DRAFT TECHNICAL MEMORANDUM



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То:	Tim Beasley Senior Engineer Raleigh Water One Exchange Plaza Raleigh, NC 27601	Copies:	Mike Isaac, P.E. Senior Project Manager Crosland Southeast 801 East Boulevard Charlotte, NC 28203
Date:	December 28, 2022	Proj. No.:	CSE2201
From:	Greg Fields, PE Brian Oschwald, PE		
Subject:	Wallbrook Development Gravity Sewer Capacity Evaluation		

Section 1 - Background

Crosland Southeast and Wallbrook Landco LLC are planning a land development project in Rolesville, North Carolina. The development will include retail, commercial, and multi-family units with a total area of approximately 52 acres near the intersection of Main Street and Burlington Mills Road. The wastewater generated from the Wallbrook Development will be conveyed by new and existing 8- though 18-inch gravity sewer through the development and along Virginia Water Drive, Trillick Court, and cross country toward US Highway 401.

The City of Raleigh has concerns regarding the downstream sewer capacity due to the additional wastewater being generated. The City requested a gravity sewer capacity evaluation be performed for the gravity sewer from the proposed development, starting on S. Main Street and continuing southeast for approximately 5,100 linear feet (LF) to a point before the gravity crosses under Highway 401 Bypass.

Wallbrook Landco LLC has contracted with HIGHFILL to prepare the gravity sewer capacity evaluation.

1.1 Data Acquisition and Historical Documents

The following data was provided for the purposes of this evaluation:

- Villages of Rolesville Plan and Profile Sanitary Sewer Outfalls As Built Survey prepared by Priest, Craven & Associates, Inc. dated July 26, 2002.
- Rim and Invert Survey of the manholes within the evaluation area performed by CMP Land Surveyors dated February 18, 2022, June 6, 2022, and September 30, 2022.
- GIS Data provided by the City of Raleigh received on August 31, 2022.
- Existing Sewer Basin Flowrate Tabulation provided by McAdams dated June 8, 2021 and sent to HIGHFILL on February 8, 2022.
- Erosion Control / Mass Grading / Sanitary Sewer Relocation Plans for Wallbrook provided by Ark Consulting dated July 22, 2022.

• Site Data and Estimated Daily Wastewater Flowrates – provided by Ark Consulting – dated April 20, 2022.

1.2 Initial Gravity Sewer Improvements

The mass grading and erosion control plans for the first lot to be developed conflict with the four most upstream segments of existing gravity sewer, just south of S. Main Street. To continue to provide sewer service during initial construction these segments of sewer will be re-routed through the development and tie into existing gravity sewer where Virginia Water Drive dead ends into the development. As the development progresses, the gravity sewer will be re-routed through the proposed residential development and cross an Unnamed Tributary to Wall Creek to tie into the existing gravity sewer between SMH169376 and SMH169377. As evaluated and described within, further sewer improvements are proposed downstream of this initial tie in.

Section 2 - Wastewater Flow Development

2.1 Existing Wastewater Flows

The existing wastewater flows for the sewer basin were determined using metered flow data provided by the City of Raleigh to McAdams. The data is included in Appendix A. For sub-basins that were not metered, the existing flows were calculated using the unit flow rate for single family residential properties as outlined in the 2014 City of Raleigh Handbook (250 GPD/unit). These flows were peaked using a peaking factor of 2.5.

The existing wastewater flows are summarized in Table 2.1. A detailed summary of the existing wastewater flows are included as attachments and in Appendix B.

Tributary to Node:	Description		Existing Flow (GPD)
A	Tributary from west of S. Main Street		456,480
	• Area 1	Subtotal	21,024 477,504
В	From Node A		477,504
С	• From Node B		477,504
D	 From Node C Area 2 Flow tributary to Area 2 	Subtotal	477,504 100,656 679,680 1,257,840
E	From Node DArea 3	Subtotal	1,257,840 49,104 1,306,944

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Tributary to Node:	Description		Existing Flow (GPD)
F	From Node EArea 4	Subtotal	1,306,944 8,928 1,315,872
G	From Node FArea 5	Subtotal	1,315,872 23,904 1,339,776
Н	From Node GArea 6Area 7	Subtotal	1,339,776 106,375 25,000 1,474,151
		Total	1,474,151

2.2 Proposed Wastewater Flows

The proposed wastewater flows were provided by the developer, can be viewed in detail in Appendix A, and are summarized in Table 2.2. A detailed summary of the proposed wastewater flows are included as attachments and in Appendix B.

Descript	ion	Acres or Units	Flowrate (GPD)	Peak Flowrate (GPD)		
	Lot 1	10.9	19,620	49,050		
	Lot 5	5.1	9,180	22,950		
Wallbrook	Lot 6	120 (units)	30,000	75,000		
	Lot 7	2.7	4,860	12,150		
	Lot 8	5.4	9,720	24,300		
	Lot 9	2.0	3,600	9,000		
Paris Tract	Lot 10	3.5	6,300	15,750		
	Lot 11	1.6	2,880	7,200		
MBW Tract	Lot 12	5.2	9,360	23,400		

Table 2.2 – Summary of Estimated Proposed Flows Tributary to Node B

Descript	ion	Acres or Units	Flowrate (GPD)	Peak Flowrate (GPD)
MBW Tract	Lot 13	1.5	2,700	6,750
		Total	98,220	245,550

Section 3 - Sewer Capacity Evaluation

For this evaluation, the sewer capacity was determined by using the Manning's equation for full pipe flow, which incorporates the pipe diameter, the existing pipe slope, and a Manning's "n-value" of 0.013. A rim and invert survey was performed throughout the study area to determine pipe slopes. Per the City of Raleigh Development Handbook, the calculated peak flow should not exceed 50% capacity of the pipe at full pipe flow.

The sewer capacity evaluation included three scenarios:

- 1) Existing Flows through Existing Pipes
- 2) Existing and Proposed Flows through Existing Pipes
- 3) Existing and Proposed Flows through Proposed Pipes

A summary of the worst case pipe capacity from Node to Node is included in Table 3.1. A detailed capacity of the three evaluations is shown in Figures 1-3 and in Appendix B.

			aation		
Tributary to Node:	Upstream SSMH ID	Downstream SSMH ID	Ex. Flow through Ex. Pipe	Ex. & Prop. Flows through Ex. Pipe	Ex. & Prop. Flows through Upsized Pipe
B to C	169377	152615	93%	141%	48%
C to D	111997	187382	119%	145%	49%
D to E	187382	142684	107%	130%	44%
E to F	154111	152073	106%	128%	43%
G to End	122295	121589	90%	108%	37%

Table 3.1 – Summary of Sewer Capacity Evaluation

Section 4 - Summary and Recommendation

4.1 Summary

The capacity evaluation of the existing gravity sewer illustrates that it does not have available capacity to convey the flow. As determined by the capacity evaluations, the following sewer upgrades are proposed to

convey the flows and remain below 50% pipe capacity. The specific locations of these improvements are shown on Figure 3, along with the resulting capacities.

Gravity Sewer Location	Sewer Length (feet)
Proposed 12-inch Gravity Sewer through Wallbrook	2,350
Existing Gravity Sewer Upsize from 8- to 12-inch (Virginia Water Drive)	900
Existing Gravity Sewer Upsize from 12- to 18-inch (south of Trillick Court)	1,000
Total	4,250

4.2 Recommendation

The developer plans to install the proposed 12-inch gravity sewer through the Wallbrook Development and upsize existing 8-inch to 12-inch sewer along Virginia Water Drive. The gravity sewer segments south of Trillick Court that are over capacity are recommended to be upsized from 12-inch to 18-inch. Finally, the capacity of four existing sewer segments south of Trillick Court are between 50-65% with the existing and proposed flows. Those sewer segments may be considered by the City for a fee in-lieu payment rather than upsizing.

Attachments:

- Figure 1 Existing Basin
- Figure 2 Capacity of Existing Sewer Lines
- Figure 3 Capacity of Upsized Downstream Gravity Sewer

Appendix A – Site Data & Estimated Daily Flowrates and 2021-06-08 Sewage Generation Exhibit by McAdams and City of Raleigh

Appendix B – Wastewater Flowrate Tabulation and Capacity Evaluation







Appendix A

Site Data & Estimated Daily Flowrates and 2021-06-08 Sewage Generation Exhibit by McAdams and City of Raleigh



However, the maps are produced for information purposes, and are **NOT** surveys. No warranties, expressed or implied,



Appendix B

Wastewater Flowrate Tabulation and Capacity Evaluation Opinion of Probable Construction Cost

Appendix A Wallbrook Downstream Gravity Sewer Evaluation Existing Flow thru Existing Pipes

Sub-Basin ID	Metered Flow	Peaked Flow	Sub-Basin Peak Flow (GPD)	Cumulative Peak Flow (GPD)	Line Size (inches)	Length (ft.)	Upstream SSMH	Downstream SSMH	Pipe Slope from Survey	100% Capacity (GPD)	Percentage of 100% Capacity at Existing Peak Flow	
Tributary	Х		456,480									
Area 1	Х		21,024									
Node A				477,504	8	219	169376	169377	0.73	667,302	72%	
Node B				477,504	8	282	169377	152615	0.43	512,147	93%	
				477,504	8	124	152615	169410	0.65	629,677	76%	
				477,504	8	61	169410	165692	2.10	1,131,802	42%	
				477,504	8	279	165692	165691	0.43	512,147	93%	
				477,504	8	21	165691	160905	8.01	2,210,432	22%	
				477,504	8	123	160905	114338	1.53	966,065	49%	
Tributary to Area 2	Х		679,680									
Area 2	Х		100,656									
Node C				1,257,840	12	172	160905	102574	3.46	4,283,271	29%	
				1,257,840	12	176	102574	158980	10.11	7,321,720	17%	
				1,257,840	12	68	158980	111997	9.43	7,071,204	18%	
				1,257,840	12	98	111997	187382	0.21	1,055,230	119%	
Area 3	Х		49,104									
Node D				1,306,944	12	191	187382	142684	0.28	1,218,475	107%	
Area 4	Х		8,928									
Node E				1,315,872	12	287	142684	153264	0.35	1,362,296	97%	
				1,315,872	12	245	153264	154111	1.25	2,574,498	51%	
				1,315,872	12	240	154111	152073	0.29	1,240,042	106%	
				1,315,872	12	158	152073	144447	1.71	3,011,172	44%	
Area 5	Х		23,904									
Node F				1,339,776	12	26	144447	153263	1.96	3,223,781	42%	
Area 6 (175 lots X 250												
gal/lot/day X 2.5 PF)		х	109,375									
Area 7 (40 lots X 250												
gal/lot/day X 2.5 PF)		Х	25,000									
Node G				1,474,151	12	144	153263	187381	1.70	3,002,355	49%	
				1,474,151	12	195	187381	122295	5.07	5,184,913	28%	
				1,474,151	12	146	122295	121589	0.51	1,644,457	90%	

Over 50% Capacity

Appendix A Wallbrook Downstream Gravity Sewer Evaluation Existing and Proposed Flow thru Existing Pipes

Sub-Basin ID	Metered Flow	Peaked Flow	Sub-Basin Flow (GPD)	Cumulative Flow (GPD)	Line Size (inches)	Pipe Length	Upstream SSMH	Downstream SSMH	Pipe Slope from Survey	100% Capacity (GPD)	Percentage of 100% Capacity at Existing + Proposed Flow
Tributary	Х		456,480								
Paris Tract		Х	31,950								
Wallbrook Lot 1		Х	49,050								
Wallbrook Lot 5		Х	22,950								
MBW Tract		Х	30,150								
Wallbrook Lot 6 (120 THs X		v	75.000								
250 gal/day/unit X 2.5 PF)		^	75,000								
Wallbrook Lot 7		Х	12,150								
Wallbrook Lot 8		Х	24,300								
Area 1	Х		21,024								
Node A				723,054	8	219	169376	169377	0.73	667,302	108%
Node B				723,054	8	282	169377	152615	0.43	512,147	141%
				723,054	8	124	152615	169410	0.65	629,677	115%
				723,054	8	61	169410	165692	2.10	1,131,802	64%
				723,054	8	279	165692	165691	0.43	512,147	141%
				723,054	8	21	165691	160905	8.01	2,210,432	33%
				723,054	8	123	160905	114338	1.53	966,065	75%
Tributary to Area 2	Х		679,680								
Obligated to Area 2			28,224								
Area 2	Х		100,656								
Node C				1,531,614	12	172	114338	102574	3.46	4,283,271	36%
				1,531,614	12	176	102574	158980	10.11	7,321,720	21%
				1,531,614	12	71	158980	111997	9.43	7,071,204	22%
				1,531,614	12	98	111997	187382	0.21	1,055,230	145%
Area 3	Х		49,104								
Node D				1,580,718	12	191	187382	142684	0.28	1,218,475	130%
Area 4	Х		8,928								
Node E				1,589,646	12	287	142684	153264	0.35	1,362,296	117%
				1,589,646	12	245	153264	154111	1.25	2,574,498	62%
				1,589,646	12	240	154111	152073	0.29	1,240,042	128%
				1,589,646	12	159	152073	144447	1.71	3,011,172	53%
Area 5	Х		23,904								
Node F				1,613,550	12	25	144447	153263	1.96	3,223,781	50%
Obligated		Х	31,824	, ,						, ,	
Area 6 (175 lots X 250			,								
gal/lot/day X 2.5 PF)		Х	109,375								
Area 7 (40 lots X 250											
gal/lot/day X 2.5 PF)		Х	25,000								
Node G				1,779,749	12	145	153263	187381	1.70	3,002,355	59%
-				1,779.749	12	195	187381	122295	5.07	5,184.913	34%
				1,779,749	12	146	122295	121589	0.51	1,644,457	108%
		1									

Over 50% Capacity

Appendix A Wallbrook Downstream Gravity Sewer Evaluation Existing + Proposed Flow thru Proposed Pipe Upgrades

Sub-Basin ID	Metered Flow	Peaked Flow	Sub-Basin Flow (GPD)	Cumulative Flow (GPD)	Line Size (inches)	Length (ft)	Upstream SSMH	Downstream SSMH	Pipe Slope from Design Drawings/Survey	100% Capacity (GPD)	Percentage of 100% Capacity at Existing Flow	Recommended Pipe Upsize (inches)	100% Capacity with Upsize (GPD)	Percentage of 100% Capacity with Upsized Pipe
Tributary	Х		456,480											
Paris Tract		х	31,950											
				488,430	12		MH07	MH06	2.00	3,256,511	15%			
				488,430	12		MH06	MH05	1.90	3,174,054	15%			
				488,430	12		MH05	MH04	2.40	3,567,329	14%			
Wallbrook Lot 1		X	49,050	505 100	10				0.00		200/			
				537,480	12		MH04	MH16	0.60	1,783,664	30%			
				537,480	12		MH16	IVIH14	0.60	1,783,664	30%			
Wallbrook Lot F		¥	22.050	557,460	12		IVIN14	IVIH115	0.60	1,765,004	50%			
Wallbrook Lot 5		~	22,930	560.430	12		MH113	MH112	0.57	1 738 501	32%			
				560,430	12		MH112	MH111	0.67	1 884 842	30%			
				560,430	12		MH111	MH110	2 90	3 921 358	14%			
				560,430	12		MH110	MH109	1.90	3,174,054	18%			
				560,430	12		MH109	MH107	0.68	1.898.856	30%			
MBW Tract		х	30,150	,						,,				
Wallbrook Lot 6 (120 THs X 250 gal/day/unit X 2.5 PF)		x	75,000											
Wallbrook Lot 7		х	12.150											
Wallbrook Lot 8		х	24,300											
				702,030	12		MH107	MH106	0.60	1,783,664	39%			
				702,030	12		MH106	MH105	0.66	1,870,723	38%			
				702,030	12	1	MH105	MH104	0.91	2,196,637	32%			
				702,030	12	1	MH104	MH103	1.16	2,480,085	28%			
				702,030	12		MH103	MH102	1.04	2,348,303	30%			
				702,030	12		MH102	MH101	0.60	1,783,664	39%			
				702,030	12		MH101	MH100	0.53	1,676,391	42%			
Area 1	Х		21,024											
Node A				723,054	12	219	169376	169377	0.73	1,967,428	37%			
Node B				723,054	12	282	169377	152615	0.43	1,509,982	48%			
				723,054	12	124	152615	169410/MH1	0.65	1,856,497	39%			
				723,054	12	89	169410/MH1	MH2	1.80	3,089,397	23%			
				723,054	12	258	MH2	160905/MH3	0.78	2,033,690	36%			
	v		670.600	723,054	12	124	160905/MH3	114338	1.53	2,848,284	25%			
Tributary to Area 2	X		679,680											
Obligated to Area 2	v		28,224											
Area 2	^		100,656	4 534 644	42	472	444220	400574	2.46	4 202 274	260/			
Node C				1,531,614	12	172	114338	102574	3.46	4,283,271	36%			
				1,551,014	12	71	102574	111007	0.11	7,521,720	21%			
				1 531 614	12	98	111997	187382	0.43	1 055 230	145%	18	3 111 171	49%
Area 3	x		49.104	1,331,014	12	50	111557	107302	0.21	1,033,230	14570	10	3,111,171	7370
Node D	^			1.580.718	12	191	187382	142684	0.28	1.218.475	130%	18	3.592.471	44%
Area 4	Х		8,928	.,						,, ., o			-,,	
Node E			-,	1,589,646	12	287	142684	153264	0.35	1,362,296	117%	18	4,016,504	40%
				1,589,646	12	245	153264	154111	1.25	2,574,498	62%			
				1,589,646	12	240	154111	152073	0.29	1,240,042	128%	18	3,656,059	43%
				1,589,646	12	159	152073	144447	1.71	3,011,172	53%			
Area 5 (Metered)	Х		23,904											
Node F				1,613,550	12	25	144447	153263	1.96	3,223,781	50%			
Obligated		х	31,824											
Area 6 (175 lots X 250 gal/lot/day X 2.5 PF)		х	109,375											
Area 7 (40 lots X 250		х	25,000											
gai/lot/day x 2.5 PF)				1 770 740	12	145	152262	107201	1 70	2 002 255	E0%			
Node G				1,770,749	12	145	197291	10/301	1.70	5,002,355	24%			
				1 779 749	12	146	122205	122295	0.51	1 644,913	54%	18	4 848 409	37%
				1,113,143	14	140	122233	121505	0.51	1,044,437	10070	10	4,040,403	5170

