

# **PARKERS RIDGE**

82 SCHOOL STREET ROLESVILLE, NC 27571

# STORMWATER MANAGEMENT CALCULATIONS

### **PREPARED FOR:**

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### INTRODUCTION

On behalf of our client, Lennar Corporation, BGE, Inc. (BGE) submits this Engineer's Report in support of Parker Ridge project. This report contains the approach and results of the stormwater design for the subject property. The subject property is located at 82 School Street in the Town of Rolesville (Town), North Carolina. The site is comprised of four (4) parcels identified by the following parcel identification numbers (PINs): 1758-98-8411, 1758-98-3710, 1758-88-4270 E, and 1758-88-4270 W. The project area is approximately 86.74-acre (see project aerial map).

### **EXISTING CONDITIONS**

The existing site condition is primarily undeveloped and tree-covered with several existing ponds. The predominant soil types within the proposed limit of construction are Rawlings-Rion complex (RgD), Urban land (Ur), and Wake-Rolesville complex (WaD) as taken from the Web Soil Survey 2.1 – National Cooperative Soil Survey by NRCS).

For the western parcel most of the site drains to the stream that runs through the site and into the southwest corner shown as POA #1 on the Pre-Development Exhibit. For the east parcel most of the site drains into the existing pond located in the center of the east parcel and flows into Harris Creek exiting south of our site with a small portion draining to a more southern stream connection. These areas are shown on the Pre-Development Exhibit as POA#3 and POA#2. There is a large drainage area upstream of both the east and west that drains through the site. Most of these areas drain directly to the streams. The rest of the site runs off in smaller areas shown through POA #4, POA #5 and POA #6.

### FLOODPLAIN, FLOODWAY AND WATERSHED

The proposed site does not lie within a 100-year floodplain boundary as determined by FEMA FIRM Panel(s): #3720176800K and #3720175800K dated July 18, 2022.

### PROPOSED DEVELOPMENT

The overall proposed project will include the development of 114 attached townhouse lots and 161 single-family lots with associated infrastructure. The proposed impervious buildout for the development is as follows:

**Table 1 Impervious Area** 

POST-DEVELOPMENT IMPERVIOUS AREAS			
PAVEMENT – ROADS & DRIVEWAYS	24.77	AC	
SIDEWALK	3.35	AC	
LOTS - TOWNHOMES	5.7	AC	
LOTS - SINGLE-FAMILY (MAX.)	9.66	AC _	
TOTAL ONSITE IMPERVIOUS AREA:	43.48	AC	

### STORM DRAINAGE DESIGN

The existing topographic information was used to grade the property and identify the contributing drainage areas to the stormwater devices.

This project includes four (4) separate drainage systems that will drain to four (4) different proposed wet ponds located throughout the site. All four (4) of the proposed ponds will discharge to the existing Harris Creek located at the southern portion of both parcels. With Bypass also flowing into Harris Creek. The on-site storm sewer collection system was designed to capture and convey the 1-, 10-, and 25- year storm event for the proposed development. Per local design standards, the Rational Method and Manning's Equation will be used for the storm sewer system design utilizing AutoDesk's Hydraflow Storm Sewers software. A Manning's n value of 0.013 will be used for the reinforced concrete pipe and 0.024 for HDPE. Runoff coefficients (C) used for open space and impervious cover were 0.35 and 0.95, respectively. The starting HGL used for the 10 yr calculations is the 10 yr WSE for the detention pond, and the starting HGL for the 25 yr WSE for the 25 yr calculations.

### **WATER QUALITY**

The proposed wet detention ponds (SCM's) have been designed based on the town's water quantity requirements to attenuate the post-development peak runoff rates for the 1-, 10-, and 25-year storm events to pre-developed rates. The ponds are designed with weirs to safely pass the 25-year storm event and provides a minimum of one foot of freeboard above the peak stage to the top of the embankment.

The pre-development drainage area that was established for the project area includes stormwater runoff that will be conveyed to 6 points of analysis (POA's). The post-development drainage area was established based on proposed grading conditions, where all stormwater is either conveyed into a pond, and into a post-POA. The curve numbers (CN) and time of concentration (Tc) for each drainage basin were calculated based on existing and proposed conditions using the TR-55 method. The 4 proposed ponds (SCM's) were analyzed with Hydraflow modeling software for verification that the proposed design meets the Town of Rolesville's and NCDEQ's minimum requirements. The Wake County Stormwater Design Tool was used for this project. DA #s 1 - 6 match the pre and post development maps. SCM 1 and SCM2 correlate to POA 1 and POA 2 respectively. However, SCM#s 3 and 4 both drain to POA 3. In addition, the offsite drainage for POA 1&2 includes existing drainage from Redford Place Drive while POA 3 includes offsite drainage from the future Young Street connector.

### WATER QUANTITY

The proposed wet detention ponds (SCM's) have been designed based on both the NCDEQ's MDC and the town's water quantity requirements to attenuate the post-development peak runoff rates for the 1-, 10, and 25- year, 24-hour storm events. The post development flows are required to be less than the pre-developed rates by means of stormwater detention. The wet pond is designed to reduce the flows of each storm event mentioned above with a weir, the riser and an emergency spillway to safely pass the 25-year storm event.

The post-development drainage area was established based on existing and proposed site conditions. The curve numbers (CN) and time of concentration (Tc) for each drainage basin were calculated based on existing and proposed conditions using the TR-55 method. The 4 proposed ponds (SCM's) were

analyzed with Hydraflow modeling software for verification that the proposed design meets the Town of Rolesville and NCDEQ's minimum requirements. For the pre-development condition and the tree save areas, the curve # of roughly 77 was used while 80 was used for the open space (grass) and 98 was used for the impervious areas. Information on Peak Flow Analysis is available below in Table 2.

**Table 2 Peak Flow Analysis** 

	Pre-Development	Pre-Development	Post-Development	Post-Development	% Change	% Change
	(cfs)	(cfs)	(cfs)	(cfs)		
POA#	1-yr	10-yr	1-yr	10-yr	1-yr	10-yr
POA #1	32.39	86.61	17.50	60.63	-46%	-30%
POA #2	25.18	66.23	3.395	39.44	-87%	-40%
POA #3	49.44	160.03	34.11	128.42	-31%	-20%
POA #4	9.007	24.01	1.210	3.124	-87%	-87%
POA #5	4.695	11.8	1.831	4.727	-61%	-60%
POA #6	3.117	7.835	1.145	2.955	-63%	-62%

### **SUMMARY**

Based on the results of the stormwater models, all points of analysis are reduced in the post development condition. As a result, the proposed design meets the requirements for the Town of Rolesville and NCDEQ for stormwater conveyance, and stormwater treatment and detention. The stormwater detention information is as follows:

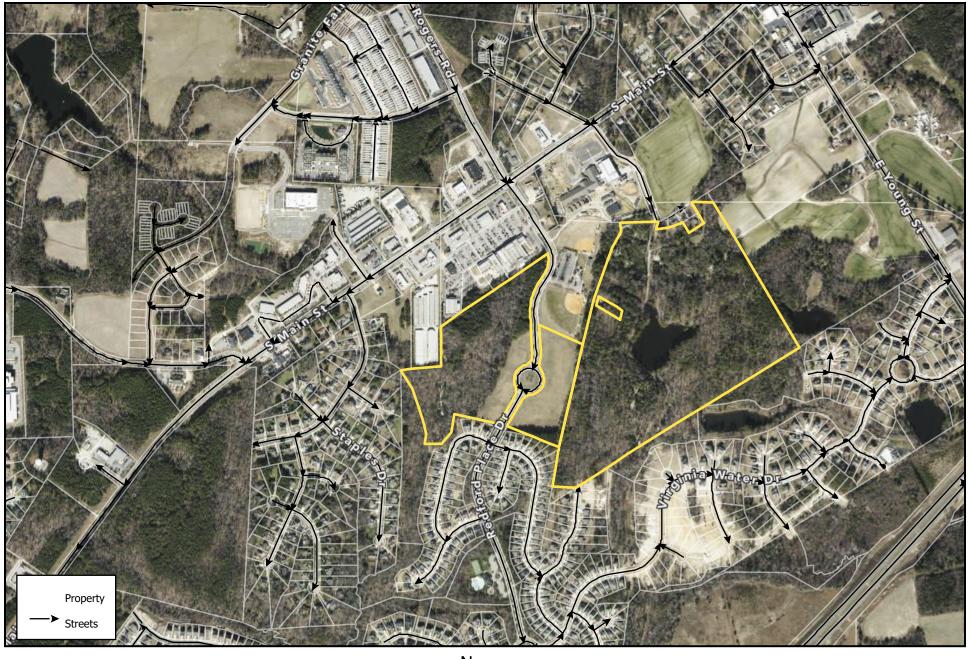
SCM #1 SCM #3

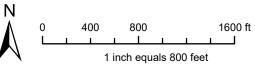
Drainage Area:	9.22 ac	Drainage Area:	12.04 ac
Impervious Area:	5.13 ac	Impervious Area:	6.23 ac
Average Pond Depth:	3.5 feet	Average Pond Depth:	3.5 feet
Surface Area Required:	7261 sf	Surface Area Required:	8910 sf
Surface Area Proposed:	8489 sf	Surface Area Proposed:	11217 sf
1" Detention Volume:	18433 cf	1" Detention Volume:	22539 cf
Top of Dam EI:	390 at 10' wide	Top of Dam El:	390 at 10' wide

SCM #2 SCM #4

Drainage Area:	20.21 ac	Drainage Area:	10.01 ac
Impervious Area:	10.42 ac	Impervious Area:	4.45 ac
Average Pond Depth:	3.5 feet	Average Pond Depth:	3.5 feet
Surface Area Required:	18693 sf	Surface Area Required:	8861 sf
Surface Area Proposed:	20384 sf	Surface Area Proposed:	14636 sf
1" Detention Volume:	37710 cf	1" Detention Volume:	16368 cf
Top of Dam El:	357 at 10' wide	Top of Dam El:	386 at 10' wide

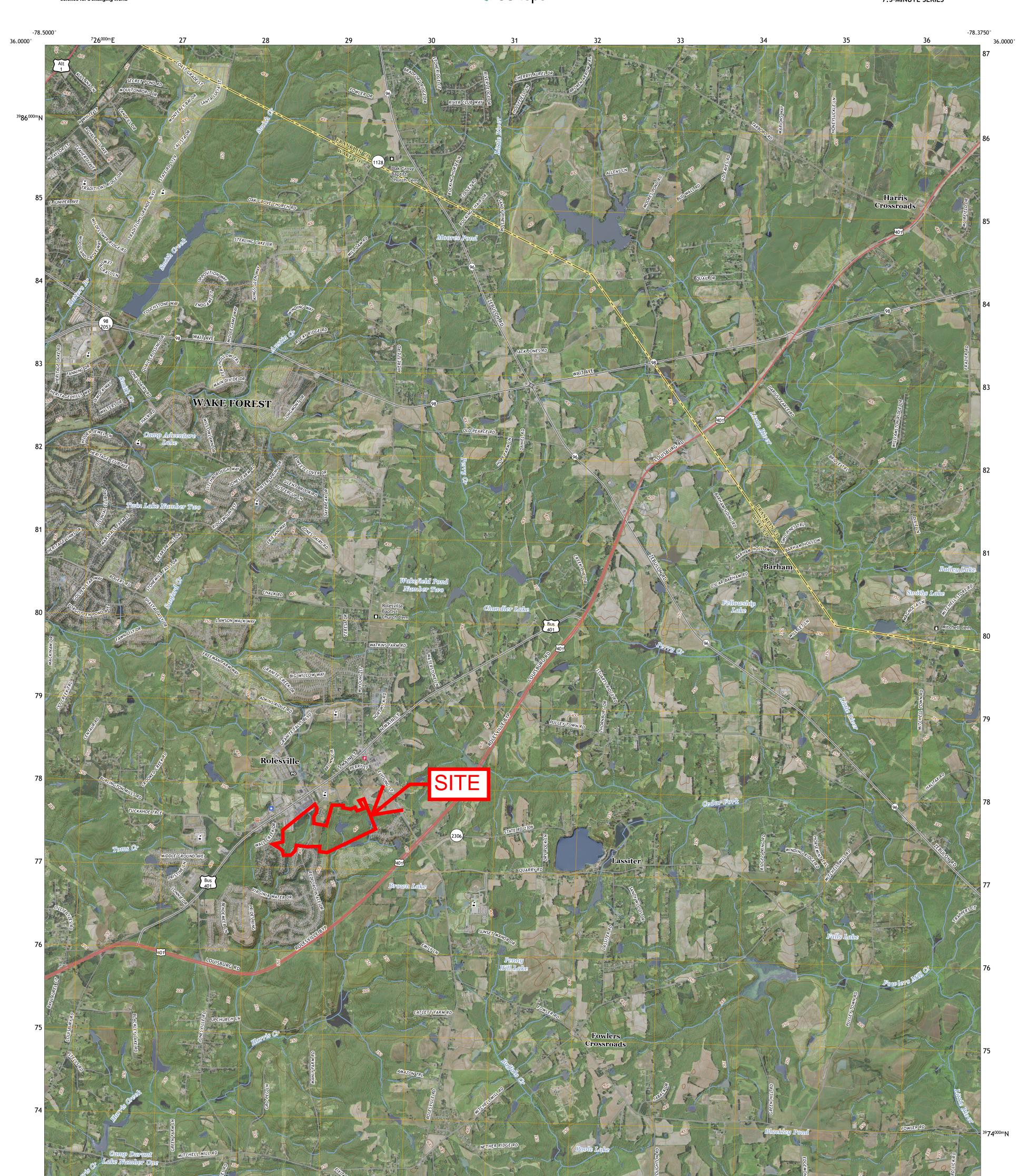
# **ATTACHMENT 1: PROJECT AERIAL MAP**

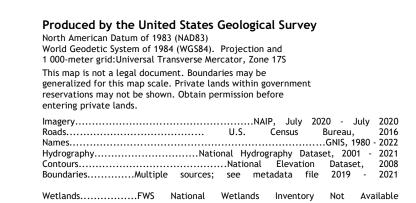




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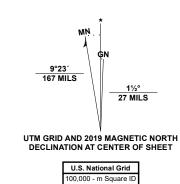
# **ATTACHMENT 2: USGS TOPO MAP**





35.8750°

-78.5000°



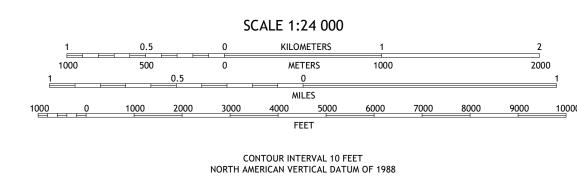
QV

Grid Zone Designation 17S

29

30

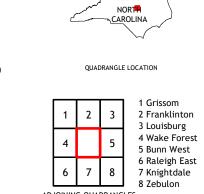
28



This map was produced to conform with the National Geospatial Program US Topo Product Standard.

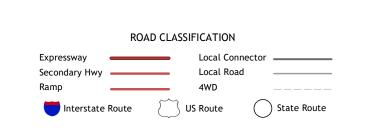
31

32



ADJOINING QUADRANGLES

33



35

-78.3750° 35.8750°

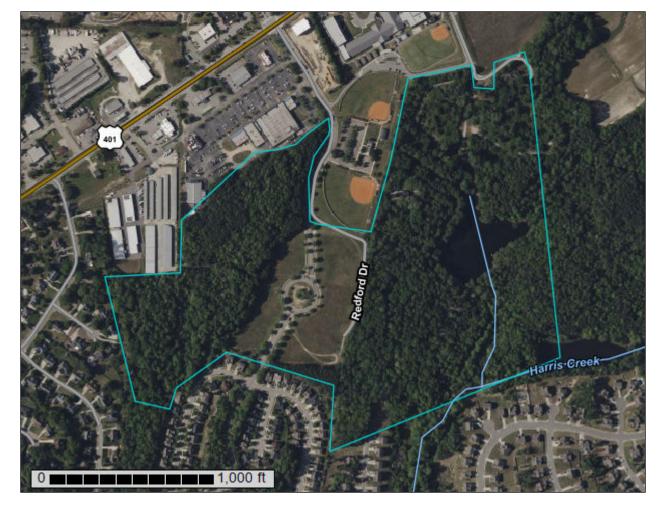
# **ATTACHMENT 3: SOIL SURVEY REPORT**



**NRCS** 

Natural Resources Conservation Service A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

# Custom Soil Resource Report for Wake County, North Carolina



# **Preface**

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2\_053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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# **How Soil Surveys Are Made**

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

# Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



### MAP LEGEND

### Area of Interest (AOI)

Area of Interest (AOI)

### Soils

Soil Map Unit Polygons

-

Soil Map Unit Lines

Soil Map Unit Points

### Special Point Features

**(**)

Blowout

 $\boxtimes$ 

Borrow Pit

Ж

Clay Spot

 $\Diamond$ 

Closed Depression

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Gravel Pit

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Gravelly Spot

0

Landfill Lava Flow

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Marsh or swamp

@

Mine or Quarry

0

Miscellaneous Water
Perennial Water

0

Rock Outcrop

+

Saline Spot

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Sandy Spot

Sodic Spot

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Severely Eroded Spot

Sinkhole

Slide or Slip

Ø

8

Spoil Area Stony Spot

Ø M

Very Stony Spot

3

Wet Spot Other

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Special Line Features

### Water Features

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Streams and Canals

### Transportation

ransp

Rails

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Interstate Highways

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US Routes

 $\sim$ 

Major Roads

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Local Roads

### Background

100

Aerial Photography

### MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24.000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Wake County, North Carolina Survey Area Data: Version 23, Sep 12, 2022

Soil map units are labeled (as space allows) for map scales 1:50.000 or larger.

Date(s) aerial images were photographed: Apr 24, 2022—May 9, 2022

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

# Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
HeB	Helena sandy loam, 2 to 6 percent slopes	11.1	13.2%
RgB	Rawlings-Rion complex, 2 to 6 percent slopes	6.1	7.2%
RgC	Rawlings-Rion complex, 6 to 10 percent slopes	0.6	0.7%
RgD	Rawlings-Rion complex, 10 to 15 percent slopes	17.4	20.5%
Ur	Urban land	16.4	19.4%
W	Water	3.9	4.6%
WaD	Wake-Rolesville complex, 10 to 15 percent slopes, very rocky	13.4	15.8%
WaE	Wake-Rolesville complex, 15 to 25 percent slopes, very rocky	11.6	13.7%
WfB	Wedowee-Saw complex, 2 to 6 percent slopes	1.2	1.4%
WgB	Wedowee-Urban land complex, 2 to 6 percent slopes	2.8	3.4%
WgC	Wedowee-Urban land complex, 6 to 15 percent slopes	0.1	0.2%
Totals for Area of Interest		84.7	100.0%

# **Map Unit Descriptions**

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties

and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

### Wake County, North Carolina

### HeB—Helena sandy loam, 2 to 6 percent slopes

### **Map Unit Setting**

National map unit symbol: 2qqqq

Elevation: 70 to 560 feet

Mean annual precipitation: 39 to 47 inches Mean annual air temperature: 55 to 63 degrees F

Frost-free period: 200 to 250 days

Farmland classification: All areas are prime farmland

### **Map Unit Composition**

Helena and similar soils: 92 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

### **Description of Helena**

### Setting

Landform: Interfluves

Landform position (two-dimensional): Summit, shoulder Landform position (three-dimensional): Side slope

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Residuum weathered from granite and gneiss

### **Typical profile**

Ap - 0 to 12 inches: sandy loam BE - 12 to 19 inches: sandy clay loam

Bt1 - 19 to 39 inches: clay Bt2 - 39 to 43 inches: clay loam BCg - 43 to 46 inches: clay loam C - 46 to 80 inches: sandy loam

### **Properties and qualities**

Slope: 2 to 6 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Moderately well drained

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.06 in/hr)

Depth to water table: About 18 to 30 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Moderate (about 8.3 inches)

### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: D

Ecological site: F136XY810SC - Acidic upland forest, seasonally wet

Hydric soil rating: No

### RgB—Rawlings-Rion complex, 2 to 6 percent slopes

### **Map Unit Setting**

National map unit symbol: 2xhb9

Elevation: 70 to 560 feet

Mean annual precipitation: 39 to 47 inches Mean annual air temperature: 55 to 63 degrees F

Frost-free period: 200 to 250 days

Farmland classification: Farmland of statewide importance

### **Map Unit Composition**

Rawlings and similar soils: 55 percent Rion and similar soils: 35 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

### **Description of Rawlings**

### Setting

Landform: Interfluves

Landform position (two-dimensional): Summit, shoulder Landform position (three-dimensional): Interfluve

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Residuum weathered from granite

### **Typical profile**

Ap - 0 to 8 inches: sandy loam

Bt - 8 to 20 inches: sandy clay loam

C - 20 to 40 inches: gravelly sandy loam

R - 40 to 80 inches: bedrock

### **Properties and qualities**

Slope: 2 to 6 percent

Depth to restrictive feature: 20 to 40 inches to lithic bedrock

Drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.06 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Low (about 4.7 inches)

### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: C

Ecological site: F136XY830NC - Acidic upland forest, dry-moist

Hydric soil rating: No

### **Description of Rion**

### Setting

Landform: Interfluves

Landform position (two-dimensional): Summit, shoulder Landform position (three-dimensional): Interfluve

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Saprolite derived from granite and gneiss

### **Typical profile**

Ap - 0 to 8 inches: sandy loam
Bt1 - 8 to 17 inches: sandy clay loam
Bt2 - 17 to 38 inches: sandy loam
C - 38 to 80 inches: sandy loam

### Properties and qualities

Slope: 2 to 6 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high

(0.57 to 1.98 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Moderate (about 7.3 inches)

### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: B

Ecological site: F136XY820GA - Acidic upland forest, moist

Hydric soil rating: No

### RgC—Rawlings-Rion complex, 6 to 10 percent slopes

### Map Unit Setting

National map unit symbol: 2xhbb

Elevation: 70 to 560 feet

Mean annual precipitation: 39 to 47 inches
Mean annual air temperature: 55 to 63 degrees F

Frost-free period: 200 to 250 days

Farmland classification: Farmland of statewide importance

### **Map Unit Composition**

Rawlings and similar soils: 55 percent Rion and similar soils: 35 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

### **Description of Rawlings**

### Setting

Landform: Interfluves

Landform position (two-dimensional): Shoulder, backslope

Landform position (three-dimensional): Interfluve

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Residuum weathered from granite

### **Typical profile**

Ap - 0 to 8 inches: sandy loam

Bt - 8 to 20 inches: sandy clay loam

C - 20 to 40 inches: gravelly sandy loam

R - 40 to 80 inches: bedrock

### **Properties and qualities**

Slope: 6 to 10 percent

Depth to restrictive feature: 20 to 40 inches to lithic bedrock

Drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.06 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Low (about 4.7 inches)

### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3e

Hydrologic Soil Group: C

Ecological site: F136XY830NC - Acidic upland forest, dry-moist

Hydric soil rating: No

### **Description of Rion**

### Setting

Landform: Interfluves

Landform position (two-dimensional): Shoulder, backslope

Landform position (three-dimensional): Interfluve

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Saprolite derived from granite and gneiss

### Typical profile

Ap - 0 to 8 inches: sandy loam

Bt1 - 8 to 17 inches: sandy clay loam

Bt2 - 17 to 38 inches: sandy loam

C - 38 to 80 inches: sandy loam

### **Properties and qualities**

Slope: 6 to 10 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high

(0.57 to 1.98 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Moderate (about 7.3 inches)

### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3e

Hydrologic Soil Group: B

Ecological site: F136XY820GA - Acidic upland forest, moist

Hydric soil rating: No

### RgD—Rawlings-Rion complex, 10 to 15 percent slopes

### **Map Unit Setting**

National map unit symbol: 2xhb8

Elevation: 70 to 560 feet

Mean annual precipitation: 39 to 47 inches
Mean annual air temperature: 55 to 63 degrees F

Frost-free period: 200 to 250 days

Farmland classification: Farmland of statewide importance

### **Map Unit Composition**

Rawlings and similar soils: 55 percent Rion and similar soils: 35 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

### **Description of Rawlings**

### Setting

Landform: Interfluves

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Interfluve

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Residuum weathered from granite

### Typical profile

Ap - 0 to 8 inches: sandy loam

Bt - 8 to 20 inches: sandy clay loam

C - 20 to 40 inches: gravelly sandy loam

R - 40 to 80 inches: bedrock

### Properties and qualities

Slope: 10 to 15 percent

Depth to restrictive feature: 20 to 40 inches to lithic bedrock

Drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.06 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Low (about 4.7 inches)

### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4e

Hydrologic Soil Group: C

Ecological site: F136XY830NC - Acidic upland forest, dry-moist

Hydric soil rating: No

### **Description of Rion**

### Setting

Landform: Interfluves

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Interfluve

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Saprolite derived from granite and gneiss

### **Typical profile**

Ap - 0 to 8 inches: sandy loam
Bt1 - 8 to 17 inches: sandy clay loam
Bt2 - 17 to 38 inches: sandy loam
C - 38 to 80 inches: sandy loam

### **Properties and qualities**

Slope: 10 to 15 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high

(0.57 to 1.98 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Moderate (about 7.3 inches)

### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4e

Hydrologic Soil Group: B

Ecological site: F136XY820GA - Acidic upland forest, moist

Hydric soil rating: No

### **Ur—Urban land**

### **Map Unit Setting**

National map unit symbol: 2qwpc

Elevation: 70 to 1,400 feet

Mean annual precipitation: 39 to 51 inches Mean annual air temperature: 54 to 63 degrees F

Frost-free period: 190 to 250 days

Farmland classification: Not prime farmland

### **Map Unit Composition**

Urban land: 100 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

### **Description of Urban Land**

### Setting

Parent material: Impervious layers over human-transported material

### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8

Hydric soil rating: No

### W-Water

### **Map Unit Setting**

National map unit symbol: 2qqjv

Elevation: 70 to 450 feet

Mean annual precipitation: 39 to 51 inches Mean annual air temperature: 55 to 63 degrees F

Frost-free period: 200 to 250 days

Farmland classification: Not prime farmland

### **Map Unit Composition**

Water: 100 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

### **Description of Water**

### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8

Hydric soil rating: No

### WaD—Wake-Rolesville complex, 10 to 15 percent slopes, very rocky

### **Map Unit Setting**

National map unit symbol: 2xhbf

Elevation: 70 to 560 feet

Mean annual precipitation: 39 to 47 inches Mean annual air temperature: 55 to 63 degrees F

Frost-free period: 200 to 250 days

Farmland classification: Not prime farmland

### **Map Unit Composition**

Wake, very rocky, and similar soils: 50 percent Rolesville, very rocky, and similar soils: 40 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

### Description of Wake, Very Rocky

### Setting

Landform: Interfluves

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Interfluve

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Residuum weathered from granite and gneiss

### Typical profile

Ap - 0 to 7 inches: gravelly loamy coarse sand C - 7 to 11 inches: gravelly loamy sand

R - 11 to 80 inches: bedrock

### **Properties and qualities**

Slope: 10 to 15 percent

Depth to restrictive feature: 10 to 20 inches to lithic bedrock

Drainage class: Excessively drained

Capacity of the most limiting layer to transmit water (Ksat): Very low to low (0.00 to

0.01 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Very low (about 1.9 inches)

### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4s

Hydrologic Soil Group: D

Ecological site: F136XY870GA - Outer piedmont acidic upland woodlands and

glades, dry *Hydric soil rating:* No

### Description of Rolesville, Very Rocky

### Settina

Landform: Interfluves

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Interfluve

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Residuum weathered from granite and gneiss

### Typical profile

Ap - 0 to 12 inches: loamy sand Bw - 12 to 26 inches: loamy sand C - 26 to 32 inches: loamy coarse sand

Cr - 32 to 38 inches: bedrock R - 38 to 80 inches: bedrock

### **Properties and qualities**

Slope: 10 to 15 percent

Depth to restrictive feature: 20 to 40 inches to paralithic bedrock; 20 to 80 inches

to lithic bedrock

Drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): Very low to low (0.00 to

0.01 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Moderate (about 6.4 inches)

### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4e

Hydrologic Soil Group: A

Ecological site: F136XY870GA - Outer piedmont acidic upland woodlands and

glades, dry *Hydric soil rating:* No

### WaE—Wake-Rolesville complex, 15 to 25 percent slopes, very rocky

### Map Unit Setting

National map unit symbol: 2xhbg

Elevation: 70 to 560 feet

Mean annual precipitation: 39 to 47 inches
Mean annual air temperature: 55 to 63 degrees F

Frost-free period: 200 to 250 days

Farmland classification: Not prime farmland

### **Map Unit Composition**

Wake, very rocky, and similar soils: 50 percent Rolesville, very rocky, and similar soils: 40 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

### **Description of Wake, Very Rocky**

### Setting

Landform: Interfluves

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Residuum weathered from granite and gneiss

### Typical profile

Ap - 0 to 7 inches: gravelly loamy coarse sand C - 7 to 11 inches: gravelly loamy sand

R - 11 to 80 inches: bedrock

### **Properties and qualities**

Slope: 15 to 25 percent

Depth to restrictive feature: 10 to 20 inches to lithic bedrock

Drainage class: Excessively drained

Capacity of the most limiting layer to transmit water (Ksat): Very low to low (0.00 to

0.01 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Very low (about 1.9 inches)

### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4s

Hydrologic Soil Group: D

Ecological site: F136XY870GA - Outer piedmont acidic upland woodlands and

glades, dry *Hydric soil rating:* No

### Description of Rolesville, Very Rocky

### Setting

Landform: Interfluves

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Residuum weathered from granite and gneiss

### **Typical profile**

Ap - 0 to 12 inches: loamy sand Bw - 12 to 26 inches: loamy sand C - 26 to 32 inches: loamy coarse sand

Cr - 32 to 38 inches: bedrock R - 38 to 80 inches: bedrock

### **Properties and qualities**

Slope: 15 to 25 percent

Depth to restrictive feature: 20 to 40 inches to paralithic bedrock; 20 to 80 inches

to lithic bedrock

Drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): Very low to low (0.00 to

0.01 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Moderate (about 6.4 inches)

### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6e

Hydrologic Soil Group: A

Ecological site: F136XY870GA - Outer piedmont acidic upland woodlands and

glades, dry *Hydric soil rating:* No

### WfB—Wedowee-Saw complex, 2 to 6 percent slopes

### **Map Unit Setting**

National map unit symbol: 2xn42

Elevation: 70 to 560 feet

Mean annual precipitation: 39 to 47 inches Mean annual air temperature: 55 to 63 degrees F

Frost-free period: 200 to 250 days

Farmland classification: Farmland of statewide importance

### Map Unit Composition

Wedowee and similar soils: 60 percent Saw and similar soils: 35 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

### **Description of Wedowee**

### Setting

Landform: Interfluves

Landform position (two-dimensional): Summit, shoulder Landform position (three-dimensional): Interfluve

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Saprolite residuum weathered from granite and gneiss and/or

saprolite residuum weathered from schist

### Typical profile

Ap - 0 to 4 inches: sandy loam
E - 4 to 7 inches: sandy loam
BC - 23 to 35 inches: clay loam
C - 35 to 80 inches: sandy clay loam

### **Properties and qualities**

Slope: 2 to 6 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high

(0.57 to 1.98 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Moderate (about 6.4 inches)

### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: B

Ecological site: F136XY820GA - Acidic upland forest, moist

Hydric soil rating: No

### **Description of Saw**

### Setting

Landform: Interfluves

Landform position (two-dimensional): Summit, shoulder Landform position (three-dimensional): Interfluve

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Residuum weathered from granite and gneiss

### **Typical profile**

Ap - 0 to 8 inches: sandy loam Bt - 8 to 20 inches: clay

BC - 20 to 26 inches: sandy clay loam
C - 26 to 29 inches: sandy loam
R - 29 to 80 inches: bedrock

### **Properties and qualities**

Slope: 2 to 6 percent

Depth to restrictive feature: 20 to 40 inches to lithic bedrock

Drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): Very low to low (0.00 to

0.01 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Low (about 3.6 inches)

### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: C

Ecological site: F136XY830NC - Acidic upland forest, dry-moist

Hydric soil rating: No

### WgB-Wedowee-Urban land complex, 2 to 6 percent slopes

### **Map Unit Setting**

National map unit symbol: 2xn43

Elevation: 70 to 560 feet

Mean annual precipitation: 39 to 47 inches
Mean annual air temperature: 55 to 63 degrees F

Frost-free period: 200 to 250 days

Farmland classification: Not prime farmland

### **Map Unit Composition**

Wedowee and similar soils: 55 percent

Urban land: 40 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

### **Description of Wedowee**

### Setting

Landform: Interfluves

Landform position (two-dimensional): Summit, shoulder Landform position (three-dimensional): Interfluve

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Saprolite residuum weathered from granite and gneiss and/or

saprolite residuum weathered from schist

### **Typical profile**

Ap - 0 to 4 inches: sandy loam
E - 4 to 7 inches: sandy loam
BC - 23 to 35 inches: clay loam
C - 35 to 80 inches: sandy clay loam

### **Properties and qualities**

Slope: 2 to 6 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high

(0.57 to 1.98 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Moderate (about 6.4 inches)

### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: B

Ecological site: F136XY820GA - Acidic upland forest, moist

Hydric soil rating: No

### **Description of Urban Land**

### Setting

Parent material: Impervious layers over human transported material

### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8

Hydric soil rating: No

### WgC—Wedowee-Urban land complex, 6 to 15 percent slopes

### **Map Unit Setting**

National map unit symbol: 2xn44

Elevation: 70 to 560 feet

Mean annual precipitation: 39 to 47 inches

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Mean annual air temperature: 55 to 63 degrees F

Frost-free period: 200 to 250 days

Farmland classification: Not prime farmland

#### Map Unit Composition

Wedowee and similar soils: 55 percent

Urban land: 40 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Wedowee**

#### Setting

Landform: Interfluves

Landform position (two-dimensional): Shoulder, backslope

Landform position (three-dimensional): Interfluve

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Saprolite residuum weathered from granite and gneiss and/or

saprolite residuum weathered from schist

#### Typical profile

Ap - 0 to 4 inches: sandy loam
E - 4 to 7 inches: sandy loam
BC - 23 to 35 inches: clay loam
C - 35 to 80 inches: sandy clay loam

#### **Properties and qualities**

Slope: 6 to 15 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high

(0.57 to 1.98 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Moderate (about 6.4 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4e

Hydrologic Soil Group: B

Ecological site: F136XY820GA - Acidic upland forest, moist

Hydric soil rating: No

#### **Description of Urban Land**

#### Setting

Parent material: Impervious layers over human transported material

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8

Hydric soil rating: No

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# **ATTACHMENT 4: FEMA FLOOD MAP**

# DATUM INFORMATION

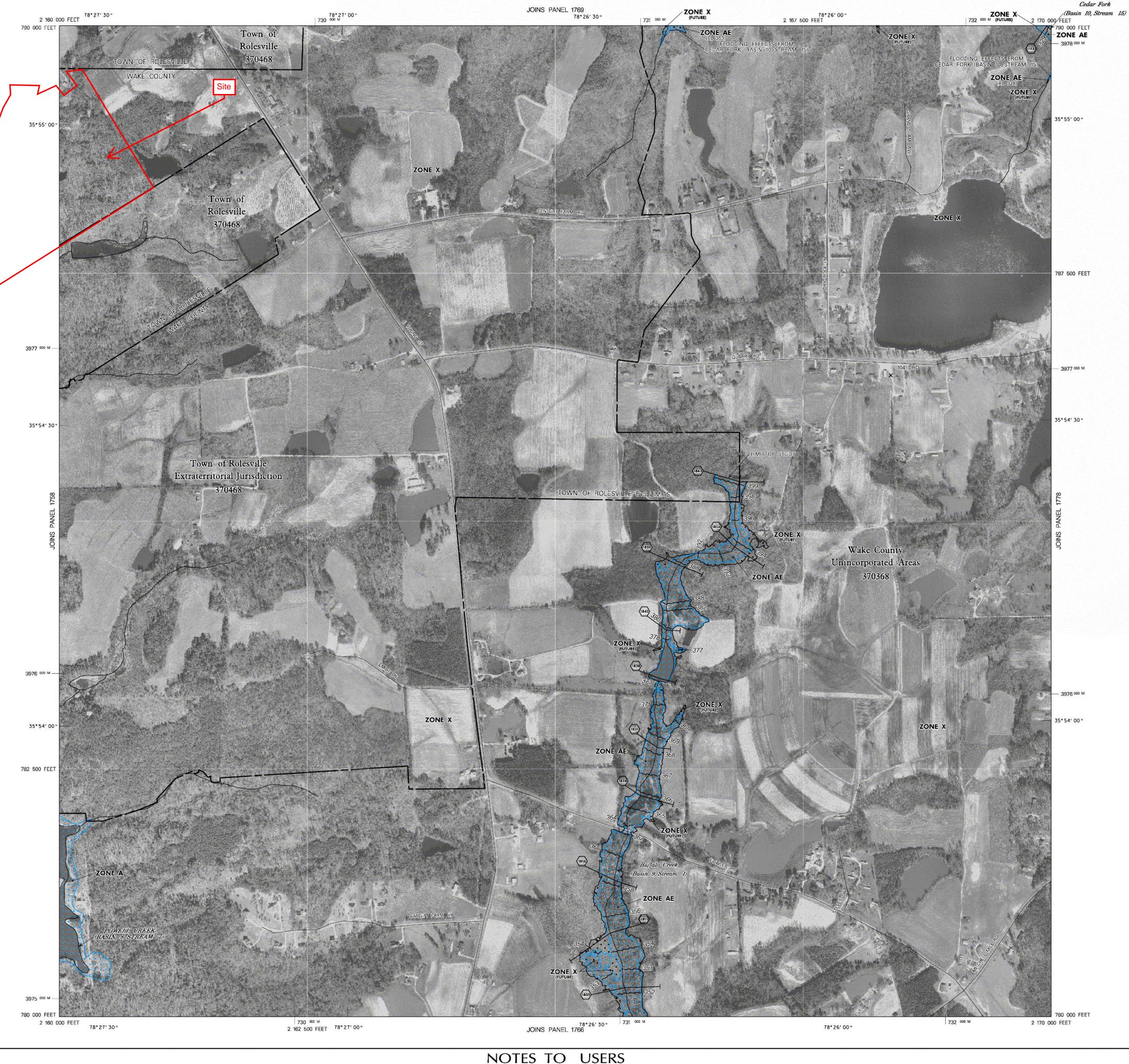
The projection used in the preparation of this map was the North Carolina State Plane (FIPSZONE 3200). The horizontal datum was the North American Datum of 1983, GRS80 ellipsoid. Differences in datum, ellipsoid, projection, or Universal Transverse Mercator zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdictional boundaries. These differences do not affect the accuracy of this FIRM. All coordinates on this map are in U.S. Survey Feet, where 1 U.S. Survey Foot = 1200/3937 Meters.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988 (NAVD 88). These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. An average offset between NAVD 88 and the National Geodetic Vertical Datum of 1929 (NGVD 29) has been computed for each North Carolina county. This offset was then applied to the NGVD 29 flood elevations that were not revised during the creation of this statewide format FIRM. The offsets for each county shown on this FIRM panel are shown in the vertical datum offset table below. Where a county boundary and a flooding source with unrevised NGVD 29 flood elevations are coincident, an individual offset has been calculated and applied during the creation of this statewide format FIRM. See Section 6.1 of the accompanying Flood Insurance Study report to obtain further information on the conversion of elevations between NAVD 88 and NGVD 29. To obtain current elevation, description, and/or location information for bench marks shown on this map, please contact the North Carolina Geodetic Survey at the address shown below. You may also contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242, or visit its website at www.ngs.noaa.gov.

North Carolina Geodetic Survey 121 West Jones Street Raleigh, NC 27601 (919) 733-3836 www.ncgs.state.nc.us

County Average Vertical Datum Offset Table Vertical Datum Offset (ft) Example: NAVD 88 = NGVD 29 + (-0.88)

All streams listed in the Flood Hazard Data Table below were studied by detailed methods using field survey. Other flood hazard data shown on this map may have been derived using either a coastal analysis or limited detailed riverine analysis. More information on the flooding sources studied by these analyses is contained in the Flood Insurance Study report.







This digital Flood Insurance Rate Map (FIRM) was produced through a unique cooperative partnership between the State of North Carolina and the Federal Emergency Management Agency (FEMA). The State of North Carolina has implemented a long term approach of floodplain management to decrease the costs associated with flooding. This is demonstrated by the State's commitment to map floodplain areas at the local level. As a part of this effort, the State of North Carolina has joined in a Cooperating Technical State agreement with FEMA to produce and maintain this digital FIRM.

www.ncfloodmaps.com

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible

updated or additional flood hazard information. To obtain more detailed information in areas where Base Flood Elevations (BFEs) and/or floodways have been determined, users are encouraged to consult the Flood Profiles, Floodway Data, Limited Detailed Flood Hazard Data, and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Boundaries of regulatory floodways shown on the FIRM for flooding sources studied by detailed methods were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data for flooding sources studied by detailed methods as well as non-encroachment widths for flooding sources studied by limited detailed methods are provided in the FIS report for this jurisdiction. The FIS report also provides instructions for determining a floodway using non-encroachment widths for flooding sources studied by limited detailed methods.

Certain areas not in Special Flood Hazard Areas may be protected by flood control structures. Refer to Section 4.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures in this jurisdiction.

Base map information and geospatial data used to develop this FIRM were obtained from various organizations, including the participating local community(ies), state and federal agencies, and/or other sources. The primary base for this FIRM is aerial imagery acquired by Wake County. The time period of collection for the imagery is 1999. Information and geospatial data supplied by the local community(ies) that met FEMA base map specifications were considered the preferred source for development of the base map. See geospatial metadata for the associated digital FIRM for additional information about base map

Base map features shown on this map, such as **corporate limits**, are based on the most up-to-date data available at the time of publication. Changes in the corporate limits may have occurred since this map was published. Map users should consult the appropriate community official or website to verify current conditions of jurisdictional boundaries and base map features. This map may contain roads that were not considered in the hydraulic analysis of streams where no new hydraulic model was created during the production of this statewide format FIRM.

This map reflects more detailed and up-to-date stream channel configurations than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map.

Please refer to the separately printed Map Index for an overview map of the county showing the layout of map panels, community map repository addresses, and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is located.

If you have questions about this map, or questions concerning the National Flood Insurance Program in general, please call 1-877-FEMA MAP (1-877-336-2627) or visit the FEMA website at www.fema.gov.

An accompanying Flood Insurance Study report, Letter of Map Revision (LOMR) or Letter of Map Amendment (LOMA) revising portions of this panel, and digital versions of this FIRM may be available. Visit the North Carolina Floodplain Mapping Program website at www.ncfloodmaps.com, or contact the FEMA Map Service Center at 1-800-358-9616 for information on all related products associated with this FIRM. The FEMA Map Service Center may also be reached by Fax at 1-800-358-9620 and its website at www.msc.fema.gov.

MAP REPOSITORY Refer to listing of Map Repositories on Map Index or visit www.ncfloodmaps.com.

> EFFECTIVE DATE OF FLOOD INSURANCE RATE MAP PANEL MAY 2, 2006

EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL

For community map revision history prior to statewide mapping, refer to the Community Map History table located in the Flood Insurance Study report for this jurisdiction. To determine if flood insurance is available in this community, contact your insurance agent, the North Carolina Division of Emergency Management or the National Flood Insurance Program at the

following phone numbers or websites: National Flood Insurance Program NC Division of Emergency Management (919) 715–8000 <u>www.nccrimecontrol.org/nfip</u> 1–800–638–6620 <u>www.fema.gov/nfip</u>

# LEGEND

SPECIAL FLOOD HAZARD AREAS (SFHAs) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD

The 1% annual chance flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equaled or exceeded in any given year. The Special Flood Hazard Area is the area subject to flooding by the 1% annual chance flood. Areas of Special Flood Hazard include Zones A, AE, AH, AO, AR, A99, V, and VE. The Base Flood Elevation is the water-surface elevation of the 1% annual chance flood.

No Base Flood Elevations determined. Base Flood Elevations determined. ZONE AE

Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations determined. Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities

Special Flood Hazard Area formerly protected from the 1% annual chance flood by a flood control system that was subsequently decertified. Zone AR indicates that the former flood control system is being restored to provide protection from the 1% annual chance or

greater flood. Area to be protected from 1% annual chance flood by a Federal flood protection system under construction; no Base Flood Elevations

Coastal flood zone with velocity hazard (wave action); Base Flood Elevations FLOODWAY AREAS IN ZONE AE

The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood heights.

# OTHER FLOOD AREAS

Areas of 0.2% annual chance flood; areas of future conditions 1% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.

OTHER AREAS Areas determined to be outside the 0.2% annual chance and future conditions 1% annual chance floodplain.

COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS

Areas in which flood hazards are undetermined, but possible.

OTHERWISE PROTECTED AREAS (OPAs) CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas.

1% annual chance floodplain boundary 0.2% annual chance floodplain boundary and future conditions 1% annual chance floodplain boundary

Floodway boundary \_\_\_\_\_\_\_ Zone D Boundary

CBRS and OPA boundary Boundary dividing Special Flood Hazard Area Zones and boundary dividing Special Flood Hazard Areas of different

Base Flood Elevations, flood depths or flood velocities. ----513----Base Flood Elevation line and value; elevation in feet\* Base Flood Elevation value where uniform within zone; (EL 987) elevation in feet\*

\*Referenced to the North American Vertical Datum of 1988 Cross section line

(23)-----(23) Transect line

97°07′30", 32°22′30" 4276000 M

• M1.5

ZONE X

1 477 500 FEET BM5510 🗸

Geographic coordinates referenced to the North American Datum of 1983 (NAD 83) 1000-meter Universal Transverse Mercator grid ticks, zone 17 2500-foot grid values: North Carolina State Plane coordinate system (FIPSZONE 3200, State Plane NAD 83 feet)

North Carolina Geodetic Survey bench mark (see explanation in the Datum Information section of this FIRM panel). National Geodetic Survey bench mark (see explanation in the Datum Information section of this FIRM panel). River Mile



MAP SCALE 1" = 500' (1 : 6,000)

PANEL 1768J

# FIRM FLOOD INSURANCE RATE MAP

(1)(0)(0)

**PANEL 1768** (SEE LOCATOR DIAGRAM OR MAP INDEX FOR FIRM

NORTH CAROLINA

PANEL LAYOUT)

ROLESVILLE, TOWN OF 370468 1768 J WAKE COUNTY 370368 1768

Notice to User: The Map Number shown below should be used when placing map orders; the Community Number shown above should be used on insurance applications for the subject

EFFECTIVE DATE MAY 2, 2006



MAP NUMBER

State of North Carolina Federal Emergency Management Agency



# DATUM INFORMATION

The projection used in the preparation of this map was the North Carolina State Plane (FIPSZONE 3200). The horizontal datum was the North American Datum of 1983, GRS80 ellipsoid. Differences in datum, ellipsoid, projection, or Universal Transverse Mercator zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdictional boundaries. These differences do not affect the accuracy of this FIRM. All coordinates on this map are in U.S. Survey Feet, where 1 U.S. Survey Foot = 1200/3937 Meters.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988 (NAVD 88). These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. An average offset between NAVD 88 and the National Geodetic Vertical Datum of 1929 (NGVD 29) has been computed for each North Carolina county. This offset was then applied to the NGVD 29 flood elevations that were not revised during the creation of this statewide format FIRM. The offsets for each county shown on this FIRM panel are shown in the vertical datum offset table below. Where a county boundary and a flooding source with unrevised NGVD 29 flood elevations are coincident, an individual offset has been calculated and applied during the creation of this statewide format FIRM. See Section 6.1 of the accompanying Flood Insurance Study report to obtain further information on the conversion of elevations between NAVD 88 and NGVD 29. To obtain current elevation, description, and/or location information for bench marks shown on this map, please contact the North Carolina Geodetic Survey at the address shown below. You may also contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242, or visit its website at www.ngs.noaa.gov.

North Carolina Geodetic Survey 121 West Jones Street Raleigh, NC 27601 (919) 733-3836 www.ncgs.state.nc.us

	et (ft)
Wake - 0.88	

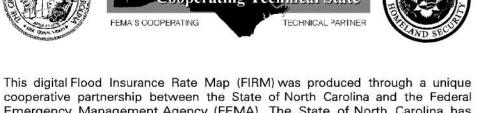
All streams listed in the Flood Hazard Data Table below were studied by detailed methods using field survey. Other flood hazard data shown on this map may have been derived using either a coastal analysis or limited detailed riverine analysis. More information on the flooding sources studied by these analyses is contained in the Flood Insurance Study report.

Fl	Floodway Width (feet)				
Cross Section	Stream Station	Flood Discharge (cfs)	1 % Annual Chance (100-year) Water-Surface Elevation (feet NAVD 88)	the Center of Stream to Encroachment Boundard (Looking Downstream) o Total Floodway Width	
TOMS CRI	EEK (BASIN 7	, STREAM 1)			
164	16,350 <sup>1</sup>	NA	275.5	50	
POWELL	CREEK (BASII	N 8, STREAM 7	<b>'</b> }		
239	23,890 <sup>2</sup>	NA	248.7	120	
272	27,200 <sup>2</sup>	NA	259.9	110	

<sup>2</sup> Feet above confluence with Hodges Creek (Basin 8, Stream 1)







cooperative partnership between the State of North Carolina and the Federal Emergency Management Agency (FEMA). The State of North Carolina has implemented a long term approach of floodplain management to decrease the costs associated with flooding. This is demonstrated by the State's commitment to map floodplain areas at the local level. As a part of this effort, the State of North Carolina has joined in a Cooperating Technical State agreement with FEMA to produce and maintain this digital FIRM.

www.ncfloodmaps.com

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MAP REPOSITORY Refer to listing of Map Repositories on Map Index or visit www.ncfloodmaps.com.

> EFFECTIVE DATE OF FLOOD INSURANCE RATE MAP PANEL MAY 2, 2006

EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL

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(919) 715–8000 <u>www.nccrimecontrol.org/nfip</u> 1–800–638–6620 <u>www.fema.gov/nfip</u>

LEGEND

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No Base Flood Elevations determined. Base Flood Elevations determined.

greater flood.

Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations determined. Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities

Special Flood Hazard Area formerly protected from the 1% annual chance flood by a flood control system that was subsequently decertified. Zone AR indicates that the former flood control system is being restored to provide protection from the 1% annual chance or

Area to be protected from 1% annual chance flood by a Federal flood protection system under construction; no Base Flood Elevations Coastal flood zone with velocity hazard (wave action); Base Flood Elevations

FLOODWAY AREAS IN ZONE AE

The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood heights.

OTHER FLOOD AREAS

Areas of 0.2% annual chance flood; areas of future conditions 1% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.

OTHER AREAS

ZONE X Areas determined to be outside the 0.2% annual chance and future conditions 1% annual chance floodplain. Areas in which flood hazards are undetermined, but possible.

COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS

OTHERWISE PROTECTED AREAS (OPAs) CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas.

1% annual chance floodplain boundary 0.2% annual chance floodplain boundary and future conditions 1% annual chance floodplain boundary

\_ \_ \_ \_ \_ Floodway boundary Zone D Boundary CBRS and OPA boundary

Boundary dividing Special Flood Hazard Area Zones and boundary dividing Special Flood Hazard Areas of different Base Flood Elevations, flood depths or flood velocities. Base Flood Elevation line and value; elevation in feet\* ----513----Base Flood Elevation value where uniform within zone;

elevation in feet\* \*Referenced to the North American Vertical Datum of 1988

> Cross section line Transect line

(23)-----(23) 97°07′30", 32°22′30"

(EL 987)

4276000 M 1 477 500 FEET BM5510 🗸

M1.5

Geographic coordinates referenced to the North American Datum of 1983 (NAD 83) 1000-meter Universal Transverse Mercator grid ticks, zone 17 2500-foot grid values: North Carolina State Plane coordinate system (FIPSZONE 3200, State Plane NAD 83 feet)

North Carolina Geodetic Survey bench mark (see explanation in the Datum Information section of this FIRM panel). National Geodetic Survey bench mark (see explanation in the Datum Information section of this FIRM panel). River Mile



MAP SCALE 1" = 500' (1 : 6,000)

PANEL 1758J

FIRM FLOOD INSURANCE RATE MAP

**PANEL 1758** 

(100)

(SEE LOCATOR DIAGRAM OR MAP INDEX FOR FIRM PANEL LAYOUT)

NORTH CAROLINA

COMMUNITY ROLESVILLE, TOWN OF

CID No. PANEL SUFFIX 370468 1758 J WAKE COUNTY

when placing map orders; the Community Number shown above should be used on insurance applications for the subject EFFECTIVE DATE MAP NUMBER

Notice to User: The Map Number shown below should be used





3720175800J

State of North Carolina Federal Emergency Management Agency

# **ATTACHMENT 5: RAINFALL DATA**



#### NOAA Atlas 14, Volume 2, Version 3 Location name: Rolesville, North Carolina, USA\* Latitude: 35.9195°, Longitude: -78.4618° Elevation: m/ft\*\*

\* source: ESRI Maps \*\* source: USGS



#### POINT PRECIPITATION FREQUENCY ESTIMATES

 $G.M.\ Bonnin,\ D.\ Martin,\ B.\ Lin,\ T.\ Parzybok,\ M.Yekta,\ and\ D.\ Riley$ 

NOAA, National Weather Service, Silver Spring, Maryland

PF tabular | PF graphical | Maps & aerials

#### PF tabular

PDS	PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches) <sup>1</sup>									
Duration				Avera	ge recurren	ce interval (	years)			
Duration	1	2	5	10	25	50	100	200	500	1000
5-min	<b>0.403</b> (0.369-0.441)	<b>0.468</b> (0.429-0.512)	<b>0.534</b> (0.489-0.582)	<b>0.599</b> (0.548-0.654)	<b>0.665</b> (0.606-0.725)	<b>0.718</b> (0.651-0.782)	<b>0.764</b> (0.689-0.832)	<b>0.805</b> (0.722-0.879)	<b>0.851</b> (0.756-0.929)	<b>0.892</b> (0.786-0.976)
10-min	<b>0.644</b> (0.590-0.704)	<b>0.749</b> (0.687-0.818)	<b>0.855</b> (0.783-0.933)	<b>0.959</b> (0.877-1.05)	<b>1.06</b> (0.965-1.16)	<b>1.14</b> (1.04-1.25)	<b>1.21</b> (1.09-1.32)	<b>1.28</b> (1.14-1.39)	<b>1.35</b> (1.20-1.47)	<b>1.41</b> (1.24-1.54)
15-min	<b>0.805</b> (0.738-0.880)	<b>0.942</b> (0.863-1.03)	<b>1.08</b> (0.991-1.18)	<b>1.21</b> (1.11-1.32)	<b>1.34</b> (1.22-1.46)	<b>1.45</b> (1.31-1.58)	<b>1.53</b> (1.38-1.67)	<b>1.61</b> (1.44-1.76)	<b>1.69</b> (1.51-1.85)	<b>1.76</b> (1.55-1.93)
30-min	<b>1.10</b> (1.01-1.21)	<b>1.30</b> (1.19-1.42)	<b>1.54</b> (1.41-1.68)	<b>1.76</b> (1.61-1.92)	<b>1.99</b> (1.81-2.17)	<b>2.18</b> (1.98-2.38)	<b>2.35</b> (2.12-2.56)	<b>2.51</b> (2.25-2.74)	<b>2.70</b> (2.40-2.94)	<b>2.86</b> (2.52-3.12)
60-min	<b>1.38</b> (1.26-1.51)	<b>1.63</b> (1.50-1.78)	<b>1.97</b> (1.81-2.15)	<b>2.29</b> (2.09-2.50)	<b>2.65</b> (2.41-2.89)	<b>2.95</b> (2.68-3.22)	<b>3.24</b> (2.92-3.53)	<b>3.52</b> (3.15-3.84)	<b>3.87</b> (3.44-4.22)	<b>4.17</b> (3.67-4.56)
2-hr	<b>1.61</b> (1.46-1.78)	<b>1.91</b> (1.75-2.10)	<b>2.34</b> (2.13-2.56)	<b>2.74</b> (2.49-3.01)	<b>3.23</b> (2.91-3.53)	<b>3.65</b> (3.28-3.99)	<b>4.06</b> (3.62-4.43)	<b>4.47</b> (3.96-4.89)	<b>5.01</b> (4.40-5.48)	<b>5.49</b> (4.78-6.02)
3-hr	<b>1.71</b> (1.55-1.89)	<b>2.03</b> (1.85-2.24)	<b>2.49</b> (2.26-2.74)	<b>2.94</b> (2.67-3.24)	<b>3.49</b> (3.15-3.84)	<b>3.99</b> (3.57-4.38)	<b>4.47</b> (3.97-4.91)	<b>4.99</b> (4.40-5.46)	<b>5.67</b> (4.94-6.21)	<b>6.29</b> (5.42-6.91)
6-hr	<b>2.05</b> (1.87-2.26)	<b>2.44</b> (2.23-2.68)	<b>2.99</b> (2.72-3.28)	<b>3.54</b> (3.22-3.88)	<b>4.22</b> (3.81-4.62)	<b>4.83</b> (4.34-5.28)	<b>5.45</b> (4.85-5.95)	<b>6.10</b> (5.37-6.65)	<b>6.98</b> (6.07-7.61)	<b>7.79</b> (6.68-8.50)
12-hr	<b>2.41</b> (2.21-2.66)	<b>2.87</b> (2.64-3.15)	<b>3.54</b> (3.24-3.88)	<b>4.21</b> (3.84-4.61)	<b>5.06</b> (4.59-5.53)	<b>5.84</b> (5.25-6.35)	<b>6.62</b> (5.90-7.20)	<b>7.47</b> (6.57-8.11)	<b>8.64</b> (7.48-9.37)	<b>9.72</b> (8.29-10.6)
24-hr	<b>2.86</b> (2.66-3.08)	<b>3.45</b> (3.22-3.72)	<b>4.34</b> (4.04-4.68)	<b>5.04</b> (4.68-5.43)	<b>6.00</b> (5.56-6.46)	<b>6.77</b> (6.25-7.28)	<b>7.56</b> (6.95-8.14)	<b>8.37</b> (7.67-9.02)	<b>9.50</b> (8.66-10.2)	<b>10.4</b> (9.42-11.2)
2-day	<b>3.32</b> (3.09-3.57)	<b>3.99</b> (3.72-4.30)	<b>4.98</b> (4.63-5.36)	<b>5.76</b> (5.35-6.20)	<b>6.81</b> (6.31-7.34)	<b>7.65</b> (7.06-8.24)	<b>8.51</b> (7.84-9.17)	<b>9.40</b> (8.62-10.1)	<b>10.6</b> (9.68-11.5)	<b>11.6</b> (10.5-12.6)
3-day	<b>3.52</b> (3.28-3.77)	<b>4.23</b> (3.95-4.53)	<b>5.24</b> (4.89-5.62)	<b>6.05</b> (5.63-6.48)	<b>7.15</b> (6.63-7.67)	<b>8.02</b> (7.42-8.60)	<b>8.91</b> (8.22-9.57)	<b>9.84</b> (9.03-10.6)	<b>11.1</b> (10.1-12.0)	<b>12.1</b> (11.0-13.1)
4-day	<b>3.72</b> (3.48-3.98)	<b>4.46</b> (4.17-4.77)	<b>5.51</b> (5.15-5.89)	<b>6.34</b> (5.91-6.77)	<b>7.48</b> (6.95-7.99)	<b>8.39</b> (7.77-8.97)	<b>9.32</b> (8.60-9.97)	<b>10.3</b> (9.45-11.0)	<b>11.6</b> (10.6-12.4)	<b>12.6</b> (11.5-13.6)
7-day	<b>4.31</b> (4.04-4.60)	<b>5.15</b> (4.82-5.50)	<b>6.28</b> (5.88-6.70)	<b>7.18</b> (6.71-7.66)	<b>8.41</b> (7.83-8.98)	<b>9.39</b> (8.72-10.0)	<b>10.4</b> (9.63-11.1)	<b>11.4</b> (10.5-12.3)	<b>12.9</b> (11.8-13.8)	<b>14.0</b> (12.8-15.0)
10-day	<b>4.91</b> (4.61-5.23)	<b>5.84</b> (5.48-6.23)	<b>7.04</b> (6.59-7.49)	<b>7.97</b> (7.46-8.49)	<b>9.24</b> (8.62-9.84)	<b>10.2</b> (9.53-10.9)	<b>11.2</b> (10.4-12.0)	<b>12.3</b> (11.4-13.1)	<b>13.7</b> (12.6-14.6)	<b>14.7</b> (13.5-15.8)
20-day	<b>6.59</b> (6.20-7.01)	<b>7.78</b> (7.32-8.28)	<b>9.21</b> (8.66-9.80)	<b>10.3</b> (9.71-11.0)	<b>11.9</b> (11.1-12.6)	<b>13.1</b> (12.2-13.9)	<b>14.3</b> (13.3-15.2)	<b>15.5</b> (14.4-16.6)	<b>17.2</b> (15.9-18.4)	<b>18.5</b> (17.0-19.8)
30-day	<b>8.18</b> (7.72-8.68)	<b>9.62</b> (9.07-10.2)	<b>11.2</b> (10.6-11.9)	<b>12.4</b> (11.7-13.2)	<b>14.1</b> (13.2-14.9)	<b>15.3</b> (14.3-16.3)	<b>16.6</b> (15.5-17.6)	<b>17.8</b> (16.6-19.0)	<b>19.5</b> (18.1-20.8)	<b>20.7</b> (19.2-22.2)
45-day	<b>10.4</b> (9.89-11.0)	<b>12.2</b> (11.6-12.9)	<b>14.0</b> (13.3-14.8)	<b>15.4</b> (14.6-16.2)	<b>17.2</b> (16.2-18.1)	<b>18.5</b> (17.5-19.5)	<b>19.9</b> (18.7-21.0)	<b>21.2</b> (19.9-22.4)	<b>22.9</b> (21.4-24.3)	<b>24.2</b> (22.6-25.7)
60-day	<b>12.5</b> (11.9-13.1)	<b>14.6</b> (13.9-15.3)	<b>16.5</b> (15.7-17.4)	<b>18.0</b> (17.1-19.0)	<b>20.0</b> (18.9-21.0)	<b>21.4</b> (20.2-22.5)	<b>22.8</b> (21.5-24.0)	<b>24.2</b> (22.8-25.5)	<b>25.9</b> (24.4-27.4)	<b>27.3</b> (25.6-28.8)

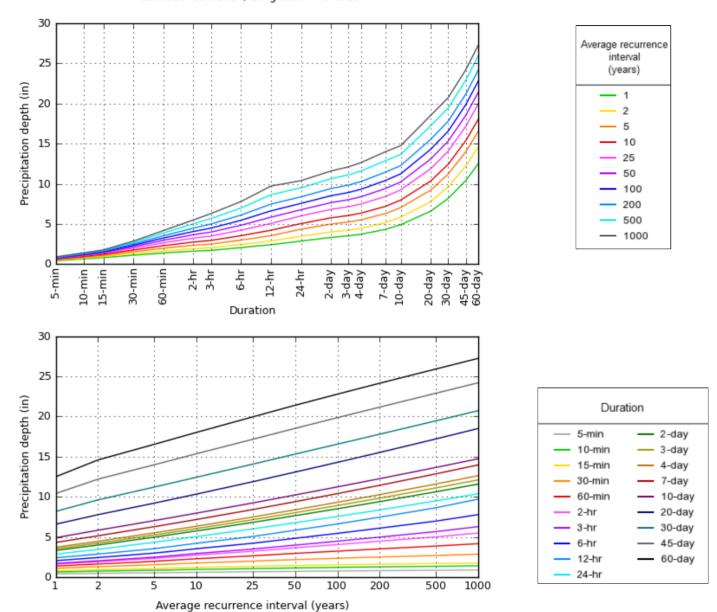
Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

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#### PDS-based depth-duration-frequency (DDF) curves Latitude: 35.9195°, Longitude: -78.4618°



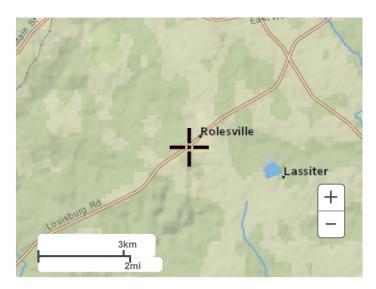
NOAA Atlas 14, Volume 2, Version 3

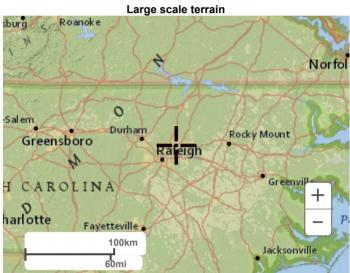
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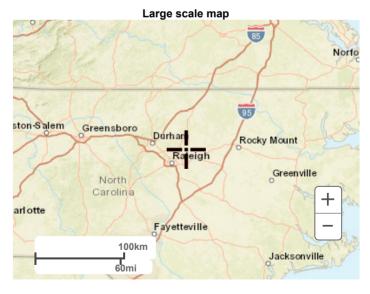
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# Maps & aerials

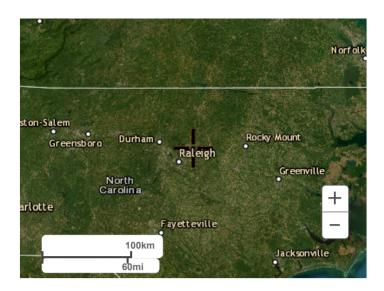
Small scale terrain







Large scale aerial



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1325 East West Highway

1325 East West Highway Silver Spring, MD 20910 Questions?: <u>HDSC.Questions@noaa.gov</u>

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#### NOAA Atlas 14, Volume 2, Version 3 Location name: Rolesville, North Carolina, USA\* Latitude: 35.9195°, Longitude: -78.4618° Elevation: 426 ft\*\*

\* source: ESRI Maps \*\* source: USGS



#### POINT PRECIPITATION FREQUENCY ESTIMATES

G.M. Bonnin, D. Martin, B. Lin, T. Parzybok, M.Yekta, and D. Riley NOAA, National Weather Service, Silver Spring, Maryland

PF tabular | PF graphical | Maps & aerials

#### PF tabular

PDS-b	S-based point precipitation frequency estimates with 90% confidence intervals (in inches/hour) <sup>1</sup>									
Duration				Avera	ge recurren	ce interval (	years)			
Duration	1	2	5	10	25	50	100	200	500	1000
5-min	<b>4.84</b> (4.43-5.29)	<b>5.62</b> (5.15-6.14)	<b>6.41</b> (5.87-6.98)	<b>7.19</b> (6.58-7.85)	<b>7.98</b> (7.27-8.70)	<b>8.62</b> (7.81-9.38)	<b>9.17</b> (8.27-9.98)	<b>9.66</b> (8.66-10.5)	<b>10.2</b> (9.07-11.1)	<b>10.7</b> (9.43-11.7)
10-min	<b>3.86</b> (3.54-4.22)	<b>4.49</b> (4.12-4.91)	<b>5.13</b> (4.70-5.60)	<b>5.75</b> (5.26-6.27)	<b>6.36</b> (5.79-6.93)	<b>6.86</b> (6.22-7.47)	<b>7.28</b> (6.56-7.94)	<b>7.66</b> (6.86-8.36)	<b>8.08</b> (7.18-8.82)	<b>8.43</b> (7.43-9.22)
15-min	<b>3.22</b> (2.95-3.52)	<b>3.77</b> (3.45-4.12)	<b>4.32</b> (3.96-4.72)	<b>4.85</b> (4.44-5.29)	<b>5.38</b> (4.89-5.86)	<b>5.79</b> (5.25-6.31)	<b>6.14</b> (5.53-6.69)	<b>6.44</b> (5.77-7.03)	<b>6.78</b> (6.02-7.40)	<b>7.05</b> (6.22-7.72)
30-min	<b>2.21</b> (2.02-2.41)	<b>2.60</b> (2.38-2.84)	<b>3.07</b> (2.82-3.35)	<b>3.51</b> (3.21-3.83)	<b>3.98</b> (3.62-4.34)	<b>4.36</b> (3.95-4.75)	<b>4.70</b> (4.24-5.12)	<b>5.02</b> (4.49-5.47)	<b>5.39</b> (4.79-5.89)	<b>5.71</b> (5.03-6.25)
60-min	<b>1.38</b> (1.26-1.50)	<b>1.63</b> (1.50-1.78)	<b>1.97</b> (1.80-2.15)	<b>2.29</b> (2.09-2.50)	<b>2.65</b> (2.41-2.89)	<b>2.95</b> (2.68-3.22)	<b>3.24</b> (2.92-3.53)	<b>3.52</b> (3.15-3.84)	<b>3.87</b> (3.44-4.22)	<b>4.17</b> (3.67-4.56)
2-hr	<b>0.804</b> (0.731-0.887)	<b>0.957</b> (0.874-1.05)	<b>1.17</b> (1.06-1.28)	<b>1.37</b> (1.24-1.50)	<b>1.61</b> (1.45-1.76)	<b>1.82</b> (1.64-2.00)	<b>2.03</b> (1.81-2.22)	<b>2.24</b> (1.98-2.44)	<b>2.51</b> (2.20-2.74)	<b>2.75</b> (2.39-3.01)
3-hr	<b>0.567</b> (0.516-0.629)	<b>0.676</b> (0.617-0.746)	<b>0.827</b> (0.753-0.913)	<b>0.979</b> (0.888-1.08)	<b>1.16</b> (1.05-1.28)	<b>1.33</b> (1.19-1.46)	<b>1.49</b> (1.32-1.63)	<b>1.66</b> (1.46-1.82)	<b>1.89</b> (1.65-2.07)	<b>2.09</b> (1.80-2.30)
6-hr	<b>0.341</b> (0.311-0.377)	<b>0.406</b> (0.372-0.448)	<b>0.498</b> (0.454-0.548)	<b>0.590</b> (0.537-0.648)	<b>0.704</b> (0.636-0.771)	<b>0.807</b> (0.724-0.882)	<b>0.909</b> (0.809-0.993)	<b>1.02</b> (0.897-1.11)	<b>1.16</b> (1.01-1.27)	<b>1.30</b> (1.12-1.42)
12-hr	<b>0.200</b> (0.183-0.220)	<b>0.238</b> (0.219-0.261)	<b>0.293</b> (0.269-0.321)	<b>0.349</b> (0.318-0.382)	<b>0.420</b> (0.380-0.458)	<b>0.484</b> (0.435-0.527)	<b>0.549</b> (0.489-0.597)	<b>0.620</b> (0.545-0.673)	<b>0.716</b> (0.620-0.778)	<b>0.806</b> (0.687-0.876)
24-hr	<b>0.119</b> (0.110-0.128)	<b>0.143</b> (0.134-0.155)	<b>0.180</b> (0.168-0.194)	<b>0.210</b> (0.195-0.226)	<b>0.250</b> (0.231-0.269)	<b>0.282</b> (0.260-0.303)	<b>0.314</b> (0.289-0.338)	<b>0.348</b> (0.319-0.375)	<b>0.395</b> (0.360-0.426)	<b>0.432</b> (0.392-0.467)
2-day	<b>0.069</b> (0.064-0.074)	<b>0.083</b> (0.077-0.089)	<b>0.103</b> (0.096-0.111)	<b>0.119</b> (0.111-0.129)	<b>0.141</b> (0.131-0.152)	<b>0.159</b> (0.147-0.171)	<b>0.177</b> (0.163-0.190)	<b>0.195</b> (0.179-0.211)	<b>0.221</b> (0.201-0.239)	<b>0.241</b> (0.219-0.261)
3-day	<b>0.048</b> (0.045-0.052)	<b>0.058</b> (0.054-0.062)	<b>0.072</b> (0.067-0.078)	<b>0.084</b> (0.078-0.090)	<b>0.099</b> (0.092-0.106)	<b>0.111</b> (0.103-0.119)	<b>0.123</b> (0.114-0.132)	<b>0.136</b> (0.125-0.146)	<b>0.154</b> (0.140-0.166)	<b>0.168</b> (0.152-0.181)
4-day	<b>0.038</b> (0.036-0.041)	<b>0.046</b> (0.043-0.049)	<b>0.057</b> (0.053-0.061)	<b>0.066</b> (0.061-0.070)	<b>0.077</b> (0.072-0.083)	<b>0.087</b> (0.080-0.093)	<b>0.097</b> (0.089-0.103)	<b>0.107</b> (0.098-0.114)	<b>0.120</b> (0.110-0.129)	<b>0.131</b> (0.119-0.141)
7-day	<b>0.025</b> (0.024-0.027)	<b>0.030</b> (0.028-0.032)	<b>0.037</b> (0.034-0.039)	<b>0.042</b> (0.039-0.045)	<b>0.050</b> (0.046-0.053)	<b>0.055</b> (0.051-0.059)	<b>0.061</b> (0.057-0.066)	<b>0.068</b> (0.062-0.072)	<b>0.076</b> (0.070-0.082)	<b>0.083</b> (0.075-0.089)
10-day	<b>0.020</b> (0.019-0.021)	<b>0.024</b> (0.022-0.025)	<b>0.029</b> (0.027-0.031)	<b>0.033</b> (0.031-0.035)	<b>0.038</b> (0.035-0.041)	<b>0.042</b> (0.039-0.045)	<b>0.046</b> (0.043-0.049)	<b>0.051</b> (0.047-0.054)	<b>0.056</b> (0.052-0.060)	<b>0.061</b> (0.056-0.065)
20-day	<b>0.013</b> (0.012-0.014)	<b>0.016</b> (0.015-0.017)	<b>0.019</b> (0.018-0.020)	<b>0.021</b> (0.020-0.022)	<b>0.024</b> (0.023-0.026)	<b>0.027</b> (0.025-0.029)	<b>0.029</b> (0.027-0.031)	<b>0.032</b> (0.030-0.034)	<b>0.035</b> (0.033-0.038)	<b>0.038</b> (0.035-0.041)
30-day	<b>0.011</b> (0.010-0.012)	<b>0.013</b> (0.012-0.014)	<b>0.015</b> (0.014-0.016)	<b>0.017</b> (0.016-0.018)	<b>0.019</b> (0.018-0.020)	<b>0.021</b> (0.019-0.022)	<b>0.022</b> (0.021-0.024)	<b>0.024</b> (0.023-0.026)	<b>0.027</b> (0.025-0.028)	<b>0.028</b> (0.026-0.030)
45-day	<b>0.009</b> (0.009-0.010)	<b>0.011</b> (0.010-0.011)	<b>0.012</b> (0.012-0.013)	<b>0.014</b> (0.013-0.015)	<b>0.015</b> (0.015-0.016)	<b>0.017</b> (0.016-0.018)	<b>0.018</b> (0.017-0.019)	<b>0.019</b> (0.018-0.020)	<b>0.021</b> (0.019-0.022)	<b>0.022</b> (0.020-0.023)
60-day	<b>0.008</b> (0.008-0.009)	<b>0.010</b> (0.009-0.010)	<b>0.011</b> (0.010-0.012)	<b>0.012</b> (0.011-0.013)	<b>0.013</b> (0.013-0.014)	<b>0.014</b> (0.014-0.015)	<b>0.015</b> (0.014-0.016)	<b>0.016</b> (0.015-0.017)	<b>0.018</b> (0.016-0.019)	<b>0.018</b> (0.017-0.020)

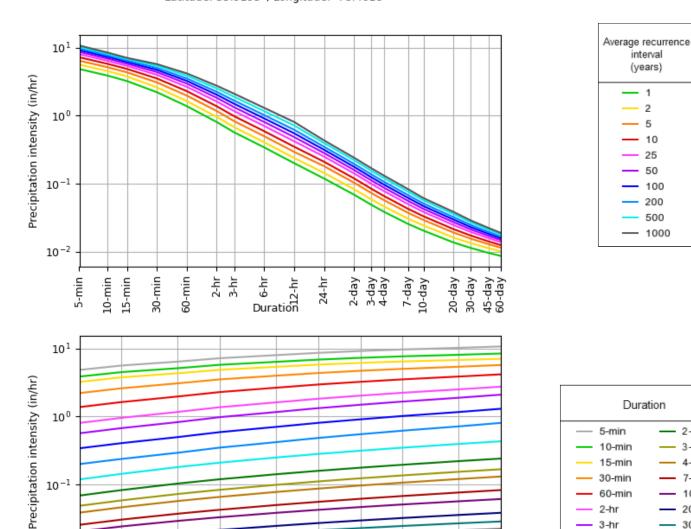
<sup>&</sup>lt;sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

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#### PDS-based intensity-duration-frequency (IDF) curves Latitude: 35.9195°, Longitude: -78.4618°



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1

2

5

10

 $10^{-2}$ 

Created (GMT): Fri Sep 22 12:13:49 2023

500

1000

2-day

3-day 4-day

7-day

10-day 20-day

30-day

45-day

60-day

6-hr

12-hr

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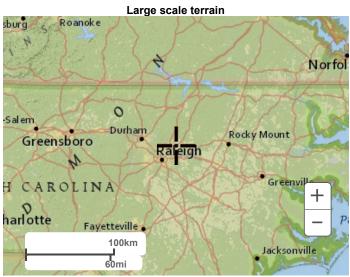
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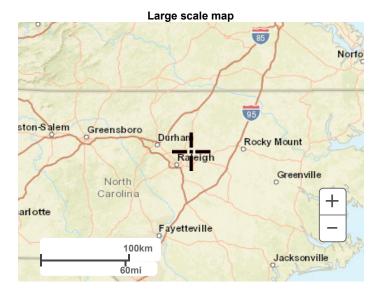
Average recurrence interval (years)

# Maps & aerials

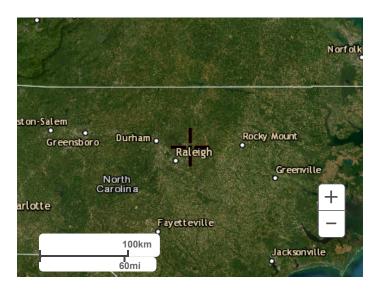
Small scale terrain







Large scale aerial

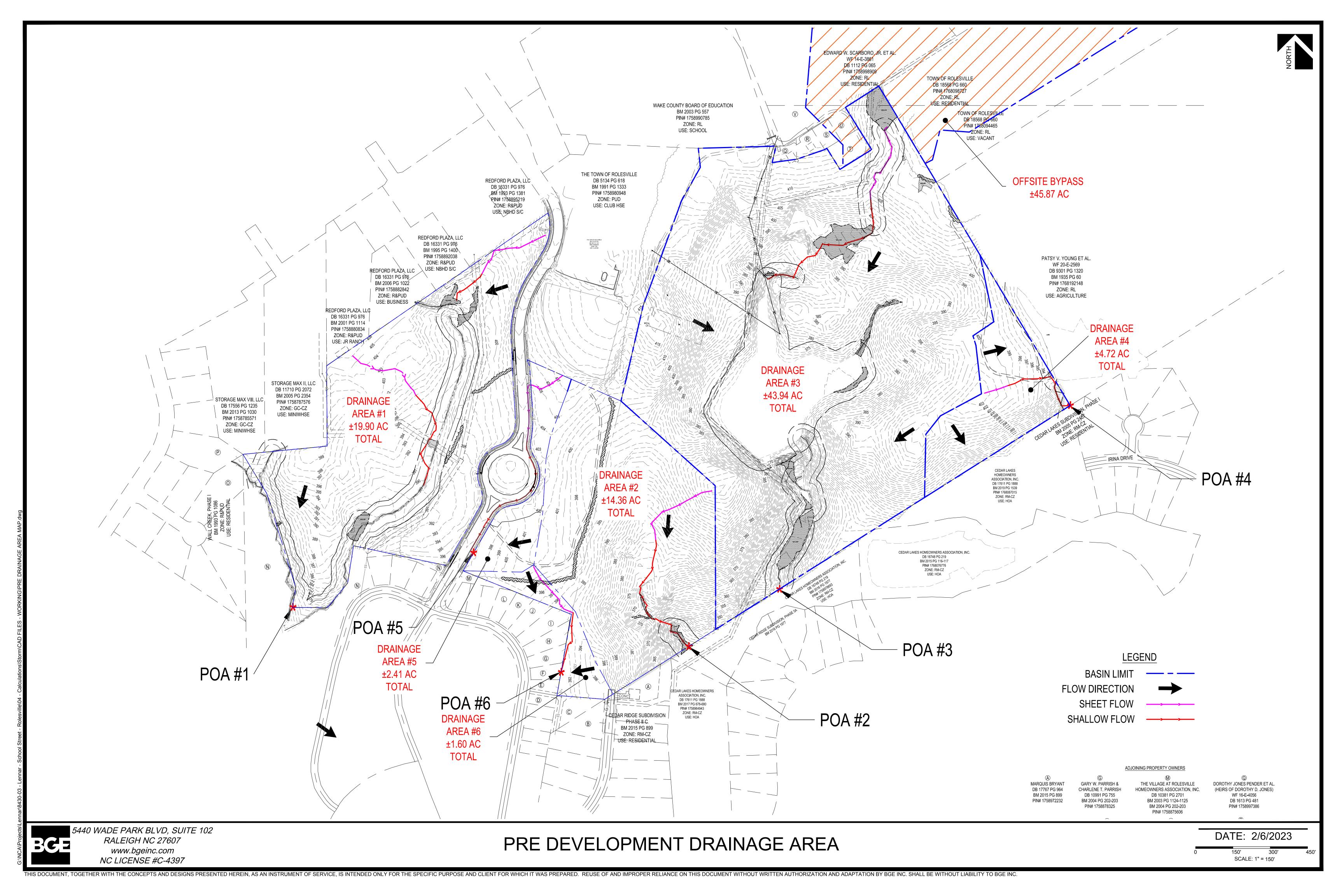


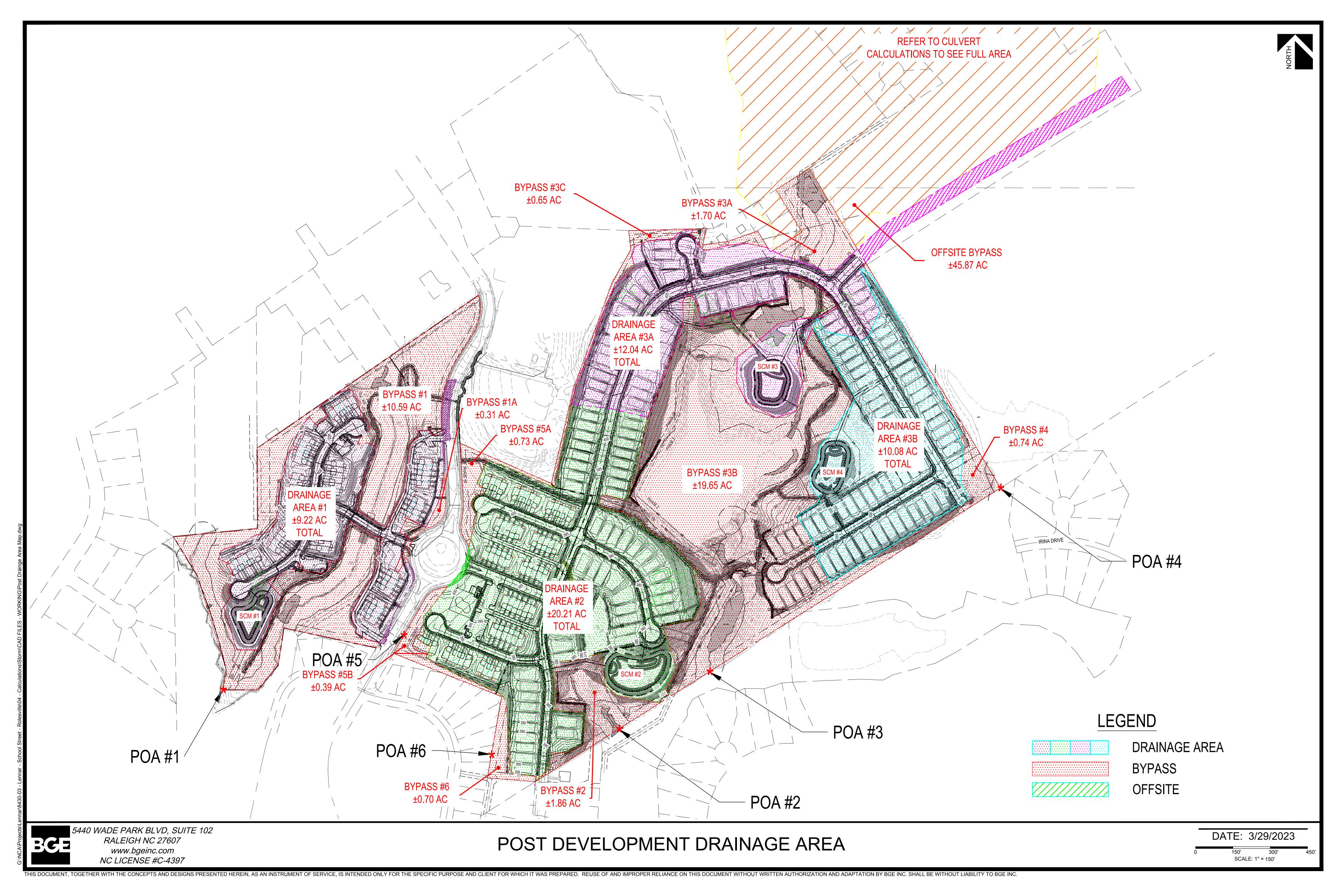
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Silver Spring, MD 20910
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# ATTACHMENT 6: PRE- AND POST-DEVELOPMENT DRAINAGE AREA MAPS





# **ATTACHMENT 7: SCM CALCULATIONS**



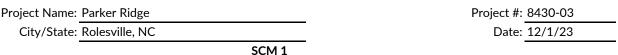


Table 1 Surface Area to Drainage Area Ratio for Permanent Pool Sizing

#### Piedmont and Mountain SA/DA Table (Adapted from Driscoll, 1986)

		Р	ermanent Poo	ol Depth (fee	t)	
% Impervious	3.0	4.0	5.0	6.0	7.0	8.0
10	0.51	0.43	0.37	0.30	0.27	0.25
20	0.84	0.69	0.61	0.51	0.44	0.40
30	1.17	0.94	0.84	0.72	0.61	0.56
40	1.51	1.24	1.09	0.91	0.78	0.71
50	1.79	1.51	1.31	1.13	0.95	0.87
60	2.09	1.77	1.49	1.31	1.12	1.03
70	2.51	2.09	1.80	1.56	1.34	1.17
80	2.92	2.41	2.07	1.82	1.62	1.40
90	3.25	2.64	2.31	2.04	1.84	1.59
100	3.55	2.79	2.52	2.34	2.04	1.75

Source: NCDEQ Stormwater Design Manual Minimum Design Criteria C-3 Wet Pond (4.18.2017)

### **Drainage Area Information**

Total Drainage Area = 9.22 acres

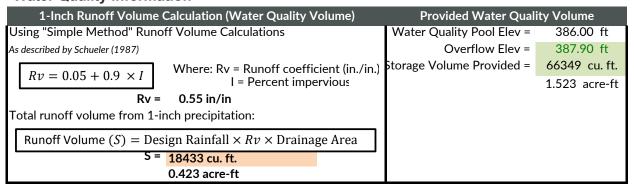
Total Impervious Area = 5.13 acres

% Impervious Surface Area = 55.64 %

#### **Normal Pool Information**

Minimum Required Permanent Pool Surface Area	Provided Permanent Pool	Surface Area
Avg Depth = 3.50 ft	Normal Pool Elevation =	384.5
SA/DA ratio = 1.81 From Table 1	Main Pool SA Provided =	8489 sq. ft.
Minimum pond surface area $(SA) = \frac{DA \times SA \div DA \ ratio}{100}$		0.195 acres
SA = 7261 sq. ft.		
0.167 acres		

#### **Water Quality Information**





Project Name: Parker Ridge Project #: 8430-03

City/State: Rolesville, NC Date: 12/1/23

SCM 1

Total Drainage Area =

9.22

#### **AVERAGE DEPTH**

Per NCDEQ "Stormwater Design Manual" Minimum Design Criteria:

The average depth of a wet pond is to be calculated by one of these two options:

			Incremental	Accumulated	
	Below Normal	Contour	Contour	Contour	
	Pool Contours	Area	Volume	Volume	
	(feet)	(SF)	(CF)	(CF)	
$A_{bot\_pond} \rightarrow$	379.00	4017			
	380.00	4627	4318	4318	←Sediment Storage Volume
	381.00	5266	4943	9261	
$A_{bot\_shelf} \rightarrow$	384.00	7367	18862	28123	•
$A_{perm pool} \rightarrow$	384.50	8489	3961	32084	←Total Pond Volume

V<sub>perm pool</sub> = Total Volume - Sediment Storage Volume = 27,765 cf

### **OPTION 1:** Use the following equation:

$$D_{avg} = \frac{V_{perm\_pool}}{A_{perm\_pool}}$$

Where:

 $D_{avg}$  = Average Depth (ft)

 $V_{perm pool}$  = Volume of Permanent Pool (ft<sup>3</sup>)

 $A_{perm pool} = Area of Permanent Pool (ft<sup>2</sup>)$ 

$$D_{avg} = 3.27 \text{ ft}$$

#### **OPTION 2:** Use the following equation:

$$D_{avg} = 0.25 \times \left(1 + \frac{A_{bot\_shelf}}{A_{perm\_pool}}\right) + \frac{A_{bot\_shelf} + A_{bot\_pond}}{2} \times \frac{Depth}{A_{bot\_shelf}}$$

Where:

 $D_{avg}$  = Average Depth (ft)

A<sub>bot shelf</sub> = Area of Wet Pond at the Bottom of the Shelf (ft<sup>2</sup>)

A<sub>bot pond</sub> = Area of Wet Pond Bottom above Sediment Storage (ft2)

 $A_{perm pool} = Area of Permanent Pool (ft<sup>2</sup>)$ 

Depth = Depth of Wet Pond from Bottom of Shelf to Sediment Storage (ft)

 $D_{avg} = 3.72 \text{ ft}$ 

Use Average Depth = 3.50 ft



Project Name: Parker Ridge	Project #: 8430-03
City/State: Rolesville, NC	Date: 12/1/23
SCM 1	

Total Drainage Area =

#### **FOREBAY DESIGN**

Per NCDEQ "Stormwater Design Manual" Minimum Design Criteria:

The forebay volume shall be 15-20% of the main pool.

Project Name:	Parker Ridge	Project #:	8430-03
City/State:	Rolesville, NC	Date:	12/1/23

### 70 Runoff Storage Volume Information

					_
	Countour	Contour	Incremental	Accumulated	
Pond Area	Elevation	Area	Contour	Contour	
	(ft)	(sf)	Volume	Volume	
	390.00	20,196	19,318	85,667	←Top of Dam
	389.00	18,453	17,603	66,349	1
Storage	388.00	16,767	15,946	48,746	]
Volume	387.00	15,138	14,344	32,800	
	386.00	13,565	12,800	18,456	1
	385.00	12,050	5,656	5,656	1
Normal Pool	384.50	10,590	0	0	←Normal Pool

#### **70 Pond Volume Information**

70 Folia vo	iume informatio	11	Incremental	Accumulated	ı
	Countour	Contour	Contour	Contour	
Pond Area	Elevation	Area	Volume	Volume	
	(ft)	(sf)	(cf)	(cf)	
	384.50	8,489	3,961	32,109	←Normal Pool
	384.00	7,367	7,001	28,148	←Bottom of Litoral Shelf
	383.00	6,641	6,287	21,147	
Main Pool	382.00	5,939	5,599	14,861	
	381.00	5,266	4,943	9,261	
	380.00	4,627	4,318	4,318	←Sediment Storage Volume
	379.00	4,017	0	0	←Pond Bottom
	384.50	2,101	927	5,775	←Normal Pool
	384.00	1,617	1,470	4,848	←Bottom of Litoral Shelf
	383.00	1,328	1,194	3,378	
Forebay	382.00	1,064	942	2,184	
	381.00	826	718	1,242	
	380.00	616	523	523	←Sediment Storage Volume
	379.00	436	0	0	←Forebay Bottom
	384.50	10,590	4,888	37,887	
	384.00	8,984	8,471	32,999	
	383.00	7,969	7,481	24,528	
Total	382.00	7,003	6,542	17,047	
	381.00	6,092	5,662	10,505	
	380.00	5,243	4,843	4,843	
	379.00	4,453	0	0	



Project Name: <b>F</b>	Parker Ridge	Project #: 84	30-03
City/State: F	Rolesville, NC	Date: 12	/1/23
_	SCM 1		

Total Drainage Area = 9.22 acres

# **OS-A Anti-Floatation Sizing Calulations**

# **Outlet Structure Dimension**

**Inside Riser Width:** 4 ft **Outside Riser Width:** 5 **ft** Wall Thickness: 6 in Top Elevation: 387.9 ft **Invert Elevation:** 384.5 ft **Bottom Elevation:** 379 ft **Extended Base:** 12 in **Extended Base Width** 7 ft

Displaced Volume: 222 cu ft
Displaced Weight: 13884 lbs

Volume of Actual Structure: 31 cu ft
Weight of Concrete Structure: 4590 lbs
Weight of Earth with Extended Base: 4488 lbs
Weight of Extra Depth: 20625 lbs
Total Weight of Structure: 29703 lbs

Factor of Safety: 2.1 OK



Project Name: Parker Ridge
City/State: Rolesville, NC

Project #: 8430-03

Date: 12/1/23

SCM 1

Total Drainage Area =

#### **ORIFICE CALCULATOR**

Per NCDEQ "Stormwater Design Manual" Minimum Design Criteria:

The design volume shall draw down to the permenant pool level in 2-5 days.

$$Q = C_d A \sqrt{2gh}$$

## 1" WATER QUALITY STORM VOLUME

**Variables Constants** WQ Volume: 0.423 Acre-ft 18433 cf g = 32.2 ft/s2 Head / Driving Head: 1.50 ft 0.50 ft Cd= 0.6 Draw down time: 48 hrs 172800 s Orifice Area = 0.031 sq. ft 4.514 sq. in

Orifice Diameter = 2.397 in

**USE 2 INCH DIAMETER ORIFICE** 



Project Name: Parker Ridge
City/State: Rolesville, NC

SCM 2

Project #: 8430-03
Date: 12/1/23

Table 1 Surface Area to Drainage Area Ratio for Permanent Pool Sizing
Piedmont and Mountain SA/DA Table (Adapted from Driscoll, 1986)

	Permanent Pool Depth (feet)					
% Impervious	3.0	4.0	5.0	6.0	7.0	8.0
10	0.51	0.43	0.37	0.30	0.27	0.25
20	0.84	0.69	0.61	0.51	0.44	0.40
30	1.17	0.94	0.84	0.72	0.61	0.56
40	1.51	1.24	1.09	0.91	0.78	0.71
50	1.79	1.51	1.31	1.13	0.95	0.87
60	2.09	1.77	1.49	1.31	1.12	1.03
70	2.51	2.09	1.80	1.56	1.34	1.17
80	2.92	2.41	2.07	1.82	1.62	1.40
90	3.25	2.64	2.31	2.04	1.84	1.59
100	3.55	2.79	2.52	2.34	2.04	1.75

Source: NCDEQ Stormwater Design Manual Minimum Design Criteria C-3 Wet Pond (4.18.2017)

### **Drainage Area Information**

Total Drainage Area = 20.21 acres
Total Impervious Area = 10.42 acres
% Impervious Surface Area = 51.56 %

#### **Normal Pool Information**

Minimum Required Permanent Pool Surface Area			Provided Permanent Pool Surface Area		
Avg Depth = 3.50 ft			Normal Pool Elevation =	351.5	
SA/DA ratio = 2.12	From Table 1		Main Pool SA Provided =	20384 sq. ft.	
Minimum pond surface	$area (SA) = \frac{DA \times SA \div DA \ ratio}{100}$			0.468 acres	
SA =	18693 sq. ft.				
	0.429 acres				

# **Water Quality Information**

1-Inch Runoff Volume Calculation (Water Quality Volume)	Provided Water Qual	ity Volume
Using "Simple Method" Runoff Volume Calculations	Water Quality Pool Elev =	352.87 ft
As described by Schueler (1987)	Overflow Elev =	355.50 ft
	torage Volume Provided =	138278 cu. ft.
$RV = 0.05 + 0.9 \times I$ I = Percent impervious		3.174 acre-ft
KV = 0.51 In/In		
Total runoff volume from 1-inch precipitation:		
Runoff Volume ( $S$ ) = Design Rainfall $\times Rv \times$ Drainage Area		
S = 37710 cu. ft.		
0.866 acre-ft		

#### Interpolation from table 10.1:

	Permanent Pool Depth					
ious		3.0	3.5	4.0		
ervic	50.0	1.79		1.51		
impe	51.6	1.84	2.12	2.41		
:≡ %	60.0	2.09		1.77		



Project Name: Parker Ridge Project #: 8430-03

City/State: Rolesville, NC Date: 12/1/23

SCM<sub>2</sub>

# Total Drainage Area = AVERAGE DEPTH

Per NCDEQ "Stormwater Design Manual" Minimum Design Criteria:

The average depth of a wet pond is to be calculated by one of these two options:

			Incremental	Accumulated	
	Below Normal	Contour	Contour	Contour	
	Pool Contours	Area	Volume	Volume	
	(feet)	(SF)	(CF)	(CF)	
$A_{bot\_pond} \rightarrow$	346.00	12020	_		
	347.00	13231	12621	12621	←Sediment Storage Volume
	348.00	14468	13845	26466	
$A_{\text{bot\_shelf}} \rightarrow 0$	351.00	18329	49081	75547	
$A_{perm pool} \rightarrow$	351.50	20384	9674	85221	←Total Pond Volume

V<sub>perm pool</sub> = Total Volume - Sediment Storage Volume = 72,600 cf

# **OPTION 1:** Use the following equation:

$$D_{avg} = \frac{V_{perm\_pool}}{A_{perm\_pool}}$$
Where:  $D_{avg} = \text{Average Depth (ft)}$ 

$$V_{perm\_pool} = \text{Volume of Permanent Pool (ft}^3)$$

$$A_{perm\_pool} = \text{Area of Permanent Pool (ft}^2)$$

$$D_{avg} = 3.56 \text{ ft}$$

# **OPTION 2:** Use the following equation:

$$D_{avg} = 0.25 \times \left(1 + \frac{A_{bot\_shelf}}{A_{perm\_pool}}\right) + \frac{A_{bot\_shelf} + A_{bot\_pond}}{2} \times \frac{Depth}{A_{bot\_shelf}}$$

Where:  $D_{avg} = Average Depth (ft)$ 

 $A_{bot\_shelf}$  = Area of Wet Pond at the Bottom of the Shelf (ft<sup>2</sup>)

 $A_{bot\_pond}$  = Area of Wet Pond Bottom above Sediment Storage (ft2)

 $A_{perm\_pool}$  = Area of Permanent Pool (ft<sup>2</sup>)

Depth = Depth of Wet Pond from Bottom of Shelf to Sediment Storage (ft)

 $D_{avg} = 3.92 \text{ ft}$  Use Average Depth = 3.50 ft



Project Name: Parker Ridge	Project #: 8430-03
City/State: Rolesville, NC	Date: 12/1/23
SCM 2	

## Total Drainage Area =

#### **FOREBAY DESIGN**

 $\label{thm:condition} \mbox{Per NCDEQ "Stormwater Design Manual" Minimum Design Criteria:}$ 

The forebay volume shall be 15-20% of the main pool.

Project Name:	Parker Ridge	Project #:	8430-03
City/State:	Rolesville, NC	Date:	12/1/23

## **50 Runoff Storage Volume Information**

	Countour	Contour	Incremental	Accumulated	
Pond Area	Elevation	Area	Contour	Contour	
	(ft)	(sf)	Volume	Volume	
	357.00	37,716	36,604	174,882	←Top of Dam
	356.00	35,504	34,421	138,278	
Storage	355.00	33,350	32,295	103,857	
Volume	354.00	31,251	30,224	71,562	
	353.00	29,209	28,211	41,337	
	352.00	27,224	13,127	13,127	
Normal Pool	351.50	25,295	0	0	←Normal Pool

#### 50 Pond Volume Information

50 FOIIU VO	iume informatio	ווע	Incremental	Accumulated	1
	Countour	Contour	Contour	Contour	
Pond Area	Elevation	Area	Volume	Volume	
	(ft)	(sf)	(cf)	(cf)	
	351.50	20,384	9,674	85,272	←Normal Pool
	351.00	18,329	17,669	75,598	←Bottom of Litoral Shelf
	350.00	17,017	16,369	57,929	
Main Pool	349.00	15,730	15,095	41,560	
	348.00	14,468	13,845	26,466	
	347.00	13,231	12,621	12,621	←Sediment Storage Volume
	346.00	12,020	0	0	←Pond Bottom
	351.50	4,911	2,185	12,993	←Normal Pool
	351.00	3,849	3,477	10,809	←Bottom of Litoral Shelf
	350.00	3,117	2,768	7,332	1
Forebay	349.00	2,434	2,111	4,564	
	348.00	1,803	1,504	2,453	1
	347.00	1,224	949	949	←Sediment Storage Volume
	346.00	698	0	0	←Forebay Bottom
	351.50	25,295	11,860	98,288	
	351.00	22,178	21,148	86,428	15.2%
	350.00	20,134	19,141	65,281	
Total	349.00	18,164	17,209	46,140	
	348.00	16,271	15,354	28,931	
	347.00	14,455	13,577	13,577	
	346.00	12,718	0	0	



Project Name: Parker Ridge	Project #: 8430-03
City/State: Rolesville, NC	Date: 12/1/23

SCM 2

Total Drainage Area =

# **OS-A Anti-Floatation Sizing Calulations**

# **Outlet Structure Dimension**

Inside Riser Width: 4 ft Outside Riser Width: 5 ft

Wall Thickness: 6 in

Top Elevation: 356 ft Invert Elevation: 351.5 ft

Bottom Elevation: 347 ft

Extended Base: 12 in Extended Base Width 7 ft

Displaced Volume: 225 cu ft
Displaced Weight: 14040 lbs

Volume of Actual Structure: 41 cu ft
leight of Concrete Structure: 6075 lbs

of Earth with Extended Base: 5940 lbs

Weight of Extra Depth: 16875 lbs

Total Weight of Structure: 28890 lbs

Factor of Safety: 2.1 OK



Project Name: Parker Ridge Project #: 8430-03

City/State: Rolesville, NC Date: 12/1/23

#### SCM<sub>2</sub>

Total Drainage Area =

#### **ORIFICE CALCULATOR**

Per NCDEQ "Stormwater Design Manual" Minimum Design Criteria:

The design volume shall draw down to the permenant pool level in 2-5 days.

$$Q = C_d A \sqrt{2gh}$$

## 1" WATER QUALITY STORM VOLUME

**Orifice Area =** 0.067 sq. ft 9.653 sq. in

Orifice Diameter = 3.506 in

**USE 4 INCH DIAMETER ORIFICE** 



 Project Name:
 Parker Ridge
 Project #: 8430-03

 City/State:
 Rolesville, NC
 Date: 12/1/23

SCM 3A

Table 1 Surface Area to Drainage Area Ratio for Permanent Pool Sizing
Piedmont and Mountain SA/DA Table (Adapted from Driscoll, 1986)

	Permanent Pool Depth (feet)					
% Impervious	3.0	4.0	5.0	6.0	7.0	8.0
10	0.51	0.43	0.37	0.30	0.27	0.25
20	0.84	0.69	0.61	0.51	0.44	0.40
30	1.17	0.94	0.84	0.72	0.61	0.56
40	1.51	1.24	1.09	0.91	0.78	0.71
50	1.79	1.51	1.31	1.13	0.95	0.87
60	2.09	1.77	1.49	1.31	1.12	1.03
70	2.51	2.09	1.80	1.56	1.34	1.17
80	2.92	2.41	2.07	1.82	1.62	1.40
90	3.25	2.64	2.31	2.04	1.84	1.59
100	3.55	2.79	2.52	2.34	2.04	1.75

Source: NCDEQ Stormwater Design Manual Minimum Design Criteria C-3 Wet Pond (4.18.2017)

## **Drainage Area Information**

Total Drainage Area = 12.04 acres
Total Impervious Area = 6.23 acres
% Impervious Surface Area = 51.74 %

Input Output

### **Normal Pool Information**

Minimum Required Permanent Pool Surface Area			Provided Permanent Pool Surface Area		
Avg Depth = 3.50 ft			Normal Pool Elevation =	384.5	
SA/DA ratio = 1.70	From Table 1		Main Pool SA Provided =	11217 sq. ft.	
Minimum pond surface area $(SA) = \frac{DA \times SA \div DA \ ratio}{100}$				0.258 acres	
SA	= 8910 sq. ft.				
	0.205 acres				

# **Water Quality Information**

1-Inch Runoff Volume Calculation (Water Quality Volume)	Provided Water Quality Volume		
Using "Simple Method" Runoff Volume Calculations	Water Quality Pool Elev =	385.93 ft	
As described by Schueler (1987)	Overflow Elev =	387.80 ft	
Where: $Rv = Runoff$ coefficient (in./in.)	torage Volume Provided =	60436 cu. ft.	
$Rv = 0.05 + 0.9 \times I$ $I = Percent impervious$ $Rv = 0.52 \text{ in/in}$ $Total runoff volume from 1-inch precipitation:}$		1.387 acre-ft	
Runoff Volume (S) = Design Rainfall $\times Rv \times$ Drainage Area			
S = 22539 cu. ft. 0.517 acre-ft			



Project Name: Parker Ridge Project #: 8430-03

City/State: Rolesville, NC Date: 12/1/23

SCM 3A

# Total Drainage Area = AVERAGE DEPTH

Per NCDEQ "Stormwater Design Manual" Minimum Design Criteria:

The average depth of a wet pond is to be calculated by one of these two options:

	Below Normal Pool Contours (feet)	Contour Area (SF)	Incremental Contour Volume (CF)	Accumulated Contour Volume (CF)	
$A_{bot\_pond} \rightarrow$	379.00 380.00	6368 7038	6700	6700	←Sediment Storage Volume
	381.00	7730	7381	14082	_
$A_{bot\_shelf} \rightarrow$	384.00	9960	26464	40546	
$A_{perm\_pool} \rightarrow$	384.50	11217	5291	45837	←Total Pond Volume

V<sub>perm pool</sub> = Total Volume - Sediment Storage Volume = 39,137 cf

# **OPTION 1:** Use the following equation:

$$D_{avg} = \frac{V_{perm\_pool}}{A_{perm\_pool}}$$

Where:  $D_{avg} = Average Depth (ft)$ 

 $V_{perm\_pool} = Volume of Permanent Pool (ft^3)$ 

 $A_{perm pool} = Area of Permanent Pool (ft^2)$ 

D<sub>avg</sub> = 3.49 ft

# **OPTION 2:** Use the following equation:

$$D_{avg} = 0.25 \times \left(1 + \frac{A_{bot\_shelf}}{A_{perm\_pool}}\right) + \frac{A_{bot\_shelf} + A_{bot\_pond}}{2} \times \frac{Depth}{A_{bot\_shelf}}$$

Where:  $D_{avg} = Average Depth (ft)$ 

 $A_{bot\_shelf}$  = Area of Wet Pond at the Bottom of the Shelf (ft<sup>2</sup>)

A<sub>bot\_pond</sub> = Area of Wet Pond Bottom above Sediment Storage (ft2)

 $A_{perm\_pool}$  = Area of Permanent Pool (ft<sup>2</sup>)

Depth = Depth of Wet Pond from Bottom of Shelf to Sediment Storage (ft)

 $D_{avg} = 3.89 \text{ ft}$ 

Use Average Depth = 3.50 ft



Project Name: Parker Ridge

City/State: Rolesville, NC

Project #: 8430-03

Date: 12/1/23

SCM 3A

Total Drainage Area = 12.04

## FOREBAY DESIGN

Per NCDEQ "Stormwater Design Manual" Minimum Design Criteria: The forebay volume shall be 15-20% of the main pool.

 Project Name:
 Parker Ridge Subdivision
 Project #:
 8430-03

 City/State:
 Rolesville, NC
 Date:
 12/1/23

#### 70 Runoff Storage Volume Information

	Countour	Contour	Incremental	Accumulated	
Pond Area	Elevation	Area	Contour	Contour	
	(ft)	(sf)	Volume	Volume	
	390.00	23,096	22,278	103,393	←Top of Dam
	389.00	21,469	20,679	81,115	
Storage	388.00	19,899	19,137	60,436	
Volume	387.00	18,385	17,651	41,299	
	386.00	16,928	16,222	23,647	
	385.00	15,52/	7,425	7,425	
Normal Pool	384.50	14,183	0	0	←Normal Pool

#### 70 Pond Volume Information

70 Pond Vo	lume Informatio	n			<u>_</u>
			Incremental	Accumulated	
Pond Area	Countour	Contour	Contour	Contour	
1 Olla Alca	Elevation	Area	Volume	Volume	
	(ft)	(sf)	(cf)	(cf)	
	384.50	11,217	5,291	45,850	←Normal Pool
	384.00	9,960	9,573	40,559	←Bottom of Litoral Shelf
	383.00	9,192	8,817	30,986	
Main Pool	382.00	8,448	8,087	22,168	
	381.00	7,730	7,381	14,082	
	380.00	7,038	6,700	6,700	←Sediment Storage Volume
	379.00	6,368	0	0	←Pond Bottom
	384.50	2,965	1,274	8,035	←Normal Pool
	384.00	2,153	1,976	6,760	←Bottom of Litoral Shelf
	383.00	1,804	1,639	4,785	
Forebay	382.00	1,480	1,328	3,145	
	381.00	1,181	1,041	1,818	
	380.00	907	777	777	←Sediment Storage Volume
	379.00	653	0	0	←Forebay Bottom
	384.50	14,182	6,567	53,891	
	384.00	12,113	11,550	47,324	
	383.00	10,996	10,458	35,774	
Total	382.00	9,928	9,415	25,317	
	381.00	8,911	8,423	15,902	
	380.00	7,945	7,478	7,478	
	379.00	7,021	0	0	



Project Name:	Parker Ridge	Project #:	8430-03
City/State:	Rolesville, NC	Date:	12/1/23
	SCM 3A		

Total Drainage Area =

# **OS-A Anti-Floatation Sizing Calulations**

# **Outlet Structure Dimension**

**Inside Riser Width:** 4 ft **Outside Riser Width:** 5 **ft** Wall Thickness: 6 in **Top Elevation:** 388.35 ft **Invert Elevation:** 384.5 ft **Bottom Elevation:** 380 ft **Extended Base:** 12 in **Extended Base Width** 7 ft **Displaced Volume:** 209 cu ft **Displaced Weight:** 13026 **lbs** 

Volume of Actual Structure: 35 cu ft
leight of Concrete Structure: 5198 lbs
of Earth with Extended Base: 5082 lbs
Weight of Extra Depth: 16875 lbs
Total Weight of Structure: 27155 lbs

Factor of Safety: 2.1 OK



Project Name: Parker Ridge Project #: 8430-03

City/State: Rolesville, NC Date: 12/1/23

SCM 3A

Total Drainage Area =

#### **ORIFICE CALCULATOR**

Per NCDEQ "Stormwater Design Manual" Minimum Design Criteria:

The design volume shall draw down to the permenant pool level in 2-5 days.

 $Q = C_d A \sqrt{2gh}$ 

#### 1" WATER QUALITY STORM VOLUME

Variables Constants

WQ Volume: 0.517 Acre-ft 22539 cf g = 32.2 ft/s2Head / Driving Head: 1.43 ft 0.48 ft Cd= 0.6

Draw down time: 48 hrs 172800 s

**Orifice Area =** 0.039 sq. ft 5.647 sq. in

Orifice Diameter = 2.681 in

**USE 3 INCH DIAMETER ORIFICE** 

#### LEVEL SPREADER FILTER STRIP CALCULATIONS

Drawdown Rate: 0.13 cfs

LS Length: 10 feet (min)



Project Name: Parker Ridge Project #: 8430-03

City/State: Rolesville, NC Date: 12/1/23

SCM 3B

Table 1 Surface Area to Drainage Area Ratio for Permanent Pool Sizing
Piedmont and Mountain SA/DA Table (Adapted from Driscoll, 1986)

	Permanent Pool Depth (feet)					
% Impervious	3.0	4.0	5.0	6.0	7.0	8.0
10	0.51	0.43	0.37	0.30	0.27	0.25
20	0.84	0.69	0.61	0.51	0.44	0.40
30	1.17	0.94	0.84	0.72	0.61	0.56
40	1.51	1.24	1.09	0.91	0.78	0.71
50	1.79	1.51	1.31	1.13	0.95	0.87
60	2.09	1.77	1.49	1.31	1.12	1.03
70	2.51	2.09	1.80	1.56	1.34	1.17
80	2.92	2.41	2.07	1.82	1.62	1.40
90	3.25	2.64	2.31	2.04	1.84	1.59
100	3.55	2.79	2.52	2.34	2.04	1.75

Source: NCDEQ Stormwater Design Manual Minimum Design Criteria C-3 Wet Pond (4.18.2017)

## **Drainage Area Information**

Total Drainage Area = 10.08 acres
Total Impervious Area = 4.45 acres
% Impervious Surface Area = 44.15 %

Input Output

#### **Normal Pool Information**

Minimum Required	d Permanent Pool Surface Area	Provided Permanent Pool Surface Area		
Avg Depth = 3.50 ft		Normal Pool Elevation =	380.5	
SA/DA ratio = 2.02	From Table 1	Main Pool SA Provided =	14636 sq. ft.	
Minimum pond surface	$area (SA) = \frac{DA \times SA \div DA \ ratio}{100}$		0.336 acres	
SA =	8861 sq. ft.			
	0.203 acres			

#### **Water Quality Information**

1-Inch Runoff Volume Calculation (Water Quality Volume)	Provided Water Quali	ty Volume
Using "Simple Method" Runoff Volume Calculations	Water Quality Pool Elev =	381.52 ft
As described by Schueler (1987)	Overflow Elev =	384.00 ft
Where: Rv = Runoff coefficient (in./in.)	torage Volume Provided =	84687 cu. ft.
$Rv = 0.05 + 0.9 \times I$ I = Percent impervious		1.944 acre-ft
Rv = 0.45 in/in		
Total runoff volume from 1-inch precipitation:		
Runoff Volume ( $S$ ) = Design Rainfall $\times Rv \times$ Drainage Area		
S = 16368 cu. ft.		
0.376 acre-ft		



Project Name: Parker Ridge Project #: 8430-03

City/State: Rolesville, NC Date: 12/1/23

SCM 3B (SCM 3B)

Total Drainage Area =

#### **AVERAGE DEPTH**

Per NCDEQ "Stormwater Design Manual" Minimum Design Criteria:

The average depth of a wet pond is to be calculated by one of these two options:

_					
			Incremental	Accumulated	
	Below Normal	Contour	Contour	Contour	
	Pool Contours	Area	Volume	Volume	
	(feet)	(SF)	(CF)	(CF)	
$A_{bot\_pond} \rightarrow$	375.00	5047	_		
	376.00	5697	5369	5369	←Sediment Storage Volum
•	377.00	6373	6032	11401	•
$A_{\text{bot\_shelf}} \rightarrow$	380.00	8550	22305	33705	
$A_{perm\_pool} \rightarrow 0$	380.50	10901	4851	38556	←Total Pond Volume

V<sub>perm pool</sub> = Total Volume - Sediment Storage Volume = 33,187 cf

#### **OPTION 1:** Use the following equation:

$$D_{avg} = rac{V_{perm\_pool}}{A_{perm\_pool}}$$
 Where:  $D_{avg} = Average Depth (ft)$   $V_{perm\_pool} = Volume of Permanent Pool (ft^3)$ 

 $A_{perm pool} = Area of Permanent Pool (ft^2)$ 

 $D_{avg} = 3.04 \text{ ft}$ 

#### **OPTION 2:** Use the following equation:

$$D_{avg} = 0.25 \times \left(1 + \frac{A_{bot\_shelf}}{A_{perm\_pool}}\right) + \frac{A_{bot\_shelf} + A_{bot\_pond}}{2} \times \frac{Depth}{A_{bot\_shelf}}$$

 $D_{avg}$  = Average Depth (ft)

 $A_{\text{bot shelf}}$  = Area of Wet Pond at the Bottom of the Shelf (ft<sup>2</sup>)

A<sub>bot pond</sub> = Area of Wet Pond Bottom above Sediment Storage (ft2)

 $A_{perm pool} = Area of Permanent Pool (ft<sup>2</sup>)$ 

Depth = Depth of Wet Pond from Bottom of Shelf to Sediment Storage (ft)

3.78 ft  $D_{avg} =$ 

Use Average Depth = 3.50 ft



Project Name: Parker Ridge	Project #: 8430-03
City/State: Rolesville, NC	Date: 12/1/23
SCM 3B	

Total Drainage Area = 10.08

#### **FOREBAY DESIGN**

Per NCDEQ "Stormwater Design Manual" Minimum Design Criteria: The forebay volume shall be 15-20% of the main pool.

 Project Name:
 Parker Ridge
 Project #:
 8430-03

 City/State:
 Rolesville, NC
 Date:
 12/1/23

### 70 Runoff Storage Volume Information

	Countour	Contour	Incremental	Accumulated	
Pond Area	Elevation	Area	Contour	Contour	
	(ft)	(sf)	Volume	Volume	
	386.00	24,300	23,419	108,106	←Top of Dam
	385.00	22,548	21,695	84,687	
Storage	384.00	20,853	20,028	62,992	
Volume	383.00	19,214	18,418	42,964	
	382.00	17,634	16,864	24,546	
	381.00	16,105	7,682	7,682	
Normal Pool	380.50	14,636	0	0	←Normal Pool

#### **70 Pond Volume Information**

	ume informatio		Incremental	Accumulated	Ī
	Countour	Contour	Contour	Contour	
Pond Area	Elevation	Area	Volume	Volume	
	(ft)	(sf)	(cf)	(cf)	
	380.50	10,901	4,851	38,576	←Normal Pool
	380.00	8,550	8,172	33,725	←Bottom of Litoral Shelf
	379.00	7,799	7,433	25,554	1
Main Pool	378.00	7,073	6,720	18,121	
	377.00	6,373	6,032	11,401	
	376.00	5,697	5,369	5,369	←Sediment Storage Volume
	375.00	5,047	0	0	←Pond Bottom
					Ī
	380.50	3,735	1,638	9,851	←Normal Pool
	380.00	2,839	2,566	8,212	←Bottom of Litoral Shelf
	379.00	2,302	2,054	5,647	
Forebay	378.00	1,816	1,592	3,592	
	377.00	1,379	1,181	2,000	
	376.00	993	819	819	←Sediment Storage Volume
	375.00	657	0	0	←Forebay Bottom
	380.50	14,636	6,489	48,435	Ī
	380.00	11,389	10,739	41,946	
	379.00	10,101	9,489	31,208	
Total	378.00	8,889	8,314	21,719	
	377.00	7,752	7,214	13,405	
	376.00	6,690	6,190	6,190	
	375.00	5,704	0	0	



Project Name:	Parker Ridge	Project #:	8430-03
City/State:	Rolesville, NC	Date:	12/1/23
	SCM 3B	'	

Total Drainage Area =

### **OS-A Anti-Floatation Sizing Calulations**

### **Outlet Structure Dimension**

**Inside Riser Width:** 4 ft **Outside Riser Width:** 5 **ft** Wall Thickness: 6 in **Top Elevation:** 386 ft **Invert Elevation:** 380.5 ft **Bottom Elevation:** 375 ft **Extended Base:** 12 in **Extended Base Width** 7 ft

Displaced Volume: 275 cu ft
Displaced Weight: 17160 lbs

Volume of Actual Structure: 50 cu ft
leight of Concrete Structure: 7425 lbs
of Earth with Extended Base: 7260 lbs
Weight of Extra Depth: 20625 lbs
Total Weight of Structure: 35310 lbs

Factor of Safety: 2.1 OK



Project Name:	Parker Ridge
City/State:	Rolesville, NC

Project #: 8430-03

Date: 12/1/23

SCM 3B

Total Drainage Area =

#### **ORIFICE CALCULATOR**

Per NCDEQ "Stormwater Design Manual" Minimum Design Criteria:

The design volume shall draw down to the permenant pool level in 2-5 days.

 $Q = C_d A \sqrt{2gh}$ 

#### 1" WATER QUALITY STORM VOLUME

Variables Constants

WQ Volume: 0.376 Acre-ft 16368 cf g = 32.2 ft/s2Head / Driving Head: 1.02 ft 0.34 ft Cd= 0.6

Draw down time: 48 hrs 172800 s

**Orifice Area =** 0.034 sq. ft 4.870 sq. in

Orifice Diameter = 2.490 in

**USE 2 INCH DIAMETER ORIFICE** 

#### LEVEL SPREADER FILTER STRIP CALCULATIONS

Drawdown Rate: 0.09 cfs

LS Length: 10 feet (min)

# ATTACHMENT 8: NUTRIENT CALCULATIONS – STORMWATER DESIGN TOOL



### SITE DATA

	Project Information				
Project Name:	Parker Ridge				
Permit No (if known):					
Applicant:	Lennar Corporation				
Applicant Contact Name:	Michael Taylor				
Applicant Contact Number:	(919) 863-6461				
Contact Email:	michael.taylor@lennar.com				
Last Modified Date:	Wednesday, October 4, 2023				
	Site Data:				
River Basin:	Neuse				
Regulatory Watershed:	N/A				
Physiographic/Geologic Region:	Piedmont				
Type of Development (Select from Dropdown menu):	Residential				
Zoning:	R-5				
Total Site Area (Ac):	87.27				
Existing Lake/Pond Area (Ac):	3.58				
Proposed Disturbed Area (Ac):	62.30				
Proposed Impervious Surface Area from DA Sheets (acre):	26.11				
Percent Built Upon Area (BUA):	30%				
Is the proposed project a site expansion?	No				
Number of Drainage Areas on Site (Points of Analysis):	6				
Annual Rainfall (in):	45.41				
One-year, 24-hour rainfall (in):	3.00				
Two-year, 24-hour rainfall (in):	3.60				
Proposed Reside	ential Stormwater Details (if applicable):				
Site Square Footage:	3,801,481				
Total Acreage in Lots:	28.52				
Lot Square Footage:	1,242,331				
Number of Lots:	275				
Average Lot Size (SF):	4,518				
Proposed Impervious Surface Area from DA sheets (SF):	1,137,352				
Proposed Impervious Surface Area Devoted to Lots (SF):	815,008				
Total Impervious Surface Area Devoted to Roads (SF):	176,418				
Other Impervious Surface Area (SF):	145,926				

SITE DATA Page 2

WAKE

JURISDICTIONAL LANDS

Riparian buffer (Zone 1 only)

Natural wetland

Open water

Site

0.00

Totals (Ac)=

Offsite

Site

0.00

Offsite

0.00

Site

0.00

Project Name: Parker Ridge

### DRAINAGE AREA 1 STORMWATER PRE-POST CALCULATIONS

LAND USE & SITE DATA PRE-DEVELOPMENT POST-DEVELOPMENT Drainage Area (Acres)= 19.90 20.54 Site Acreage within Drainages 19.90 20.29 One-year, 24-hour rainfall (in)= 3.00 Land Use (acres) by Soil Group: A Soils **B** Soils C Soils D Soils A Soils **B** Soils C Soils D Soils Commercial Site Offsite Parking lot Roof Open/Landscaped Industrial Site Offsite Parking lot Roof Open/Landscaped Transportation Site Offsite Offsite Site Offsite Site Offsite Site Offsite Site Offsite Site Offsite Offsite High Density (interstate, main) High Density (Grassed Right-of-ways) Low Density (secondary, feeder) Low Density (Grassed Right-of-ways) Rural Rural (Grassed Right-of-ways) Sidewalk Misc. Pervious Site Offsite Managed pervious (Open Space) 3.89 Unmanaged (pasture) 11.56 Woods (not on lots) Residential Site Offsite 1.71 0.24 Roadway Grassed Right-of-ways Driveway Parking lot Roof 2.75 Sidewalk (Includes Patios) 0.90 1.10 Lawn Managed pervious (Open Space) 9.21 0.01 Woods (on lots) Land Taken up by BMP 0.46

Offsite

0.00

Site

0.12

4.33

19.90

Offsite

0.00

Site

0.00

Offsite

0.00

Site

0.00

Offsite

Site

0.00

Offsite

0.00

Site

0.12

4.04

20.29

Offsite

0.25

DA1 Page 4

Sheet Flow	SITE FLOW	PRE-DEVELOP!	MENT T <sub>c</sub>	POST-DEVELOPMENT Tc			
Slope (Pift)	Sheet Flow						
Surface Cover   Paved, Gravel, or Bare Soil   Paved, Gravel, or Bare Soil   O.01   O.011	Length (ft)=	300.00		300.00			
Novalue	Slope (ft/ft)=	0.05		0.01			
Tr, (hrs)	Surface Cover:	Paved, Gravel, or	Bare Soil	Paved, Gravel, or Bare Soil			
Shallow Flow   Length (ft)	n-value=	0.01		0.011			
Length (ft)=	T <sub>t</sub> (hrs)=	0.03		0.07			
Slope (lift)	Shallow Flow						
Surface Cover	Length (ft)=	150.00		150.00			
Average Velocity (ft/sec)	Slope (ft/ft)=	0.04		0.00			
T <sub>1</sub> (hrs) =	Surface Cover:	Unpaved		Paved			
Channel Flow 1	Average Velocity (ft/sec)=	3.02		0.91			
Length (ft) =   3240.00     Slope (ft/ft) =   0.01     Cross Sectional Flow Area (ft²) =   16.00     Wetted Perimeter (ft) =   20.00     Channel Lining:	T <sub>t</sub> (hrs)=	0.01		0.05			
Slope (ft/ft)	Channel Flow 1						
Cross Sectional Flow Area (ft²) =   16.00     Wetted Perimeter (ft) =   20.00     Channel Lining:   Asphalt	Length (ft)=	3240.00					
Wetted Perimeter (ft)=	Slope (ft/ft)=	0.01					
Channel Lining:	Cross Sectional Flow Area (ft <sup>2</sup> )=	16.00					
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Wetted Perimeter (ft)=	20.00					
Hydraulic Radius (ft)	Channel Lining:	Asphalt					
Average Velocity (ft/sec) = 8.03 0.00  T, (hrs) = 0.11 0.00  Tc (hrs) = 0.16 0.08  RESULTS PRE-DEVELOPMENT POST-DEVELOPMENT  Site Impervious Surface Area (Ac) = 0.00 5.36  Lot Impervious Surface Area (Ac) = 0.00 3.65  1-year, 24-hour storm (Peak Flow)  Volume of runoff (ft³) = 82,562 123,982  Volume change (ft³) = 41,420  Runoff (inches) = Q* = 1.1429 1.6628  Peak Discharge (cfs) = Q = 29.6047 56.7214	n-value=	0.02					
$T_{t} (hrs) = 0.11                                 $	Hydraulic Radius (ft)=	0.80		0.00			
Tc (hrs)=         0.16         0.08           RESULTS         PRE-DEVELOPMENT         POST-DEVELOPMENT           Site Impervious Surface Area (Ac) =         0.00         5.36           Lot Impervious Surface Area (Ac) =         0.00         3.65           1-year, 24-hour storm (Peak Flow)         Volume of runoff (ft³) =         82,562         123,982           Volume change (ft³) =         41,420         41,420           Runoff (inches) = Q*=         1.1429         1.6628           Peak Discharge (cfs) = Q =         29.6047         56.7214	Average Velocity (ft/sec)=	8.03		0.00			
RESULTS         PRE-DEVELOPMENT         POST-DEVELOPMENT           Site Impervious Surface Area (Ac) =         0.00         5.36           Lot Impervious Surface Area (Ac) =         0.00         3.65           1-year, 24-hour storm (Peak Flow)         Volume of runoff (ft³) =         82,562         123,982           Volume change (ft³) =         41,420         41,420           Runoff (inches) = Q*=         1.1429         1.6628           Peak Discharge (cfs) = Q =         29.6047         56.7214	T <sub>t</sub> (hrs)=	0.11		0.00			
Site Impervious Surface Area (Ac) =       0.00       5.36         Lot Impervious Surface Area (Ac) =       0.00       3.65         1-year, 24-hour storm (Peak Flow)       0.00       3.65         Volume of runoff (ft³) =       82,562       123,982         Volume change (ft³) =       41,420       1.6628         Runoff (inches) = Q*=       1.1429       1.6628         Peak Discharge (cfs) = Q =       29.6047       56.7214	Tc (hrs)=	0.16		0.08			
Lot Impervious Surface Area (Ac) = 0.00 3.65  1-year, 24-hour storm (Peak Flow)  Volume of runoff (ît³) = 82,562 123,982  Volume change (ît³) = 41,420  Runoff (inches) = Q*= 1.1429 1.6628  Peak Discharge (cfs) = Q = 29.6047 56.7214	RESULTS	PRE-DEVELOR	MENT	POST-DEVELOPMENT			
1-year, 24-hour storm (Peak Flow)       Volume of runoff (ft³) =     82,562     123,982       Volume change (ft³) =     41,420       Runoff (inches) = Q*=     1.1429     1.6628       Peak Discharge (cfs) = Q=     29.6047     56.7214	Site Impervious Surface Area (Ac) =	0.00		5.36			
Volume of runoff (ft³) =     82,562     123,982       Volume change (ft³) =     41,420       Runoff (inches) = Q*=     1.1429     1.6628       Peak Discharge (cfs) = Q=     29.6047     56.7214	Lot Impervious Surface Area (Ac) =	0.00		3.65			
Volume change (ft³) =     41,420       Runoff (inches) = Q*=     1.1429       Peak Discharge (cfs) = Q=     29.6047       56.7214	1-year, 24-hour storm (Peak Flow)						
Runoff (inches) = Q*= 1.1429 1.6628  Peak Discharge (cfs)= Q= 29.6047 56.7214	Volume of runoff (ft <sup>3</sup> ) =	82,562		123,982			
Peak Discharge (cfs)= Q= 29.6047 56.7214	Volume change (ft <sup>3</sup> ) =		41	,420			
	Runoff (inches) = Q*=	1.1429		1.6628			
	Peak Discharge (cfs)= Q=	29.6047		56.7214			
Composite Curve Number (DA)= 78 85	Composite Curve Number (DA)=	78		85			
Composite Curve Number (Site only)= 78 85	Composite Curve Number (Site only)=	78		85			
DISCONNECTED IMPERVIOUS - Credit given only to residential development with drainage area with less than 30% impervious	DISCONNECTED IMPERVIOUS - Credit given onl	y to residential development with drainage a	rea with less than 30% impervious				
Percent Disconnected Impervious Credit (Residential Only) =	Percent Disconnected Impervious Credit (Residentia	ıl Only) =					
Disconnected impervious area (Ac) = 0.00	Disconnected impervious area (Ac) =		0.00				
Drainage Area CN <sub>adjusted</sub> = 85	Drainage Area CN <sub>adjusted</sub> =		85				
Site Only CN <sub>adjusted</sub> = 85	Site Only CN <sub>adjusted</sub> =		85				

Post-development peak flow exceeds pre-development peak flow for this DA!

DA1 Page 5

Project Name:

Parker Ridge



#### DRAINAGE AREA 2 STORMWATER PRE-POST CALCULATIONS

LAND USE & SITE DATA		PRE-DEVELOPMENT								POST-DEVELOPMENT								
Drainage Area (Acres)=		14.36							22.07									
Site Acreage within Drainage=		14.36							22.00									
One-year, 24-hour rainfall (in)=								3.0	3.00									
Land Use (acres) by Soil Group:	AS	Soils	BS	Soils	C S	Soils	DS	ioils		Soils	BS	Soils	C S	oils	D Soils			
Commercial	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite		
Parking lot																		
Roof																		
Open/Landscaped												<u> </u>		<u> </u>				
Industrial	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite		
Parking lot		-		-		-				-		-		-				
Roof																ļ		
Open/Landscaped																<u> </u>		
Transportation	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite		
High Density (interstate, main)	0.10	Onone	0.10	Onone	0.10	Onone	O.LO	Onone	0.10	Onone	0.10	Cilono	Oito	Cilono	O.LO	O.I.O.II.O		
High Density (Grassed Right-of-ways)																<del> </del>		
Low Density (secondary, feeder)												1		1		1		
Low Density (Grassed Right-of-ways)								<del> </del>				1		1				
Rural												<del> </del>		<del> </del>		1		
Rural (Grassed Right-of-ways)																		
Sidewalk		<del> </del>		<del> </del>		<del> </del>				<del> </del>		<del> </del>		<del> </del>		<del> </del>		
Misc. Pervious	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite		
Managed pervious (Open Space)	Oito	Ollono	Oito	Ollono	Oito	Ollono	3.34	Onone	Oito	Ollono	Oito	Onoice	Oito	Onoice	Oito	Onone		
Unmanaged (pasture)							3.34											
Woods (not on lots)							10.66											
Residential	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite		
Roadway	Oite	Olisite	Oite	Olisite	Oite	Olisite	Oite	Olisite	Oite	Olisite	Oite	Olisite	Oite	Olisite	3.02	0.07		
Grassed Right-of-ways															3.02	0.07		
Driveway																		
Parking lot												1		1				
Roof															6.37	<u> </u>		
Sidewalk (Includes Patios)															0.96	<u> </u>		
Lawn															2.89			
Managed pervious (Open Space)								<u>:</u>				<del> </del>		<del> </del>	7.53	<u> </u>		
Woods (on lots)												į		į	1.00	İ		
Land Taken up by BMP															0.87			
JURISDICTIONAL LANDS	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite		
Natural wetland	Sile	Olisite	Sile	Olisite	Sile	Olisite	0.03	Olisite	Site	Olisite	Sile	Olisite	Sile	Olisite	0.03	Olisite		
Riparian buffer (Zone 1 only)							0.03								0.03			
Open water		1		1		1	0.33	!		1		1		1	0.33	-		
Totals (Ac)=	0.00	0.00	0.00	0.00	0.00	0.00	14.36	0.00	0.00	0.00	0.00	0.00	0.00	0.00	22.00	0.07		

DA2 Page 6

SITE FLOW	PRI	E-DEVELOPMENT T <sub>c</sub>	POST-DEVELOPMENT Tc				
Sheet Flow							
Length (ft)=		300.00					
Slope (ft/ft)=		0.02					
Surface Cover:	Pa	ved, Gravel, or Bare Soil					
n-value=		0.01					
T <sub>t</sub> (hrs)=		0.04	0.00				
Shallow Flow							
Length (ft)=		850.00					
Slope (ft/ft)=		0.06					
Surface Cover:		Paved					
Average Velocity (ft/sec)=		4.98	0.00				
T <sub>t</sub> (hrs)=		0.05	0.00				
Channel Flow 1							
Length (ft)=							
Slope (ft/ft)=							
Cross Sectional Flow Area (ft²)=							
Wetted Perimeter (ft)=							
Channel Lining:							
n-value=							
Hydraulic Radius (ft)=		0.00	0.00				
Average Velocity (ft/sec)=		0.00	0.00				
T <sub>t</sub> (hrs)=		0.00	0.00				
Tc (hrs)=		0.09	0.08				
RESULTS	PF	RE-DEVELOPMENT	POST-DEVELOPMENT				
Site Impervious Surface Area (Ac) =		0.00	10.35				
Lot Impervious Surface Area (Ac) =		0.00	7.33				
1-year, 24-hour storm (Peak Flow)							
Volume of runoff (ft³) =		58,131	157,550				
Volume change (ft³) =			419				
Runoff (inches) = Q*=		1.1152	1.9666				
Peak Discharge (cfs)= Q=		25.2653	72.7664				
Composite Curve Number (DA)=		78	88				
Composite Curve Number (Site only)=		78	88				
DISCONNECTED IMPERVIOUS - Credit given only to residential development with drainage area with less than 30% impervious							
Percent Disconnected Impervious Credit (Residenti	al Only) =						
Disconnected impervious area (Ac) =			0.00				
Drainage Area CN <sub>adjusted</sub> =		88					
Site Only CN <sub>adjusted</sub> =		88					

Post-development peak flow exceeds pre-development peak flow for this DA!

DA2 Page 7

Parker Ridge Project Name:

### DRAINAGE AREA 3 STORMWATER PRE-POST CALCULATIONS

LAND USE & SITE DATA			Р	RE-DEVE	LOPME	NT		POST-DEVELOPMENT									
Drainage Area (Acres)=	1	43.94									44.12						
Site Acreage within Drainage=				43	.94				42.42								
One-year, 24-hour rainfall (in)=								3.	3.00								
Land Use (acres) by Soil Group:	Αŝ	Soils	В	Soils	C S	ioils	DS	Soils	AS	Soils	ВЯ	Soils	c s	ioils	DS	Soils	
Commercial	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	
Parking lot																	
Roof		1		1		1		<del> </del>				1		1		!	
Open/Landscaped																	
Industrial	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	
Parking lot						ļ		ļ.									
Roof																	
Open/Landscaped																	
Transportation	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	
High Density (interstate, main)		İ		İ		İ		İ		ļ		İ		İ		ļ	
High Density (Grassed Right-of-ways)		ļ		ļ		İ		ļ				ļ		ļ		ļ	
Low Density (secondary, feeder)						İ											
Low Density (Grassed Right-of-ways)																	
Rural		i		i		İ		i		İ		i		i		İ	
Rural (Grassed Right-of-ways)						İ		1		i						l	
Sidewalk																	
Misc. Pervious	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	
Managed pervious (Open Space)																	
Unmanaged (pasture)						i		i		i						i	
Woods (not on lots)						1	33.72									1	
Residential	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	
Roadway															2.67	1.70	
Grassed Right-of-ways																	
Driveway							0.13										
Parking lot																	
Roof															6.24		
Sidewalk (Includes Patios)															1.49		
Lawn		ļ.		ļ.		!		ļ.		ļ		ļ.		ļ.	3.12	ļ	
Managed pervious (Open Space)															17.96	!	
Woods (on lots)																	
Land Taken up by BMP															1.05	ļ	
JURISDICTIONAL LANDS	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	
Natural wetland						ļ	0.78								0.74	į	
Riparian buffer (Zone 1 only)							5.73								5.57		
Open water							3.58								3.58		
Totals (Ac)=	0.00	0.00	0.00	0.00	0.00	0.00	43.94	0.00	0.00	0.00	0.00	0.00	0.00	0.00	42.42	1.70	

SITE FLOW	PRI	E-DEVELOPMENT T <sub>c</sub>	POST-DEVELOPMENT Tc				
Sheet Flow							
Length (ft)=		300.00					
Slope (ft/ft)=		0.07					
Surface Cover:	Pa	ved, Gravel, or Bare Soil					
n-value=		0.01					
T <sub>t</sub> (hrs)=		0.03	0.00				
Shallow Flow							
Length (ft)=		193.00					
Slope (ft/ft)=		0.04					
Surface Cover:		Paved					
Average Velocity (ft/sec)=		4.22	0.00				
T <sub>t</sub> (hrs)=		0.01	0.00				
Channel Flow 1							
Length (ft)=		500.00					
Slope (ft/ft)=		0.05					
Cross Sectional Flow Area (ft²)=		30.00					
Wetted Perimeter (ft)=		16.00					
Channel Lining:	Gr	avel Bottom/riprap sides					
n-value=		0.03					
Hydraulic Radius (ft)=		1.88	0.00				
Average Velocity (ft/sec)=		15.35	0.00				
T <sub>t</sub> (hrs)=		0.01	0.00				
Tc (hrs)=		0.05	0.08				
RESULTS	PF	RE-DEVELOPMENT	POST-DEVELOPMENT				
Site Impervious Surface Area (Ac) =		0.13	10.40				
Lot Impervious Surface Area (Ac) =		0.13	7.73				
1-year, 24-hour storm (Peak Flow)							
Volume of runoff (ft <sup>3</sup> ) =		122,982	209,900				
Volume change (ft <sup>3</sup> ) =		86	917				
Runoff (inches) = Q*=		0.7710	1.3106				
Peak Discharge (cfs)= Q=		63.4382	95.0684				
Composite Curve Number (DA)=		71	78				
Composite Curve Number (Site only)=		71	78				
DISCONNECTED IMPERVIOUS - Credit given only	y to residential development wi	th drainage area with less than 30% impervious					
Percent Disconnected Impervious Credit (Residentia	ıl Only) =						
Disconnected impervious area (Ac) =		0.00					
Drainage Area CN <sub>adjusted</sub> =		78					
Site Only CN <sub>adjusted</sub> =		78					

Post-development peak flow exceeds pre-development peak flow for this DA!

\*
WAKE
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Project Name:

Parker Ridge

#### <u>DRAINAGE AREA 4</u> <u>STORMWATER PRE-POST CALCULATIONS</u>

LAND USE & SITE DATA			Р	RE-DEVE	LOPME	NT					PC	OST-DEV	ELOPME	NT		
Drainage Area (Acres)=				4.	72							0.	74			
Site Acreage within Drainage=				4.	72							0.	74			
One-year, 24-hour rainfall (in)=								3.0	00							
Land Use (acres) by Soil Group:	A S	Soils	В	Soils	C S	ioils	DS	oils	AS	Soils	В	Soils	c s	ioils	D S	Soils
Commercial	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite
Parking lot				ļ								ļ		ļ		ļ
Roof																
Open/Landscaped																
Industrial	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite
Parking lot																
Roof																
Open/Landscaped						İ				İ						İ
Transportation	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite
High Density (interstate, main)		İ		İ		İ		i		İ		İ		İ		İ
High Density (Grassed Right-of-ways)				İ		İ				İ		İ		İ		į
Low Density (secondary, feeder)				ļ		İ				İ		ļ		ļ		İ
Low Density (Grassed Right-of-ways)																
Rural		İ		ļ		ļ		į		ļ		ļ		ļ		ļ
Rural (Grassed Right-of-ways)		!						İ								
Sidewalk																
Misc. Pervious	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite
Managed pervious (Open Space)																
Unmanaged (pasture)																
Woods (not on lots)							4.52									
Residential	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite
Roadway				1								İ		1		i
Grassed Right-of-ways				İ								İ		İ		İ
Driveway				i		i				i		i		i		i
Parking lot				İ		İ				İ		İ		İ		
Roof				Ì		İ				İ		İ		Ì		İ
Sidewalk (Includes Patios)																
Lawn		İ		ļ				İ				ļ		ļ		Ť T
Managed pervious (Open Space)				!								!		!	0.54	!
Woods (on lots)																
Land Taken up by BMP																
JURISDICTIONAL LANDS	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite
Natural wetland																
Riparian buffer (Zone 1 only)							0.20								0.20	
Open water																
Totals (Ac)=	0.00	0.00	0.00	0.00	0.00	0.00	4.72	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.74	0.00
Totals (AC)-	0.00	0.00	0.00	0.00	0.00	0.00	7.12	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.74	0.00

SITE FLOW	PRE	-DEVELOPMENT T <sub>c</sub>	POST-DEVELOPMENT Tc			
Sheet Flow						
Length (ft)=		300.00				
Slope (ft/ft)=		0.02				
Surface Cover:	Pav	red, Gravel, or Bare Soil				
n-value=		0.01				
T <sub>t</sub> (hrs)=		0.05	0.00			
Shallow Flow						
Length (ft)=		30.00				
Slope (ft/ft)=		0.08				
Surface Cover:		Paved				
Average Velocity (ft/sec)=		5.75	0.00			
T <sub>t</sub> (hrs)=		0.00	0.00			
Channel Flow 1						
Length (ft)=						
Slope (ft/ft)=						
Cross Sectional Flow Area (ft <sup>2</sup> )=						
Wetted Perimeter (ft)=						
Channel Lining:						
n-value=						
Hydraulic Radius (ft)=		0.00	0.00			
Average Velocity (ft/sec)=		0.00	0.00			
T <sub>t</sub> (hrs)=		0.00	0.00			
Tc (hrs)=		0.05	0.08			
RESULTS	PR	RE-DEVELOPMENT	POST-DEVELOPMENT			
Site Impervious Surface Area (Ac) =		0.00	0.00			
Lot Impervious Surface Area (Ac) =		0.00	0.00			
1-year, 24-hour storm (Peak Flow)						
Volume of runoff (ft³) =		18,475	3,358			
Volume change (ft³) =			-15,117			
Runoff (inches) = Q*=		1.0783	1.2500			
Peak Discharge (cfs)= Q=		9.6116	1.5147			
Composite Curve Number (DA)=		77	80			
Composite Curve Number (Site only)=		77	80			
DISCONNECTED IMPERVIOUS - Credit given onl	y to residential development w	rith drainage area with less than 30% im	pervious			
Percent Disconnected Impervious Credit (Residentia						
Disconnected impervious area (Ac) =		0.00				
Drainage Area CN <sub>adjusted</sub> =		80				
Site Only CN <sub>adjusted</sub> =		80				

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Project Name:

Parker Ridge



### DRAINAGE AREA 5 STORMWATER PRE-POST CALCULATIONS

		Р	PRE-DEVELOPMENT POST-DEVELOPMENT												
			2.4	41							1.	12			
			2.4	41							1.	12			
							3.0	00							
AS	Soils	ВЯ	Soils	C S	oils	D.S			Soils	BS	Soils	C S	oils	D.S	Soils
Site	Offsite	Site	Offsite	Site	Offsite			Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite
											1				
Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite
															-
											<u> </u>				
Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite
							1		Ì		1				1
															1
															<del> </del>
							į		į		į				i e
															1
	<del>                                     </del>		<del>                                     </del>		<del>                                     </del>						1		<del>                                     </del>		1
Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite
						2.41									
Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite
							Ì		Ì		Ì				1
							i		i		i				†
							İ		İ		İ				1
	†		†		†						1		†	1.12	1
Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite
0.00	0.00	0.00	0.00	0.00	0.00	2.41	0.00	0.00	0.00	0.00	0.00	0.00	0.00	1.10	0.00
	Site Site Site	Site Offsite  Site Offsite  Site Offsite  Site Offsite  Site Offsite	Site Offsite Site  Site Offsite Site  Site Offsite Site  Site Offsite Site  Site Offsite Site  Site Offsite Site	A Soils B Soils  Site Offsite Site Offsite  Site Offsite Site Offsite  Site Offsite Site Offsite  Site Offsite Site Offsite  Site Offsite Site Offsite  Site Offsite Site Offsite	Site Offsite Site Offsite Site  Site Offsite Site Offsite Site  Site Offsite Site Offsite Site  Site Offsite Site Offsite Site  Site Offsite Site Offsite Site  Site Offsite Site Offsite Site  Site Offsite Site Offsite Site	A Soils  Site Offsite Site Offsite Site Offsite  Site Offsite Site Offsite Site Offsite  Site Offsite Site Offsite Site Offsite  Site Offsite Site Offsite Site Offsite  Site Offsite Site Offsite Site Offsite  Site Offsite Site Offsite Site Offsite  Site Offsite Site Offsite Site Offsite  Site Offsite Site Offsite Site Offsite  Site Offsite Site Offsite Site Offsite	A Solls  B Solls  C Soils  D S  Site Offsite Site Offsite Site Offsite Site  Site Offsite Site Offsite Site Offsite Site  Site Offsite Site Offsite Site Offsite Site  Site Offsite Site Offsite Site Offsite Site  Site Offsite Site Offsite Site Offsite Site  Site Offsite Site Offsite Site Offsite Site  Site Offsite Site Offsite Site Offsite Site  Site Offsite Site Offsite Site Offsite Site  Site Offsite Site Offsite Site Offsite Site Site Site Site Site Site Site S	A Soils B Soils C Soils D Soils  Site Offsite Site Offsite Site Offsite Site Offsite  Site Offsite Site Offsite Site Offsite Site Offsite  Site Offsite Site Offsite Site Offsite Site Offsite  Site Offsite Site Offsite Site Offsite Site Offsite  Site Offsite Site Offsite Site Offsite Site Offsite  Site Offsite Site Offsite Site Offsite Site Offsite  Site Offsite Site Offsite Site Offsite Site Offsite  Site Offsite Site Offsite Site Offsite Site Offsite  Site Offsite Site Offsite Site Offsite Site Offsite	3.00  A Soils B Soils C Soils D Soils A S Site Offsite Site Offsite Site Offsite Site Offsite Site  Site Offsite Site Offsite Site Offsite Site Offsite Site  Site Offsite Site Offsite Site Offsite Site Offsite Site  Site Offsite Site Offsite Site Offsite Site Offsite Site  Site Offsite Site Offsite Site Offsite Site Offsite Site  Site Offsite Site Offsite Site Offsite Site Offsite Site  Site Offsite Site Offsite Site Offsite Site Offsite Site Site  Site Offsite Site Offsite Site Offsite Site Offsite Site Site Site Site Site Site Site S	A Soils B Soils C Soils D Soils A Soils  Site Offsite Site Offsite Site Offsite Site Offsite Site Offsite Site Offsite  Site Offsite Si	A Soils B Soils C Soils D Soils A Soils B Site Offsite Si	A Soils B Soils C Soils D Soils A Soils B Soils  Site Offsite Site Off	A Soils B Soils C Soils D Soils A Soils B Soils C Soils C Soils D Soils A Soils B Soils C Soil	A Soils B Soils C Soils D Soils A Soils B Soils C Soils  Site Offsite	3.00  A Soils B Soils C Soils D Soils A Soils B Soils C Soils D Site Offsite Site O

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SITE FLOW	PRI	E-DEVELOPMENT T <sub>c</sub>	POST-DEVELOPMENT Tc
Sheet Flow			
Length (ft)=		300.00	
Slope (ft/ft)=		0.03	
Surface Cover:	Pa	ved, Gravel, or Bare Soil	
n-value=		0.01	
T <sub>t</sub> (hrs)=		0.04	0.00
Shallow Flow			
Length (ft)=		253.00	
Slope (ft/ft)=		0.02	
Surface Cover:		Unpaved	
Average Velocity (ft/sec)=		2.46	0.00
T <sub>t</sub> (hrs)=		0.03	0.00
Channel Flow 1			
Length (ft)=			
Slope (ft/ft)=			
Cross Sectional Flow Area (ft²)=			
Wetted Perimeter (ft)=			
Channel Lining:			
n-value=	<u> </u>		
Hydraulic Radius (ft)=		0.00	0.00
Average Velocity (ft/sec)=		0.00	0.00
T <sub>t</sub> (hrs)=	<u> </u>	0.00	0.00
Tc (hrs)=		0.07	0.08
RESULTS	PF	RE-DEVELOPMENT	POST-DEVELOPMENT
Site Impervious Surface Area (Ac) =		0.00	0.00
Lot Impervious Surface Area (Ac) =		0.00	0.00
1-year, 24-hour storm (Peak Flow)			
Volume of runoff (ft <sup>3</sup> ) =	<del> </del>	10,935	5,082
Volume change (ft <sup>3</sup> ) =			,853 T
Runoff (inches) = Q*=	<u> </u>	1.2500	1.2500
Peak Discharge (cfs)= Q=		5.2625	2.2926
Composite Curve Number (DA)=	<u> </u>	80	80
Composite Curve Number (Site only)=		80	80
DISCONNECTED IMPERVIOUS - Credit given on	ly to residential development v	with drainage area with less than 30% impervious	
Percent Disconnected Impervious Credit (Residentia	al Only) =		
Disconnected impervious area (Ac) =			0.00
Drainage Area CN <sub>adjusted</sub> =			80
Site Only CN <sub>adjusted</sub> =			80

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Project Name:

Parker Ridge



### DRAINAGE AREA 6 STORMWATER PRE-POST CALCULATIONS

LAND USE & SITE DATA			Р	RE-DEVE	LOPME	NT					PC	ST-DEVI	ELOPME	NT		
Drainage Area (Acres)=				1.6	60							0.	70			
Site Acreage within Drainage=				1.6	60							0.	70			
One-year, 24-hour rainfall (in)=								3.	00							
Land Use (acres) by Soil Group:	AS	Soils	В	Soils	C S	Soils	DS	Soils	AS	Soils	В	Soils	C S	ioils	DS	Soils
Commercial	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite
Parking lot																
Roof																
Open/Landscaped						1										
Industrial	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite
Parking lot																
Roof						1		1				1		1		1
Open/Landscaped																
Transportation	Site	Site Offsite Site Offsite Site Offsite Site Offsite Site Offsite Site Offsite Site Offsite								Offsite	Site	Offsite				
High Density (interstate, main)		i		i		İ		İ				İ		İ		İ
High Density (Grassed Right-of-ways)																
Low Density (secondary, feeder)						Ì		Ì		Ì		Ì		Ì		Ì
Low Density (Grassed Right-of-ways)		į				İ		ļ		ļ		ļ		ļ		ļ
Rural		ļ														
Rural (Grassed Right-of-ways)																
Sidewalk						1										
Misc. Pervious	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite
Managed pervious (Open Space)							1.60									
Unmanaged (pasture)																
Woods (not on lots)								İ								
Residential	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite
Roadway						1		1				1		1		1
Grassed Right-of-ways																
Driveway						į										
Parking lot		j .				į		ļ				ļ		ļ		ļ
Roof																
Sidewalk (Includes Patios)						ļ										
Lawn		1														
Managed pervious (Open Space)						}									0.70	
Woods (on lots)																
Land Taken up by BMP																
JURISDICTIONAL LANDS	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite
Natural wetland																
Riparian buffer (Zone 1 only)																
Open water																
Totals (Ac)=	0.00	0.00	0.00	0.00	0.00	0.00	1.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.70	0.00

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SITE FLOW	PRI	E-DEVELOPMENT T <sub>c</sub>	POST-DEVELOPMENT Tc				
Sheet Flow							
Length (ft)=		146.00					
Slope (ft/ft)=		0.03					
Surface Cover:	Par	ved, Gravel, or Bare Soil					
n-value=		0.01					
T <sub>t</sub> (hrs)=		0.02	0.00				
Shallow Flow							
Length (ft)=		437.00					
Slope (ft/ft)=		0.02					
Surface Cover:		Unpaved					
Average Velocity (ft/sec)=		2.47	0.00				
$T_t$ (hrs)=	<u> </u>	0.05	0.00				
Channel Flow 1							
Length (ft)=							
Slope (ft/ft)=							
Cross Sectional Flow Area (ft²)=							
Wetted Perimeter (ft)=							
Channel Lining:							
n-value=							
Hydraulic Radius (ft)=		0.00	0.00				
Average Velocity (ft/sec)=		0.00	0.00				
T <sub>t</sub> (hrs)=		0.00	0.00				
Tc (hrs)=		0.07	0.08				
RESULTS	PF	RE-DEVELOPMENT	POST-DEVELOPMENT				
Site Impervious Surface Area (Ac) =		0.00	0.00				
Lot Impervious Surface Area (Ac) =		0.00	0.00				
1-year, 24-hour storm (Peak Flow)							
Volume of runoff (ft <sup>3</sup> ) =		7,260	3,176				
Volume change (ft³) =		-4,	.084				
Runoff (inches) = Q*=		1.2500	1.2500				
Peak Discharge (cfs)= Q=		3.4358	1.4329				
Composite Curve Number (DA)=		80	80				
Composite Curve Number (Site only)=		80	80				
DISCONNECTED IMPERVIOUS - Credit given on	ly to residential development v	vith drainage area with less than 30% impervious					
Percent Disconnected Impervious Credit (Residentia	al Only) =						
Disconnected impervious area (Ac) =			0.00				
Drainage Area CN <sub>adjusted</sub> =		80					
Site Only CN <sub>adjusted</sub> =			80				

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Project Name: Parker Ridge

### DA SITE SUMMARY STORMWATER PRE-POST CALCULATIONS

SITE SUMMARY								
DRAINAGE AREA SUMMARIES								
DRAINAGE AREA:	DA1	DA2	DA3	DA4	DA5	DA6		
Pre-Development (1-year, 24-hour storm)								
Runoff (in)=Q* =	1.143	1.115	0.771	1.078	1.250	1.250		
Peak Flow (cfs)=Q <sub>post</sub> =	29.605	25.265	63.438	9.612	5.263	3.436		
Post-Development (1-year, 24-hour storm)								
Proposed Impervious Surface (acre) =	5.36	10.35	10.40					
Runoff (in)=Q* =	1.663	1.967	1.311	1.250	1.250	1.250		
Peak Flow (cfs)=Q <sub>post</sub> =	56.721	72.766	95.068	1.515	2.293	1.433		
TARGET CURVE NUMBER (TCN) - Residential Only								
SITE \SOIL COMPOSITION			_					
HYDROLOGIC SOIL GROUP	Site	e Area	9	<u>6</u>	<u>Targe</u>	et CN		
А	(	0.00	0	%	4	<u>3</u>		
В	(	0.00	0	%	6	3		
С	(	0.00	0	%	7	<u>6</u>		
D	87.27 100			0%	<u>1</u>			
Total Site Area (acres) =								
Zoning =			R-5	5				
Target Curve Number (TCN) =								
% Impervious =								
Post Development CN <sub>adjusted</sub> =	= 82							
Required Volume to be Managed (TCN)= ft <sup>3</sup> =	= 22,290							
SITE NITROGEN AND PHOSPHORUS LOADING								
Nitrogen and Phosphorus Targets (Based on Regulatory Watershed)								
Target Nitrogen Load (lb/ac/yr)=			3.6	1				
Target Phosphorus Load (Falls and Jordan Lakes Only) (lb/ac/yr)=			N/A	١				
% N Loading Reduction Option for Expansions ( <u>Falls and Jordan Lakes Only</u> ) =			N/A	١				
% Loading Reduction Nitrogen Target ( <u>Falls and Jordan Lakes Only</u> ) (lb/ac/yr)=			N/A	١				
% P Loading Reduction Option for Expansions ( <u>Falls and Jordan Lakes Only</u> ) =	= N/A							
% Loading Reduction Phosphorus Target ( <u>Falls and Jordan Lakes Only</u> ) (lb/ac/yr)=			N/A	<b>\</b>				
Pre Development Nitrogen and Phosphorus Load								
Total Nitrogen (lb/ac/yr)=			0.89					
Total Phosphorus (lb/ac/yr)=			N/A	1				
Post Development Nitrogen and Phosphorus Load								
Total Nitrogen (lb/ac/yr)=			4.89					
Total Phosphorus (lb/ac/yr)=			N/A	١				

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WAKE COUNTY

Project Name:

Parker Ridge

### DRAINAGE AREA 1 BMP CALCULATIONS

DRAINAGE AREA 1 - BMP DEVICES	AND ADJUSTMENTS											
DA1 Site Acreage=					20.29							
DA1 Off-Site Acreage=					0.25							
Total Required Storage Volume for Site					22.200							
TCN Requirement (ft <sup>3</sup> )=					22,290							
Will site use underground water harvesting?	No	Enter %	volume re deci	eduction in mal form=					submitte	formation/ d to demo		
ENTER AREA <u>TREATED BY BMP</u>												
Land Use (acres)	)		DA1(a) Ac)		DA1(b) (c)	1	0A1(c) .c)		Sub-DA1(d) (Ac)		·DA1(e) Ac)	
Commercial		Site	Off-site	Site	Off-site	Site	Off-site	Site	Off-site	Site	Off-site	
Parking lot												
Roof					<u> </u>							
Open/Landscaped												
Industrial		Site	Off-site	Site	Off-site	Site	Off-site	Site	Off-site	Site	Off-site	
Parking lot												
Roof					İ				j		<u> </u>	
Open/Landscaped			i								i	
Transportation		Site	Off-site	Site	Off-site	Site	Off-site	Site	Off-site	Site	Off-site	
High Density (interstate, main)		0.1.0	On one	00	On one	0.10	011 0110	0.1.0	011 0110	0.10	0 0	
High Density (Grassed Right-of-ways)					i				i			
Low Density (secondary, feeder)												
Low Density (Grassed Right-of-ways)												
Rural			<u> </u>		-							
Rural (Grassed Right-of-ways)			<u> </u>		<u> </u>				<u> </u>		<del> </del>	
Sidewalk												
Misc. Pervious		Site	Off-site	Site	Off-site	Site	Off-site	Site	Off-site	Site	Off-site	
Managed pervious												
Unmanaged (pasture)			i e								İ	
Woods (not on lots)												
Residential		Site	Off-site	Site	Off-site	Site	Off-site	Site	Off-site	Site	Off-site	
		1.64	0.24	0.07	OII-3IIC	Oile	OII-3IIC	Oile	Oll-Site	Oile	OII-3ILC	
Roadway Grassed Right-of-ways		1.04	0.24	0.07	<u> </u>				<u> </u>			
Driveway  Parking let			<u> </u>		<u> </u> 				<u> </u>		<u> </u>	
Parking lot Roof		2.75									<u> </u>	
Sidewalk		0.50	-	0.40								
Lawn		1.10		0.40							•	
Managed pervious		2.52	0.01	6.27	! !				<u>.                                    </u>		1	
Woods (on lots)		2.02	i 0.01	0.21							i	
Land Taken up by BMP		0.46	-		! 				! 			
JURISDICTIONAL LANDS		Site	Off-site	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	
Natural wetland				0.12	555		20.1.0	_,,,	255		255	
Riparian buffer (Zone 1 only)				4.04								
	Totals (Ac)=	8.97	0.25	10.90	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
Sub-DA1(a) BMP(s)												
Device Name (As Shown on Plan)	Device Type	Water Quality	Inflow N EMC	Total Inflow N	Inflow P	Total Inflow P	Outflow N EMC	Total Outflow	Outflow P EMC	Total Outflow	Provided Volume	
Device Haine (AS SHOWN ON Flatt)	Device Type	Volume (c.f.)	(mg/L)	(lb/ac/yr)	(mg/L)	(lb/ac/yr)	(mg/L)	N (lb/ac/yr)	(mg/L)	P (lb/ac/yr)	Managed (c.f.)	
SCM 1	Wet Detention Pond		1.26	7.66	0.36	2.20	1.04	5.65	0.14	0.77	85,659	
		18,433										
		10,400										
Outfle	ow Total Nitrogen (lb/ac/yr)=	5.	.65			Outflov	/ Total Ph	osphorus	(lb/ac/yr)=	0	.77	
Sub-DA1(b) BMP(s)												

If Sub-DA1(b) is connected to upstream sub-	basin(s), select all contributir	ıg sub-bas	in(s from								
dropdown menus):  Device Name (As Shown on Plan)	Device Type	Water Quality Volume (c.f.)	Inflow N EMC (mg/L)	Total Inflow N (lb/ac/yr)	Inflow P EMC (mg/L)	Total Inflow P (lb/ac/yr)	Outflow N EMC (mg/L)	Total Outflow N (lb/ac/yr)	Outflow P EMC (mg/L)	Total Outflow P (lb/ac/yr)	Provided Volume Managed (c.f.)
		` '		1.78		0.67					` '
Bypass #1		2,759									
		2,.00									
0.49	T ( 1 )					0.15	T DI				
Sub-DA1 (c) BMP(s)	ow Total Nitrogen (lb/ac/yr)=					Outriow	/ Total Ph	osphorus (	ib/ac/yr)=		
If Sub-DA1(c) is connected to upstream sub-l	hasin(s) select all contributin	a suh-has	in(s):								
Device Name (As Shown on Plan)	Device Type	Water Quality Volume (c.f.)	Inflow N EMC (mg/L)	Total Inflow N (lb/ac/yr)	Inflow P EMC (mg/L)	Total Inflow P (lb/ac/yr)	Outflow N EMC (mg/L)	Total Outflow N (lb/ac/yr)	Outflow P EMC (mg/L)	Total Outflow P (lb/ac/yr)	Provided Volume Managed (c.f.)
										_	
Outfl	ow Total Nitrogen (lb/ac/yr)=					Outflow	Total Ph	osphorus (	lb/ac/yr)=		
Sub-DA1 (d) BMP(s)				ı							
If Sub-DA1(d) is connected to upstream sub-	basin(s), select all contributir	g sub-bas	sin(s):								
Device Name (As Shown on Plan)	Device Type	Water Quality Volume (c.f.)	Inflow N EMC (mg/L)	Total Inflow N (lb/ac/yr)	Inflow P EMC (mg/L)	Total Inflow P (lb/ac/yr)	Outflow N EMC (mg/L)	Total Outflow N (lb/ac/yr)	Outflow P EMC (mg/L)	Total Outflow P (lb/ac/yr)	Provided Volume Managed (c.f.)
Outfl	ow Total Nitrogen (lb/ac/yr)=		I			Outflow	/ Total Ph	osphorus (	lb/ac/yr)=		
Sub-DA1 (e) BMP(s)									• • •		
If Sub-DA1(e) is connected to upstream sub-	basin(s), select all contributir	ıg sub-bas	sin(s):								
Device Name (As Shown on Plan)	Device Type	Water Quality Volume (c.f.)	Inflow N EMC (mg/L)	Total Inflow N (lb/ac/yr)		Total Inflow P (lb/ac/yr)	Outflow N EMC (mg/L)	Total Outflow N (lb/ac/yr)	Outflow P EMC (mg/L)	Total Outflow P (lb/ac/yr)	Provided Volume Managed (c.f.)
Outfl	ow Total Nitrogen (lb/ac/yr)=					Outflow	Total Ph	osphorus (	lb/ac/yr)=		
		DA1 BN	IP SUMI	MARY							
	Total Volume Treated (c.f.)=					85	659				
DA1 Outfl	ow Total Nitrogen (lb/ac/yr)=					5.	65				
DA1 Outflow	Total Phosphorus (lb/ac/yr)=					0.	77				
1-year, 24-hour storm											
Pre Development Pe	eak Discharge (cfs)= Q <sub>1-year</sub> =					29	.60				
Post BMP Pe	eak Discharge (cfs)= Q <sub>1-year</sub> =	Q <sub>1-year</sub> = 16.85									

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WAKE

Project Name:

Parker Ridge

### DRAINAGE AREA 2 BMP CALCULATIONS

DRAINAGE AREA 2 - BMP DEVICES AND ADJUSTMENTS DA2 Site Acreage= 22.00 DA2 Off-Site Acreage= 0.07 Total Required Storage Volume for Site 22,290 TCN Requirement (ft3)= Note: Supporting information/details Enter % volume reduction in Will site use underground water harvesting? No should be submitted to demonstrate decimal form water usage. ENTER AREA TREATED BY BMP Sub-DA2(a) Sub-DA2(b) Sub-DA2(c) Sub-DA2(d) Sub-DA2(e) Land Use (acres) (Ac) (Ac) (Ac) (Ac) (Ac) Off-site Site Off-site Off-site Site Site Off-site Off-site Commercial Site Site Parking lot Roof Open/Landscaped Site Site Off-site Off-site Off-site Off-site Off-site ndustrial Site Site Site Parking lot Roof Open/Landscaped Site Off-site Off-site Off-site Site Off-site Off-site Transportation High Density (interstate, main) High Density (Grassed Right-of-ways) Low Density (secondary, feeder) Low Density (Grassed Right-of-ways) Rural Rural (Grassed Right-of-ways) Sidewalk Misc. Pervious Site Off-site Site Off-site Site Off-site Site Off-site Off-site Managed pervious Unmanaged (pasture) Woods (not on lots) Site Off-site Off-site Off-site Site Off-site Off-site Residential Site Site Roadway 3.02 0.07 Grassed Right-of-ways Driveway Parking lot Roof 6.37 Sidewalk 0.96 Lawn 2.89 Managed pervious 6.00 1.53 Woods (on lots) 0.87 and Taken up by BMP JURISDICTIONAL LANDS Site Off-site Site Offsite Site Offsite Site Offsite Offsite Natural wetland 0.03 Riparian buffer (Zone 1 only) 0.33 Totals (Ac)= 20.14 0.07 1.86 0.00 0.00 0.00 0.00 0.00 0.00 0.00 Sub-DA2(a) BMP(s) Water Provided Total Total Inflow N Outflow Outflow Total Inflow P Total Quality Outflow Outflow Volume Inflow P Device Type N EMC P EMC Device Name (As Shown on Plan) **EMC** Inflow N EMC Volume Ν Р Manageo (lb/ac/vr) (mg/L) (lb/ac/yr) (mg/L) (mg/L) (mg/L) (c.f.) lb/ac/yr (lb/ac/yr) (c.f.) Wet Detention Pond 1.26 7.16 0.34 1.96 1.04 5.31 0.14 174,865 37,705 Outflow Total Nitrogen (lb/ac/yr)= 5.31 Outflow Total Phosphorus (lb/ac/yr)= 0.71 Sub-DA2(b) BMP(s)

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If Sub-DA2(b) is connected to upstream sub-	basin(s), select all contributir	ng sub-bas	in(s from								
dropdown menus):		Water	Inflow N	Total	Inflow P	Total	Outflow	Total	Outflow	Total	Provided
Device Name (As Shown on Plan)	Device Type	Quality Volume (c.f.)	EMC (mg/L)	Inflow N (lb/ac/yr)	EMC (mg/L)	Inflow P (lb/ac/yr)	N EMC (mg/L)	Outflow N (lb/ac/yr)	P EMC (mg/L)	Outflow P (lb/ac/yr)	Volume Managed (c.f.)
Bypasss #2				1.43		0.27					
3)pacco #2		278									
Outfl	I ow Total Nitrogen (lb/ac/yr)=					Outflow	Total Ph	osphorus (	(lb/ac/yr)=		
Sub-DA2 (c) BMP(s)									• • •		
If Sub-DA2(c) is connected to upstream sub-l	pasin(s), select all contributin	ıa sub-bas	in(s):								
Device Name (As Shown on Plan)	Device Type	Water Quality Volume (c.f.)	Inflow N EMC (mg/L)	Total Inflow N (lb/ac/yr)	Inflow P EMC (mg/L)	Total Inflow P (lb/ac/yr)	Outflow N EMC (mg/L)	Total Outflow N (lb/ac/yr)	Outflow P EMC (mg/L)	Total Outflow P (lb/ac/yr)	Provided Volume Managed (c.f.)
Outfl	I ow Total Nitrogen (lb/ac/yr)=					Outflow	Total Ph	osphorus (	(lb/ac/yr)=		
Sub-DA2 (d) BMP(s)									• • •		
If Sub-DA2(d) is connected to upstream sub-	basin(s), select all contributir	ıg sub-bas	sin(s):								
Device Name (As Shown on Plan)	Device Type	Water Quality	Inflow N EMC	Total Inflow N	Inflow P	Total Inflow P	Outflow N EMC	Total Outflow	Outflow P EMC	Total Outflow	Provided Volume
		Volume (c.f.)	(mg/L)	(lb/ac/yr)	(mg/L)	(lb/ac/yr)	(mg/L)	N (lb/ac/yr)	(mg/L)	P (lb/ac/yr)	Managed (c.f.)
Outfl	ow Total Nitrogen (lb/ac/yr)=					Outflow	Total Ph	osphorus (	(lb/ac/yr)=		
Sub-DA2 (e) BMP(s)											
If Sub-DA2(e) is connected to upstream sub-	basin(s), select all contributir	ıg sub-bas	sin(s):								
Device Name (As Shown on Plan)	Device Type	Water Quality Volume (c.f.)	Inflow N EMC (mg/L)	Total Inflow N (lb/ac/yr)		Total Inflow P (lb/ac/yr)	Outflow N EMC (mg/L)	Total Outflow N (lb/ac/yr)	Outflow P EMC (mg/L)	Total Outflow P (lb/ac/yr)	Provided Volume Managed (c.f.)
Outfl	ow Total Nitrogen (lb/ac/yr)=					Outflow	Total Ph	osphorus (	(lb/ac/yr)=		
		DA2 BN	IP SUMI	MARY							
	Total Volume Treated (c.f.)=					174	1865				
DA2 Outfl	ow Total Nitrogen (lb/ac/yr)=					5.	31				
DA2 Outflow	Total Phosphorus (lb/ac/yr)=					0.	71				
1-year, 24-hour storm		1									
Pre Development Pe	eak Discharge (cfs)= Q <sub>1-year</sub> =					25	.27				
Post BMP Pe	k Discharge (cfs)= Q <sub>1-year</sub> = 3.46										

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Project Name:

Parker Ridge

# DRAINAGE AREA 3 BMP CALCULATIONS

DRAINAGE AREA 3 - BMP DEVICES	AND ADJUSTMENTS											
	AND ADJUSTINIENTS				40.40							
DA3 Site Acreage=					42.42							
DA3 Off-Site Acreage=					1.70							
Total Required Storage Volume for Site TCN Requirement (ft³)=					22,290	)						
Will site use underground water harvesting?	No	Enter %	volume re deci	duction in mal form=					submitte		ormation/details I to demonstrate	
ENTER AREA TREATED BY BMP												
Land Use (acres)	)		DA3(a) ac)		DA3(b) Ac)	Sub-DA3(c) (Ac) Site Off-site			DA3(d) ac)		DA3(e) Ac)	
Commercial		Site	Off-site	Site	Off-site	Site	Off-site	Site	Off-site	Site	Off-site	
Parking lot												
Roof					!						ļ	
Open/Landscaped												
Industrial		Site	Off-site	Site	Off-site	Site	Off-site	Site	Off-site	Site	Off-site	
Parking lot							į					
Roof					İ						į	
Open/Landscaped					<u> </u>						<u> </u>	
Transportation		Site	Off-site	Site	Off-site	Site	Off-site	Site	Off-site	Site	Off-site	
High Density (interstate, main)							į					
High Density (Grassed Right-of-ways)			İ		i		İ		İ		į	
Low Density (secondary, feeder)			İ				İ		İ			
Low Density (Grassed Right-of-ways)			i		<u> </u>		i		i		<u> </u>	
Rural							<u> </u>					
Rural (Grassed Right-of-ways)												
Sidewalk					!						<u> </u>	
Misc. Pervious		Site	Off-site	Site	Off-site	Site	Off-site	Site	Off-site	Site	Off-site	
Managed pervious			!				!		!			
Unmanaged (pasture)					!		ļ 				ļ	
Woods (not on lots)			!		!		!		!		!	
Residential		Site	Off-site	Site	Off-site	Site	Off-site	Site	Off-site	Site	Off-site	
Roadway		1.49	1.70	0.98	!	0.20	ļ		İ		!	
Grassed Right-of-ways			į		<u> </u>		<u> </u>		į		<u> </u>	
Driveway			<u> </u>		<u> </u>		<u> </u>		<u> </u>		<u> </u>	
Parking lot			<u> </u>		<u> </u>		<u> </u>		<u> </u>		<u> </u>	
Roof		2.52	ļ	3.12	<u> </u>	0.60	ļ		ļ		ļ	
Sidewalk		0.52	<u> </u>	0.35	<u> </u>	0.62	<u> </u>		<u> </u>		<u> </u>	
Lawn		1.26	; 	1.56	: 	0.30	; 		; 		: 	
Managed pervious		4.06	<u> </u>	3.51	<u> </u>	10.39	<u>:</u>		<u> </u>		<u> </u>	
Woods (on lots)		0.49	i	0.56			i		i			
Land Taken up by BMP JURISDICTIONAL LANDS		Site	Off-site	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	
Natural wetland		Oito	OII OILO	Oilo	Onoito	0.74	Onone	Oilo	Onoice	Oito	Onone	
Riparian buffer (Zone 1 only)			! !			5.57	! :		! !		<u> </u>	
	Totals (Ac)=	10.34	1.70	10.08	0.00	18.42	0.00	0.00	0.00	0.00	0.00	
Sub-DA3(a) BMP(s)	. ,				,							
, , , ,		1,47										
Device Name (As Shown on Plan)	Device Type	Water Quality Volume (c.f.)	Inflow N EMC (mg/L)	Total Inflow N (lb/ac/yr)	Inflow P EMC (mg/L)	Total Inflow P (lb/ac/yr)	Outflow N EMC (mg/L)	Total Outflow N (lb/ac/yr)	Outflow P EMC (mg/L)	Total Outflow P (lb/ac/yr)	Provided Volume Managed (c.f.)	
SCM 3	Wet Detention Pond		1.29	6.52	0.37	1.88	1.04	4.71	0.14	0.64	101,479	
		22,539										
Outflo	ow Total Nitrogen (lb/ac/yr)=	4.	71		<u>I</u>	Outflov	v Total Ph	osphorus (	(lb/ac/yr)=	0	.64	
	3 ( 37											
Sub-DA3(b) BMP(s)												

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If Sub-DA3(b) is connected to upstream sub-	pasin(s), select all contributin	ıg sub-bas	in(s from								
dropdown menus):  Device Name (As Shown on Plan)	Device Type	Water Quality Volume (c.f.)	Inflow N EMC (mg/L)	Total Inflow N (lb/ac/yr)	Inflow P EMC (mg/L)	Total Inflow P (lb/ac/yr)	Outflow N EMC (mg/L)	Total Outflow N (lb/ac/yr)	Outflow P EMC (mg/L)	Total Outflow P (lb/ac/yr)	Provided Volume Managed (c.f.)
SCM 4	Wet Detention Pond		1.25	6.42	0.30	1.57	1.04	4.79	0.13	0.62	109,845
50M 4		16,368									
Outfle	ow Total Nitrogen (lb/ac/yr)=	4.	79			Outflow	Total Ph	osphorus (	(lb/ac/yr)=	0.	.62
Sub-DA3 (c) BMP(s)											
If Sub-DA3(c) is connected to upstream sub-b	pasin(s) select all contributin	ın sub-bas	in(s)·								
Device Name (As Shown on Plan)	Device Type	Water Quality Volume (c.f.)	Inflow N EMC (mg/L)	Total Inflow N (lb/ac/yr)	Inflow P EMC (mg/L)	Total Inflow P (lb/ac/yr)	Outflow N EMC (mg/L)	Total Outflow N (lb/ac/yr)	Outflow P EMC (mg/L)	Total Outflow P (lb/ac/yr)	Provided Volume Managed (c.f.)
Bypass #3				2.12		0.70					
,		6,837									
Outflo	ow Total Nitrogen (lb/ac/yr)=					Outflow	Total Ph	osphorus (	(lb/ac/yr)=		
Sub-DA3 (d) BMP(s)		l.								l.	
If Sub-DA3(d) is connected to upstream sub-t	pasin(s), select all contributin	ıg sub-bas	in(s):								
Device Name (As Shown on Plan)	Device Type	Water Quality Volume (c.f.)	Inflow N EMC (mg/L)	Total Inflow N (lb/ac/yr)	Inflow P EMC (mg/L)	Total Inflow P (lb/ac/yr)	Outflow N EMC (mg/L)	Total Outflow N (lb/ac/yr)	Outflow P EMC (mg/L)	Total Outflow P (lb/ac/yr)	Provided Volume Managed (c.f.)
Outflo	ow Total Nitrogen (lb/ac/yr)=					Outflow	/ Total Ph	osphorus (	(lb/ac/yr)=		
Sub-DA3 (e) BMP(s)											
If Sub-DA3(e) is connected to upstream sub-t	pasin(s), select all contributin	ıg sub-bas	in(s):								
Device Name (As Shown on Plan)	Device Type	Water Quality Volume (c.f.)	Inflow N EMC (mg/L)	Total Inflow N (lb/ac/yr)		Total Inflow P (lb/ac/yr)	Outflow N EMC (mg/L)	Total Outflow N (lb/ac/yr)	Outflow P EMC (mg/L)	Total Outflow P (lb/ac/yr)	Provided Volume Managed (c.f.)
Outfle	ow Total Nitrogen (lb/ac/yr)=					Outflow	Total Ph	osphorus (	(lb/ac/yr)=		
		DA3 BN	IP SUMI	MARY							
	Total Volume Treated (c.f.)=					21	1324				
DA3 Outfle	ow Total Nitrogen (lb/ac/yr)=					4.	79				
DA3 Outflow	Total Phosphorus (lb/ac/yr)=					0.	62				
1-year, 24-hour storm											
Pre Development Pe	eak Discharge (cfs)= Q <sub>1-year</sub> =					63	.44				
Post BMP Pe	Post BMP Peak Discharge (cfs)= Q <sub>1-year</sub> = 34.43										

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WAKE COUNTY

Project Name:	

Parker Ridge

### DRAINAGE AREA 4 BMP CALCULATIONS

DRAINAGE AREA 4 - BMP DEVICES AND ADJUSTMENTS DA4 Site Acreage= 0.74 DA4 Off-Site Acreage= 0.00 Total Required Storage Volume for Site 22,290 TCN Requirement (ft3)= Note: Supporting information/details Enter % volume reduction in Will site use underground water harvesting? should be submitted to demonstrate decimal form water usage. ENTER AREA TREATED BY BMP Sub-DA4(a) Sub-DA4(b) Sub-DA4(c) Sub-DA4(d) Sub-DA4(e) Land Use (acres) (Ac) (Ac) (Ac) (Ac) (Ac) Off-site Off-site Off-site Site Off-site Site Site Off-site Site Commercial Site Parking lot Roof Open/Landscaped Site Site Off-site Off-site Off-site Off-site Off-site ndustrial Site Site Site Parking lot Roof Open/Landscaped Transportation Site Off-site Off-site Off-site Site Off-site Off-site High Density (interstate, main) High Density (Grassed Right-of-ways) Low Density (secondary, feeder) Low Density (Grassed Right-of-ways) Rural Rural (Grassed Right-of-ways) Sidewalk Misc. Pervious Site Off-site Site Off-site Site Off-site Site Off-site Off-site Managed pervious Unmanaged (pasture) Woods (not on lots) Site Off-site Off-site Off-site Site Off-site Off-site Residential Site Site Roadway Grassed Right-of-ways Driveway Parking lot Roof Sidewalk Lawn Managed pervious Woods (on lots) and Taken up by BMP JURISDICTIONAL LANDS Site Off-site Site Offsite Site Offsite Site Offsite Offsite Natural wetland Riparian buffer (Zone 1 only) Totals (Ac)= 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 Sub-DA4(a) BMP(s) Water Provided Total Total Outflow Outflow Inflow N Total Inflow P Total Quality Outflow Outflow Volume Inflow P N EMC P EMC Device Name (As Shown on Plan) Device Type EMC Inflow N EMC Volume Ν Ρ Manageo (lb/ac/yr) (mg/L) (lb/ac/yr) (mg/L) (mg/L) (mg/L) (c.f.) (lb/ac/yr (lb/ac/yr) (c.f.) Outflow Total Nitrogen (lb/ac/yr)= Outflow Total Phosphorus (lb/ac/yr)= Sub-DA4(b) BMP(s)

If Sub-DA4(b) is connected to upstream sub-l	pasin(s), select all contributing	g sub-bas	in(s from								
dropdown menus):  Device Name (As Shown on Plan)	Device Type	Water Quality Volume (c.f.)	Inflow N EMC (mg/L)	Total Inflow N (lb/ac/yr)	Inflow P EMC (mg/L)	Total Inflow P (lb/ac/yr)	Outflow N EMC (mg/L)	Total Outflow N (lb/ac/yr)	Outflow P EMC (mg/L)	Total Outflow P (lb/ac/yr)	Provided Volume Managed (c.f.)
Outfl	ow Total Nitrogen (lb/ac/yr)=					Outflow	Total Pho	osphorus (	(lb/ac/yr)=		
Sub-DA4 (c) BMP(s)											
If Sub-DA4(c) is connected to upstream sub-l	pasin(s), select all contributin	g sub-bas	in(s):								
Device Name (As Shown on Plan)	Device Type	Water Quality Volume (c.f.)	Inflow N EMC (mg/L)	Total Inflow N (lb/ac/yr)	Inflow P EMC (mg/L)	Total Inflow P (lb/ac/yr)	Outflow N EMC (mg/L)	Total Outflow N (lb/ac/yr)	Outflow P EMC (mg/L)	Total Outflow P (lb/ac/yr)	Provided Volume Managed (c.f.)
Outfl	ow Total Nitrogen (lb/ac/yr)=					Outflow	Total Pho	osphorus (	(lb/ac/yr)=		
Sub-DA4 (d) BMP(s)										I.	
If Sub-DA4(d) is connected to upstream sub-l	pasin(s), select all contributing	g sub-bas	in(s):								
Device Name (As Shown on Plan)	Device Type	Water Quality Volume (c.f.)	Inflow N EMC (mg/L)	Total Inflow N (lb/ac/yr)	Inflow P EMC (mg/L)	Total Inflow P (lb/ac/yr)	Outflow N EMC (mg/L)	Total Outflow N (lb/ac/yr)	Outflow P EMC (mg/L)	Total Outflow P (lb/ac/yr)	Provided Volume Managed (c.f.)
Outfl	ow Total Nitrogen (lb/ac/yr)=					Outflow	Total Ph	osphorus (	(lb/ac/vr)=		
Sub-DA4 (e) BMP(s)	ow rotal maggin (ib/do/yr)					Outilovi	Totalii	- Coprior do 1	(ID/GO/y1)		
If Sub-DA4(e) is connected to upstream sub-l	agein(s) select all contributin	ia eub bae	in(e):								
Device Name (As Shown on Plan)	Device Type	Water Quality Volume (c.f.)	Inflow N EMC	Total Inflow N (lb/ac/yr)		Total Inflow P (lb/ac/yr)	Outflow N EMC (mg/L)	Total Outflow N (lb/ac/yr)	Outflow P EMC (mg/L)	Total Outflow P (lb/ac/yr)	Provided Volume Managed (c.f.)
Outfl	ow Total Nitrogen (lb/ac/yr)=		1		1	Outflow	Total Pho	osphorus (	(lb/ac/yr)=		
		DA4 BN	IP SUMI	MARY						<u> </u>	
	Total Volume Treated (c.f.)=						0				
DA4 Outfle	ow Total Nitrogen (lb/ac/yr)=										
	Total Phosphorus (lb/ac/yr)=										
1-year, 24-hour storm											
	eak Discharge (cfs)= Q <sub>1-year</sub> =					9.	61				
	eak Discharge (cfs)= Q <sub>1-year</sub> =						51				
	3 ( / i-year										

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WAKE COUNTY

Project Name:

Parker Ridge

### DRAINAGE AREA 5 BMP CALCULATIONS

DRAINAGE AREA 5 - BMP DEVICES	AND ADJUSTMENTS											
DA5 Site Acreage=		1.12										
DA5 Off-Site Acreage=					0.00							
Total Required Storage Volume for Site TCN Requirement (ft³)=					22,290							
Will site use underground water harvesting?	Enter % volume reduction in decimal form=											
ENTER AREA TREATED BY BMP								ı.				
Land Use (acres)	)		DA5(a)	Sub-D	DA5(b) Sub-DA5(c) Ac) (Ac)			Sub-DA5(d) (Ac)			DA5(e) Ac)	
Commercial		Site	Off-site	Site	Off-site	Site	Off-site	Site	Off-site	Site	Off-site	
Parking lot												
Roof							!					
Open/Landscaped			ļ				į					
Industrial		Site	Off-site	Site	Off-site	Site	Off-site	Site	Off-site	Site	Off-site	
Parking lot		0.10	On one	0.10	011 0110	0.00	On one	5.1.5	0 0	0.1.0	0.1. 0.1.0	
Roof			! !				! 					
Open/Landscaped							<u> </u>					
•		0.11	000 11	0.11	0" "	0.11	000 11	011	000 11	011	0" "	
Transportation		Site	Off-site	Site	Off-site	Site	Off-site	Site	Off-site	Site	Off-site	
High Density (interstate, main)							<u> </u>					
High Density (Grassed Right-of-ways)			<u> </u>				ļ					
Low Density (secondary, feeder)			<u> </u>				<u> </u>					
Low Density (Grassed Right-of-ways)			ļ				<u> </u>					
Rural			i 				i 					
Rural (Grassed Right-of-ways)							<u> </u>					
Sidewalk												
Misc. Pervious		Site	Off-site	Site	Off-site	Site	Off-site	Site	Off-site	Site	Off-site	
Managed pervious			i				i					
Unmanaged (pasture)												
Woods (not on lots)			<b> </b>				} 					
Residential		Site	Off-site	Site	Off-site	Site	Off-site	Site	Off-site	Site	Off-site	
Roadway			ļ				!					
Grassed Right-of-ways			<u> </u>				!					
Driveway							<u> </u>					
Parking lot			<u> </u>				<u>i</u>					
Roof							 					
Sidewalk							<u> </u>					
Lawn												
Managed pervious							!					
Woods (on lots)			!				!					
Land Taken up by BMP												
JURISDICTIONAL LANDS		Site	Off-site	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite	
Natural wetland			<u> </u>				<u> </u>					
Riparian buffer (Zone 1 only)			i				i					
	Totals (Ac)=	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
Sub-DA5(a) BMP(s)												
Device Name (As Shown on Plan)	Device Type	Water Quality Volume (c.f.)	Inflow N EMC (mg/L)	Total Inflow N (lb/ac/yr)	Inflow P EMC (mg/L)	Total Inflow P (lb/ac/yr)	Outflow N EMC (mg/L)	Total Outflow N (lb/ac/yr)	Outflow P EMC (mg/L)	Total Outflow P (lb/ac/yr)	Provided Volume Managed (c.f.)	
Outflo	ow Total Nitrogen (lb/ac/yr)=					Outflow	/ Total Ph	osphorus (	(lb/ac/yr)=			
Sub-DA5(b) BMP(s)												
. ( )												

If Sub-DA5(b) is connected to upstream sub-t	basin(s), select all contributir	ıg sub-bas	in(s from								
dropdown menus):  Device Name (As Shown on Plan)	Device Type	Water Quality Volume (c.f.)	Inflow N EMC (mg/L)	Total Inflow N (lb/ac/yr)	Inflow P EMC (mg/L)	Total Inflow P (lb/ac/yr)	Outflow N EMC (mg/L)	Total Outflow N (lb/ac/yr)	Outflow P EMC (mg/L)	Total Outflow P (lb/ac/yr)	Provided Volume Managed (c.f.)
Outfle	ow Total Nitrogen (lb/ac/yr)=					Outflow	Total Ph	osphorus (	(lb/ac/yr)=		
Sub-DA5 (c) BMP(s)										,	
If Sub-DA5(c) is connected to upstream sub-b	pasin(s), select all contributin	ıg sub-bas	in(s):								
Device Name (As Shown on Plan)	Device Type	Water Quality Volume (c.f.)	Inflow N EMC (mg/L)	Total Inflow N (lb/ac/yr)	Inflow P EMC (mg/L)	Total Inflow P (lb/ac/yr)	Outflow N EMC (mg/L)	Total Outflow N (lb/ac/yr)	Outflow P EMC (mg/L)	Total Outflow P (lb/ac/yr)	Provided Volume Managed (c.f.)
Outfle	ow Total Nitrogen (lb/ac/yr)=					Outflow	Total Ph	osphorus (	(lb/ac/yr)=		
Sub-DA5 (d) BMP(s)		I.									
If Sub-DA5(d) is connected to upstream sub-l	basin(s), select all contributin	ıg sub-bas	in(s):								
Device Name (As Shown on Plan)	Device Type	Water Quality Volume (c.f.)	Inflow N EMC (mg/L)	Total Inflow N (lb/ac/yr)	Inflow P EMC (mg/L)	Total Inflow P (lb/ac/yr)	Outflow N EMC (mg/L)	Total Outflow N (lb/ac/yr)	Outflow P EMC (mg/L)	Total Outflow P (lb/ac/yr)	Provided Volume Managed (c.f.)
Outfl	 ow Total Nitrogen (lb/ac/yr)=					Outflow	Total Ph	osphorus (	(lb/ac/vr)=		
Sub-DA5 (e) BMP(s)	ow rotal ritingen (ib/do/yr)					Outilovi		- Coprior do 1	ibraoryty		
If Sub-DA5(e) is connected to upstream sub-t											
ii cab 27 to(o) io connected to apolicam cab i	hasin(s) select all contributing	na suh-has	in(s)·								
Device Name (As Shown on Plan)	pasin(s), select all contributin	Water Quality Volume (c.f.)	Inflow N EMC	Total Inflow N (lb/ac/yr)		Total Inflow P (lb/ac/yr)	Outflow N EMC (mg/L)	Total Outflow N (lb/ac/yr)	Outflow P EMC (mg/L)	Total Outflow P (lb/ac/yr)	Provided Volume Managed (c.f.)
Device Name (As Shown on Plan)		Water Quality Volume	Inflow N EMC	Inflow N	EMC	Inflow P	N EMC	Outflow N	P EMC	Outflow P	Volume Managed
Device Name (As Shown on Plan)		Water Quality Volume	Inflow N EMC	Inflow N	EMC	Inflow P	N EMC	Outflow N	P EMC	Outflow P	Volume Managed
Device Name (As Shown on Plan)		Water Quality Volume	Inflow N EMC	Inflow N	EMC	Inflow P	N EMC	Outflow N	P EMC	Outflow P	Volume Managed
		Water Quality Volume	Inflow N EMC	Inflow N	EMC	Inflow P (lb/ac/yr)	N EMC (mg/L)	Outflow N	P EMC (mg/L)	Outflow P	Volume Managed
	Device Type	Water Quality Volume (c.f.)	Inflow N EMC	Inflow N (lb/ac/yr)	EMC	Inflow P (lb/ac/yr)	N EMC (mg/L)	Outflow N (lb/ac/yr)	P EMC (mg/L)	Outflow P	Volume Managed
Outfle	Device Type	Water Quality Volume (c.f.)	Inflow N EMC (mg/L)	Inflow N (lb/ac/yr)	EMC	Inflow P (lb/ac/yr)	N EMC (mg/L)	Outflow N (lb/ac/yr)	P EMC (mg/L)	Outflow P	Volume Managed
Outfle	Device Type  Device Type  Ow Total Nitrogen (lb/ac/yr)=	Water Quality Volume (c.f.)	Inflow N EMC (mg/L)	Inflow N (lb/ac/yr)	EMC	Inflow P (lb/ac/yr)	N EMC (mg/L)	Outflow N (lb/ac/yr)	P EMC (mg/L)	Outflow P	Volume Managed
Outfle DA5 Outfle	Device Type  ow Total Nitrogen (lb/ac/yr)=  Total Volume Treated (c.f.)=	Water Quality Volume (c.f.)	Inflow N EMC (mg/L)	Inflow N (lb/ac/yr)	EMC	Inflow P (lb/ac/yr)	N EMC (mg/L)	Outflow N (lb/ac/yr)	P EMC (mg/L)	Outflow P	Volume Managed
Outfle DA5 Outfle	Device Type  ow Total Nitrogen (lb/ac/yr)=  Total Volume Treated (c.f.)=  ow Total Nitrogen (lb/ac/yr)=	Water Quality Volume (c.f.)	Inflow N EMC (mg/L)	Inflow N (lb/ac/yr)	EMC	Inflow P (lb/ac/yr)	N EMC (mg/L)	Outflow N (lb/ac/yr)	P EMC (mg/L)	Outflow P	Volume Managed
Outflow DA5 Outflow 1-year, 24-hour storm	Device Type  ow Total Nitrogen (lb/ac/yr)=  Total Volume Treated (c.f.)=  ow Total Nitrogen (lb/ac/yr)=	Water Quality Volume (c.f.)	Inflow N EMC (mg/L)	Inflow N (lb/ac/yr)	EMC	Inflow P (lb/ac/yr)	N EMC (mg/L)	Outflow N (lb/ac/yr)	P EMC (mg/L)	Outflow P	Volume Managed

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WAKE COUNTY

Project Name:

Parker Ridge

### DRAINAGE AREA 6 BMP CALCULATIONS

DRAINAGE AREA 6 - BMP DEVICES	AND ADJUSTMENTS										
DA6 Site Acreage=	0.70										
DA6 Off-Site Acreage=					0.00						
Total Required Storage Volume for Site		22,290									
TCN Requirement (ft <sup>3</sup> )=											
Will site use underground water harvesting?	Enter % volume reduction in decimal form=  Note: Supporting inf should be submitted water usage.										
ENTER AREA <u>TREATED BY BMP</u>											
Land Use (acres	)		DA6(a) Ac)		DA6(b)		DA6(c)		DA6(d) Ac)		
Commercial		Site	Off-site	Site	Off-site	Site	Off-site	Site	Off-site	Site	Off-site
Parking lot					-		!		!		
Roof			!		!		!		!		
Open/Landscaped							İ				
Industrial		Site	Off-site	Site	Off-site	Site	Off-site	Site	Off-site	Site	Off-site
Parking lot											
Roof			i		i		i		i		
Open/Landscaped			i				i		i		
Transportation		Site	Off-site	Site	Off-site	Site	Off-site	Site	Off-site	Site	Off-site
		Oito	On one	Oilo	On one	Oito	On one	Oito	On one	Oito	On one
High Density (interstate, main)  High Density (Grassed Right-of-ways)											
Low Density (Secondary, feeder)					 		! :				
Low Density (Secondary, reeder)  Low Density (Grassed Right-of-ways)					<u> </u>		<u> </u>				
Rural			<del>!                                    </del>		<del>                                     </del>		<del> </del>		!		
Rural (Grassed Right-of-ways)			<u> </u>				ļ — —				
Sidewalk			<del>                                     </del>		<del>                                     </del>		<del>                                     </del>		<del>                                     </del>		
		0:4-	Off -:t-	0:1-	0# -:+-	0:4-	0# -:+-	0:4-	O# -:t-	0:4-	0# -:4-
Misc. Pervious		Site	Off-site	Site	Off-site	Site	Off-site	Site	Off-site	Site	Off-site
Managed pervious			1		<u> </u>		<u> </u>		<u> </u>		
Unmanaged (pasture)											
Woods (not on lots)							!				
Residential		Site	Off-site	Site	Off-site	Site	Off-site	Site	Off-site	Site	Off-site
Roadway			<u> </u>		<u> </u>		!		!		
Grassed Right-of-ways							<u> </u>		<u> </u>		
Driveway			<u> </u>		<u> </u>		<u> </u>		<u> </u>		
Parking lot			<u> </u>		<u> </u>		į		<u> </u>		
Roof			<u> </u>		ļ		ļ		<u> </u>		
Sidewalk			<u> </u>		! 		: 		! 		
Lawn							<u> </u>		<u> </u>		
Managed pervious					<u> </u>		<u> </u>				
Woods (on lots)					!		<u> </u>				
Land Taken up by BMP		0:4-	Off -:t-	0:4-	0#-:4-	0:4-	0#-:-	0:4-	0#-:-	O:t-	O#-:t-
JURISDICTIONAL LANDS		Site	Off-site	Site	Offsite	Site	Offsite	Site	Offsite	Site	Offsite
Natural wetland					 		 				
Riparian buffer (Zone 1 only)	Totals (Ac)=	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Sub-DA6(a) BMP(s)	Totals (AC)-	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
			I		I	I	I	I		I	
Device Name (As Shown on Plan)	Device Type	Water Quality Volume (c.f.)	Inflow N EMC (mg/L)	Total Inflow N (lb/ac/yr)	Inflow P EMC (mg/L)	Total Inflow P (lb/ac/yr)	Outflow N EMC (mg/L)	Total Outflow N (lb/ac/yr)	Outflow P EMC (mg/L)	Total Outflow P (lb/ac/yr)	Provided Volume Managed (c.f.)
		-	<u> </u>	-		-		-	-	-	
				<u> </u>		<u></u>		<u></u>	<u> </u>	<u></u>	
Outfl	ow Total Nitrogen (lb/ac/yr)=		1		<u> </u>	Outflow	/ Total Ph	osphorus	  lb/ac/vr\=	<u> </u>	
						Cathor	. rotairii	- Spriorus	(, aoi yi )—		
Sub-DA6(b) BMP(s)											

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If Sub-DA6(b) is connected to upstream sub-l	basin(s), select all contributir	g sub-bas	in(s from								
dropdown menus):  Device Name (As Shown on Plan)	Device Type	Water Quality Volume (c.f.)	Inflow N EMC (mg/L)	Total Inflow N (lb/ac/yr)	Inflow P EMC (mg/L)	Total Inflow P (lb/ac/yr)	Outflow N EMC (mg/L)	Total Outflow N (lb/ac/yr)	Outflow P EMC (mg/L)	Total Outflow P (lb/ac/yr)	Provided Volume Managed (c.f.)
Sub-DA6 (c) BMP(s)	ow Total Nitrogen (lb/ac/yr)=					Outflow	/ Total Ph	osphorus (	(lb/ac/yr)=		
If Sub-DA6(c) is connected to upstream sub-t	pasin(s) select all contributin	a sub-has	in(s):								
iii oub Brio(o) is commoded to apparoum oub i	saoin(o), soleot all contribution		(0).					Total		Tatal	Dravidad
Device Name (As Shown on Plan)	Device Type	Water Quality Volume (c.f.)	Inflow N EMC (mg/L)	Total Inflow N (lb/ac/yr)	Inflow P EMC (mg/L)	Total Inflow P (lb/ac/yr)	Outflow N EMC (mg/L)	Total Outflow N (lb/ac/yr)	Outflow P EMC (mg/L)	Total Outflow P (lb/ac/yr)	Provided Volume Managed (c.f.)
	ow Total Nitrogen (lb/ac/yr)=					Outflow	Total Ph	osphorus (	(lb/ac/yr)=		
Sub-DA6 (d) BMP(s)											
If Sub-DA6(d) is connected to upstream sub-l	basin(s), select all contributir	g sub-bas	sin(s):		Π						I
Device Name (As Shown on Plan)	Device Type	Water Quality Volume (c.f.)	Inflow N EMC (mg/L)	Total Inflow N (lb/ac/yr)	Inflow P EMC (mg/L)	Total Inflow P (lb/ac/yr)	Outflow N EMC (mg/L)	Total Outflow N (lb/ac/yr)	Outflow P EMC (mg/L)	Total Outflow P (lb/ac/yr)	Provided Volume Managed (c.f.)
Outfl	ow Total Nitrogen (lb/ac/yr)=			Outflow Total Phosphorus (lb/ac/yr)=							
Sub-DA6 (e) BMP(s)											
If Sub-DA6(e) is connected to upstream sub-	basin(s), select all contributir	g sub-bas	sin(s):		ľ						
Device Name (As Shown on Plan)	Device Type	Water Quality Volume (c.f.)	Inflow N EMC (mg/L)	Total Inflow N (lb/ac/yr)		Total Inflow P (lb/ac/yr)	Outflow N EMC (mg/L)	Total Outflow N (lb/ac/yr)	Outflow P EMC (mg/L)	Total Outflow P (lb/ac/yr)	Provided Volume Managed (c.f.)
Outfl	ow Total Nitrogen (lb/ac/yr)=					Outflow	Total Ph	osphorus (	(lb/ac/yr)=		
		DA6 BN	IP SUMI	MARY							
	Total Volume Treated (c.f.)=						0				
	ow Total Nitrogen (lb/ac/yr)=										
	Total Phosphorus (lb/ac/yr)=										
1-year, 24-hour storm											
	eak Discharge (cfs)= Q <sub>1-year</sub> =						44				
Post BMP Pe	eak Discharge (cfs)= Q <sub>1-year</sub> =	Q <sub>1,year</sub> = 1.43									

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Project Name:	Parker Ridge

## DA SITE SUMMARY BMP CALCULATIONS

BMP SUMMARY										
DRAINAGE AREA SUMMARIES										
DRAINAGE AREA:	DA1	DA2	DA3	DA4	DA5	DA6				
Post-Development (1-year, 24-hour storm)										
Peak Flow (cfs)=Q <sub>1-year</sub> =	56.72	72.77	95.07	1.52	2.29	1.43				
Post-Development with BMPs (1-year, 24-hour storm)										
% Impervious =			30	)%						
Volume Managed (CF)=			471	,848						
Post BMP Peak Discharge (cfs)= Q <sub>1-year</sub> =	16.85	3.46	34.43	1.52	2.29	1.43				
Have Target Curve Number Requirements been met?			YI	ES						
Pre Development Ni	trogen and	d Phospho	rus Load							
Total Nitrogen (lb/ac/yr)=			0.	89						
Total Phosphorus (lb/ac/yr)=			N	/A						
Post Development N	itrogen an	d Phospho	orus Load							
Total Nitrogen (lb/ac/yr)=			4.	89						
Total Phosphorus (lb/ac/yr)=			N	/A						
Post-BMF	Nitrogen	Loading								
Outflow Total Nitrogen (lb/ac/yr)=			3.	10						
Outflow Total Phosphorus (lb/ac/yr)=			0.	42						
Has site met the Target?			YI	ES						
Has site met requirements for offsetting?			YI	ES						