int. Total
07:00 AM	4	17	13	34	8	73	5	86	6	11	3	20	0	74	1	75	215
07:15 AM	4	36	7	47	8	101	2	111	3	26	1	30	0	32	1	33	221
07:30 AM	6	34	5	45	16	87	3	106	0	24	0	24	1	33	1	35	210
07:45 AM	2	43	6	51	8	49	1	58	2	15	0	17	1	24	4	29	155
Total	16	130	31	177	40	310	11	361	11	76	4	91	2	163	7	172	801
	_									_							
08:00 AM	7	31	12	50	4	53	1	58	1	8	2	11	0	28	3	31	150
08:15 AM	12	17	3	32	1	37	1	39	1	7	0	8	1	24	1	26	105
08:30 AM	6	4	2	12	3	49	2	54	1	4	2	7	0	19	0	19	92
08:45 AM	1	13	3	17	4	32	1	37	1	3	1	5	1	18	2	21	80
Total	26	65	20	111	12	171	5	188	4	22	5	31	2	89	6	97	427
Grand Total	42	195	51	288	52	481	16	549	15	98	9	122	4	252	13	269	1228
Apprch %	14.6	67.7	17.7	200	9.5	87.6	2.9	545	12.3	80.3	7.4	122	1.5	93.7	4.8	200	1220
Total %	3.4	15.9	4.2	23.5	4.2	39.2	1.3	44.7	12.5	8	0.7	9.9	0.3	20.5	1.1	21.9	
	42	195	<u>4.2</u> 50	23.5	<u>4.2</u> 52	<u> </u>	16	<u>44.7</u> 547	1.2	98	<u> </u>	<u>9.9</u> 122		249	13	21.9	1222
Cars +				-		-		-			-		4	-			
<u>% Cars +</u>	100	100	98	99.7	100	99.6	100	99.6	100	100	100	100	100	98.8	100	98.9	99.5
Trucks	0	0	1	1	0	2	0	2	0	0	0	0	0	3	0	3	6
% Trucks	0	0	2	0.3	0	0.4	0	0.4	0	0	0	0	0	1.2	0	1.1	0.5



File Name : Rolesville(Jonesville and Mitchell Mill)AM Peak Site Code : Start Date : 11/30/2021 Page No : 2

			s Road	ł			ell Mill				s Road				ell Mill]
		South	bound			West	bound			North	bound			East	bound		
Start Time	Right	Thru	Left	App. Total	Right	Thru	Left	App. Total	Right	Thru	Left	App. Total	Right	Thru	Left	App. Total	Int. Total
Peak Hour Ana	alysis Fro	om 07:0	00 AM t	o 08:45 A	M - Pea	ak 1 of 1											
Peak Hour for	Entire In	tersecti	on Beg	ins at 07:	00 AM												
07:00 AM	4	17	13	34	8	73	5	86	6	11	3	20	0	74	1	75	215
07:15 AM	4	36	7	47	8	101	2	111	3	26	1	30	0	32	1	33	221
07:30 AM	6	34	5	45	16	87	3	106	0	24	0	24	1	33	1	35	210
07:45 AM	2	43	6	51	8	49	1	58	2	15	0	17	1	24	4	29	155
Total Volume	16	130	31	177	40	310	11	361	11	76	4	91	2	163	7	172	801
% App. Total	9	73.4	17.5		11.1	85.9	3		12.1	83.5	4.4		1.2	94.8	4.1		
PHF	.667	.756	.596	.868	.625	.767	.550	.813	.458	.731	.333	.758	.500	.551	.438	.573	.906





File Name : Rolesville(Jonesville and Mitchell Mill)PM Peak Site Code : Start Date : 11/30/2021 Page No : 1

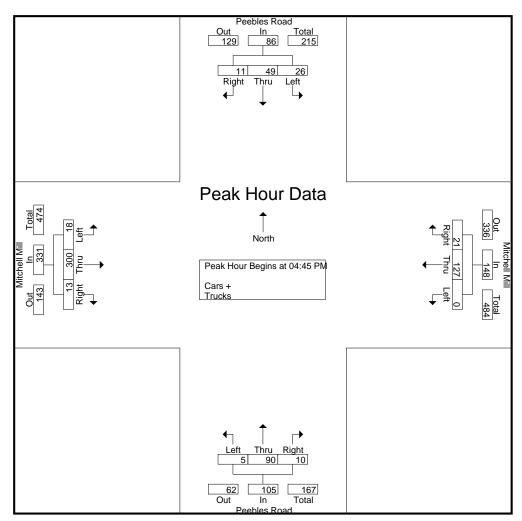
Groups Printed- Cars + - Trucks

		Peeble	s Road bound	ł		Mitch	ell Mill bound			Peeble	s Road	1			ell Mill oound		
Start Time	Right	Thru	Left	App. Total	Right	Thru	Left	App. Total	Right	Thru	Left	App. Total	Right	Thru	Left	App. Total	Int. Total
04:00 PM	7	11	13	31	6	25	1	32	1	14	1	16	2	44	6	52	131
04:15 PM	6	11	4	21	2	27	2	31	1	17	3	21	1	62	4	67	140
04:30 PM	3	13	3	19	4	30	2	36	0	27	1	28	3	64	3	70	153
04:45 PM	2	8	5	15	4	37	0	41	3	18	0	21	3	71	3	77	154
Total	18	43	25	86	16	119	5	140	5	76	5	86	9	241	16	266	578
05:00 PM	1	15	6	22	5	31	0	36	3	19	2	24	1	78	5	84	166
05:15 PM	3	15	6	24	4	23	Ō	27	3	26	1	30	4	89	7	100	181
05:30 PM	5	11	9	25	8	36	0	44	1	27	2	30	5	62	3	70	169
05:45 PM	1	7	4	12	2	21	1	24	2	13	2	17	4	55	6	65	118
Total	10	48	25	83	19	111	1	131	9	85	7	101	14	284	21	319	634
Grand Total	28	91	50	169	35	230	6	271	14	161	12	187	23	525	37	585	1212
Apprch %	16.6	53.8	29.6		12.9	84.9	2.2		7.5	86.1	6.4		3.9	89.7	6.3		
Total %	2.3	7.5	4.1	13.9	2.9	19	0.5	22.4	1.2	13.3	1	15.4	1.9	43.3	3.1	48.3	
Cars +	28	91	50	169	35	229	6	270	14	161	12	187	23	524	37	584	1210
% Cars +	100	100	100	100	100	99.6	100	99.6	100	100	100	100	100	99.8	100	99.8	99.8
Trucks	0	0	0	0	0	1	0	1	0	0	0	0	0	1	0	1	2
% Trucks	0	0	0	0	0	0.4	0	0.4	0	0	0	0	0	0.2	0	0.2	0.2



File Name : Rolesville(Jonesville and Mitchell Mill)PM Peak Site Code : Start Date : 11/30/2021 Page No : 2

	Peebles Road				Mitchell Mill				Peebles Road				Mitchell Mill]
	Southbound				Westbound				Northbound				Eastbound				
Start Time	Right	Thru	Left	App. Total	Right	Thru	Left	App. Total	Right	Thru	Left	App. Total	Right	Thru	Left	App. Total	Int. Total
Peak Hour Ana	eak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1																
Peak Hour for	Peak Hour for Entire Intersection Begins at 04:45 PM																
04:45 PM	2	8	5	15	4	37	0	41	3	18	0	21	3	71	3	77	154
05:00 PM	1	15	6	22	5	31	0	36	3	19	2	24	1	78	5	84	166
05:15 PM	3	15	6	24	4	23	0	27	3	26	1	30	4	89	7	100	181
05:30 PM	5	11	9	25	8	36	0	44	1	27	2	30	5	62	3	70	169
Total Volume	11	49	26	86	21	127	0	148	10	90	5	105	13	300	18	331	670
% App. Total	12.8	57	30.2		14.2	85.8	0		9.5	85.7	4.8		3.9	90.6	5.4		
PHF	.550	.817	.722	.860	.656	.858	.000	.841	.833	.833	.625	.875	.650	.843	.643	.828	.925



APPENDIX C

ADJACENT DEVELOPMENT INFORMATION

TRAFFIC IMPACT ANALYSIS

FOR

COBBLESTONE CROSSING MIXED-USE

LOCATED

IN

ROLESVILLE, NORTH CAROLINA

Prepared For: Town of Rolesville 502 Southtown Circle Rolesville, NC 27571

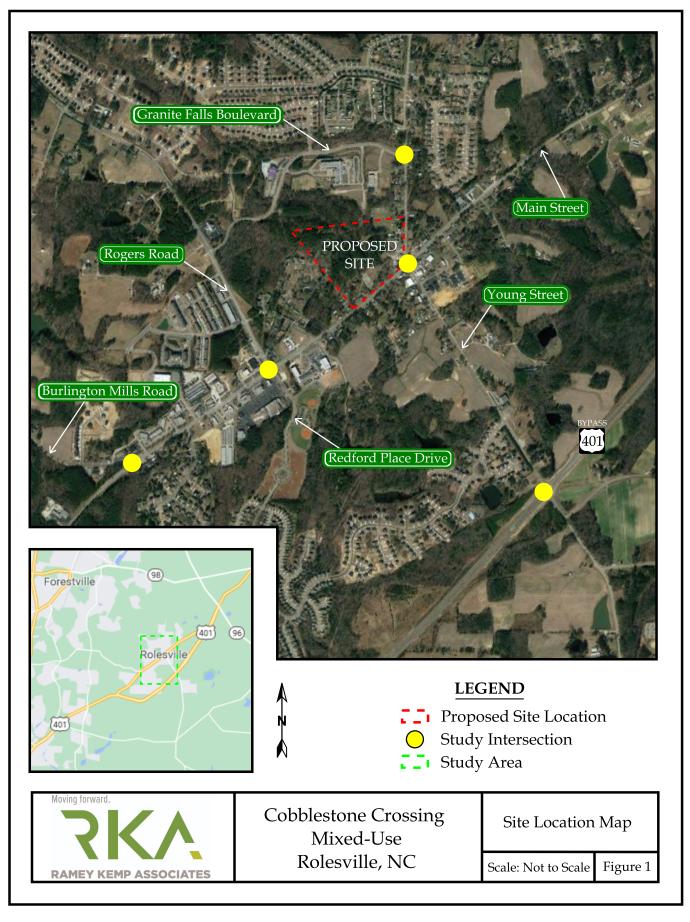
Prepared By: Ramey Kemp & Associates, Inc. 5808 Faringdon Place, Suite 100 Raleigh, NC 27609 License #C-0910

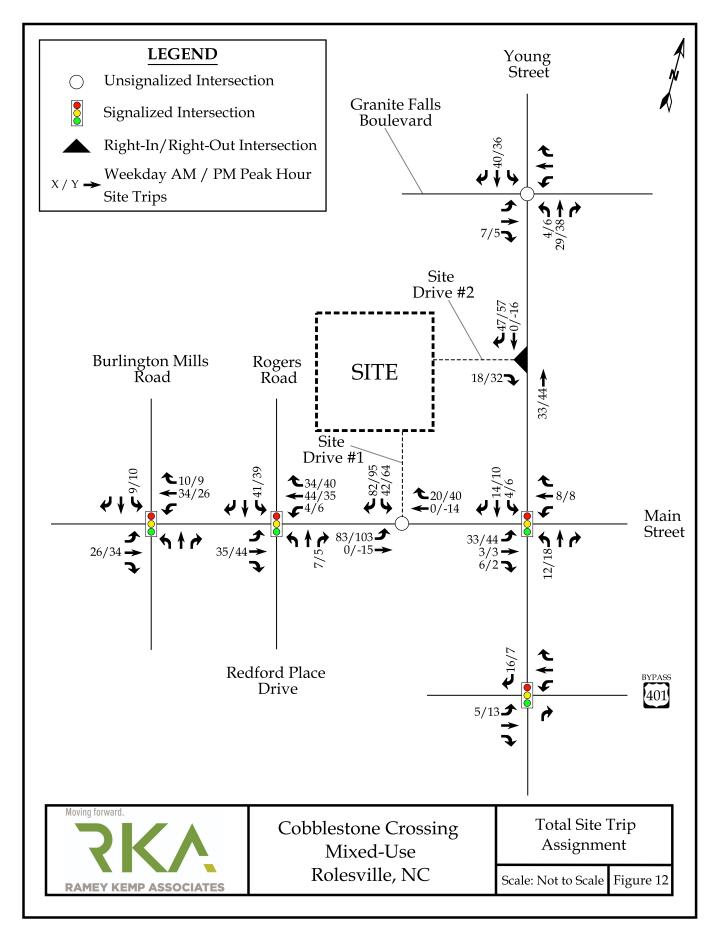
MARCH 2021



Prepared By: TF Reviewed By: MK

RKA Project No. 20498





9. RECOMMENDATIONS

Based on the findings of this study, specific geometric improvements have been identified and are recommended to accommodate future traffic conditions. See a more detailed description of the recommended improvements below. Refer to Figure 14 for an illustration of the recommended lane configuration for the proposed development.

Improvements by STIP U-6241

STIP U-6241 is expected to realign Burlington Mills Road and install a traffic signal at the relocated intersection on Main Street. STIP U-6241 is also expected to provide improvements to the pedestrian and bike facilities along Main Street and add a concrete median island along Main Street west of Rogers Road. These improvements associated with STIP U-6241 will alter the existing lane configurations at the study intersections along Main Street.

Recommended Improvements by Developer

Main Street and Site Drive 1

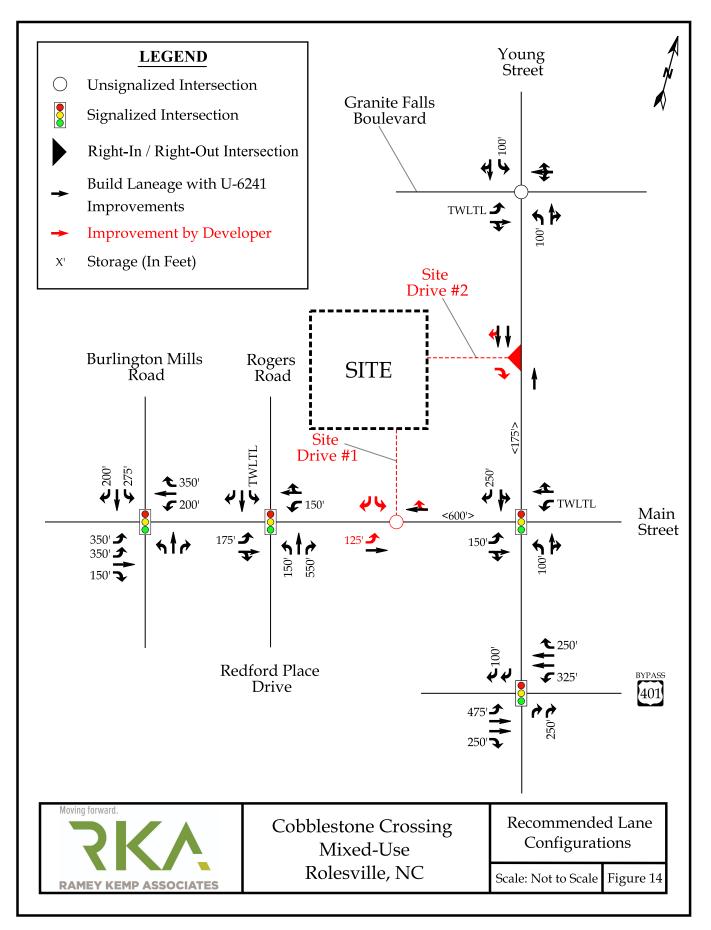
- Construct the southbound approach with one ingress and two egress lanes.
- Provide stop control for the southbound approach. ٠
- Install an eastbound left-turn lane with at least 125 feet of storage and appropriate decel ٠ and taper.

Young Street and Site Drive 2

- Construct the eastbound approach with one ingress and egress lane. •
- Provide stop control for the eastbound approach.



Consulting that moves us forward.



Revised Traffic Impact Analysis for

Young Street PUD

Rolesville, North Carolina

Prepared for: Ashton Woods Raleigh, North Carolina

Prepared by:

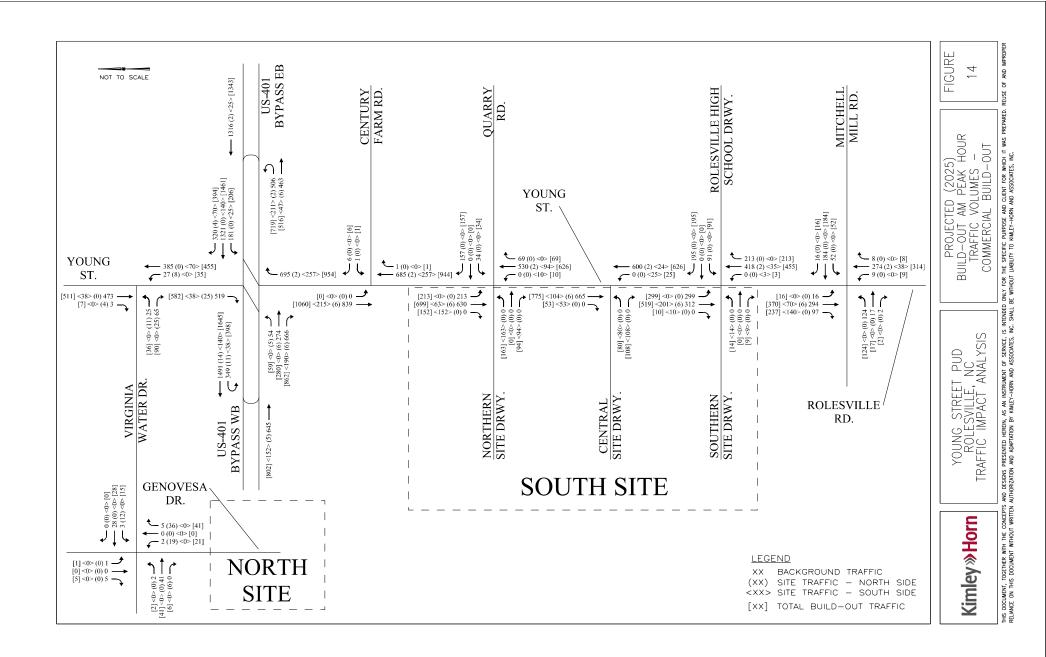
Kimley-Horn and Associates, Inc. NC License #F-0102 421 Fayetteville Street, Suite 600 Raleigh, NC 27601 (919) 677-2000

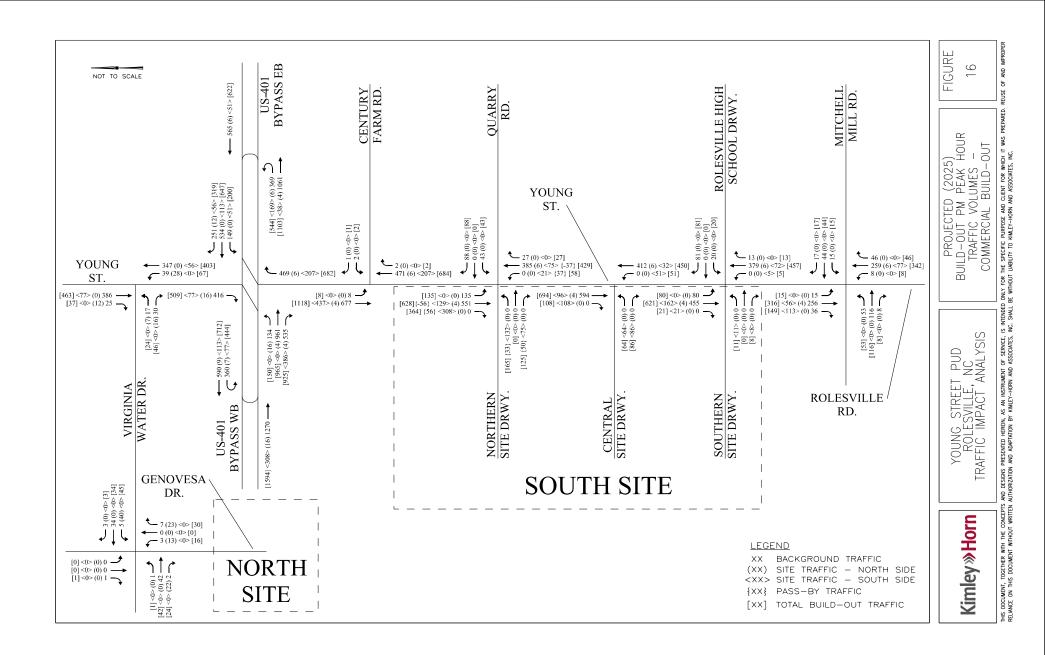
> June 2019 015956012





THIS DOCUMENT, TOGETHER WITH THE CONCEPTS AND DESIGNS PRESENTED HEREIN, AS AN INSTRUMENT OF SERVICE, IS INTENDED ONLY FOR THE SPECIFIC PURPOSE AND CLIENT FOR WHICH IT WAS PREPARED. REUSE OF AND IMPROPER RELIANCE ON THIS DOCUMENT WITHOUT WRITTEN AUTHORIZATION AND ADAPTATION BY KIMLEY-HORN AND ASSOCIATES, INC. SHALL BE WITHOUT LIABILITY TO KIMLEY-HORN AND ASSOCIATES, INC.





7.0 Recommendations

Residential Build-out

The following improvements are recommended to be performed to accommodate projected site traffic volumes at build-out of the residential portion of the development:

US 401 Bypass:

• Coordinate the traffic signals at the intersections of US 401 at Young Street and the Superstreet U-turns

Young Street at Quarry Road/North Site Driveway:

- Construct a northbound left-turn lane on Young Street with 100 feet of storage and appropriate tapers
- Construct a southbound right-turn lane on Young Street with 100 feet of storage and appropriate tapers
- Restripe the existing westbound left-turn lane on Quarry Road to a shared left/through lane
- Provide an exclusive left-turn lane with 275 feet of storage and appropriate tapers and a shared through/right lane on the North Site Driveway
- Install a traffic signal when warranted

Young Street at Central Site Driveway:

- Construct a northbound left-turn lane on Young Street with 100 feet of storage and appropriate tapers
- Construct a southbound right-turn lane on Young Street with 100 feet of storage and appropriate tapers
- Provide exclusive left and right-turn lanes on the Central Site Driveway with 125 feet of storage and appropriate tapers for the left-turn lane

Young Street at Rolesville High School Driveway/South Site Driveway:

- Construct a northbound left-turn lane on Young Street with 50 feet of storage and appropriate tapers
- Provide one egress lane on the South Site Driveway

Rolesville Road at Mitchell Mill Road:

• Install a traffic signal when warranted

Analyses indicate that with the recommended improvements in place, all of the study intersections except for Young Street at Century Farm Road and Young Street at Rolesville High School Driveway/South Site Driveway are expected to operate at an acceptable LOS at build-out of the residential-only phase of the development.

Kimley »Horn

Analyses indicate that the intersection of Young Street at Century Farm Road is expected to operate with long delays on the minor street approach (Century Farm Road) in the AM peak hour at project build-out. However, it is typical for stop sign controlled side streets and driveways intersecting major streets to experience long delays during peak hours while the majority of the traffic moving through the intersection on the major street experiences little or no delay. SimTraffic traffic simulations indicate that no queuing issues are expected at this intersection.

Analyses indicate that the intersection of Young Street at the Rolesville High School Driveway/South Site Driveway is expected to operate with long delays on the minor street approach (Rolesville High School Driveway) in the AM peak hour and school PM peak hour with or without the proposed project in place in the study year 2025. SimTraffic traffic simulations also indicate the possibility of long queues on the westbound left-turn movement at this intersection in the AM peak hour and school PM peak hour. However, it is typical for stop sign controlled side streets and driveways intersecting major streets to experience long delays during peak hours, while the majority of the traffic moving through the intersection on the major street experiences little or no delay. This intersection is not expected to meet 4-hour or 8-hour MUTCD traffic signal warrants.

Commercial Build-out

The following additional improvements are recommended to be performed in addition to those recommended above for the residential phase to accommodate projected site traffic volumes when the retail portion of the site is developed:

US 401 Bypass Eastbound at Young Street:

• Extend the storage of the existing eastbound right-turn lane on US 401 Bypass by approximately 175 feet to provide 400 feet of storage and appropriate tapers

Young Street at Quarry Road/North Site Driveway:

- Construct a northbound right-turn lane on Young Street with 100 feet of storage and appropriate tapers
- Modify the traffic signal to accommodate the additional laneage

Analyses indicate that with the recommended improvements in place, all of the study intersections except for Young Street at Century Farm Road, Young Street at the Central Site Driveway, and Young Street at Rolesville High School Driveway/South Site Driveway are expected to operate at acceptable LOS at commercial build-out of the development.

Analyses indicate that the intersection of Young Street at Century Farm Road is expected to operate with long delays on the minor street approach (Century Farm Road) in the AM peak hour at project build-out. It is typical for stop sign controlled side streets and driveways intersecting major streets to experience long delays during peak hours, while the majority of the traffic moving through the intersection on the major street experiences little or no delay. SimTraffic

Kimley *Whorn*

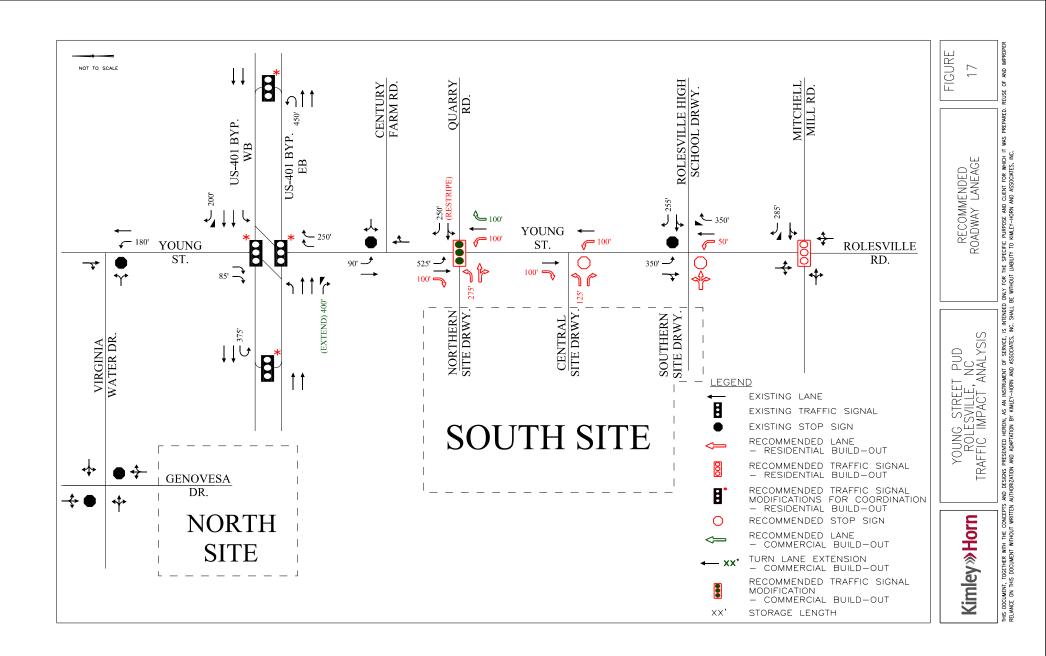
traffic simulations indicate that short queues are likely on the minor street approach in the AM peak hour at commercial build-out.

Analyses indicate that the intersection of Young Street at the Central Site Driveway is expected to operate with long delays on the minor street approach (Central Site Driveway) in the AM peak hour in the commercial build-out traffic condition. It is typical for stop sign controlled side streets and driveways intersecting major streets to experience long delays during peak hours, while the majority of the traffic moving through the intersection on the major street experiences little or no delay. SimTraffic traffic simulations indicate the possibility of long queues on the eastbound left-turn movement at this intersection in the AM peak hour in the commercial build-out condition.

Analyses indicate that the intersection of Young Street at the Rolesville High School Driveway/South Site Driveway is expected to operate with long delays on the minor street approach (Rolesville High School Driveway) in the AM peak hour and school PM peak hour with or without the proposed project in place in the study year 2025. SimTraffic traffic simulations also indicate the possibility of long queues on the westbound left-turn movement at this intersection in the AM peak hour and school PM peak hour. However, it is typical for stop sign controlled side streets and driveways intersecting major streets to experience long delays during peak hours, while the majority of the traffic moving through the intersection on the major street experiences little or no delay. This intersection is not expected to meet 4-hour or 8-hour MUTCD traffic signal warrants.

As shown in the analysis, the impact of site traffic associated with the commercial build-out of this proposed PUD is generally consistent with the currently-approved PUD for the site. The proposed PUD is expected to generate no more than 50 additional peak hour trips in each of the studied peak hours compared to the approved PUD, and delays at commercial build-out of both plans are generally consistent at each of the study intersections.

The recommended laneage for the development is shown on Figure 17.



TRAFFIC IMPACT ANALYSIS

FOR

WHEELER TRACT

LOCATED

IN

ROLESVILLE, NC

Prepared For: Hopper Communities 173 Paraggi Court Clayton, NC 27527

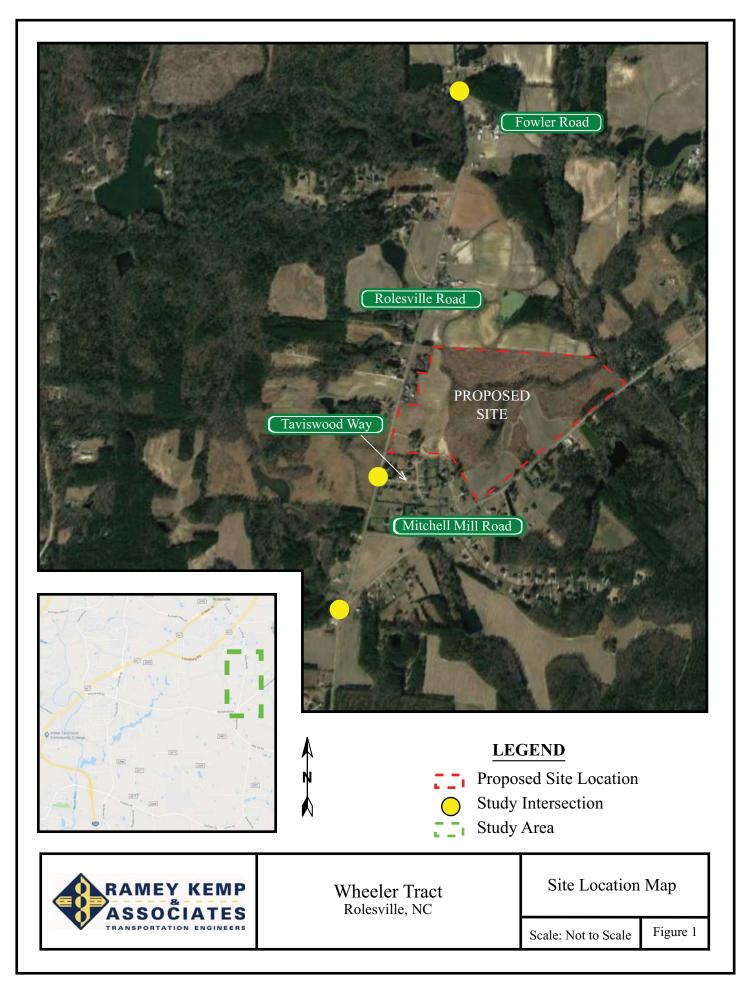
Prepared By: Ramey Kemp & Associates, Inc. 5808 Faringdon Place, Suite 100 Raleigh, NC 27609 License #C-0910

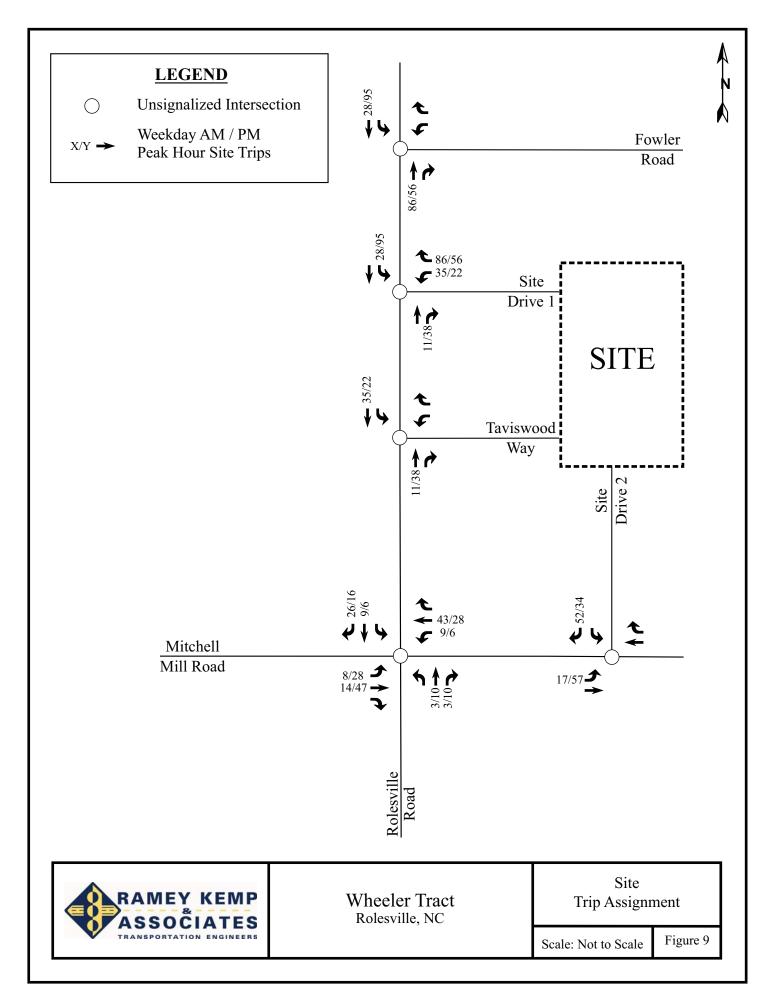
June 2019



Prepared By: <u>CAB</u> Reviewed By: JTR

RKA Project No. 19045





9. **RECOMMENDATIONS**

Based on the findings of this study, specific geometric improvements have been identified and are recommended to accommodate future traffic conditions. See a more detailed description of the recommended improvements below. Refer to Figure 11 for an illustration of the recommended lane configuration for the proposed development.

Recommended Improvements by Developer

Rolesville Road and Mitchell Mill Road

• Monitor intersection for signalization.

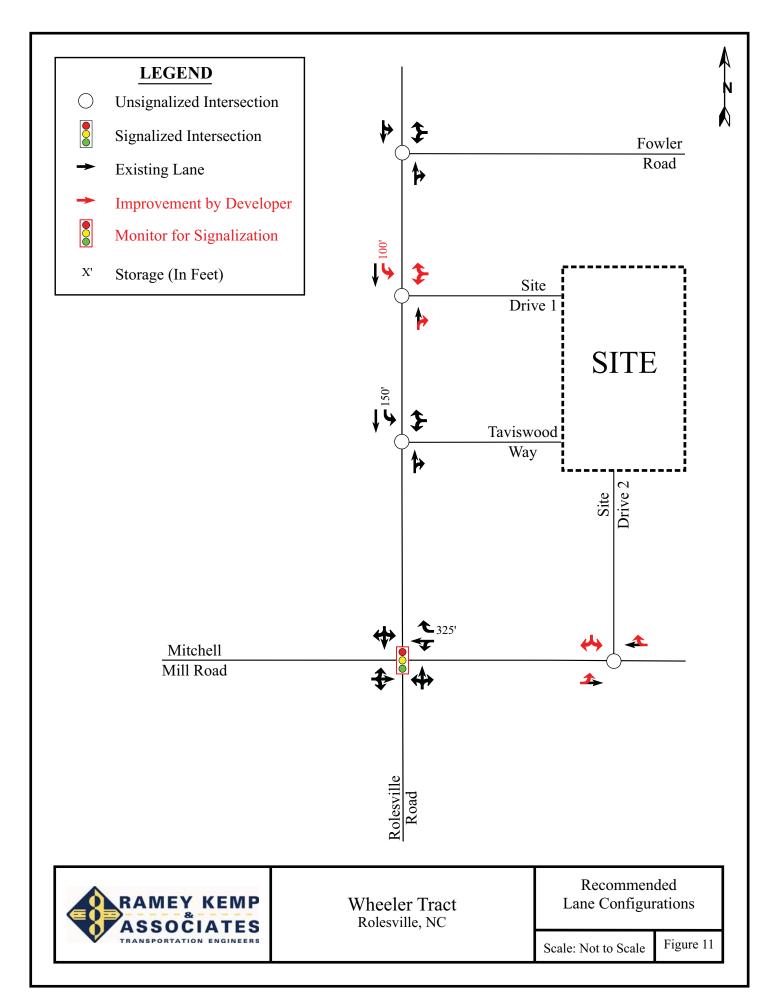
Rolesville Road and Site Drive 1

- Provide site access via a full movement intersection with one ingress lane and one egress lane.
- Provide stop control for westbound Site Drive 1 approach.
- Provide a designated southbound left-turn lane with at least 100 feet of storage and appropriate deceleration and taper.

Mitchell Mill Road and Site Drive 2

- Provide site access via a full movement intersection with one ingress lane and one egress lane.
- Provide stop control for southbound Site Drive 2 approach.





TRAFFIC IMPACT ANALYSIS

FOR

LOUISBURY ROAD ASSEMBLAGE

LOCATED

IN

RALEIGH, NC

Prepared For: McAdams Company 2905 Meridian Parkway Durham, NC 27713

Prepared By: Ramey Kemp & Associates, Inc. 5808 Faringdon Place, Suite 100 Raleigh, NC 27609 License #C-0910

andrew Ryle Rithe

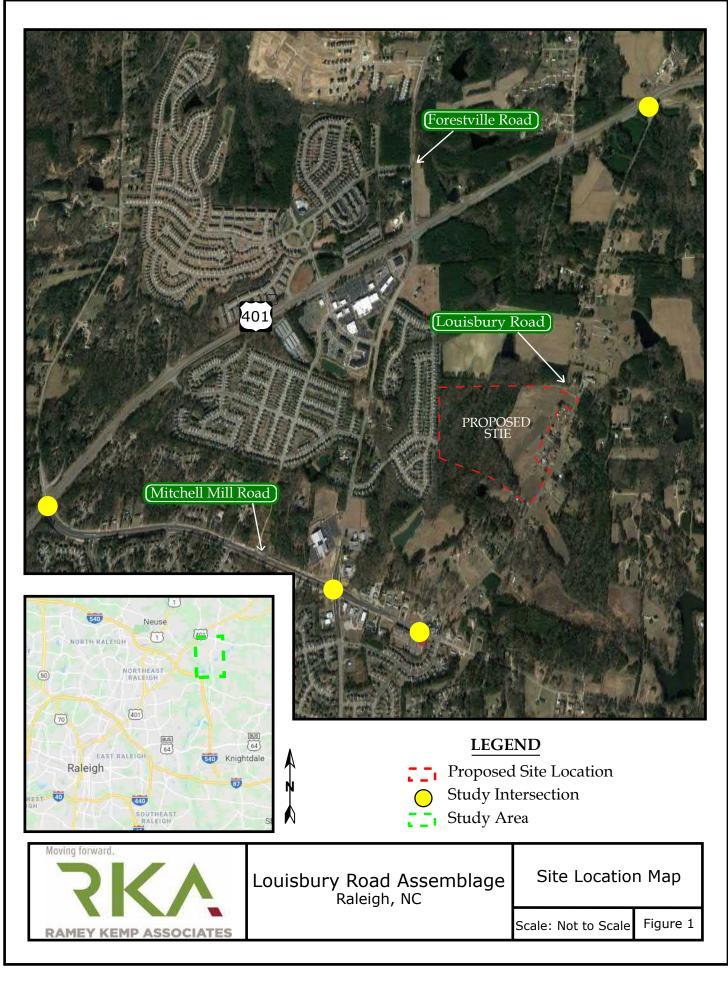
SEAL 047058 5/8/2020

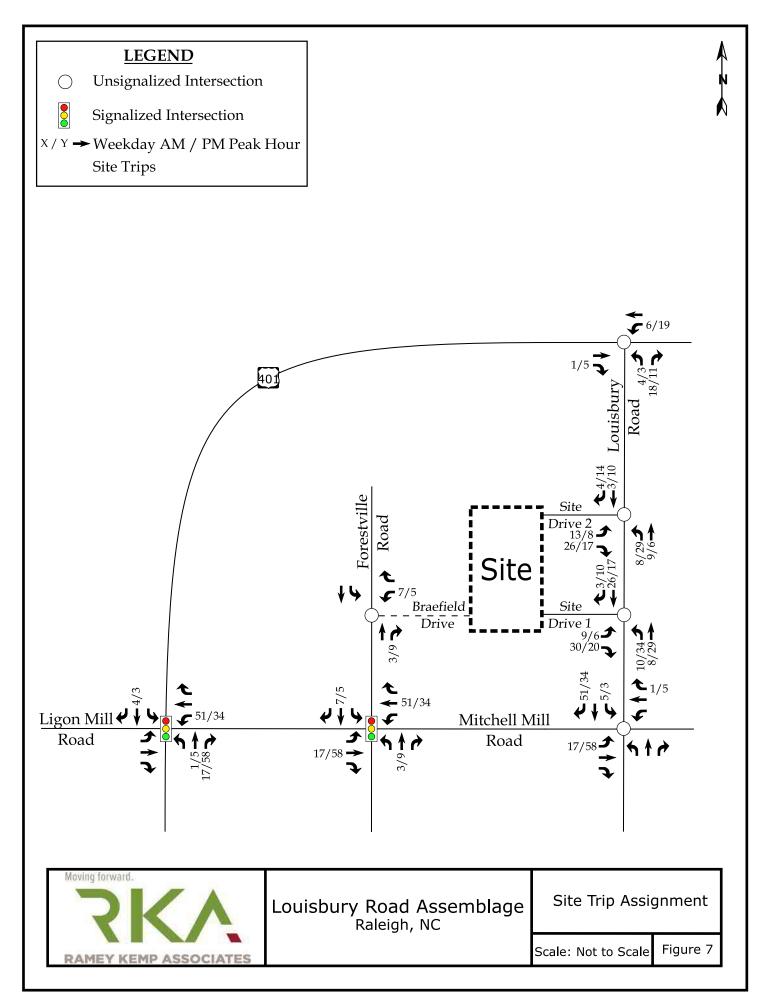
May 2020

Prepared By: <u>DT</u>

Reviewed By: DR

RKA Project No. 19418





12. RECOMMENDATIONS

Based on the findings of this study, specific geometric improvements have been identified and are recommended to accommodate future traffic conditions. See a more detailed description of the recommended improvements below. Refer to Figure 9 for an illustration of the recommended lane configuration for the proposed development.

Recommended Improvements by Developer

Mitchell Mill Road and Louisbury Road

• Monitor for signalization after site is constructed.

US 401 and Louisbury Road

- Per NCDOT, extend northbound left turn lane to 175' of storage.
- Monitor for signalization after site is constructed.

Louisbury Road and Site Drive 1

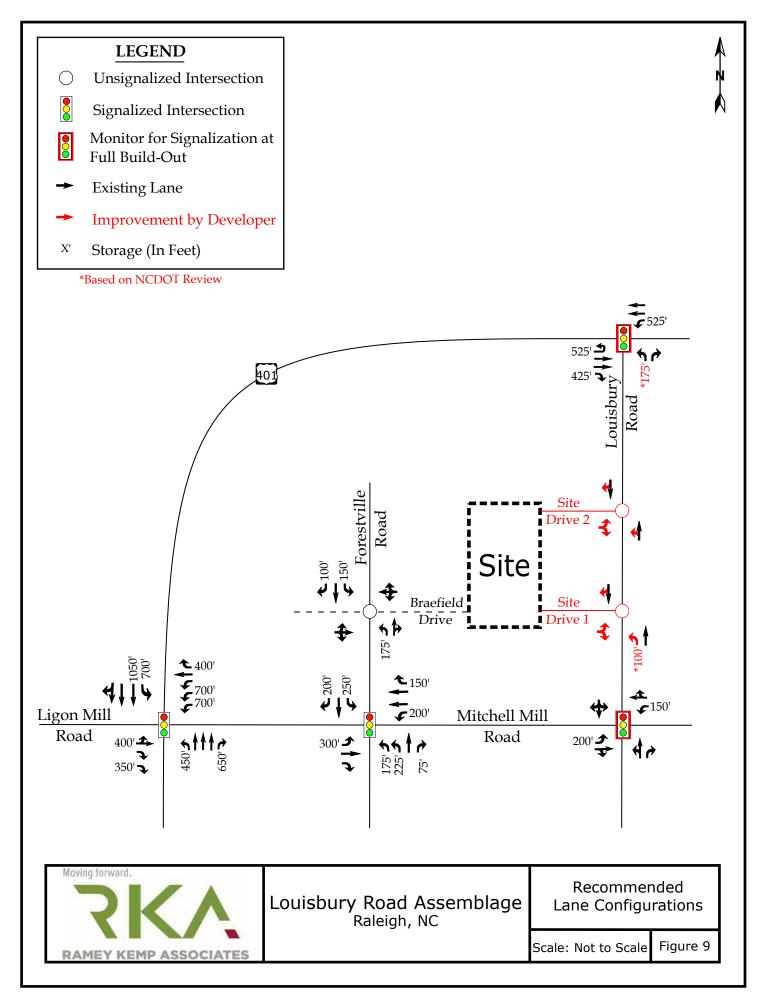
- Provide site access via full movement intersection with one (1) ingress lane and one (1) egress lane.
- Per NCDOT, provide northbound left turn lane with 100' of storage.
- Provide stop control for eastbound approach.

Louisbury Road and Site Drive 2

- Provide site access via full movement intersection with one (1) ingress lane and one (1) egress lane.
- Provide stop control for eastbound approach.



Transportation Consulting that moves us forward.





Kalas / Watkins Family Property Traffic Impact Analysis

Rolesville Road, Rolesville, North Carolina

August 24, 2019

Prepared for:

Mitchell Mill Road Investors LLC PO Box 3557 Cary, NC 27519

Prepared by:

Stantec Consulting Services Inc.

801 Jones Franklin Road Suite 300 Raleigh, NC 27606

Sign-off Sheet

This document entitled Kalas / Watkins Family Property Traffic Impact Analysis was prepared by Stantec Consulting Services Inc. ("Stantec") for the account of Mitchell Mill Road Investors LLC (the "Client"). Any reliance on this document by any third party is strictly prohibited. The material in it reflects Stantec's professional judgment in light of the scope, schedule and other limitations stated in the document and in the contract between Stantec and the Client. The opinions in the document are based on conditions and information existing at the time the document was published and do not take into account any subsequent changes. In preparing the document, Stantec did not verify information supplied to it by others. Any use which a third party makes of this document is the responsibility of such third party. Such third party agrees that Stantec shall not be responsible for costs or damages of any kind, if any, suffered by it or any other third party as a result of decisions made or actions taken based on this document.

Prepared by

(signature)

Maggie Rogers

Reviewed by __

2

(signature)

Matt Peach, PE, PTOE une Approved by

(signature)

Christa Greene, PE



Introduction August 24, 2019

1.0 INTRODUCTION

The purpose of this report is to evaluate the transportation impacts of the proposed Kalas / Watkins Family Property development located on the west side of Rolesville Road just north of Mitchell Mill Road in Rolesville, NC. The project location is shown below in Figure 1.

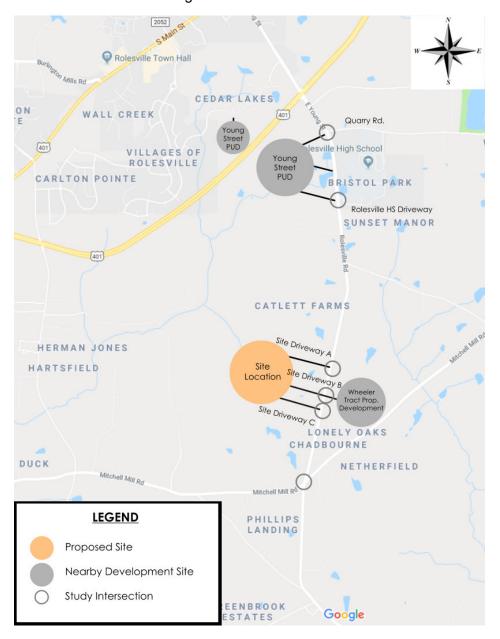


Figure 1: Site Location

KALAS / WATKINS FAMILY PROPERTY TRAFFIC IMPACT ANALYSIS

Trip Generation and Distribution August 24, 2019

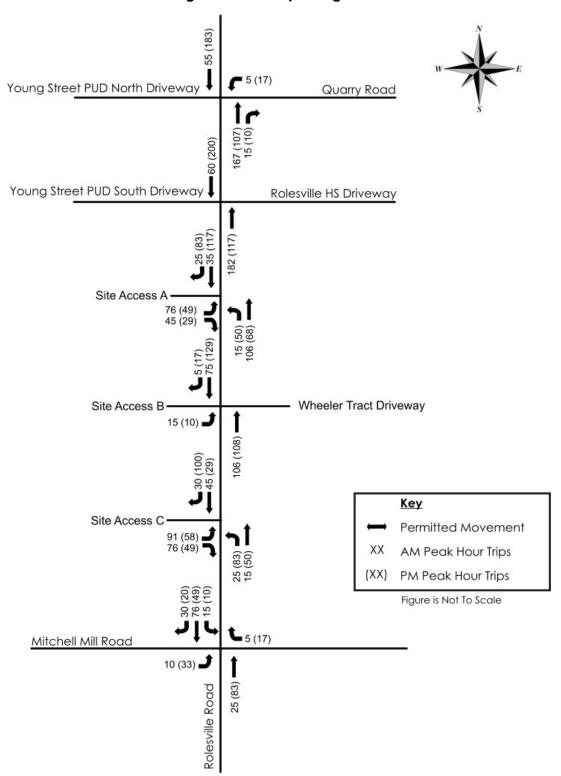


Figure 6: Site Trip Assignment

Traffic Analysis August 24, 2019

5.4 2025 BUILD WITH IMPROVEMENTS

Geometric improvements such as the installation of turn-lanes are recommended and therefore analyzed in this scenario. These items are listed below as well as in the recommendations section.

Rolesville Road at Site Driveway A

- Construct Driveway A as a full-movement access point onto Rolesville Road with one ingress lane and one
 egress lane.
- Construct an exclusive eastbound right-turn lane with 100 feet of full-width storage and appropriate taper on Driveway A.
- Construct an exclusive northbound left-turn lane with 100 feet of full-width storage and appropriate taper on Rolesville Road.
- Construct an exclusive southbound right-turn lane with 100 feet of full-width storage and appropriate taper on Rolesville Road.

Rolesville Road at Site Driveway B / Wheeler Tract Driveway

- Construct Driveway B as a full-movement access point onto Rolesville Road with one ingress lane and one egress lane.
- Construct an exclusive northbound left-turn lane with 100 feet of full-width storage and appropriate taper on Rolesville Road.
- Construct an exclusive southbound right-turn lane with 50 feet of full-width storage and appropriate taper on Rolesville Road.

Rolesville Road at Site Driveway C

- Construct Driveway C as a full-movement access point onto Rolesville Road with one ingress lane and one egress lane.
- Construct an exclusive eastbound right-turn lane with 100 feet of full-width storage and appropriate taper on Driveway C.
- Construct an exclusive northbound left-turn lane with 100 feet of full-width storage and appropriate taper on Rolesville Road.
- Construct an exclusive southbound right-turn lane with 100 feet of full-width storage and appropriate taper on Rolesville Road.

Accordingly, all study area intersections and approaches operate at acceptable levels of service with the following exceptions:

- The east and westbound approaches to the intersection of Rolesville Road at Rolesville High School Driveway / Young Street PUD Southern Driveway operates at LOS F in the AM peak hour. This causes high overall delays at the intersection. Furthermore, the eastbound approach operates at LOS F and westbound approach operates at LOS E in the PM peak hour.
- The east and westbound approaches at the intersection of Rolesville Road at Site Driveway B / Wheeler Tract Driveway operate at LOS E in the AM peak hour.

The east and westbound approaches to the intersection of Rolesville Road at Rolesville High School Driveway / Young Street PUD Southern Driveway performs unacceptably across analysis scenarios. These delays can be



KALAS / WATKINS FAMILY PROPERTY TRAFFIC IMPACT ANALYSIS

Traffic Analysis August 24, 2019

attributed to both the Young Street PUD and High School traffic on the side street approaches. The Kalas / Watkins development is projected to only add through volumes to the intersection and are anticipated to have a minimal impact on overall delays at this intersection.

Delays on the eastbound approach of Site Driveway B at Rolesville Road can be attributed to high thru volumes on Rolesville Road during the AM peak hour. Traffic volumes using this approach are anticipated to be minor (i.e. 15 vehicles in the AM peak hour and 10 vehicles in the PM peak hour) and side street delays should dissipate after High School Traffic passes through the network. Table 8 lists the results of the capacity analysis under the 2025 build-improved traffic conditions. The recommended improvements are illustrated in figure 14.

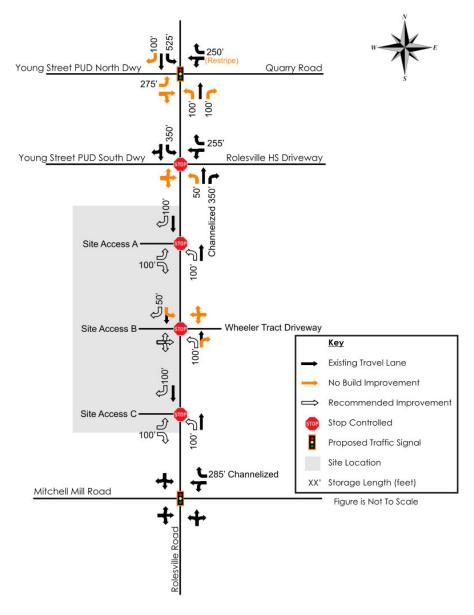


Figure 14: Recommended Improvements



APPENDIX D

CAPACITY ANALYSIS CALCULATIONS US 401 BYPASS & JONESVILLE ROAD

Intersection

Int Delay, s/veh

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	
Lane Configurations		^	1						1		^		
Traffic Vol, veh/h	0	590	80	0	0	0	0	0	136	0	86	0	
Future Vol, veh/h	0	590	80	0	0	0	0	0	136	0	86	0	
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0	
Sign Control	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop	Stop	Stop	Stop	
RT Channelized	-	-	Yield	-	-	None	-	-	None	-	-	None	
Storage Length	-	-	125	-	-	-	-	-	0	-	-	-	
Veh in Median Storage,	# -	0	-	-	16983	-	-	0	-	-	0	-	
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-	
Peak Hour Factor	90	90	90	90	90	90	90	90	90	90	90	90	
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2	
Mvmt Flow	0	656	89	0	0	0	0	0	151	0	96	0	

Major/Minor	Major1				Minor1		Ν	/linor2			
Conflicting Flow All	-	0	0		-	-	328	-	656	-	
Stage 1	-	-	-		-	-	-	-	0	-	
Stage 2	-	-	-		-	-	-	-	656	-	
Critical Hdwy	-	-	-		-	-	6.94	-	6.54	-	
Critical Hdwy Stg 1	-	-	-		-	-	-	-	-	-	
Critical Hdwy Stg 2	-	-	-		-	-	-	-	5.54	-	
Follow-up Hdwy	-	-	-		-	-	3.32	-	4.02	-	
Pot Cap-1 Maneuver	0	-	-		0	0	668	0	384	0	
Stage 1	0	-	-		0	0	-	0	-	0	
Stage 2	0	-	-		0	0	-	0	460	0	
Platoon blocked, %		-	-								
Mov Cap-1 Maneuver	-	-	-		-	-	668	-	384	-	
Mov Cap-2 Maneuver	-	-	-		-	-	-	-	384	-	
Stage 1	-	-	-		-	-	-	-	-	-	
Stage 2	-	-	-		-	-	-	-	460	-	
Approach	EB				NB			SB			
HCM Control Delay, s	0				12			17.5			
HCM LOS					В			C			
Minor Lane/Major Mvm	nt N	BLn1	EBT	EBR SBLn1							
Capacity (veh/h)		668	-	- 384							
HCM Lane V/C Ratio	().226	-	- 0.249							
HCM Control Delay (s)		12	-	- 17.5							
HCM Lane LOS		В	-	- C							

1

HCM 95th %tile Q(veh)

0.9

Intersection

Int Delay, s/veh

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	
	EDL		EDK	VVDL	VVDI	VVDR	INDL	INDI		SDL	301	JDK	
Lane Configurations		- 11	7						7		- †		
Traffic Vol, veh/h	0	873	88	0	0	0	0	0	150	0	95	0	
Future Vol, veh/h	0	873	88	0	0	0	0	0	150	0	95	0	
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0	
Sign Control	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop	Stop	Stop	Stop	
RT Channelized	-	-	Yield	-	-	None	-	-	None	-	-	None	
Storage Length	-	-	125	-	-	-	-	-	0	-	-	-	
Veh in Median Storage,	# -	0	-	-	16983	-	-	0	-	-	0	-	
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-	
Peak Hour Factor	90	90	90	90	90	90	90	90	90	90	90	90	
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2	
Mvmt Flow	0	970	98	0	0	0	0	0	167	0	106	0	

Major/Minor M	Major1				Minor1		Ν	/linor2				
Conflicting Flow All	-	0	0		-	-	485	-	970	-		
Stage 1	-	-	-		-	-	-	-	0	-		
Stage 2	-	-	-		-	-	-	-	970	-		
Critical Hdwy	-	-	-		-	-	6.94	-	6.54	-		
Critical Hdwy Stg 1	-	-	-		-	-	-	-	-	-		
Critical Hdwy Stg 2	-	-	-		-	-	-	-	5.54	-		
Follow-up Hdwy	-	-	-		-	-	3.32	-	4.02	-		
Pot Cap-1 Maneuver	0	-	-		0	0	528	0	252	0		
Stage 1	0	-	-		0	0	-	0	-	0		
Stage 2	0	-	-		0	0	-	0	330	0		
Platoon blocked, %		-	-									
Mov Cap-1 Maneuver	-	-	-		-	-	528	-	252	-		
Mov Cap-2 Maneuver	-	-	-		-	-	-	-	252	-		
Stage 1	-	-	-		-	-	-	-	-	-		
Stage 2	-	-	-		-	-	-	-	330	-		
Approach	EB				NB			SB				
HCM Control Delay, s	0				14.9			29.2				
HCM LOS					В			D				
Minor Lane/Major Mvm	it NE	3Ln1	EBT	EBR SBLn1								
Capacity (veh/h)		528	-	- 252								
HCM Lane V/C Ratio	0	.316	-	- 0.419								
HCM Control Delay (s)		14.9	-	- 29.2								

 HCM Control Delay (s)
 14.9
 29.2

 HCM Lane LOS
 B
 D

 HCM 95th %tile Q(veh)
 1.3
 2

nt Delay, s/veh 5.9
Novement EBL EBT EBR WBL WBT WBR NBL NBT NBR SBL SBT SBR
ane Configurations 👫 🌈
Traffic Vol, veh/h 0 873 122 0 0 0 0 0 236 0 112 0
Future Vol, veh/h 0 873 122 0 0 0 0 0 236 0 112 0
Conflicting Peds, #/hr 0 0 0 0 0 0 0 0 0 0 0 0 0
Sign Control Free Free Free Stop Stop Stop Stop Stop Stop Stop Stop
RT Channelized Yield None None None
Storage Length 125 0
Veh in Median Storage, # - 0 0 0 - 0 -
Grade, % - 0 0 0 0 -
Peak Hour Factor 90 90 90 90 90 90 90 90 90 90 90 90 90
Heavy Vehicles, % 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
Vivmt Flow 0 970 136 0 0 0 0 0 262 0 124 0
Major/Minor Major1 Minor2
Conflicting Flow All - 0 0 485 - 970 -
Stage 1 0 -
Stage 2 970 -
Critical Hdwy 6.94 - 6.54 -
Critical Hdwy Stg 1
Critical Hdwy Stg 2 5.54 -
Follow-up Hdwy
Pot Cap-1 Maneuver 0 0 0 528 0 252 0
Stage 1 0 0 0 0 - 0 - 0
Stage 2 0 0 330 0
Platoon blocked, %
Mov Cap-1 Maneuver
Nov Cap-2 Maneuver 252 -
Stage 1
Stage 2
Approach EB NB SB
HCM Control Delay, s 0 18.4 32.5
HCM LOS C D
Vinor Lane/Major Mvmt NBLn1 EBT EBR SBLn1
Capacity (veh/h) 528 - 252
HCM Lane V/C Ratio 0.497 - 0.494
HCM Control Delay (s) 18.4 32.5
HCM Lane LOS C D

Intersection

Int Delay, s/veh

Lane Configurations Image: Configuration in the image: Configuration	Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	,
Traffic Vol, veh/h 0 1220 59 0 0 0 125 0 37 0 Future Vol, veh/h 0 1220 59 0 0 0 0 125 0 37 0 Conflicting Peds, #/hr 0 <td></td> <td>LDL</td> <td></td> <td></td> <td>VVDL</td> <td>VVDI</td> <td>VUIN</td> <td>NDL</td> <td>NDT</td> <td></td> <td>JDL</td> <td>301</td> <td></td> <td></td>		LDL			VVDL	VVDI	VUIN	NDL	NDT		JDL	301		
Future Vol, veh/h 0 1220 59 0 0 0 0 125 0 37 0 Conflicting Peds, #/hr 0 <			TT.	- r						C.		T		
Conflicting Peds, #/hr 0 <td>Traffic Vol, veh/h</td> <td>0</td> <td>1220</td> <td>59</td> <td>0</td> <td>0</td> <td>0</td> <td>0</td> <td>0</td> <td>125</td> <td>0</td> <td>37</td> <td>0</td> <td></td>	Traffic Vol, veh/h	0	1220	59	0	0	0	0	0	125	0	37	0	
Sign ControlFreeFreeFreeStop <td>Future Vol, veh/h</td> <td>0</td> <td>1220</td> <td>59</td> <td>0</td> <td>0</td> <td>0</td> <td>0</td> <td>0</td> <td>125</td> <td>0</td> <td>37</td> <td>0</td> <td></td>	Future Vol, veh/h	0	1220	59	0	0	0	0	0	125	0	37	0	
RT Channelized - - None - - None - - None Storage Length - - 125 - - - 0 - - - None Veh in Median Storage, # 0 - - 16983 - - 0 - - 0 - Grade, % - 0 - - 0 - - 0 - - 0 - Peak Hour Factor 90	Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0	
Storage Length - - 125 - - - 0 -	Sign Control	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop	Stop	Stop	Stop	
Veh in Median Storage, # 0 - - 16983 - - 0 - - 0 - Grade, % - 0 - - 0 - - 0 - Peak Hour Factor 90	RT Channelized	-	-	Yield	-	-	None	-	-	None	-	-	None	
Grade, % - 0 0 0 0 - Peak Hour Factor 90 90 90 90 90 90 90 90 90 90 90 90	Storage Length	-	-	125	-	-	-	-	-	0	-	-	-	
Peak Hour Factor 90 90 90 90 90 90 90 90 90 90 90 90 90	Veh in Median Storage	, # -	0	-	-	16983	-	-	0	-	-	0	-	
	Grade, %	-	0	-	-	0	-	-	0	-	-	0	-	
Heavy Vehicles, % 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	Peak Hour Factor	90	90	90	90	90	90	90	90	90	90	90	90	
	Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2	
Mvmt Flow 0 1356 66 0 0 0 0 0 139 0 41 0	Mvmt Flow	0	1356	66	0	0	0	0	0	139	0	41	0	

Major1					Minor	1		Ν	linor2					
-	0	0				-	-	678	-	1356	-			
-	-	-				-	-	-	-	0	-			
-	-	-				-	-	-	-	1356	-			
-	-	-				-	-	6.94	-	6.54	-			
-	-	-				-	-	-	-	-	-			
-	-	-				-	-	-	-	5.54	-			
-	-	-				-	-		-		-			
0	-	-					0	395	0	148	0			
	-	-				0	0	-		-	0			
0	-	-				0	0	-	0	216	0			
	-	-												
-	-	-				-	-	395	-	148	-			
-	-	-				-	-	-	-	148	-			
-	-	-				-	-	-	-	-	-			
-	-	-				-	-	-	-	216	-			
EB					Ν	В			SB					
0					1	9			38.4					
						С			Е					
nt N	BLn1	EBT	EBR	SBLn1										
	395	-	-	148										
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Intersection

Int Delay, s/veh

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	
Lane Configurations		^	1						1		1		
Traffic Vol, veh/h	0	1835	65	0	0	0	0	0	138	0	41	0	
Future Vol, veh/h	0	1835	65	0	0	0	0	0	138	0	41	0	
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0	
Sign Control	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop	Stop	Stop	Stop	
RT Channelized	-	-	Yield	-	-	None	-	-	None	-	-	None	
Storage Length	-	-	125	-	-	-	-	-	0	-	-	-	
Veh in Median Storage,	# -	0	-	-	16983	-	-	0	-	-	0	-	
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-	
Peak Hour Factor	90	90	90	90	90	90	90	90	90	90	90	90	
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2	
Mvmt Flow	0	2039	72	0	0	0	0	0	153	0	46	0	

Major/Minor	Major1				Minor1		Ν	/linor2			
Conflicting Flow All	-	0	0		-	-	1020	-	2039	-	
Stage 1	-	-	-		-	-	-	-	0	-	
Stage 2	-	-	-		-	-	-	-	2039	-	
Critical Hdwy	-	-	-		-	-	6.94	-	6.54	-	
Critical Hdwy Stg 1	-	-	-		-	-	-	-	-	-	
Critical Hdwy Stg 2	-	-	-		-	-	-	-	5.54	-	
Follow-up Hdwy	-	-	-		-	-	3.32	-	4.02	-	
Pot Cap-1 Maneuver	0	-	-		0	0	234	0	56	0	
Stage 1	0	-	-		0	0	-	0	-	0	
Stage 2	0	-	-		0	0	-	0	99	0	
Platoon blocked, %		-	-								
Mov Cap-1 Maneuver	-	-	-		-	-	234	-	56	-	
Mov Cap-2 Maneuver	-	-	-		-	-	-	-	56	-	
Stage 1	-	-	-		-	-	-	-	-	-	
Stage 2	-	-	-		-	-	-	-	99	-	
Approach	EB				NB			SB			
HCM Control Delay, s	0				45.5			186.4			
HCM LOS					E			F			
Minor Lane/Major Mvm	nt <u>N</u> E	3Ln1	EBT	EBR SBLn1							
Capacity (veh/h)		234	-	- 56							
HCM Lane V/C Ratio	0	.655	-	- 0.813							
HCM Control Delay (s)		45.5	-	- 186.4							
HCM Lane LOS		Е	-	- F							

3.5

4.1

HCM 95th %tile Q(veh)

Int Delay, s/veh	17.9				WDT			NET		0.51	0.D.T	0.0.0	
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	
Lane Configurations	0		7	0	•	0	•	0	7	0		0	
Traffic Vol, veh/h	0	1835	117	0	0	0	0	0	192	0	67	0	
Future Vol, veh/h	0	1835	117	0	0	0	0	0	192	0	67	0	
Conflicting Peds, #/hr	_ 0	0	_ 0	0	0	0	0	0	0	0	0	0	
Sign Control	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop	Stop	Stop	Stop	
RT Channelized	-	-	Yield	-	-	None	-	-	None	-	-	None	
Storage Length	-	-	125	-	-	-	-	-	0	-	-	-	
Veh in Median Storage,	# -	0	-	-	0	-	-	0	-	-	0	-	
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-	
Peak Hour Factor	90	90	90	90	90	90	90	90	90	90	90	90	
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2	
Mvmt Flow	0	2039	130	0	0	0	0	0	213	0	74	0	
Major/Minor M	ajor1					Ν	/linor1			Ainor2			
Conflicting Flow All	-	0	0				-	-	1020	-	2039	-	
Stage 1	-	-	-				-	-	-	-	0	-	
Stage 2	-	-	-				-	-	-	-	2039	-	
Critical Hdwy	-	-	-				-	-	6.94	-	6.54	-	
Critical Hdwy Stg 1	-	-	-				-	-	-	-	-	-	
Critical Hdwy Stg 2	-	-	-				-	-	-	-	5.54	-	
Follow-up Hdwy	-	-	-				-	-	3.32	-	4.02	-	
Pot Cap-1 Maneuver	0	-	-				0	0	234	0	~ 56	0	
Stage 1	0	-	-				Ũ	0	-	0	-	0	
Stage 2	0	_	_				0	0	-	0	99	0	
Platoon blocked, %	U	_	_				U	U		0	,,	0	
Mov Cap-1 Maneuver	_	_	_				_	_	234	_	~ 56	_	
Mov Cap-2 Maneuver	-	-	-				-	-	234	-	~ 56	-	
Stage 1	-	-	-				-	-	-	-	~ 50	-	
	-	-	-				-	-	-	-	- 99	-	
Stage 2	-	-	-				-	-	-	-	99	-	
Approach	EB						NB			SB			
HCM Control Delay, s	0						82.4			\$ 353			
HCM LOS	U						02.4 F			φ 355 F			
							I			I			
Minor Lane/Major Mvmt	ſ	VBLn1	EBT	FBR	SBLn1								
Capacity (veh/h)	1	234			56								
HCM Lane V/C Ratio		234 0.912	-	-	50 1.329								
			-										
HCM Control Delay (s)		82.4	-	-	\$ 353								
HCM Lane LOS		F	-	-	F								
HCM 95th %tile Q(veh)		7.7	-	-	6.6								
Notes													

6

Intersection

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	
Lane Configurations					11	1				002	001	1	
Traffic Vol, veh/h	0	0	0	0	1352	185	0	36	0	0	0	225	
Future Vol, veh/h	0	0	0	0	1352	185	0	36	0	0	0	225	
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0	
Sign Control	Stop	Stop	Stop	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop	
RT Channelized	-	-	None										
Storage Length	-	-	-	-	-	150	-	-	-	-	-	0	
Veh in Median Storage,	# -	0	-	-	0	-	-	0	-	-	0	-	
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-	
Peak Hour Factor	90	90	90	90	90	90	90	90	90	90	90	90	
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2	
Mvmt Flow	0	0	0	0	1502	206	0	40	0	0	0	250	

Major/Minor		I	Major2		Mi	nor1		Mi	nc	or2	or2
Conflicting Flow All			-	-	0	-	1708	-		-	
Stage 1			-	-	-	-	0	-	-		-
Stage 2			-	-	-	-	1708	-	-		-
Critical Hdwy			-	-	-	-	6.54	-	-		-
Critical Hdwy Stg 1			-	-	-	-	-	-	-		-
Critical Hdwy Stg 2			-	-	-	-	5.54	-	-		-
Follow-up Hdwy			-	-	-	-	4.02	-	-		-
Pot Cap-1 Maneuver			0	-	-	0	90	0	0		0
Stage 1			0	-	-	0	-	0	0		0
Stage 2			0	-	-	0	145	0	0	C)
Platoon blocked, %				-	-						
Mov Cap-1 Maneuver			-	-	-	-	90	-	-	-	
Mov Cap-2 Maneuver			-	-	-	-	90	-	-	-	
Stage 1			-	-	-	-	-	-	-	-	
Stage 2			-	-	-	-	145	-	-	-	
Approach			WB			NB			SB		
HCM Control Delay, s			0			73.7			36.5		
HCM LOS						F			Е		
Minor Lane/Major Mvmt	NBLn1	WBT	WBR S	SBLn1							
Capacity (veh/h)	90	-	-	353							
HCM Lane V/C Ratio	0.444	-	-	0.708							
HCM Control Delay (s)	73.7	-	-	36.5							
HCM Lane LOS	F	-	-	Е							
HCM 95th %tile Q(veh)	1.9	-	-	5.2							

Intersection

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	
Lane Configurations				WDL	44	1				ODL		1	
Traffic Vol, veh/h	0	0	0	0	1796	204	0	40	0	0	0	248	
Future Vol, veh/h	0	0	0	0	1796	204	0	40	0	0	0	248	
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0	
Sign Control	Stop	Stop	Stop	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop	
RT Channelized	-	-	None										
Storage Length	-	-	-	-	-	150	-	-	-	-	-	0	
Veh in Median Storage,	,# -	0	-	-	0	-	-	0	-	-	0	-	
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-	
Peak Hour Factor	90	90	90	90	90	90	90	90	90	90	90	90	
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2	
Mvmt Flow	0	0	0	0	1996	227	0	44	0	0	0	276	

Major/Minor		I	/lajor2		М	inor1		Μ	linor2				
Conflicting Flow All			-	-	0	-	2223	-	-	-	998		
Stage 1			-	-	-	-	0	-	-	-	-		
Stage 2			-	-	-	-	2223	-	-	-	-		
Critical Hdwy			-	-	-	-	6.54	-	-	-	6.94		
Critical Hdwy Stg 1			-	-	-	-	-	-	-	-	-		
Critical Hdwy Stg 2			-	-	-	-	5.54	-	-	-	-		
Follow-up Hdwy			-	-	-	-	4.02	-	-	-	3.32		
Pot Cap-1 Maneuver			0	-	-	0	~ 43	0	0	0	~ 242		
Stage 1			0	-	-	0	-	0	0	0	-		
Stage 2			0	-	-	0	79	0	0	0	-		
Platoon blocked, %				-	-								
Mov Cap-1 Maneuver			-	-	-	-	~ 43	-	-	-	~ 242		
Mov Cap-2 Maneuver			-	-	-	-	~ 43	-	-	-	-		
Stage 1			-	-	-	-	-	-	-	-	-		
Stage 2			-	-	-	-	79	-	-	-	-		
Approach			WB			NB			SB				
HCM Control Delay, s			0		4	293.8		·	143.8				
HCM LOS						F			F				
Minor Lane/Major Mvmt	NBLn1	WBT	WBR S	BLn1									
Capacity (veh/h)	43	-	-	242									
HCM Lane V/C Ratio	1.034	-	-	1.139									
HCM Control Delay (s)	293.8	-	-	143.8									
HCM Lane LOS	F	-	-	F									
HCM 95th %tile Q(veh)	4.2	-	-	12.5									
Notes													
~: Volume exceeds capacity	\$: De	lay exc	eeds 30	0s	+: Comp	utation	Not De	fined	*: All m	ajor v	olume in	platoon	

Int Delay, s/veh	23.4											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations					- 11	1		↑				1
Traffic Vol, veh/h	0	0	0	0	1853	204	0	40	0	0	0	248
Future Vol, veh/h	0	0	0	0	1853	204	0	40	0	0	0	248
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	150	-	-	-	-	-	0
Veh in Median Storage	,# -	1	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	90	90	90	90	90	90	90	90	90	90	90	90
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	0	0	0	0	2059	227	0	44	0	0	0	276

Major/Minor	Major2		Mi	nor1		Mi	nor2	
Conflicting Flow All	-	-	0	-	2286	-	-	- 1030
Stage 1	-	-	-	-	0	-	-	
Stage 2	-	-	-	-	2286	-	-	
Critical Hdwy	-	-	-	-	6.54	-	-	- 6.94
Critical Hdwy Stg 1	-	-	-	-	-	-	-	
Critical Hdwy Stg 2	-	-	-	-	5.54	-	-	
Follow-up Hdwy	-	-	-	-	4.02	-	-	- 3.32
Pot Cap-1 Maneuver	0	-	-	0	~ 39	0	0	0 ~ 231
Stage 1	0	-	-	0	-	0	0	0 -
Stage 2	0	-	-	0	74	0	0	0 -
Platoon blocked, %		-	-					
Mov Cap-1 Maneuver	-	-	-	-	~ 39	-	-	- ~ 231
Mov Cap-2 Maneuver	-	-	-	-	~ 39	-	-	
Stage 1	-	-	-	-	-	-	-	
Stage 2	-	-	-	-	74	-	-	
Approach	WB			NB			SB	
HCM Control Delay, s	0		\$ 3	48.5		1	65.2	
HCM LOS				F			F	
Minor Lane/Major Mvmt NBLn1	WBT WBR SB	_n1						
Capacity (veh/h) 39		231						
HCM Lane V/C Ratio 1.14	1.1							
HCM Control Delay (s) \$348.5	16							
HCM Lane LOS F		F						
HCM 95th %tile Q(veh) 4.4	1	3.3						
Notes								
~: Volume exceeds capacity \$: De	elay exceeds 300	S +	: Comp	utatio	n Not De	fined	*: All	major volume in platoon

Intersection

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	
Lane Configurations					^	1		1				1	
Traffic Vol, veh/h	0	0	0	0	555	74	0	116	0	0	0	114	
Future Vol, veh/h	0	0	0	0	555	74	0	116	0	0	0	114	
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0	
Sign Control	Stop	Stop	Stop	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop	
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None	
Storage Length	-	-	-	-	-	150	-	-	-	-	-	0	
Veh in Median Storage,	# -	0	-	-	0	-	-	0	-	-	0	-	
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-	
Peak Hour Factor	90	90	90	90	90	90	90	90	90	90	90	90	
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2	
Mvmt Flow	0	0	0	0	617	82	0	129	0	0	0	127	

Major/Minor		Ν	Major2		Mi	nor1		Mi	nor2			
Conflicting Flow All			-	-	0	-	699	-	-	-	309	
Stage 1			-	-	-	-	0	-	-	-	-	
Stage 2			-	-	-	-	699	-	-	-	-	
Critical Hdwy			-	-	-	-	6.54	-	-	-	6.94	
Critical Hdwy Stg 1			-	-	-	-	-	-	-	-	-	
Critical Hdwy Stg 2			-	-	-	-	5.54	-	-	-	-	
Follow-up Hdwy			-	-	-	-	4.02	-	-	-	3.32	
Pot Cap-1 Maneuver			0	-	-	0	362	0	0	0	687	
Stage 1			0	-	-	0	-	0	0	0	-	
Stage 2			0	-	-	0	440	0	0	0	-	
Platoon blocked, %				-	-							
Mov Cap-1 Maneuver			-	-	-	-	362	-	-	-	687	
Mov Cap-2 Maneuver			-	-	-	-	362	-	-	-	-	
Stage 1			-	-	-	-	-	-	-	-	-	
Stage 2			-	-	-	-	440	-	-	-	-	
Approach			WB			NB			SB			
HCM Control Delay, s			0			20.3			11.4			
HCM LOS						С			В			
Minor Lane/Major Mvmt	NBLn1	WBT	WBR 3	SBLn1								
Capacity (veh/h)	362	-	-	687								
HCM Lane V/C Ratio	0.356	-	-	0.184								
HCM Control Delay (s)	20.3	-	-	11.4								
HCM Lane LOS	С	-	-	В								
HCM 95th %tile Q(veh)	1.6	-	-	0.7								

Intersection

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	
Lane Configurations					^	1		†				1	
Traffic Vol, veh/h	0	0	0	0	843	82	0	128	0	0	0	126	
Future Vol, veh/h	0	0	0	0	843	82	0	128	0	0	0	126	
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0	
Sign Control	Stop	Stop	Stop	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop	
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None	
Storage Length	-	-	-	-	-	150	-	-	-	-	-	0	
Veh in Median Storage,	# -	0	-	-	0	-	-	0	-	-	0	-	
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-	
Peak Hour Factor	90	90	90	90	90	90	90	90	90	90	90	90	
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2	
Mvmt Flow	0	0	0	0	937	91	0	142	0	0	0	140	

Major/Minor		Ν	Major2		Mi	nor1		Mi	nor2			
Conflicting Flow All			-	-	0	-	1028	-	-	-	469	
Stage 1			-	-	-	-	0	-	-	-	-	
Stage 2			-	-	-	-	1028	-	-	-	-	
Critical Hdwy			-	-	-	-	6.54	-	-	-	6.94	
Critical Hdwy Stg 1			-	-	-	-	-	-	-	-	-	
Critical Hdwy Stg 2			-	-	-	-	5.54	-	-	-	-	
Follow-up Hdwy			-	-	-	-	4.02	-	-	-	3.32	
Pot Cap-1 Maneuver			0	-	-	0	233	0	0	0	541	
Stage 1			0	-	-	0	-	0	0	0	-	
Stage 2			0	-	-	0	310	0	0	0	-	
Platoon blocked, %				-	-							
Mov Cap-1 Maneuver			-	-	-	-	233	-	-	-	541	
Mov Cap-2 Maneuver			-	-	-	-	233	-	-	-	-	
Stage 1			-	-	-	-	-	-	-	-	-	
Stage 2			-	-	-	-	310	-	-	-	-	
Approach			WB			NB			SB			
HCM Control Delay, s			0			42			14			
HCM LOS						Е			В			
Minor Lane/Major Mvmt	NBLn1	WBT	WBR	SBLn1								
Capacity (veh/h)	233	-	-	541								
HCM Lane V/C Ratio	0.61	-	-	0.259								
HCM Control Delay (s)	42	-	-	14								
HCM Lane LOS	E	-	-	В								
HCM 95th %tile Q(veh)	3.6	-	-	1								

Int Delay, s/veh	6.4											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations					- 11	1		•				1
Traffic Vol, veh/h	0	0	0	0	879	82	0	128	0	0	0	126
Future Vol, veh/h	0	0	0	0	879	82	0	128	0	0	0	126
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop
RT Channelized	-	-	None									
Storage Length	-	-	-	-	-	150	-	-	-	-	-	0
Veh in Median Storage	,# -	1	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	90	90	90	90	90	90	90	90	90	90	90	90
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	0	0	0	0	977	91	0	142	0	0	0	140

	Major2		М	inor1		Mi	nor2					
	-	-	0	-	1068	-	-	-	489			
	-	-	-	-	0	-	-	-	-			
	-	-	-	-	1068	-	-	-	-			
	-	-	-	-	6.54	-	-	-	6.94			
	-	-	-	-	-	-	-	-	-			
	-	-	-	-	5.54	-	-	-	-			
	-	-	-	-	4.02	-	-	-	3.32			
	0	-	-	0	220	0	0	0	525			
	0	-	-	0	-	0	0	0	-			
	0	-	-	0	296	0	0	0	-			
		-	-									
	-	-	-	-	220	-	-	-	525			
	-	-	-	-	220	-	-	-	-			
	-	-	-	-	-	-	-	-	-			
	-	-	-	-	296	-	-	-	-			
	WB			NB			SR					
	0			47.1 E			B					
	WBT WBR SE	BLn1										
220		525										
0.646												
	220		NBLn1 WBT WBR SBLn1 220 - 525 0.646 - 0.267	- - 0 - - - - - - - - - - - - - - - - - - 0 - - 0 - - 0 - - 0 - - 0 - - - - - - - - 0 - - WB WB - 0 - - NBLn1 WBT WBR SBLn1 220 - - 220 - - 0.646 - 0.267	- - 0 - - - - - - - - - - - - - - - - - - - - 0 0 - 10 0 0 - - 0 0 - - 0 0 - - 0 - - 0 -	- - 0 - 1068 - - - 0 - 1068 - - - - 1068 - - - - 1068 - - - - 1068 - - - - 6.54 - - - - - - - - - - - - - - - 5.54 - - - - - - 5.54 - - - 0 - 0 - 0 220 - - 0 220 0 - 0 - 0 - 220 - - 220 - - 220 - - 220 - - - - - - - - - - - - - - - - - - 20 - - 2	- - 0 - 1068 - - - - 0 - 0 - - - - - 1068 - - - - - - 1068 - - - - - - 1068 - - - - - - - 1068 - - - - - - 6.54 - - - - - 5.54 - - - - - 0 220 0 0 0 - 0 220 0 0 - 0 0 - - 0 220 0 - 0 220 - - - 10 10 - 10 -	- - 0 - 1068 - - - - 0 - 1068 - - - - - 1068 - - - - - - 1068 - - - - - - 1068 - - - - - - 5.54 - - - - - - 5.54 - - - - - - 4.02 - - - 0 - 0 220 0 0 0 0 - 0 220 0 0 0 0 - 0 296 0 0 0 - - - 220 - - - - - - 220 - - - - - - 296 - - - WB NB NB	- - 0 - 1068 -	- - 0 - 1068 - - 489 - - 0 - - - - - - - - - 0.54 - - - 6.94 - - - 5.54 - - - - - - - 5.54 - - - - - - - 4.02 - - 3.32 0 - 0 220 0 0 0 525 0 - 0 220 0 0 0 - 0 - 0 296 0 0 0 - - - - 220 - - 525 - - - 220 - - 525 - - - 220 - - - - - - 296 - - - - -	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$

HCM Control Delay (s)	47.1	-	-	14.3
HCM Lane LOS	E	-	-	В
HCM 95th %tile Q(veh)	3.9	-	-	1.1

APPENDIX E

CAPACITY ANALYSIS CALCULATIONS US 401 BYPASS & EASTERN U-TURN LOCATION

Int Delay, s/veh	1.3					
Movement	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations				^	5	
Traffic Vol, veh/h	0	0	0	1532	91	0
Future Vol, veh/h	0	0	0	1532	91	0
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage,	# 0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	90	90	90	90	90	90
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	0	0	0	1702	101	0

Major/Minor	N	Major2	Ν	/linor1		
Conflicting Flow All			-	851	-	
Stage 1		-	-	0	-	
Stage 2		-	-	851	-	
Critical Hdwy		-	-	6.84	-	
Critical Hdwy Stg 1		-	-	-	-	
Critical Hdwy Stg 2		-	-	5.84	-	
Follow-up Hdwy		-	-	3.52	-	
Pot Cap-1 Maneuver		0	-	299	0	
Stage 1		0	-	-	0	
Stage 2		0	-	379	0	
Platoon blocked, %			-			
Mov Cap-1 Maneuver		-	-	299	-	
Mov Cap-2 Maneuver		-	-	299	-	
Stage 1		-	-	-	-	
Stage 2		-	-	379	-	
Approach		WB		NB		
HCM Control Delay, s		0		23.1		
HCM LOS		-		С		
Minor Long/Major Munt	NDL #4					
Minor Lane/Major Mvmt	NBLn1	WBT				
Capacity (veh/h)	299	-				
HCM Lane V/C Ratio	0.338	-				
HCM Control Delay (s)	23.1	-				
HCM Lane LOS	С	-				

1.4

HCM 95th %tile Q(veh)

Int Delay, s/veh	2					
Movement	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations				^	٦	
Traffic Vol, veh/h	0	0	0	1994	100	0
Future Vol, veh/h	0	0	0	1994	100	0
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage,	# 0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	90	90	90	90	90	90
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	0	0	0	2216	111	0

Major/Minor	Ν	/lajor2	1	Minor1	
Conflicting Flow All	•	_		1108	-
Stage 1		-	-	0	-
Stage 2		-	-	1108	-
Critical Hdwy		-	-	6.84	-
Critical Hdwy Stg 1		-	-	-	-
Critical Hdwy Stg 2		-	-	5.84	-
Follow-up Hdwy		-	-	3.52	-
Pot Cap-1 Maneuver		0	-	204	0
Stage 1		0	-	-	0
Stage 2		0	-	278	0
Platoon blocked, %			-		
Mov Cap-1 Maneuver		-	-	204	-
Mov Cap-2 Maneuver		-	-	204	-
Stage 1		-	-	-	-
Stage 2		-	-	278	-
Approach		WB		NB	
HCM Control Delay, s		0		41.9	
HCM LOS		U		E	
Minor Lane/Major Mvmt	NBLn1	WBT			
Capacity (veh/h)	204	-			
HCM Lane V/C Ratio	0.545	-			
HCM Control Delay (s)	41.9	-			
HCM Lane LOS	E	-			
HCM 95th %tile Q(veh)	2.9	-			

Intersection						
Int Delay, s/veh	5.9					
Movement	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations				^	1	
Traffic Vol, veh/h	0	0	0	2011	157	0
Future Vol, veh/h	0	0	0	2011	157	0
Conflicting Peds, #/hr	0	0	0	0	0	0
0	Stop	Stop	Free	Free	Stop	Stop
RT Channelized		None	-	None		None
Storage Length	-	-	-	-	0	-
Veh in Median Storage,	# 2	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	90	90	90	90	90	90
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	0	0	0	2234	174	0
	Ū	0	Ũ	2201	.,	U
N A a i a w/N A i w a w			4		1:	
Major/Minor		ľ	Major2		<u>/linor1</u> 1117	
Conflicting Flow All			-	-	0	-
Stage 1			-	-		-
Stage 2			-	-	1117	-
Critical Hdwy			-	-	6.84	-
Critical Hdwy Stg 1			-	-	-	-
Critical Hdwy Stg 2			-	-	5.84	-
Follow-up Hdwy			-	-	3.52	-
Pot Cap-1 Maneuver			0	-	201	0
Stage 1			0	-	-	0
Stage 2			0	-	275	0
Platoon blocked, %				-		
Mov Cap-1 Maneuver			-	-	201	-
Mov Cap-2 Maneuver			-	-	201	-
Stage 1			-	-	-	-
Stage 2			-	-	275	-
U ¹						
Approach			WB		NB	
HCM Control Delay, s			0		81.9	
HCM LOS			0		F	
···· = = =					•	
Minor Lane/Major Mvmt	I	NBLn1	WBT			
Capacity (veh/h)		201	-			
HCM Lane V/C Ratio		0.868	-			
HCM Control Delay (s)		0.868 81.9	-			
			-			
HCM Lane LOS		F	-			
HCM 95th %tile Q(veh)		6.6	-			

Int Delay, s/veh	1.1					
Movement	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations				^	5	
Traffic Vol, veh/h	0	0	0	600	66	0
Future Vol, veh/h	0	0	0	600	66	0
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage,	# 0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	90	90	90	90	90	90
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	0	0	0	667	73	0

Major/Minor	Ν	Major2	1	Minor1	
Conflicting Flow All		-	-	334	-
Stage 1		-	-	0	-
Stage 2		-	-	334	-
Critical Hdwy		-	-	6.84	-
Critical Hdwy Stg 1		-	-	-	-
Critical Hdwy Stg 2		-	-	5.84	-
Follow-up Hdwy		-	-	3.52	-
Pot Cap-1 Maneuver		0	-	636	0
Stage 1		0	-	-	0
Stage 2		0	-	697	0
Platoon blocked, %			-		
Mov Cap-1 Maneuver		-	-	636	-
Mov Cap-2 Maneuver		-	-	636	-
Stage 1		-	-	-	-
Stage 2		-	-	697	-
Approach		WB		NB	
HCM Control Delay, s		0		11.4	
HCM LOS		•		В	
				_	
		WDT			
Minor Lane/Major Mvmt	NBLn1	WBT			
Capacity (veh/h)	636	-			
HCM Lane V/C Ratio	0.115	-			
HCM Control Delay (s)	11.4	-			
HCM Lane LOS	B	-			
HCM 95th %tile Q(veh)	0.4	-			

1

Intersection

Int Delay, s/veh

Movement	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations				^	7	
Traffic Vol, veh/h	0	0	0	892	73	0
Future Vol, veh/h	0	0	0	892	73	0
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage,	,# 0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	90	90	90	90	90	90
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	0	0	0	991	81	0

Major/Minor	Ν	Major2	N.	1inor1			
		najuiz					
Conflicting Flow All		-	-	496 0	-		
Stage 1		-	-		-		
Stage 2		-	-	496	-		
Critical Hdwy		-	-	6.84	-		
Critical Hdwy Stg 1		-	-	-	-		
Critical Hdwy Stg 2		-	-	5.84	-		
Follow-up Hdwy		-	-	3.52	-		
Pot Cap-1 Maneuver		0	-	503	0		
Stage 1		0	-	-	0		
Stage 2		0	-	577	0		
Platoon blocked, %			-				
Mov Cap-1 Maneuver		-	-	503	-		
Mov Cap-2 Maneuver		-	-	503	-		
Stage 1		-	-	-	-		
Stage 2		-	-	577	-		
Approach		WB		NB			
Approach							
HCM Control Delay, s		0		13.5			
HCM LOS				В			
Minor Lane/Major Mvmt	NBLn1	WBT				 	
Capacity (veh/h)	503	-					
HCM Lane V/C Ratio	0.161	-					
HCM Control Delay (s)	13.5	-					
HCM Lane LOS	В	-					

0.6

HCM 95th %tile Q(veh)

Intersection						
Int Delay, s/veh	1.6					
Movement	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations				^	ኘ	
Traffic Vol, veh/h	0	0	0	918	109	0
Future Vol, veh/h	0	0	0	918	109	0
Conflicting Peds, #/hr	0	0	0	0	0	0
	Stop	Stop	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage,	# 2	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	90	90	90	90	90	90
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	0	0	0	1020	121	0
	Ū	0	Ũ	1020		U
Major/Minor			Major2		Minor1	
Conflicting Flow All			-	-	510	-
Stage 1			-	-	0	-
Stage 2			-	-	510	-
Critical Hdwy			-	-	6.84	-
Critical Hdwy Stg 1			-	-	-	-
Critical Hdwy Stg 2			-	-	5.84	-
Follow-up Hdwy			-	-	3.52	-
Pot Cap-1 Maneuver			0	-	493	0
Stage 1			0	-	-	0
Stage 2			0	-	568	0
Platoon blocked, %				-		
Mov Cap-1 Maneuver			-	-	493	-
Mov Cap-2 Maneuver			-	-	493	-
Stage 1			-	-	-	-
Stage 2			-	-	568	-
Oldge Z					000	
Approach			WB		NB	
HCM Control Delay, s			0		14.7	
HCM LOS			0		14.7 B	
					D	
Minor Lane/Major Mvmt	I	NBLn1	WBT			
	I					
Capacity (veh/h)		493	-			
HCM Lane V/C Ratio		0.246	-			
HCM Control Delay (s)		14.7	-			
HCM Lane LOS		B	-			
HCM 95th %tile Q(veh)		1	-			

APPENDIX F

CAPACITY ANALYSIS CALCULATIONS MITCHELL MILL ROAD & JONESVILLE ROAD / PEEBLES ROAD

Intersection Delay, s/veh Intersection LOS

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eh 12.7
B
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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			\$			\$			\$	
Traffic Vol, veh/h	7	166	4	11	316	41	4	78	11	32	133	16
Future Vol, veh/h	7	166	4	11	316	41	4	78	11	32	133	16
Peak Hour Factor	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	8	184	4	12	351	46	4	87	12	36	148	18
Number of Lanes	0	1	0	0	1	0	0	1	0	0	1	0
Approach	EB			WB			NB			SB		
Opposing Approach	WB			EB			SB			NB		
Opposing Lanes	1			1			1			1		
Conflicting Approach Left	SB			NB			EB			WB		
Conflicting Lanes Left	1			1			1			1		
Conflicting Approach Right	NB			SB			WB			EB		
Conflicting Lanes Right	1			1			1			1		
HCM Control Delay	10.8			14.9			10.1			11.4		
HCM LOS	В			В			В			В		

lana	NBLn1	EBLn1	WBLn1	SBLn1
Lane				
Vol Left, %	4%	4%	3%	18%
Vol Thru, %	84%	94%	86%	73%
Vol Right, %	12%	2%	11%	9%
Sign Control	Stop	Stop	Stop	Stop
Traffic Vol by Lane	93	177	368	181
LT Vol	4	7	11	32
Through Vol	78	166	316	133
RT Vol	11	4	41	16
Lane Flow Rate	103	197	409	201
Geometry Grp	1	1	1	1
Degree of Util (X)	0.168	0.297	0.577	0.318
Departure Headway (Hd)	5.85	5.433	5.079	5.696
Convergence, Y/N	Yes	Yes	Yes	Yes
Сар	612	661	711	629
Service Time	3.904	3.477	3.114	3.743
HCM Lane V/C Ratio	0.168	0.298	0.575	0.32
HCM Control Delay	10.1	10.8	14.9	11.4
HCM Lane LOS	В	В	В	В
HCM 95th-tile Q	0.6	1.2	3.7	1.4

50.6 F

Intersection

Intersection Delay, s/veh Intersection LOS

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		\$			\$			4			\$	
Traffic Vol, veh/h	8	240	4	12	569	45	4	86	12	35	147	18
Future Vol, veh/h	8	240	4	12	569	45	4	86	12	35	147	18
Peak Hour Factor	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	9	267	4	13	632	50	4	96	13	39	163	20
Number of Lanes	0	1	0	0	1	0	0	1	0	0	1	0
Approach	EB			WB			NB			SB		
Opposing Approach	WB			EB			SB			NB		
Opposing Lanes	1			1			1			1		
Conflicting Approach Left	SB			NB			EB			WB		
Conflicting Lanes Left	1			1			1			1		
Conflicting Approach Right	NB			SB			WB			EB		
Conflicting Lanes Right	1			1			1			1		
HCM Control Delay	15.2			82.4			12.5			15		
HCM LOS	С			F			В			В		

Lane	NBLn1	EBLn1	WBLn1	SBLn1
Vol Left, %	4%	3%	2%	17%
Vol Thru, %	84%	95%	91%	73%
Vol Right, %	12%	2%	7%	9%
Sign Control	Stop	Stop	Stop	Stop
Traffic Vol by Lane	102	252	626	200
LT Vol	4	8	12	35
Through Vol	86	240	569	147
RT Vol	12	4	45	18
Lane Flow Rate	113	280	696	222
Geometry Grp	1	1	1	1
Degree of Util (X)	0.223	0.481	1.081	0.417
Departure Headway (Hd)	7.412	6.42	5.595	7.067
Convergence, Y/N	Yes	Yes	Yes	Yes
Сар	487	566	647	513
Service Time	5.412	4.42	3.663	5.067
HCM Lane V/C Ratio	0.232	0.495	1.076	0.433
HCM Control Delay	12.5	15.2	82.4	15
HCM Lane LOS	В	С	F	В
HCM 95th-tile Q	0.8	2.6	19.6	2

Intersection												
Intersection Delay, s/veh Intersection LOS	142.1 F											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		- 4 >			- 4 >			- 4 >			- ↔	
Traffic Vol, veh/h	8	279	4	31	635	131	4	86	23	86	147	18
Future Vol, veh/h	8	279	4	31	635	131	4	86	23	86	147	18
Peak Hour Factor	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	9	310	4	34	706	146	4	96	26	96	163	20
Number of Lanes	0	1	0	0	1	0	0	1	0	0	1	0
Approach	EB			WB			NB			SB		
Opposing Approach	WB			EB			SB			NB		
Opposing Lanes	1			1			1			1		
Conflicting Approach Left	SB			NB			EB			WB		
Conflicting Lanes Left	1			1			1			1		
Conflicting Approach Right	NB			SB			WB			EB		
Conflicting Lanes Right	1			1			1			1		
HCM Control Delay	20.4			242.9			14.7			20.4		
HCM LOS	С			F			В			С		
Lano		NBLn1	EBLn1	WBLn1	SBLn1							
Lane												
Vol Left, %		4% 76%	3% 96%	4% 80%	34% 59%							
Vol Thru, %		20%	90% 1%	80% 16%	59% 7%							
Vol Right, %												
Sign Control		Stop 113	Stop 291	Stop 797	Stop 251							
Traffic Vol by Lane LT Vol			291	31	201 86							
Through Vol		4 86	279	635	147							
RT Vol		23	4	131	147							
Lane Flow Rate		126	323	886	279							
		120	525 1	1	279							
Geometry Grp Degree of Util (X)		0.26	0.59	ı 1.481	0.545							
Departure Headway (Hd)		8.674	7.367	6.021	0.545 8.087							
Convergence, Y/N		Ves	Yes	Yes	Yes							
Convergence, ma		417	495	602	449							
Service Time		6.674	5.367	4.101	6.087							
HCM Lane V/C Ratio		0.302	0.653	1.472	0.621							
HCM Control Delay		14.7	20.4	242.9	20.4							
HCM Lane LOS		14.7 B	20.4 C	242.9 F	20.4 C							
HCM 95th-tile Q		1	3.8	43.1	3.2							
		I	3.0	43.1	J.Z							

Intersection												
Intersection Delay, s/veh Intersection LOS	103.4 F											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		- 4 >			ન ી	1		- ↔		ሻ	4	
Traffic Vol, veh/h	8	279	4	31	635	131	4	86	23	86	147	18
Future Vol, veh/h	8	279	4	31	635	131	4	86	23	86	147	18
Peak Hour Factor	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	9	310	4	34	706	146	4	96	26	96	163	20
Number of Lanes	0	1	0	0	1	1	0	1	0	1	1	0
Approach	EB			WB			NB			SB		
Opposing Approach	WB			EB			SB			NB		
Opposing Lanes	2			1			2			1		
Conflicting Approach Left	SB			NB			EB			WB		
Conflicting Lanes Left	2			1			1			2		
Conflicting Approach Right	NB			SB			WB			EB		
Conflicting Lanes Right	1			2			2			1		
HCM Control Delay	23.8			172.6			15.5			15.6		
HCM LOS	С			F			С			С		
Lane		NBLn1	EBLn1	WBLn1	WBLn2	SBLn1	SBLn2					
Vol Left, %		4%	3%	5%	0%	100%	0%					
Vol Thru, %		76%	96%	9 5%	0%	0%	89%					
Vol Right, %		20%	1%	0%	100%	0%	11%					
Sign Control		Stop	Stop	Stop	Stop	Stop	Stop					
Traffic Vol by Lane		113	291	666	131	86	165					
LT Vol		4	8	31	0	86	0					
Through Vol		86	279	635	0	0	147					
RT Vol		23	4	0	131	0	18					
Lane Flow Rate		126	323	740	146	96	183					
Geometry Grp		6	6	7	7	7	7					
Degree of Util (X)		0.283	0.645	1.385	0.243	0.218	0.39					
Departure Headway (Hd)		8.975	7.746	6.739	6	8.989	8.391					
Convergence, Y/N		Yes	Yes	Yes	Yes	Yes	Yes					
Сар		403	469	540	595	402	433					
Service Time		6.975	5.746	4.513	3.774	6.689	6.091					
HCM Lane V/C Ratio		0.313	0.689	1.37	0.245	0.239	0.423					
HCM Control Delay		15.5	23.8	204.5	10.7	14.2	16.4					
HCM Lane LOS		С	С	F	В	В	С					
HCM 95th-tile Q		1.1	4.5	33.6	0.9	0.8	1.8					

В

Intersection

Intersection Delay, s/veh Intersection LOS

10.8

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			\$			\$			\$	
Traffic Vol, veh/h	18	306	13	4	130	21	5	92	10	27	50	11
Future Vol, veh/h	18	306	13	4	130	21	5	92	10	27	50	11
Peak Hour Factor	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	20	340	14	4	144	23	6	102	11	30	56	12
Number of Lanes	0	1	0	0	1	0	0	1	0	0	1	0
Approach	EB			WB			NB			SB		
Opposing Approach	WB			EB			SB			NB		
Opposing Lanes	1			1			1			1		
Conflicting Approach Left	SB			NB			EB			WB		
Conflicting Lanes Left	1			1			1			1		
Conflicting Approach Right	NB			SB			WB			EB		
Conflicting Lanes Right	1			1			1			1		
HCM Control Delay	12.2			9.5			9.6			9.4		
HCM LOS	В			А			А			А		

Laws				0014
Lane	NBLn1	EBLn1	WBLn1	SBLn1
Vol Left, %	5%	5%	3%	31%
Vol Thru, %	86%	91%	84%	57%
Vol Right, %	9%	4%	14%	12%
Sign Control	Stop	Stop	Stop	Stop
Traffic Vol by Lane	107	337	155	88
LT Vol	5	18	4	27
Through Vol	92	306	130	50
RT Vol	10	13	21	11
Lane Flow Rate	119	374	172	98
Geometry Grp	1	1	1	1
Degree of Util (X)	0.175	0.489	0.233	0.146
Departure Headway (Hd)	5.312	4.702	4.878	5.379
Convergence, Y/N	Yes	Yes	Yes	Yes
Сар	668	760	728	659
Service Time	3.407	2.766	2.957	3.477
HCM Lane V/C Ratio	0.178	0.492	0.236	0.149
HCM Control Delay	9.6	12.2	9.5	9.4
HCM Lane LOS	А	В	А	А
HCM 95th-tile Q	0.6	2.7	0.9	0.5

С

Intersection

Intersection Delay, s/veh Intersection LOS

```
19.4
```

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			\$			\$			\$	
Traffic Vol, veh/h	20	436	14	4	339	23	6	102	11	30	55	12
Future Vol, veh/h	20	436	14	4	339	23	6	102	11	30	55	12
Peak Hour Factor	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	22	484	16	4	377	26	7	113	12	33	61	13
Number of Lanes	0	1	0	0	1	0	0	1	0	0	1	0
Approach	EB			WB			NB			SB		
Opposing Approach	WB			EB			SB			NB		
Opposing Lanes	1			1			1			1		
Conflicting Approach Left	SB			NB			EB			WB		
Conflicting Lanes Left	1			1			1			1		
Conflicting Approach Right	NB			SB			WB			EB		
Conflicting Lanes Right	1			1			1			1		
HCM Control Delay	24.7			17.3			11.8			11.5		
HCM LOS	С			С			В			В		

Lana	NBLn1	EBLn1	WBLn1	SBLn1
Lane				
Vol Left, %	5%	4%	1%	31%
Vol Thru, %	86%	93%	93%	57%
Vol Right, %	9%	3%	6%	12%
Sign Control	Stop	Stop	Stop	Stop
Traffic Vol by Lane	119	470	366	97
LT Vol	6	20	4	30
Through Vol	102	436	339	55
RT Vol	11	14	23	12
Lane Flow Rate	132	522	407	108
Geometry Grp	1	1	1	1
Degree of Util (X)	0.245	0.777	0.621	0.203
Departure Headway (Hd)	6.682	5.357	5.493	6.79
Convergence, Y/N	Yes	Yes	Yes	Yes
Сар	541	668	651	531
Service Time	4.682	3.437	3.578	4.796
HCM Lane V/C Ratio	0.244	0.781	0.625	0.203
HCM Control Delay	11.8	24.7	17.3	11.5
HCM Lane LOS	В	С	С	В
HCM 95th-tile Q	1	7.4	4.3	0.8

Intersection												
Intersection Delay, s/veh	53.1											
Intersection LOS	F											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			\$			4			4	
Traffic Vol, veh/h	20	496	14	12	382	77	6	102	28	108	55	12
Future Vol, veh/h	20	496	14	12	382	77	6	102	28	108	55	12
Peak Hour Factor	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	22	551	16	13	424	86	7	113	31	120	61	13
Number of Lanes	0	1	0	0	1	0	0	1	0	0	1	0
Approach	EB			WB			NB			SB		
Opposing Approach	WB			EB			SB			NB		
Opposing Lanes	1			1			1			1		
Conflicting Approach Left	SB			NB			EB			WB		
Conflicting Lanes Left	1			1			1			1		
Conflicting Approach Right	NB			SB			WB			EB		
Conflicting Lanes Right	1			1			1			1		
HCM Control Delay	79.1			48.3			15.1			16.9		
HCM LOS	F			E			С			С		
Lane		NBLn1	EBLn1	WBLn1	SBLn1							
Vol Left, %		4%	4%	3%	62%							
Vol Thru, %		75%	94%	81%	31%							
Vol Right, %		21%	3%	16%	7%							
Sign Control		Stop	Stop	Stop	Stop							
Traffic Vol by Lane		136	530	471	175							
LT Vol		6	20	12	108							
Through Vol		102	496	382	55							
RT Vol		28	14	77	12							
Lane Flow Rate		151	589	523	194							
Geometry Grp		1	1	1	1							
Degree of Util (X)		0.329	1.056	0.928	0.422							
Departure Headway (Hd)		8.141	6.455	6.582	8.1							
Convergence, Y/N		Yes	Yes	Yes	Yes							
Сар		444	565	555	447							
Service Time		6.141	4.503	4.582	6.1							
HCM Lane V/C Ratio		0.34	1.042	0.942	0.434							
HCM Control Delay		15.1	79.1	48.3	16.9							
HCM Lane LOS		С	F	E	С							
HCM 95th-tile Q		1.4	16.9	11.6	2.1							

Intersection												
Intersection Delay, s/veh Intersection LOS	60.7 F											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		- 4 >			ન ી	1		- 4 >		ሻ	4	
Traffic Vol, veh/h	20	496	14	12	382	77	6	102	28	108	55	12
Future Vol, veh/h	20	496	14	12	382	77	6	102	28	108	55	12
Peak Hour Factor	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90
Heavy Vehicles, %	2	2	2	2		2	2	2	2	2	2	2
Mvmt Flow	22	551	16	13	424	86	7	113	31	120	61	13
Number of Lanes	0	1	0	0	1	1	0	1	0	1	1	0
Approach	EB			WB			NB			SB		
Opposing Approach	WB			EB			SB			NB		
Opposing Lanes	2			1			2			1		
Conflicting Approach Left	SB			NB			EB			WB		
Conflicting Lanes Left	2			1			1			2		
Conflicting Approach Right	NB			SB			WB			EB		
Conflicting Lanes Right	1			2			2			1		
HCM Control Delay	112.5			32.4			16.3			14.4		
HCM LOS	F			D			С			В		
Lane		NBLn1	EBLn1	WBLn1	WBLn2	SBLn1	SBLn2					
Vol Left, %		4%	4%	3%	0%	100%	0%					
Vol Thru, %		75%	94%	97%	0%	0%	82%					
Vol Right, %		21%	3%	0%	100%	0%	18%					
Sign Control		Stop	Stop	Stop	Stop	Stop	Stop					
Traffic Vol by Lane		136	530	394	77	108	67					
LT Vol		6	20	12	0	108	0					
Through Vol		102	496	382	0	0	55					
RT Vol		28	14	0	77	0	12					
Lane Flow Rate		151	589	438	86	120	74					
Geometry Grp		6	6	7	7	7	7					
Degree of Util (X)		0.345	1.149	0.835	0.146	0.286	0.165					
Departure Headway (Hd)		8.785	7.023	7.215	6.48	9.089	8.439					
Convergence, Y/N		Yes	Yes	Yes	Yes	Yes	Yes					
Cap		413	524	503	557	398	428					
Service Time		6.785	5.023	4.915	4.18	6.789	6.139					
HCM Lane V/C Ratio		0.366	1.124	0.871	0.154	0.302	0.173					
HCM Control Delay		16.3	112.5	36.7	10.3	15.4	12.8					
HCM Lane LOS		С	F	E	В	С	В					
HCM 95th-tile Q		1.5	20.4	8.4	0.5	1.2	0.6					

APPENDIX G

CAPACITY ANALYSIS CALCULATIONS MITCHELL MILL ROAD & SITE ACCESS 1

Intersection						
Int Delay, s/veh	0.4					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations		↑	ef 👘			1
Traffic Vol, veh/h	0	388	765	4	0	32
Future Vol, veh/h	0	388	765	4	0	32
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	-	0
Veh in Median Storage	e,# -	0	0	-	0	-
Grade, %	-	0	0	-	0	-
Peak Hour Factor	90	90	90	90	90	90
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	0	431	850	4	0	36
Major/Minor	Major1	N	Major2	Λ	/linor2	
Conflicting Flow All	- יומן	0	- 10/2	0	-	852
Stage 1	_	0	_	0	_	0.52
Stage 2	_		_	_	_	_
Critical Hdwy	-	-	-	-	-	- 6.22
Critical Hdwy Stg 1	-	-	-	-	-	0.22
Critical Hdwy Stg 2	-	-	-	-	-	-
Follow-up Hdwy	-	-	-	-	-	- 3.318
	-	-	-	-	-	359
Pot Cap-1 Maneuver	0 0	-	-	-	0 0	309
Stage 1	0	-	-	-		-
Stage 2	0	-	-	-	0	-
Platoon blocked, %		-	-	-		250
Mov Cap-1 Maneuver	-	-	-	-	-	359
Mov Cap-2 Maneuver	-	-	-	-	-	-
Stage 1	-	-	-	-	-	-
Stage 2	-	-	-	-	-	-
Approach	EB		WB		SB	
HCM Control Delay, s	0		0		16.1	
HCM LOS					С	
Minor Lane/Major Mvm	nt	EBT	WBT	WBR S	SBLn1	
Capacity (veh/h)					359	
HCM Lane V/C Ratio		_	-	_	0.099	
HCM Control Delay (s)		-	-	_	16.1	
HCM Lane LOS		-	-	_	C	
HCM 95th %tile Q(veh))	_	-	-	0.3	
	/	-	-	-	0.5	

Intersection						
Int Delay, s/veh	0.2					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations		↑	¢,			1
Traffic Vol, veh/h	0	632	451	4	0	20
Future Vol, veh/h	0	632	451	4	0	20
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	-	0
Veh in Median Storage,	,# -	0	0	-	0	-
Grade, %	-	0	0	-	0	-
Peak Hour Factor	90	90	90	90	90	90
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	0	702	501	4	0	22
Major/Minor N	1ajor1	Ν	Major2	Ν	/linor2	
Conflicting Flow All	-	0	-	0	-	503
Stage 1	-	-	-	-	-	-
Stage 2	-	-	-	-	-	-
Critical Hdwy	-	-	-	-	-	6.22
Critical Hdwy Stg 1	-	-	-	-	-	-
Critical Hdwy Stg 2	-	-	-	-	-	-
Follow-up Hdwy	-	-	-	-	-	3.318
Pot Cap-1 Maneuver	0	-	-	-	0	569
Stage 1	0	-	-	-	0	-
Stage 2	0	-	-	-	0	-
Platoon blocked, %		-	-	-		
Mov Cap-1 Maneuver	-	-	-	-	-	569
Mov Cap-2 Maneuver	-	-	-	-	-	-
Stage 1	-	-	-	-	-	-
Stage 2	-	-	-	-	-	-
U U						
Approach	EB		WB		SB	
HCM Control Delay, s	0		0		11.6	
HCM LOS	-		2		В	
					_	
Minor Lane/Major Mvm	t	EBT	WBT	WBR S	SBLn1	
Capacity (veh/h)	-			-	569	
HCM Lane V/C Ratio		-	-		0.039	
HCM Control Delay (s)		-	-	-	11.6	
HCM Lane LOS		-	-	-	B	
HCM 95th %tile Q(veh)		-	-	-	0.1	
					5.1	

APPENDIX H

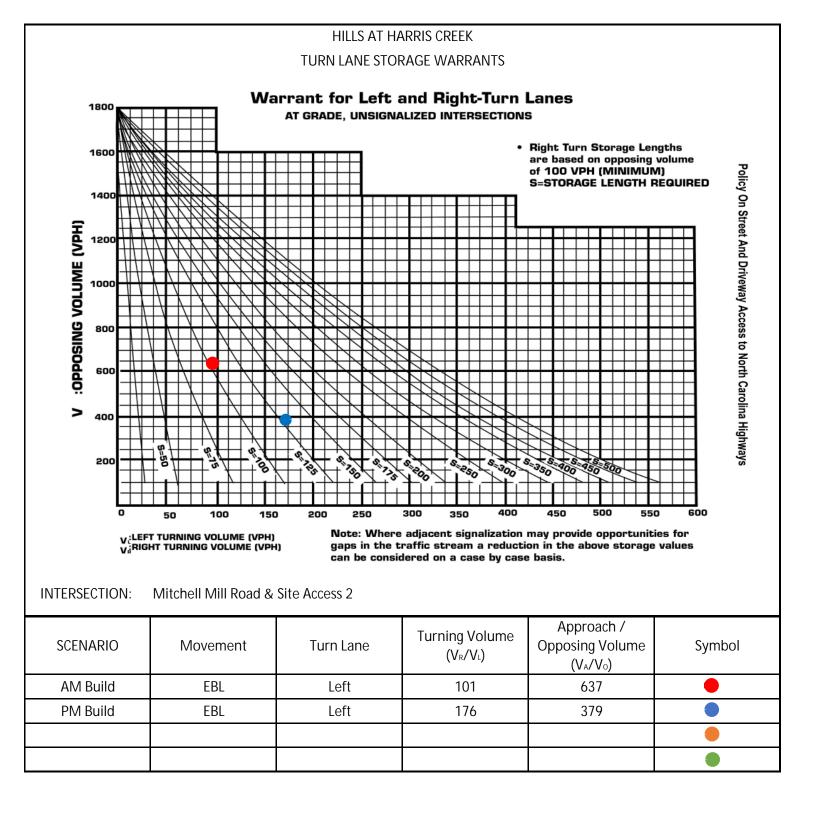
CAPACITY ANALYSIS CALCULATIONS MITCHELL MILL ROAD & SITE ACCESS 2

Intersection						
Int Delay, s/veh	3.9					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations	1	↑	•	1	۰Y	
Traffic Vol, veh/h	101	287	626	11	19	139
Future Vol, veh/h	101	287	626	11	19	139
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None		None
Storage Length	150	-	-	100	0	-
Veh in Median Storage	e,# -	0	0	-	0	-
Grade, %	-	0	0	-	0	-
Peak Hour Factor	90	90	90	90	90	90
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	112	319	696	12	21	154
		017	070			101
				-		
-	Major1		Major2		Minor2	
Conflicting Flow All	708	0	-	0	1239	696
Stage 1	-	-	-	-	696	-
Stage 2	-	-	-	-	543	-
Critical Hdwy	4.12	-	-	-	6.42	6.22
Critical Hdwy Stg 1	-	-	-	-	5.42	-
Critical Hdwy Stg 2	-	-	-	-	5.42	-
Follow-up Hdwy	2.218	-	-	-	3.518	3.318
Pot Cap-1 Maneuver	891	-	-	-	194	442
Stage 1	-	-	-	-	495	-
Stage 2	-	-	-	-	582	-
Platoon blocked, %		-	-	-		
Mov Cap-1 Maneuver	891	-	-	-	170	442
Mov Cap-2 Maneuver	-	-	-	-	170	-
Stage 1	-	-	-	-	433	-
Stage 2			_	_	582	
Stage 2					502	
Approach	EB		WB		SB	
HCM Control Delay, s	2.5		0		23.1	
HCM LOS					С	
Minor Lane/Major Mvm	nt	EBL	EBT	WBT	WBR	SBLn1
Capacity (veh/h)		891	-	-	-	371
HCM Lane V/C Ratio		0.126	-	-	-	0.473
HCM Control Delay (s)		9.6	-	-	-	
HCM Lane LOS		A	-	-	_	23.1 C
HCM 95th %tile Q(veh))	0.4	-	-	_	2.4
	/	0.4				2.7

Intersection						
Int Delay, s/veh	3.9					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations	٦	1	•	1	۰Y	
Traffic Vol, veh/h	176	456	353	26	33	98
Future Vol, veh/h	176	456	353	26	33	98
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	150	-	-	100	0	-
Veh in Median Storage		0	0	-	0	-
Grade, %	-	0	0	-	0	-
Peak Hour Factor	90	90	90	90	90	90
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	196	507	392	29	37	109
	190	507	392	29	57	109
Major/Minor N	Major1	Ι	Najor2	[Vinor2	
Conflicting Flow All	421	0	-	0	1291	392
Stage 1	-	-	-	-	392	-
Stage 2	-	-	-	-	899	-
Critical Hdwy	4.12	-	-	-	6.42	6.22
Critical Hdwy Stg 1	-	-	-	-	5.42	-
Critical Hdwy Stg 2	-	-	-	-	5.42	-
	2.218	-	-	-	3.518	3.318
Pot Cap-1 Maneuver	1138	-	-	-	180	657
Stage 1	-	-	-	-	683	-
Stage 2	-	_		-	397	_
Platoon blocked, %		_	_		577	
Mov Cap-1 Maneuver	1138				149	657
Mov Cap-2 Maneuver	1150	-	-	-	149	057
-	-	-	-	-		-
Stage 1	-	-	-	-	566	-
Stage 2	-	-	-	-	397	-
Approach	EB		WB		SB	
HCM Control Delay, s	2.5		0		22.2	
HCM LOS					С	
Minor Lane/Major Mvm	nt	EBL	EBT	WRT	WBR	SBI n1
Capacity (veh/h)		1138				353
HCM Lane V/C Ratio		0.172	-	-	-	
			-	-		0.412
HCM Control Delay (s)		8.8	-	-	-	22.2
HCM Lane LOS	`	A	-	-	-	С
HCM 95th %tile Q(veh))	0.6	-	-	-	2

APPENDIX I

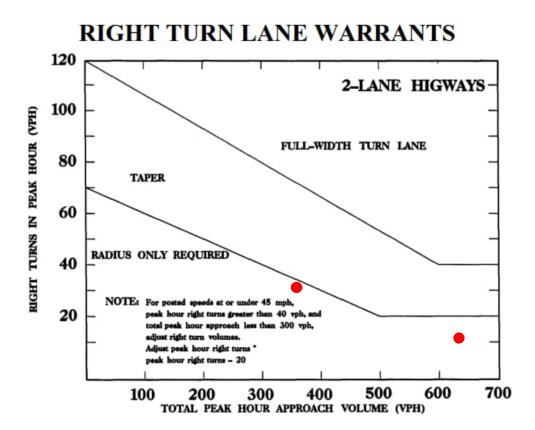
TURN LANE WARRANTS





Mitchell Mill Road and Site Access 2

2027 Build								
Peak Hour	Approach	Right Turn Volume	Approach Volume	Warranted?				
AM	Westbound	11	637	No				
PM	Westbound	26	379	No				



APPENDIX J

MUTCD / ITRE SIGNAL WARRANT ANALYSIS

Warrants 1 - 3 (Volume Warrants)

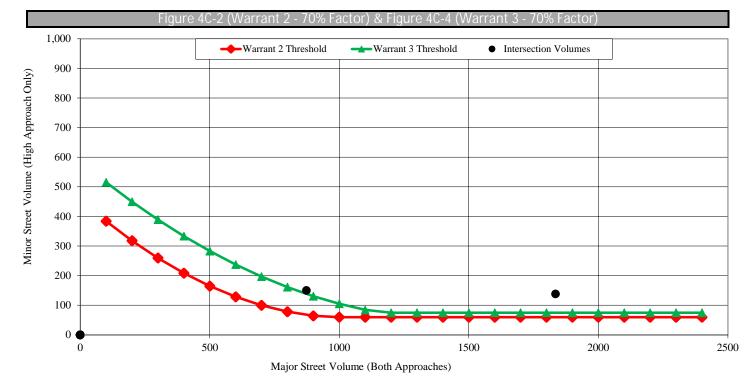
Project Name	Hills at H	Hills at Harris Creek						
Project/File #	204	98 - 05	7					
Scenario	2027]						
Intersection Information								
Major Street (E/W Road)	US 401 Bypass	Minor Street (N/S Road)	Jonesville Road / WB Left-Over					
Analyzed with	2 or more approach lanes	Analyzed with	1 Approach Lane					
Total Approach Volume	2861 vehicles	Total Approach Volume	424 vehicles					
Total Ped/Bike Volume	0 crossings	Total Ped/Bike Volume	0 crossings					
Right turn reduction of	100 percent applied	Right turn reduction of	0 percent applied					

No high speed or isolated community reduction applied to the Volume Warrant thresholds.

Warrant T, Eight Hour Vehicular Volume							
	Condition A	Condition B	Condition A+B*				
Condition Satisfied?	Not Satisfied	Not Satisfied	Not Satisfied				
Required values reached for	2 hours	2 hours	2 (Cond. A) & 2 (Cond. B)				
Criteria - Major Street (veh/hr)	420	630	336 (Cond. A) & 504 (Cond. B)				
Criteria - Minor Street (veh/hr)	105	53	84 (Cond. A) & 42 (Cond. B)				

Warrant 2, Four Hour Vehicular Volume							
Condition Satisfied?	Not Satisfied						
Required values reached for	2 hours						
Criteria	See Figure Below						

Warrant 3, Peak Hour Vehicular Volume								
	Condition A	Condition B						
Condition Satisfied?	Not Satisfied	Satisfied						
Required values reached for	1941 total, 41 minor, 0 delay	2 hours						
Criteria - Total Approach Volume (veh in one hour)	800							
Criteria - Minor Street High Side Volume (veh in one hour)	100	See Figure Below						
Criteria - Minor Street High Side Delay (veh-hrs)	4							



US 401 Bypass & Jonesville Road [Major-Street Left-Turn] [No-Build]

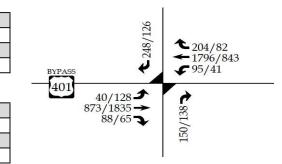
AM Peak Hour				
vph	g/c	а	b	С
900	0.7	0.00004	0.0097	0.4284
961	0.7	4.0E-05	0.009192	0.460018
1080	0.7	0.00004	0.0082	0.5217

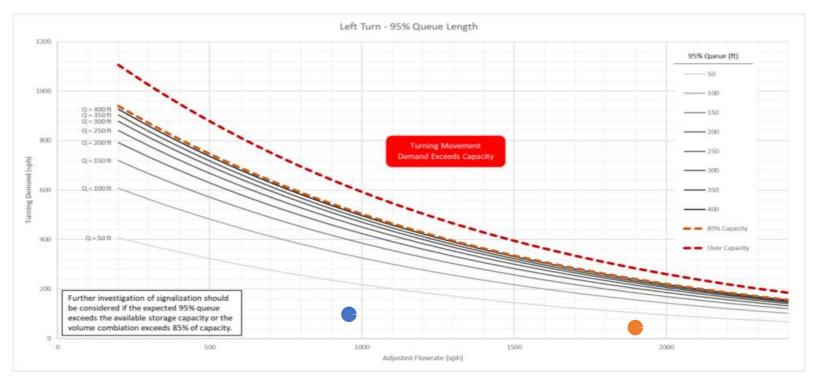
PM F	Peak Hour			
vph	g/c	а	b	с
1800	0.7	0.00004	0.0097	0.4284
1900	0.7	4.0E-05	0.008867	0.480233
1980	0.7	0.00004	0.0082	0.5217

Distance to Upstream Signal	8800	ft
Posted Speed Limit	55	mph
Travel Time	109.09	S

CVAF	1
Conflicting Volume (vph)	961
Adjusted Conflicting (vph)	961
Turning Volume (vph)	95
Adjusted Conflicting (vph)	961

-		
	CVAF	1
	Conflicting Volume (vph)	1900
	Adjusted Conflicting (vph)	1900
	Turning Volume (vph)	41





US 401 Bypass & Jonesville Road [Minor-Street Right-Turn] [No-Build]

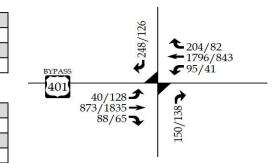
AM Pea	ak Hour			
vph	g/c	а	b	С
720	0.7	0.00004	0.0108	0.2587
873	0.7	3.2E-05	0.009525	0.34557
900	0.7	0.00003	0.0093	0.3609

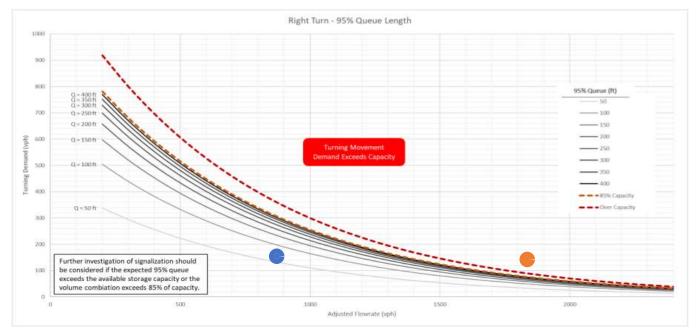
PM Pea	ak Hour			
vph	g/c	а	b	С
1800	0.7	0.00004	0.0108	0.2587
1835	0.7	3.8E-05	0.010508	0.278572
1980	0.7	0.00003	0.0093	0.3609

Distance to Upstream Signal	8800	ft
Posted Speed Limit	55	mph
Travel Time	109.09	S

CVAF	1
Conflicting Volume (vph)	873
Adjusted Conflicting (vph)	873
Turning Volume (vph)	150

CVAF	1
Conflicting Volume (vph)	1835
Adjusted Conflicting (vph)	1835
Turning Volume (vph)	138





Warrants 1 - 3 (Volume Warrants)

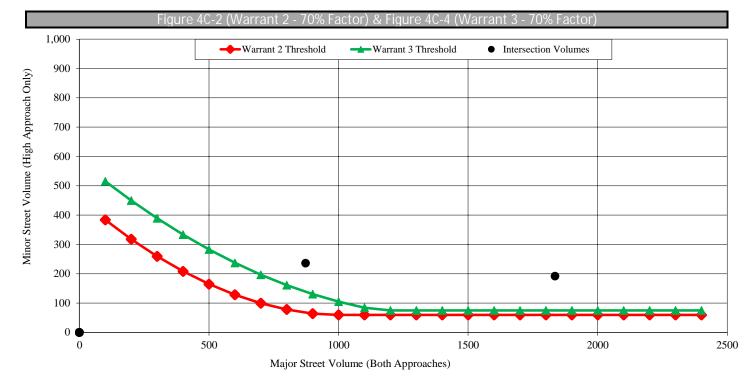
Project Name	Hills at H	Hills at Harris Creek		
Project/File #	204	20498 - 05		
Scenario	202	2027 Build		
	Intersectio	on Information		
Major Street (E/W Road)	US 401 Bypass	Minor Street (N/S Road)	Jonesville Road / WB Left-Over	
Analyzed with	2 or more approach lanes	Analyzed with	1 Approach Lane	
Total Approach Volume	2947 vehicles	Total Approach Volume	607 vehicles	
Total Ped/Bike Volume	0 crossings	Total Ped/Bike Volume	0 crossings	
Right turn reduction of	100 percent applied	Right turn reduction of	0 percent applied	

No high speed or isolated community reduction applied to the Volume Warrant thresholds.

Warrant T, Eight Hour Vehicular Volume				
	Condition A	Condition B	Condition A+B*	
Condition Satisfied?	Not Satisfied	Not Satisfied	Not Satisfied	
Required values reached for	2 hours	2 hours	2 (Cond. A) & 2 (Cond. B)	
Criteria - Major Street (veh/hr)	420	630	336 (Cond. A) & 504 (Cond. B)	
Criteria - Minor Street (veh/hr)	105	53	84 (Cond. A) & 42 (Cond. B)	

Warrant 2, Four Hour Vehicular Volume			
Condition Satisfied?	Not Satisfied		
Required values reached for	2 hours		
Criteria	See Figure Below		

Warrant 3, Peak Hour venicular volume			
	Condition A	Condition B	
Condition Satisfied?	Not Satisfied	Satisfied	
Required values reached for	2019 total, 67 minor, 0 delay	2 hours	
Criteria - Total Approach Volume (veh in one hour)	800		
Criteria - Minor Street High Side Volume (veh in one hour)	100	See Figure Below	
Criteria - Minor Street High Side Delay (veh-hrs)	4		



US 401 Bypass & Jonesville Road [Major-Street Left-Turn] [Build]

AM Peak Hour

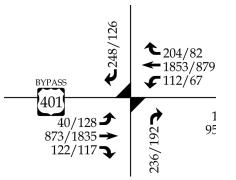
vph	g/c	а	b	С
900	0.7	0.00004	0.0097	0.4284
995	0.7	4.0E-05	0.008908	0.477642
1080	0.7	0.00004	0.0082	0.5217

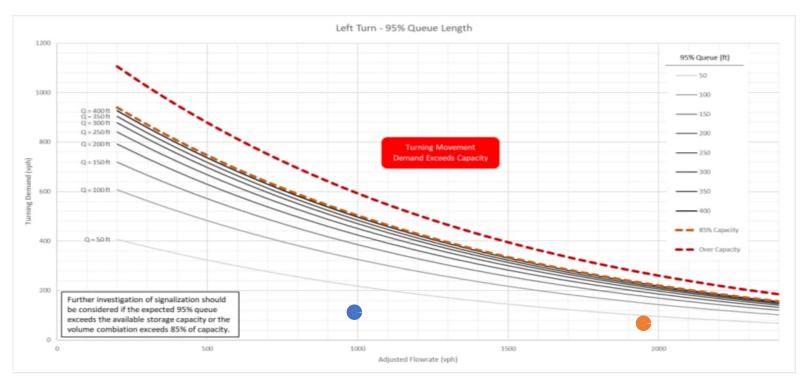
PM Pea	ak Hour			
vph	g/c	а	b	С
1800	0.7	0.00004	0.0097	0.4284
1952	0.7	4.0E-05	0.008433	0.507187
1980	0.7	0.00004	0.0082	0.5217

Distance to Upstream Signal	8800	ft
Posted Speed Limit	55	mph
Travel Time	109.09	S

CVAF	1
Conflicting Volume (vph)	995
Adjusted Conflicting (vph)	995
Turning Volume (vph)	112

CVAF	1
Conflicting Volume (vph)	1952
Adjusted Conflicting (vph)	1952
Turning Volume (vph)	67





US 401 Bypass & Jonesville Road [Minor-Street Right-Turn] [Build]

AM Peak Hour

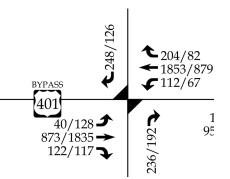
vph	g/c	а	b	С
720	0.7	0.00004	0.0108	0.2587
873	0.7	3.2E-05	0.009525	0.34557
900	0.7	0.00003	0.0093	0.3609

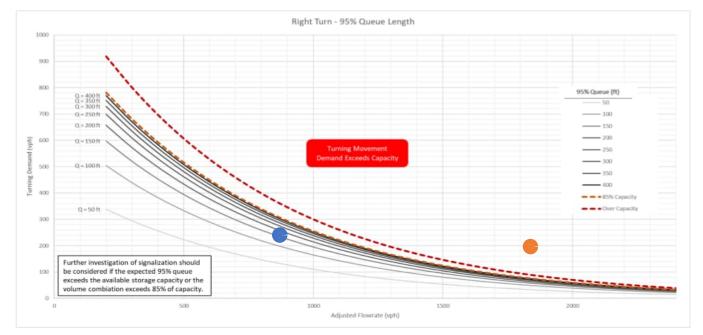
PM Pea	ak Hour			
vph	g/c	а	b	С
1800	0.7	0.00004	0.0108	0.2587
1835	0.7	3.8E-05	0.010508	0.278572
1980	0.7	0.00003	0.0093	0.3609

Distance to Upstream Signal	8800	ft
Posted Speed Limit	55	mph
Travel Time	109.09	S

CVAF	1
Conflicting Volume (vph)	873
Adjusted Conflicting (vph)	873
Turning Volume (vph)	236

CVAF	1
Conflicting Volume (vph)	1835
Adjusted Conflicting (vph)	1835
Turning Volume (vph)	192





Warrants 1 - 3 (Volume Warrants)

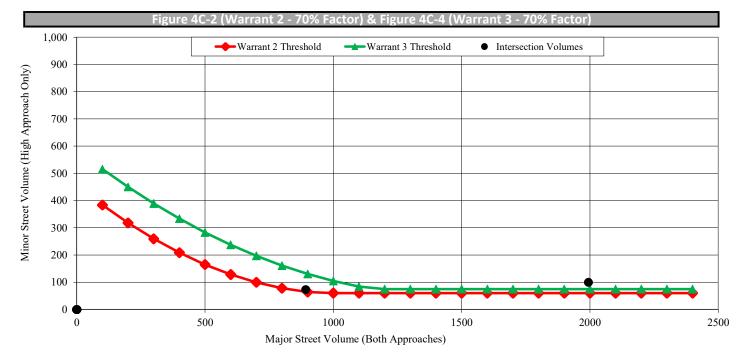
Project Name	Hills at Harris Creek		
Project/File #	20498 - 05		
Scenario	2027	2027 No-Build	
Major Street (E/W Road)	US 401 Bypass	Minor Street (N/S Road)	Eastern U-Turn Location
Analyzed with	2 or more approach lanes	Analyzed with	1 Approach Lane
Total Approach Volume	2886 vehicles	Total Approach Volume	173 vehicles
Total Ped/Bike Volume	0 crossings	Total Ped/Bike Volume	0 crossings
Right turn reduction of	0 percent applied	Right turn reduction of	0 percent applied

No high speed or isolated community reduction applied to the Volume Warrant thresholds.

Warrant 1, Eight Hour Vehicular Volume				
	Condition A	Condition B	Condition A+B*	
Condition Satisfied?	Not Satisfied	Not Satisfied	Not Satisfied	
Required values reached for	0 hours	2 hours	1 (Cond. A) & 2 (Cond. B)	
Criteria - Major Street (veh/hr)	420	630	336 (Cond. A) & 504 (Cond. B)	
Criteria - Minor Street (veh/hr)	105	53	84 (Cond. A) & 42 (Cond. B)	

Warrant 2, Four Hour Vehicular Volume			
Condition Satisfied?	Not Satisfied		
Required values reached for	2 hours		
Criteria	See Figure Below		

Warrant 3, Peak Hour Vehicular Volume				
Condition A Condition				
Condition Satisfied?	Not Satisfied	Satisfied		
Required values reached for	2094 total, 100 minor, 0 delay	1 hour		
Criteria - Total Approach Volume (veh in one hour)	650			
Criteria - Minor Street High Side Volume (veh in one hour)	100	See Figure Below		
Criteria - Minor Street High Side Delay (veh-hrs)	4			



US 401 Bypass & Eastern U-Turn Location [Major-Street U-Turn] [No-Build]

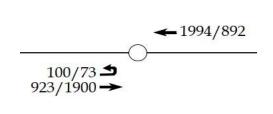
AM Pea	ak Hour			
vph	g/c	а	b	С
1800	0.7	0.00003	0.0072	0.5106
1994	0.7	3.0E-05	0.006984	0.539484
1980	0.7	0.00003	0.007	0.5374

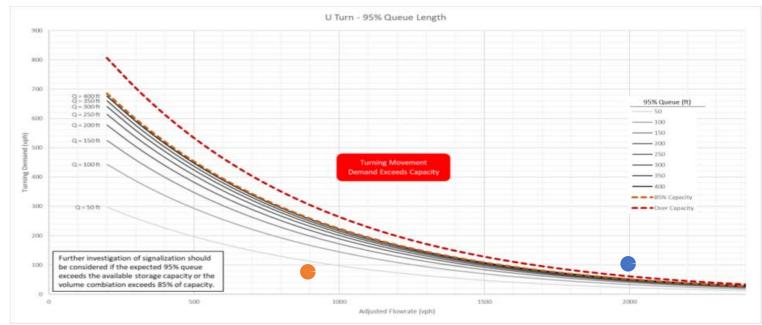
PM Pea	ak Hour			
vph	g/c	а	b	С
720	0.7	0.00003	0.0072	0.5106
892	0.7	3.0E-05	0.007009	0.536209
900	0.7	0.00003	0.007	0.5374

Distance to Upstream Signal	10000	ft
Posted Speed Limit	55	mph
Travel Time	123.97	S

CVAF	1
Conflicting Volume (vph)	1994
Adjusted Conflicting (vph)	1994
Turning Volume (vph)	100

CVAF	1
Conflicting Volume (vph)	892
Adjusted Conflicting (vph)	892
Turning Volume (vph)	73





Warrants 1 - 3 (Volume Warrants)

Proiect Name	lame Hills at Harris Creek		
Project/File #		20498 - 05	
Scenario 2027 Build]
	Intersection	on Information	
Major Street (E/W Road)	US 401 Bypass	Minor Street (N/S Road)	Eastern U-Turn Location
Analyzed with	2 or more approach lanes	Analyzed with	1 Approach Lane
Total Approach Volume	2929 vehicles	Total Approach Volume	266 vehicles
Total Ped/Bike Volume	0 crossings	Total Ped/Bike Volume	0 crossings

No high speed or isolated community reduction applied to the Volume Warrant thresholds.

Right turn reduction of

0 percent applied

Warrant I, Eight Hour Vehicular Volume			
	Condition A	Condition B	Condition A+B*
Condition Satisfied?	Not Satisfied	Not Satisfied	Not Satisfied
Required values reached for	2 hours	2 hours	2 (Cond. A) & 2 (Cond. B)
Criteria - Major Street (veh/hr)	420	630	336 (Cond. A) & 504 (Cond. B)
Criteria - Minor Street (veh/hr)	105	53	84 (Cond. A) & 42 (Cond. B)

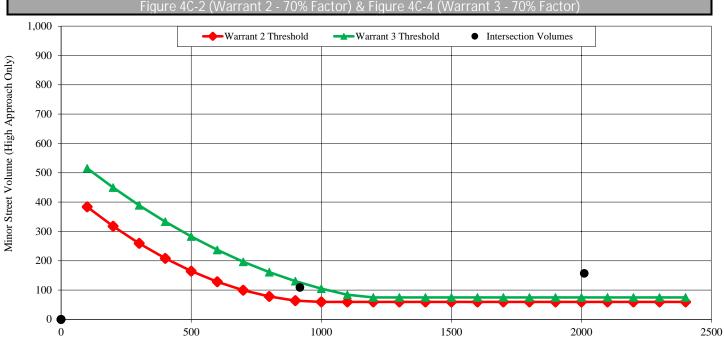
Right turn reduction of

0 percent applied

* Should be applied only after an adequate trial of other alternatives that could cause less delay and inconvenience to traffic has failed to solve the traffic problems.

Warrant 2, Four Hour Venicular Volume		
Condition Satisfied?	Not Satisfied	
Required values reached for	2 hours	
Criteria	See Figure Below	

vvarrant 3, Peak Hour venicular volume			
	Condition A	Condition B	
Condition Satisfied?	Not Satisfied	Satisfied	
Required values reached for	2168 total, 157 minor, 0 delay	1 hour	
Criteria - Total Approach Volume (veh in one hour)	650		
Criteria - Minor Street High Side Volume (veh in one hour)	100	See Figure Below	
Criteria - Minor Street High Side Delay (veh-hrs)	4		



Major Street Volume (Both Approaches)

US 401 Bypass & Eastern U-Turn Location [Major-Street U-Turn] [Build]

AM Peak Hour

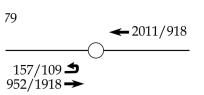
vph	g/c	а	b	С
1980	0.7	0.00003	0.007	0.5374
2011	0.7	3.0E-05	0.006966	0.544651
2160	0.7	0.00003	0.0068	0.5795

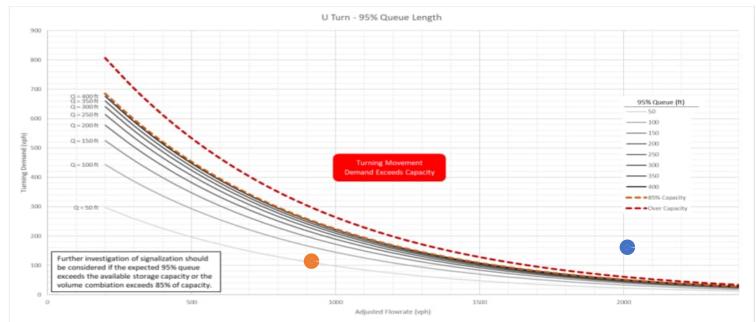
PM Pea	ak Hour			
vph	g/c	а	b	С
900	0.7	0.00003	0.007	0.5374
918	0.7	3.0E-05	0.00698	0.54161
1080	0.7	0.00003	0.0068	0.5795

Distance to Upstream Signal	10000	ft
Posted Speed Limit	55	mph
Travel Time	123.97	S

CVAF	1
Conflicting Volume (vph)	2011
Adjusted Conflicting (vph)	2011
Turning Volume (vph)	157

CVAF	1
Conflicting Volume (vph)	918
Adjusted Conflicting (vph)	918
Turning Volume (vph)	109





Warrants 1 - 3 (Volume Warrants)

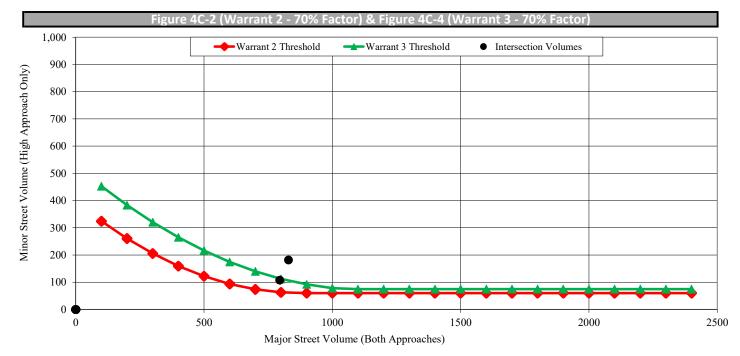
Project Name	Hills at Harris Creek		
Project/File #	20	20498 - 05	
Scenario	2027 No-Build		
	Intersect	ion Information	
Major Street (E/W Road)	Mitchell Mill Road	Minor Street (N/S Road)	Jonesville Road
Analyzed with	1 approach lane	Analyzed with	1 Approach Lane
Total Approach Volume	1708 vehicles	Total Approach Volume	518 vehicles
Total Ped/Bike Volume	0 crossings	Total Ped/Bike Volume	0 crossings
Right turn reduction of	100 percent applied Right turn reduction of		100 percent applied

No high speed or isolated community reduction applied to the Volume Warrant thresholds.

Warrant 1, Eight Hour Vehicular Volume				
	Condition A	Condition B	Condition A+B*	
Condition Satisfied?	Not Satisfied	Not Satisfied	Not Satisfied	
Required values reached for	2 hours	2 hours	2 (Cond. A) & 2 (Cond. B)	
Criteria - Major Street (veh/hr)	350	525	280 (Cond. A) & 420 (Cond. B)	
Criteria - Minor Street (veh/hr)	105	53	84 (Cond. A) & 42 (Cond. B)	

Warrant 2, Four Hour Vehicular Volume				
Condition Satisfied?	Not Satisfied			
Required values reached for	2 hours			
Criteria	See Figure Below			

Warrant 3, Peak Hour Vehicular Volume				
Condition A Condition B				
Condition Satisfied?	Not Satisfied	Satisfied		
Required values reached for	1178 total, 200 minor, 0 delay	1 hour		
Criteria - Total Approach Volume (veh in one hour)	800			
Criteria - Minor Street High Side Volume (veh in one hour)	100	See Figure Below		
Criteria - Minor Street High Side Delay (veh-hrs)	4			



Warrants 1 - 3 (Volume Warrants)

Project Name	Hills at Harris Creek		
Project/File #	20498 - 05		
Scenario	2027 Build		
	Intersect	ion Information	
Major Street (E/W Road)	Mitchell Mill Road	Minor Street (N/S Road)	Jonesville Road
Analyzed with	1 approach lane	Analyzed with	1 Approach Lane
Total Approach Volume	2087 vehicles	Total Approach Volume	675 vehicles
Total Ped/Bike Volume	0 crossings	Total Ped/Bike Volume	0 crossings
Right turn reduction of	100 percent applied	Right turn reduction of	100 percent applied

No high speed or isolated community reduction applied to the Volume Warrant thresholds.

Warrant T, Eight Hour Vehicular Volume				
	Condition A	Condition B	Condition A+B*	
Condition Satisfied?	Not Satisfied	Not Satisfied	Not Satisfied	
Required values reached for	2 hours	2 hours	2 (Cond. A) & 2 (Cond. B)	
Criteria - Major Street (veh/hr)	350	525	280 (Cond. A) & 420 (Cond. B)	
Criteria - Minor Street (veh/hr)	105	53	84 (Cond. A) & 42 (Cond. B)	

Warrant 2, Four Hour Venicular Volume				
Condition Satisfied?	Not Satisfied			
Required values reached for	2 hours			
Criteria	See Figure Below			

warrant 3, Peak Hour venicular volume				
	Condition A	Condition B		
Condition Satisfied?	Not Satisfied	Satisfied		
Required values reached for	1450 total, 251 minor, 0 delay	2 hours		
Criteria - Total Approach Volume (veh in one hour)	800			
Criteria - Minor Street High Side Volume (veh in one hour)	100	See Figure Below		
Criteria - Minor Street High Side Delay (veh-hrs)	4			

