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## **STORMWATER CALCULATIONS**

**COBBLESTONE VILLAGE  
SOUTH MAIN STREET  
ROLESVILLE, NORTH CAROLINA  
SP 21-01 COBBLESTONE VILLAGE**



**PREPARED BY  
BASS, NIXON & KENNEDY, INC.  
FEBRUARY 2021  
MAY 2021  
REVISED MAY 2022**

*Cobblestone Village  
May 2021*



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**Cobblestone Village  
Rolesville, North Carolina  
Stormwater Control Calculations  
February, 2021**

The site for the Cobblestone Village project is located on the west side of Main Street (US 401) at the intersection of East Young Street (SR 1945) in Rolesville, North Carolina. The current property consists of 10 individual properties that will be recombined into one lot. The new lot will be 10.96 acres to be used for Residential, Mixed Use development. The existing properties have some old buildings with gravel drives. The property is mostly undeveloped. The site drains to the northwest and eventually to Sanford Creek, then the Neuse River.

Stormwater management is required for this site. An SCM is designed for the Cobblestone Village project. The total drainage area to the SCM is 9.33 ac with 1.63 acres bypassing the SCM. Note the SCM (Wet Pond) will be located on the west side of the property.

There is one point of interest (POI) used for the pre-development hydrologic analysis of the site. POI # 1 is the exit point at the west side of the site. Most of the site drains in that direction. For the post-development hydrologic analysis POI #1 is the portion of the site that discharges to the west side of the site. This area is routed through the SCM. We have a Post Development Detained that is a portion of the site routed through the SCM at the west side of the site. Post Development Not Detained is a portion of the site that is not captured in the SCM and this drainage drains to the west side of the site and is not captured in the SCM.

The wet pond outlet control structure is designed to control the peak stormwater run-off for the 1-year 24-hour storm to be less than the pre-existing conditions. The SCM will meet the 85% total suspended solids (TSS) requirement.

Stormwater routing was evaluated using a 10-year storm for pipe capacity sizing.

# **DETENTION CALCULATIONS**

**STORMWATER RUNOFF SUMMARY  
PRE VS. POST DESIGN PARAMETERS  
SCM 1 CALCULATIONS  
1, 10, AND 100 – YEAR ROUTING CALCULATIONS**

## Water Quality Retention Calculations

Project Name: Cobblestone Village

### Determine Surface Area Required for Permanent Pool:

Drainage Area:	9.33 ac
Impervious Area:	7.01 ac
Percent Impervious:	75.1%
Permanent Pool Elevation:	424.50 ( $\frac{1}{2}$ way up vegetated shelf)
Volume:	28431.50 cf
Surface Area:	12926.00 sf
Hydraulic Depth:	3.34 ft (Option 2 Calculation BMP Manual)
SA/DA Required:	2.95%
SA/DA Provided:	3.18% OK

### Forebay Volume Check:

Forebay Volume at Crest of Berm:	5459.50 cf
Permanent Pool Volume:	28431.50 cf
Forebay Volume % of Perm. Volume:	19.20% OK - Approximately 20% of total perm. volume

### Calculate the Volume Required to Treat the First Flush:

Rainfall to Treat: 1 in

Runoff Coefficient ( $R_v$ ) =  $0.05 + 0.009 * (\% \text{ Impervious})$   
Runoff Coefficient ( $R_v$ ): 0.73 in/in

Runoff Volume ( $V$ ) = Rainfall \* ( $R_v$ ) \* (Drainage Area)  
Runoff Volume ( $V$ ): 24,588 cf

### Calculate the Depth Required for the Temporary Pool:

Temporary Pool Volume (Required):	24,588 cf
Total Volume (Perm. + Temp.):	53,019 cf
Temporary Pool Elevation between:	426.00 and 427.00
Temporary Pool Elevation:	426.15
Temporary Pool Depth:	1.65 measured from Permanent Pool Elevation

### Determine the Orifice Size for 2-5 Day Drawdown of Temporary Pool:

Orifice Invert Elevation: 424.50  
Temporary Pool Elevation: 426.15  
Orifice Diameter: 2.50 in

Use the orifice equation to determine flow and drawdown time:

Orifice Equation: $Q = CA(2gh)^{0.5}$	
Volume to Draw Down:	24,588 cf
Flow for 2-Day Drawdown:	0.14 cfs
Flow for 5-Day Drawdown:	0.06 cfs
C:	0.60
g:	32.20 ft/s <sup>2</sup>
A:	0.03 sf
Number of Increments for Orifice Flow:	10 Increments
Depth of Temp. Pool from Top of Orifice:	1.44 ft

### Incremental Orifice Flow Drawdown Calculations

For Temp Pool above top of orifice (Equations III-13, Malcom):

Index:	Avg Driving Head (ft)	Q (from Orifice Eq)	Drawdown Time (s)	Drawdown Time (Days)
0	1.4019	0.1943	11,054.75	0.1279
1	1.2577	0.1841	11,671.26	0.1351
2	1.1135	0.1732	12,403.93	0.1436
3	0.9693	0.1616	13,294.54	0.1539
4	0.8251	0.1491	14,409.42	0.1668
5	0.6809	0.1354	15,861.86	0.1836
6	0.5368	0.1203	17,865.86	0.2068
7	0.3926	0.1028	20,891.01	0.2418
8	0.2484	0.0818	26,264.45	0.3040
9	0.1042	0.0530	40,555.12	0.4694
<b>Total</b>				<b>2.1328</b>

For Temp Pool below top of orifice (Equations III-13, Malcom):

Index:	Avg Driving Head (ft)	Q (Malcom III-13)	Drawdown Time (s)	Drawdown Time (Days)
0	0.2083	0.0531	29249.56	0.3385
1	0.1042	0.0188	82730.25	0.9575
<b>Total</b>				<b>1.2961</b>

Drawdown Time:

**3.43 days (OK - Drawdown is between 2 and 5 days)**

COBBLESTONE VILLAGE – ROLEVILLE, NC

## **Stormwater Attenuation Requirements Using Rational Methodology**

The following calculations summarize the pre-development and post development discharge calculations for the 1-year and 100-year 24-hr storm events using the Rational Method. The Q1 and Q100 pre-developed discharge was calculated based on the actual site pre-developed conditions. Hydraflow computer software was used for performing the analysis. Calculations were done in accordance to the Town of Knightdale standards and specifications. All hydrographs and supporting calculations are provided in the Detention Calculations section of this report. Supporting drainage area maps and rainfall data are provided in the Appendix. The following summarizes the findings of the analysis:

Description	Rational Method Storm Event (cfs)				
	Q1				Q100
Pre-Development Discharge	20.69				43.65
Post-Development Discharge	37.34				78.78
Attenuation Required	<b>16.65</b>				<b>N/A</b>
Discharge into SCM	34.37				72.50
Discharge out of SCM	0.14				0.20
Combined Discharge (including bypass)	3.77				7.90
<b>Attenuation Provided</b>	<b>33.57</b>				<b>70.88</b>

The proposed attenuation provided by the Wet Pond provides enough stormwater attenuation so that the Q1 and Q100 post-developed discharge does not exceed the pre-development discharge.

Pre/Post Design Parameters								
POI #1	Drainage Area	Land Use Areas (ac)				Design Storm Flows (cfs)		
		ac	Impervious	Managed Pervious	Wooded Area	Off-Site 70% Imp	1"	Q1
PR to SCM	9.33	7.01	2.32	0.00	0.00	---	33.94	71.59
PR to Bypass SCM	1.63	0.47	1.16	0.00	0.00	---	3.68	7.76
SCM Outfall	0.00	---	---	---	---	---	0.14	0.20
PR Final	10.96	7.48	3.48	0.00	0.00	---	3.77	7.90
EX	10.96	1.83	9.13	0.00	0.00	---	20.69	43.65
Surface Area at SCM		Design Storm Surface Elevations (ft)				426.15	425.29	426.09
12,926		Freeboard (ft)				1.35	2.21	1.41

## Average Depth Calculation

Project Name: Cobblestone Village

Permanent Pool Elevation:	424.50 (1/2 way up vegetated shelf)
Surface Area at Perm. Pool:	12926.00 sf
Elevation of Bottom of Shelf:	424.00
Surface Area at Bottom Shelf:	8026.00
Area at Bottom of Pond:	3739.00
Depth (from bottom of shelf to pond bottom):	4.00
<b>Hydraulic Depth:</b>	<b>3.34 ft (Option 2 Calculation BMP Manual)</b>

# Hydraflow Table of Contents

02.05.21 Cobblestone Village.gpw

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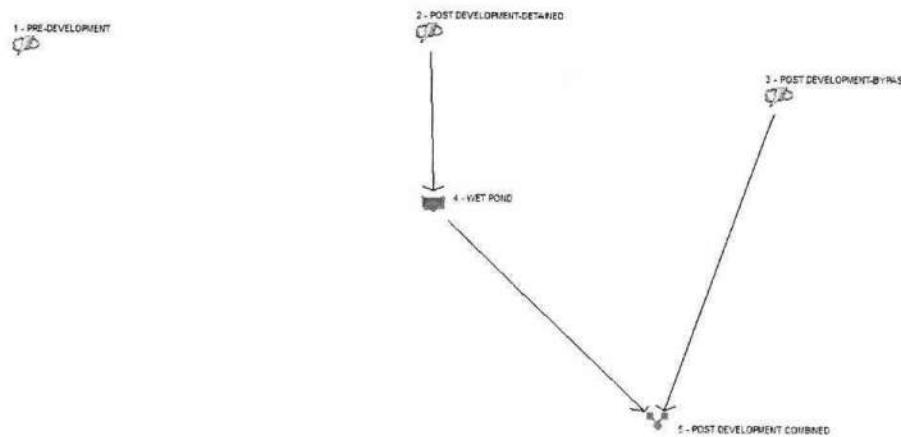
Hydraflow Hydrographs by Intelisolve v9.01

Friday, Feb 5, 2021

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# Watershed Model Schematic

Hydraflow Hydrographs by Intelisolve v9.01



## Legend

<u>Hyd. Origin</u>	<u>Description</u>
--------------------	--------------------

- |  |  |
| --- | --- |
| 1 Rational | PRE-DEVELOPMENT |
| 2 Rational | POST DEVELOPMENT-DETAINED |
| 3 Rational | POST DEVELOPMENT-BYPASS |
| 4 Reservoir | WET POND |
| 5 Combine | POST DEVELOPMENT COMBINED |

# Hydrograph Return Period Recap

Hydraflow Hydrographs by InteliSolve v9.01

Hyd. No.	Hydrograph type (origin)	Inflow Hyd(s)	Peak Outflow (cfs)								Hydrograph description
			1-Yr	2-Yr	3-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr	
1	Rational	----	20.69	----	----	----	----	----	----	43.65	PRE-DEVELOPMENT
2	Rational	----	34.37	----	----	----	----	----	----	72.50	POST DEVELOPMENT-DETAINED
3	Rational	----	3.677	----	----	----	----	----	----	7.758	POST DEVELOPMENT-BYPASS
4	Reservoir	2	0.137	----	----	----	----	----	----	0.201	WET POND
5	Combine	3, 4	3.768	----	----	----	----	----	----	7.899	POST DEVELOPMENT COMBINE

# Hydrograph Summary Report

Hydraflow Hydrographs by Intelisolve v9.01

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph description
1	Rational	20.69	1	5	6,207	----	----	----	PRE-DEVELOPMENT
2	Rational	34.37	1	5	10,310	----	----	----	POST DEVELOPMENT-DETAINED
3	Rational	3.677	1	5	1,103	---	----	----	POST DEVELOPMENT-BYPASS
4	Reservoir	0.137	1	10	9,280	2	425.30	10,266	WET POND
5	Combine	3.768	1	5	10,383	3, 4	----	----	POST DEVELOPMENT COMBINE

# Hydrograph Report

Hydraflow Hydrographs by Intelisolve v9.01

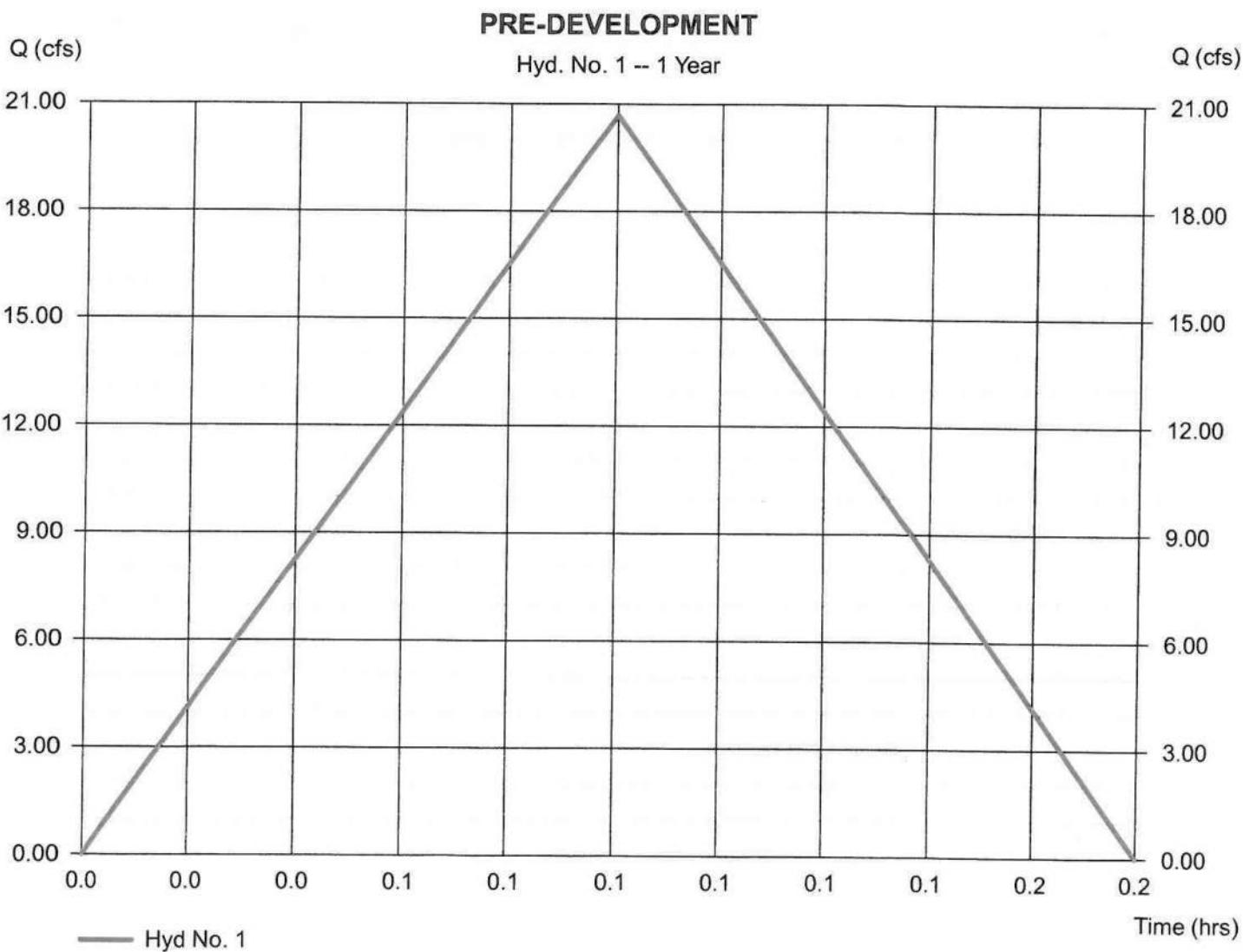
Friday, Feb 5, 2021

## Hyd. No. 1

### PRE-DEVELOPMENT

Hydrograph type	= Rational	Peak discharge	= 20.69 cfs
Storm frequency	= 1 yrs	Time to peak	= 0.08 hrs
Time interval	= 1 min	Hyd. volume	= 6,207 cuft
Drainage area	= 10.960 ac	Runoff coeff.	= 0.41*
Intensity	= 4.604 in/hr	Tc by User	= 5.00 min
IDF Curve	= WakeCounty.IDF	Asc/Rec limb fact	= 1/1

\* Composite (Area/C) = [(1.830 x 0.95) + (9.130 x 0.30)] / 10.960



# Hydrograph Report

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Hydraflow Hydrographs by Intelisolve v9.01

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## Hyd. No. 2

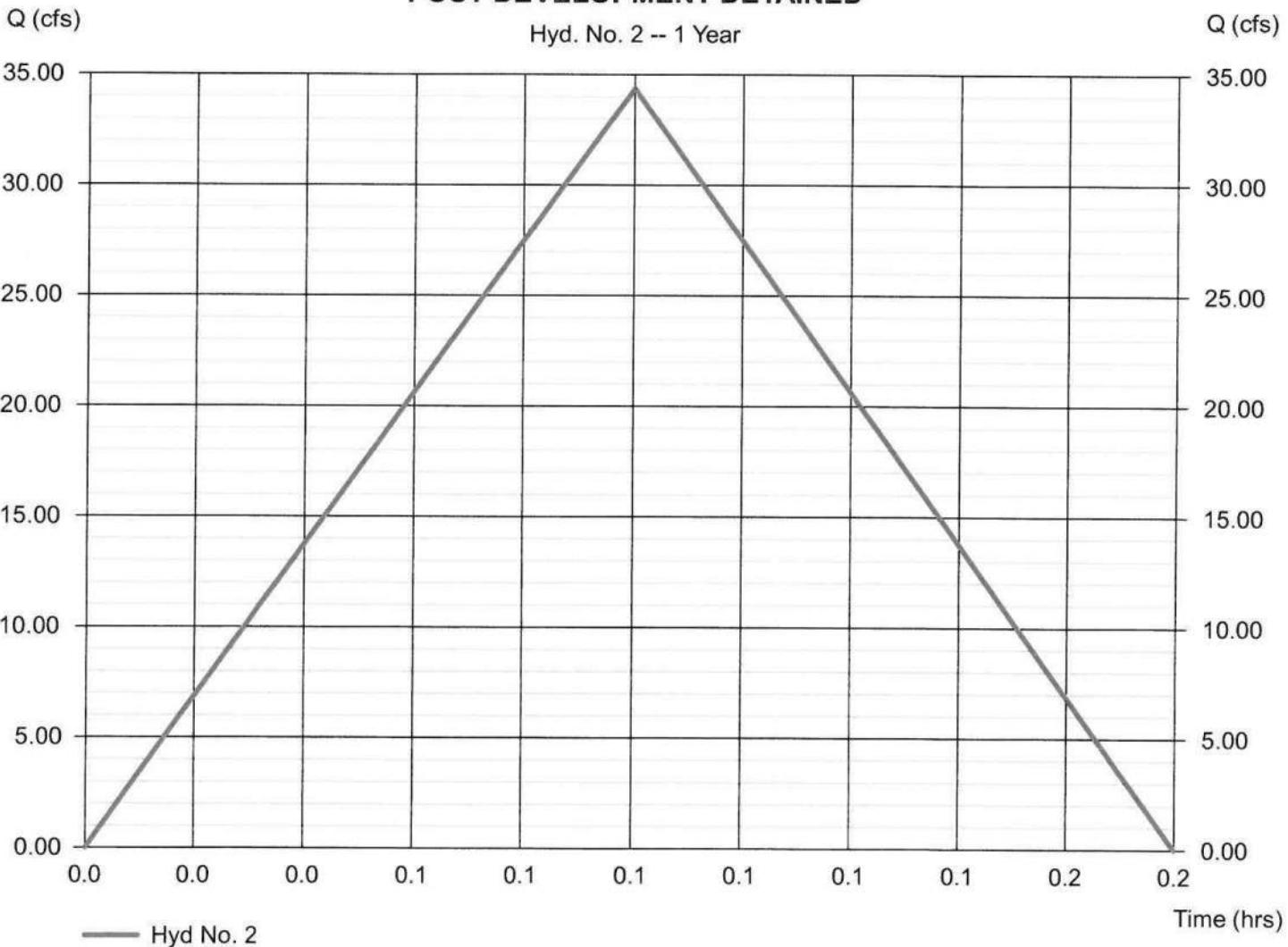
### POST DEVELOPMENT-DETAINED

Hydrograph type = Rational  
Storm frequency = 1 yrs  
Time interval = 1 min  
Drainage area = 9.330 ac  
Intensity = 4.604 in/hr  
IDF Curve = WakeCounty.IDF

Peak discharge = 34.37 cfs  
Time to peak = 0.08 hrs  
Hyd. volume = 10,310 cuft  
Runoff coeff. = 0.8\*  
Tc by User = 5.00 min  
Asc/Rec limb fact = 1/1

\* Composite (Area/C) =  $[(2.320 \times 0.30) + (7.010 \times 0.95)] / 9.330$

### POST DEVELOPMENT-DETAINED



# Hydrograph Report

Hydraflow Hydrographs by Intelisolve v9.01

Friday, Feb 5, 2021

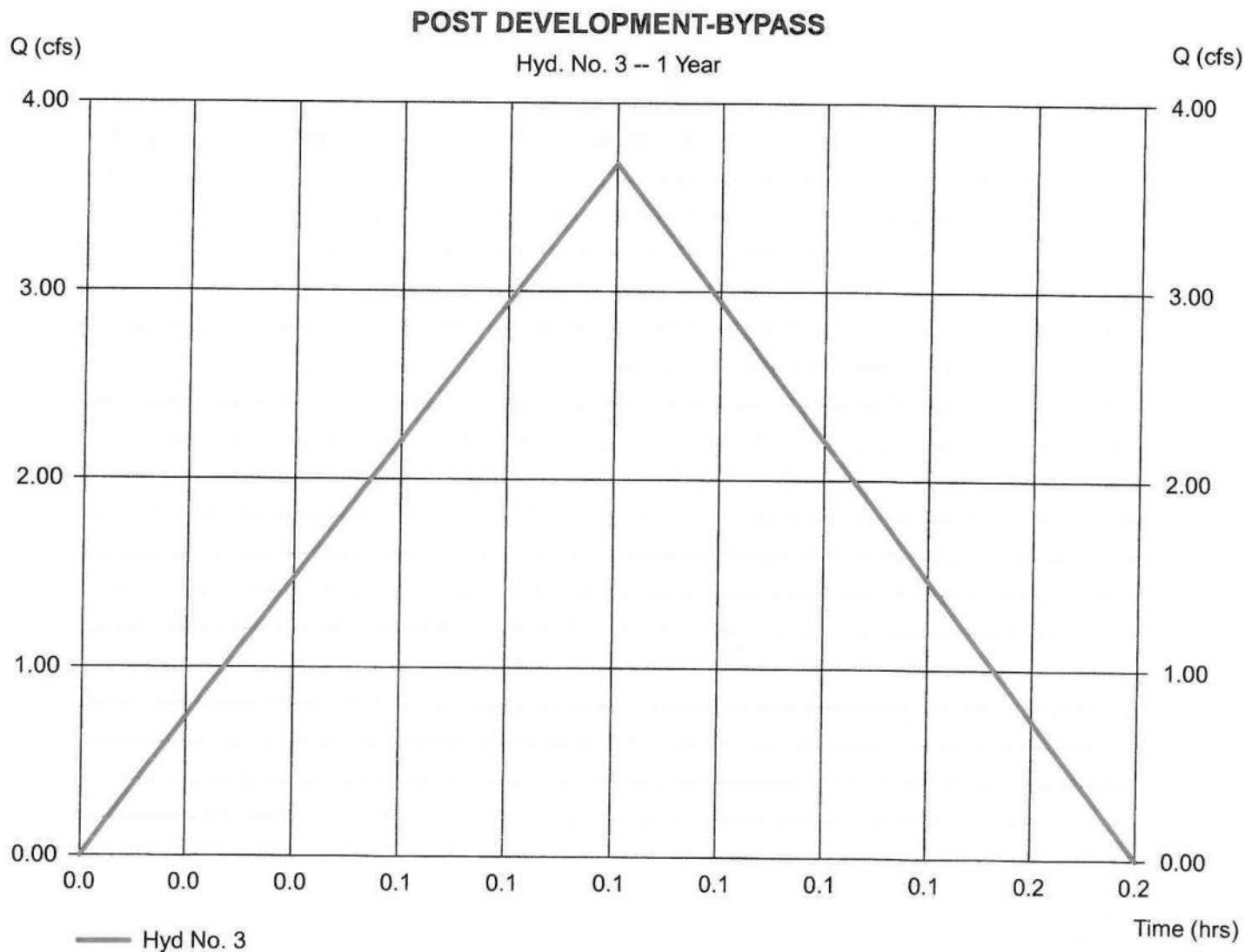
## Hyd. No. 3

### POST DEVELOPMENT-BYPASS

Hydrograph type = Rational  
 Storm frequency = 1 yrs  
 Time interval = 1 min  
 Drainage area = 1.630 ac  
 Intensity = 4.604 in/hr  
 IDF Curve = WakeCounty.IDF

Peak discharge = 3.677 cfs  
 Time to peak = 0.08 hrs  
 Hyd. volume = 1,103 cuft  
 Runoff coeff. = 0.49\*  
 Tc by User = 5.00 min  
 Asc/Rec limb fact = 1/1

\* Composite (Area/C) =  $[(1.160 \times 0.30) + (0.470 \times 0.95)] / 1.630$



# Hydrograph Report

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Hydraflow Hydrographs by Intelisolve v9.01

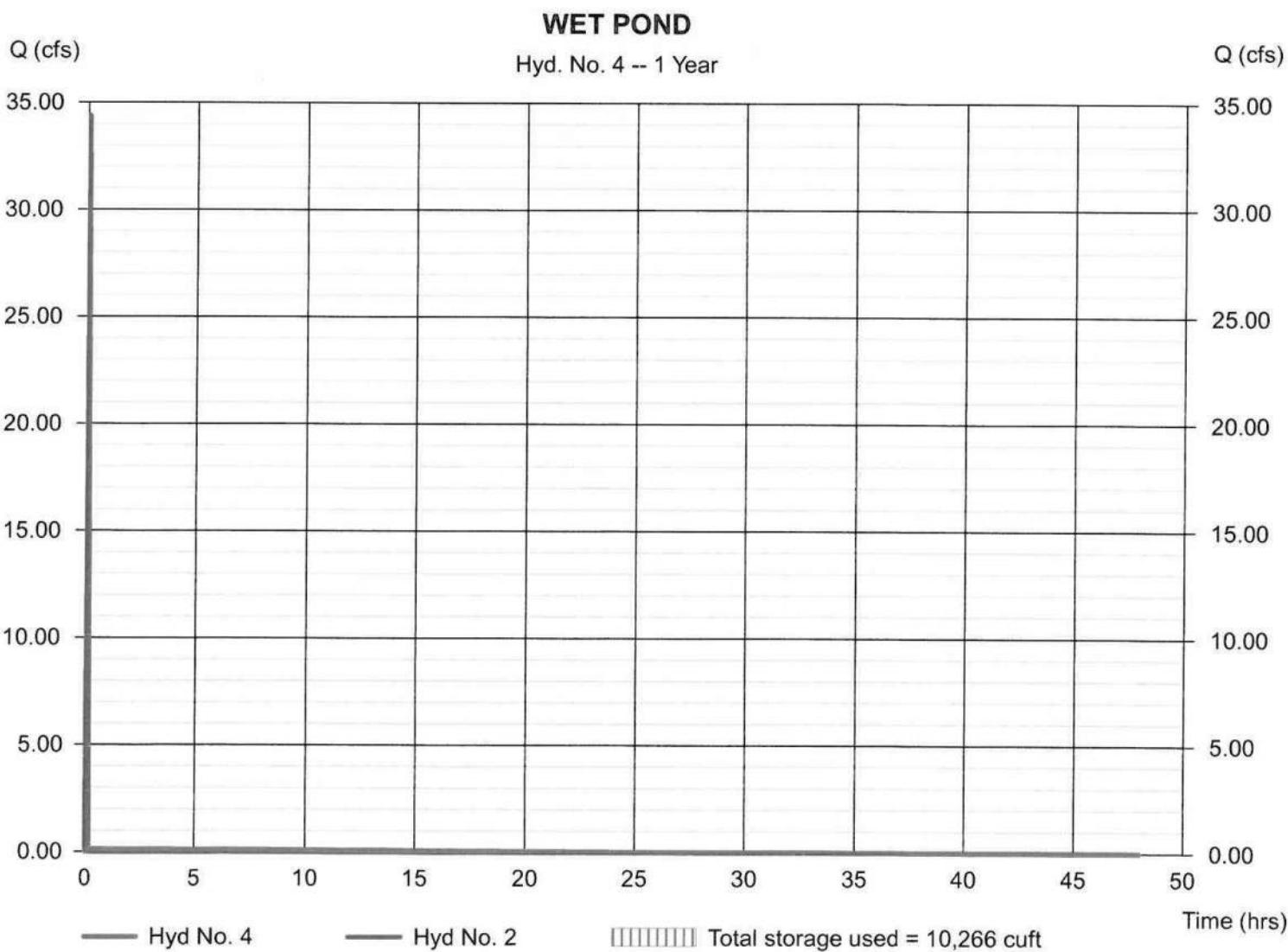
Friday, Feb 5, 2021

## Hyd. No. 4

### WET POND

Hydrograph type	= Reservoir	Peak discharge	= 0.137 cfs
Storm frequency	= 1 yrs	Time to peak	= 0.17 hrs
Time interval	= 1 min	Hyd. volume	= 9,280 cuft
Inflow hyd. No.	= 2 - POST DEVELOPMENT-DETAINED	Max. Elevation	= 425.30 ft
Reservoir name	= WET POND	Max. Storage	= 10,266 cuft

Storage Indication method used.



# Pond Report

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Hydraflow Hydrographs by Intelisolve v9.01

Friday, Feb 5, 2021

## Pond No. 1 - WET POND

### Pond Data

Trapezoid - Bottom L x W = 200.0 x 61.0 ft, Side slope = 3.0:1, Bottom elev. = 424.50 ft, Depth = 3.00 ft

### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	424.50	12,200	0	0
0.30	424.80	12,673	3,731	3,731
0.60	425.10	13,153	3,874	7,604
0.90	425.40	13,639	4,019	11,623
1.20	425.70	14,131	4,165	15,788
1.50	426.00	14,630	4,314	20,102
1.80	426.30	15,135	4,465	24,567
2.10	426.60	15,647	4,617	29,184
2.40	426.90	16,166	4,772	33,956
2.70	427.20	16,691	4,928	38,884
3.00	427.50	17,222	5,087	43,971

### Culvert / Orifice Structures

	[A]	[B]	[C]	[PrfRsr]
Rise (in)	= 24.00	2.50	0.00	0.00
Span (in)	= 24.00	2.50	0.00	0.00
No. Barrels	= 1	1	0	0
Invert El. (ft)	= 420.00	424.50	0.00	0.00
Length (ft)	= 1.00	2.00	0.00	0.00
Slope (%)	= 1.00	1.00	0.00	n/a
N-Value	= .013	.013	.013	n/a
Orifice Coeff.	= 0.60	0.60	0.60	0.60
Multi-Stage	= n/a	No	No	No

### Weir Structures

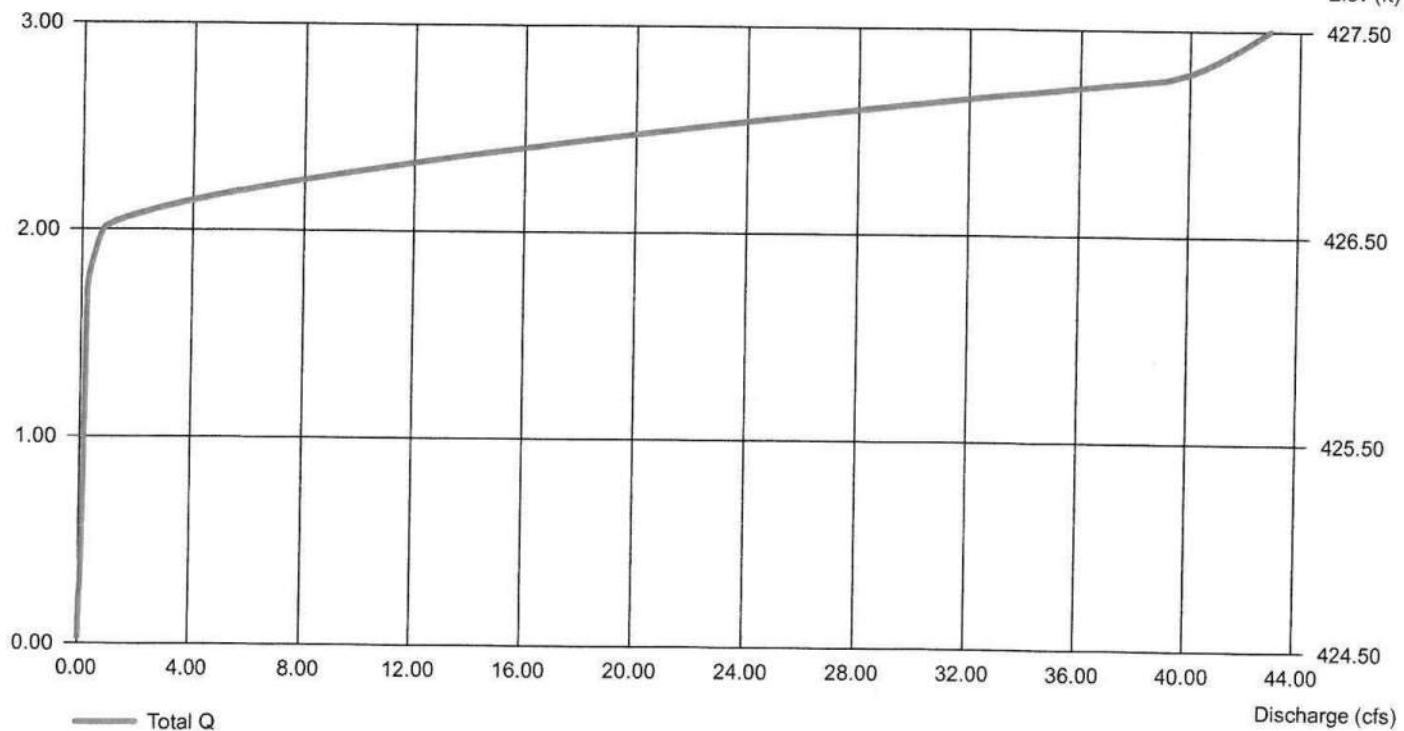
	[A]	[B]	[C]	[D]
Crest Len (ft)	= 16.00	1.00	0.00	0.00
Crest El. (ft)	= 426.50	426.20	0.00	0.00
Weir Coeff.	= 3.33	3.33	3.33	3.33
Weir Type	= Riser	Rect	---	---
Multi-Stage	= Yes	No	No	No
Exfil.(in/hr)				= 0.000 (by Contour)
TW Elev. (ft)				= 0.00

Note: Culvert/Orifice outflows are analyzed under inlet and outlet control. Weir risers are checked for orifice conditions.

Stage (ft)

### Stage / Discharge

Elev (ft)



# Hydrograph Report

Hydraflow Hydrographs by Intelisolve v9.01

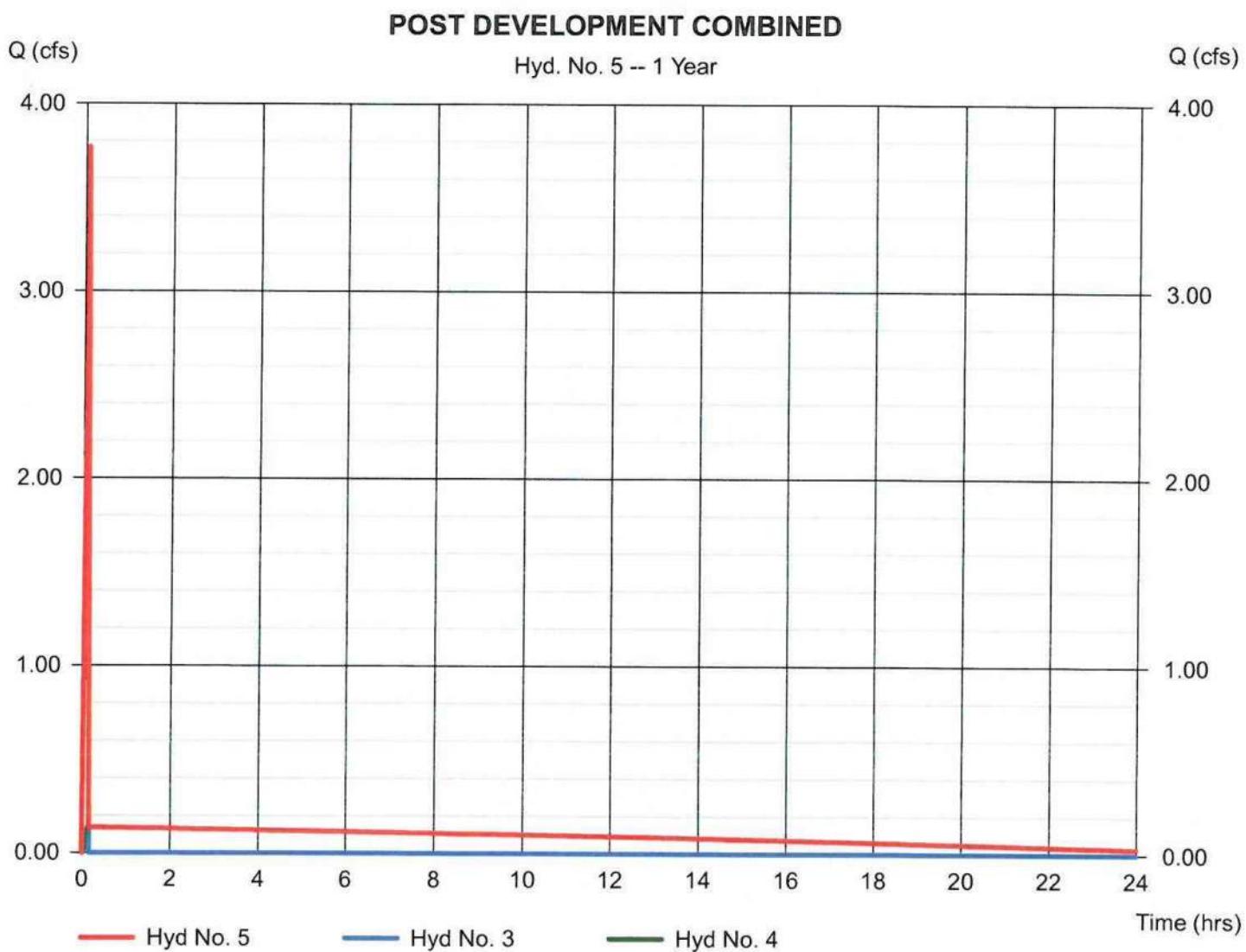
Friday, Feb 5, 2021

## Hyd. No. 5

### POST DEVELOPMENT COMBINED

Hydrograph type = Combine  
Storm frequency = 1 yrs  
Time interval = 1 min  
Inflow hyds. = 3, 4

Peak discharge = 3.768 cfs  
Time to peak = 0.08 hrs  
Hyd. volume = 10,383 cuft  
Contrib. drain. area= 1.630 ac



# Hydrograph Summary Report

Hydraflow Hydrographs by InteliSolve v9.01

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph description
1	Rational	43.65	1	5	13,094	----	-----	-----	PRE-DEVELOPMENT
2	Rational	72.50	1	5	21,749	----	-----	-----	POST DEVELOPMENT-DETAINED
3	Rational	7.758	1	5	2,327	----	-----	-----	POST DEVELOPMENT-BYPASS
4	Reservoir	0.201	1	10	19,606	2	426.11	21,678	WET POND
5	Combine	7.899	1	5	21,933	3, 4	-----	-----	POST DEVELOPMENT COMBINE
02.05.21 Cobblestone Village.gpw				Return Period: 100 Year			Friday, Feb 5, 2021		

# Hydrograph Report

Hydraflow Hydrographs by Intelisolve v9.01

Friday, Feb 5, 2021

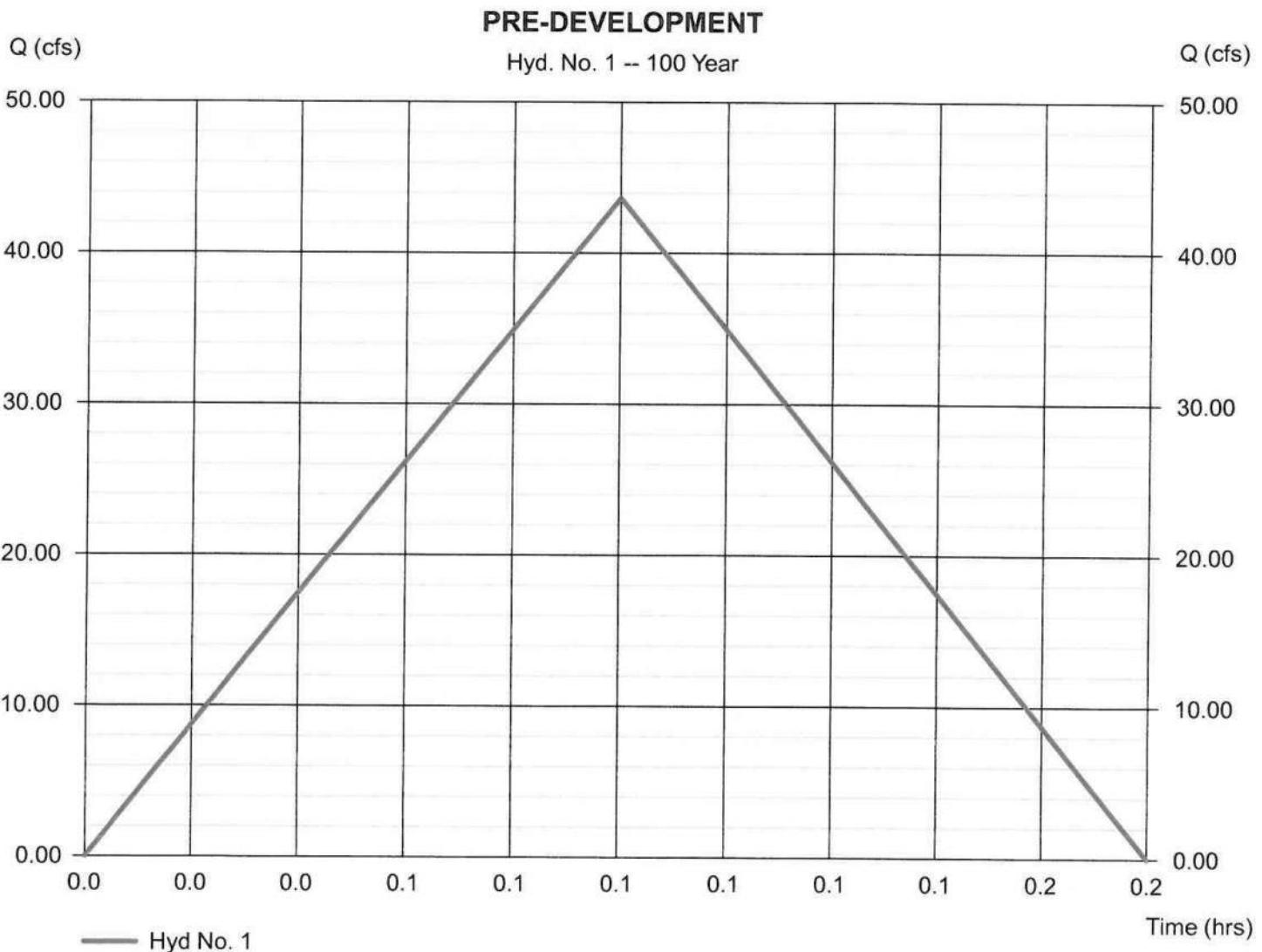
## Hyd. No. 1

### PRE-DEVELOPMENT

Hydrograph type = Rational  
 Storm frequency = 100 yrs  
 Time interval = 1 min  
 Drainage area = 10.960 ac  
 Intensity = 9.713 in/hr  
 IDF Curve = WakeCounty.IDF

Peak discharge = 43.65 cfs  
 Time to peak = 0.08 hrs  
 Hyd. volume = 13,094 cuft  
 Runoff coeff. = 0.41\*  
 Tc by User = 5.00 min  
 Asc/Rec limb fact = 1/1

\* Composite (Area/C) = [(1.830 x 0.95) + (9.130 x 0.30)] / 10.960



# Hydrograph Report

Hydraflow Hydrographs by Intelisolve v9.01

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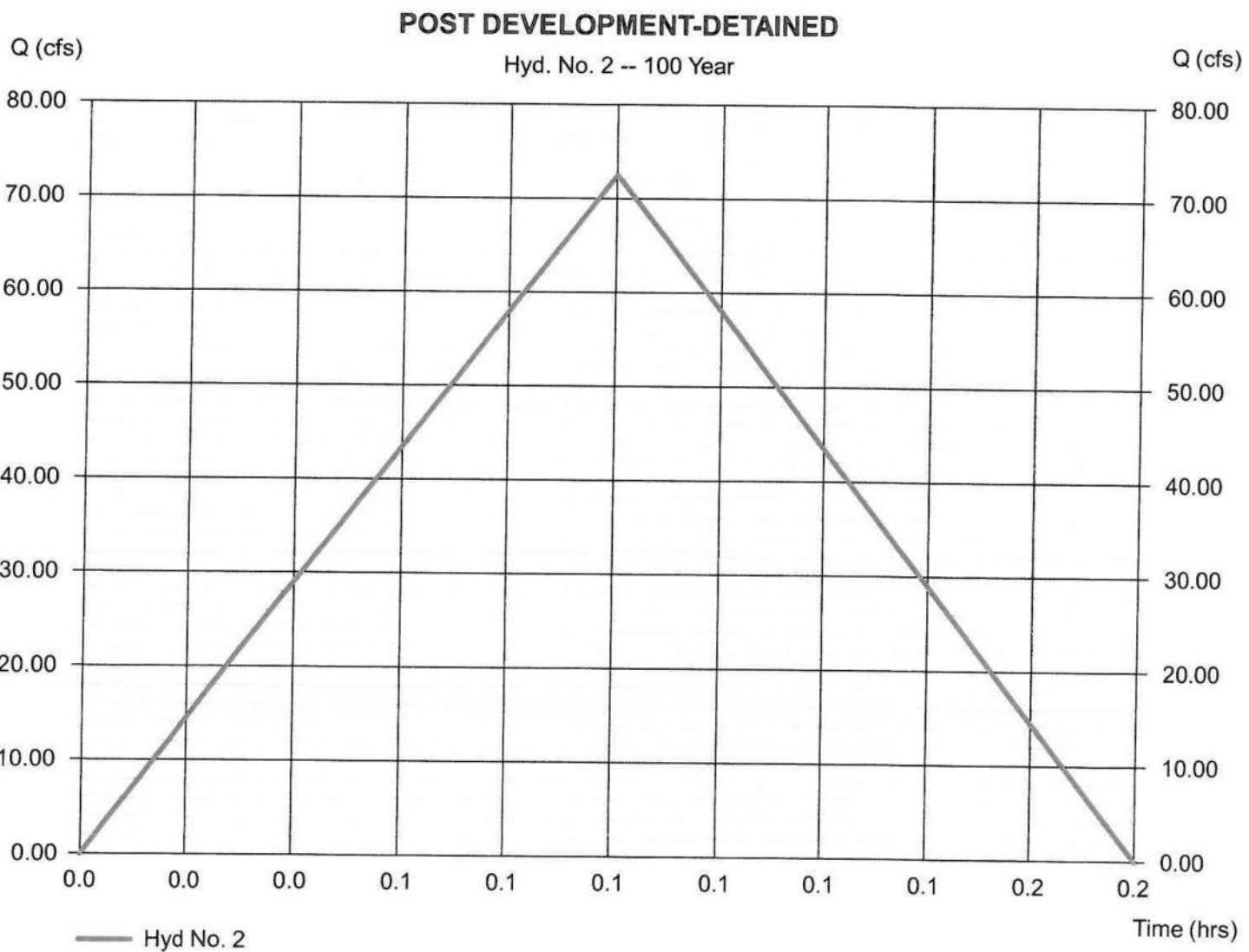
## Hyd. No. 2

### POST DEVELOPMENT-DETAINED

Hydrograph type = Rational  
 Storm frequency = 100 yrs  
 Time interval = 1 min  
 Drainage area = 9.330 ac  
 Intensity = 9.713 in/hr  
 IDF Curve = WakeCounty.IDF

Peak discharge = 72.50 cfs  
 Time to peak = 0.08 hrs  
 Hyd. volume = 21,749 cuft  
 Runoff coeff. = 0.8\*  
 Tc by User = 5.00 min  
 Asc/Rec limb fact = 1/1

\* Composite (Area/C) =  $[(2.320 \times 0.30) + (7.010 \times 0.95)] / 9.330$



# Hydrograph Report

Hydraflow Hydrographs by Intelisolve v9.01

Friday, Feb 5, 2021

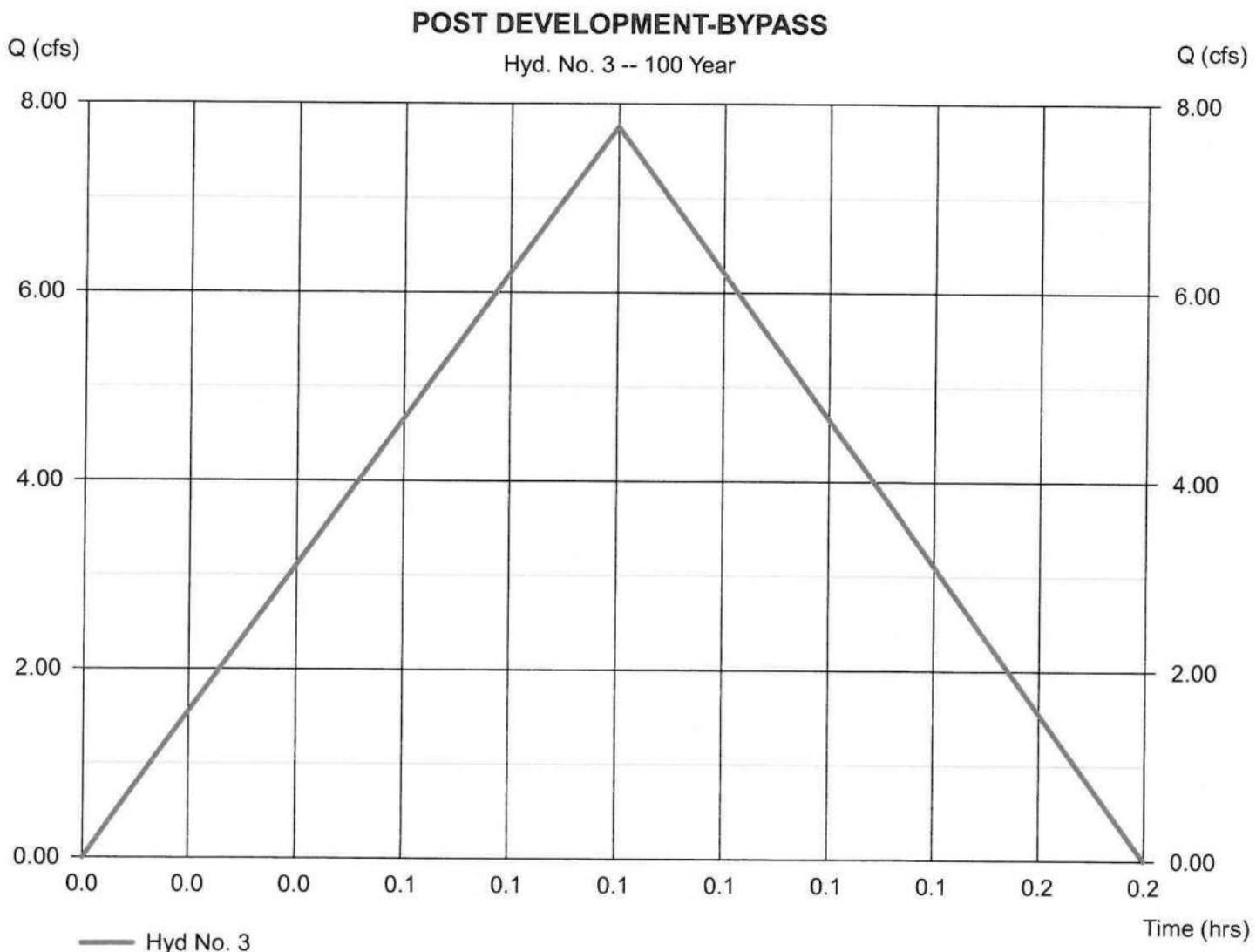
## Hyd. No. 3

### POST DEVELOPMENT-BYPASS

Hydrograph type = Rational  
 Storm frequency = 100 yrs  
 Time interval = 1 min  
 Drainage area = 1.630 ac  
 Intensity = 9.713 in/hr  
 IDF Curve = WakeCounty.IDF

Peak discharge = 7.758 cfs  
 Time to peak = 0.08 hrs  
 Hyd. volume = 2,327 cuft  
 Runoff coeff. = 0.49\*  
 Tc by User = 5.00 min  
 Asc/Rec limb fact = 1/1

\* Composite (Area/C) = [(1.160 x 0.30) + (0.470 x 0.95)] / 1.630



# Hydrograph Report

Hydraflow Hydrographs by Intelisolve v9.01

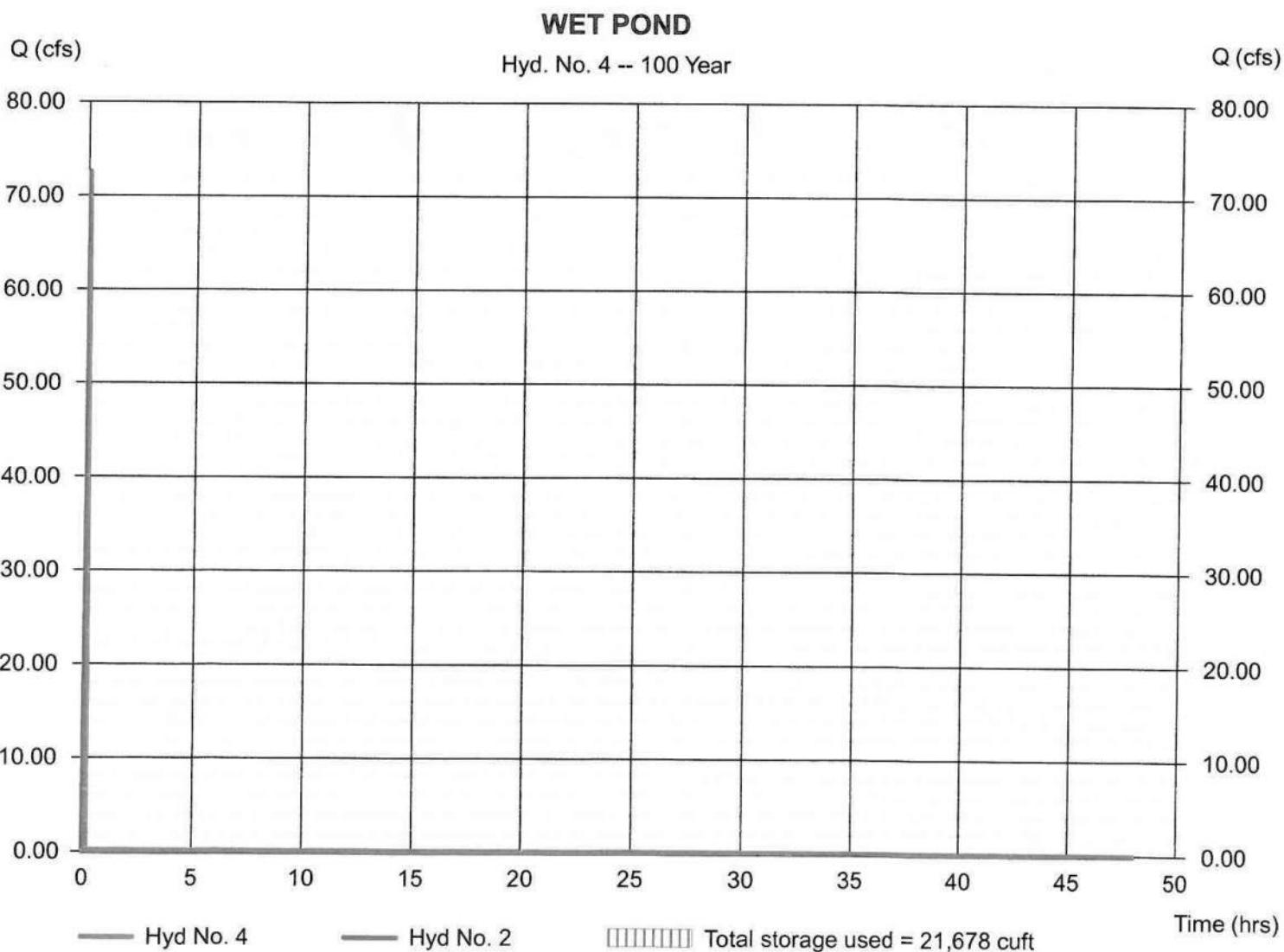
Friday, Feb 5, 2021

## Hyd. No. 4

### WET POND

Hydrograph type	= Reservoir	Peak discharge	= 0.201 cfs
Storm frequency	= 100 yrs	Time to peak	= 0.17 hrs
Time interval	= 1 min	Hyd. volume	= 19,606 cuft
Inflow hyd. No.	= 2 - POST DEVELOPMENT-DETAINED	Max. Elevation	= 426.11 ft
Reservoir name	= WET POND	Max. Storage	= 21,678 cuft

Storage Indication method used.



# Hydrograph Report

Hydraflow Hydrographs by Intelisolve v9.01

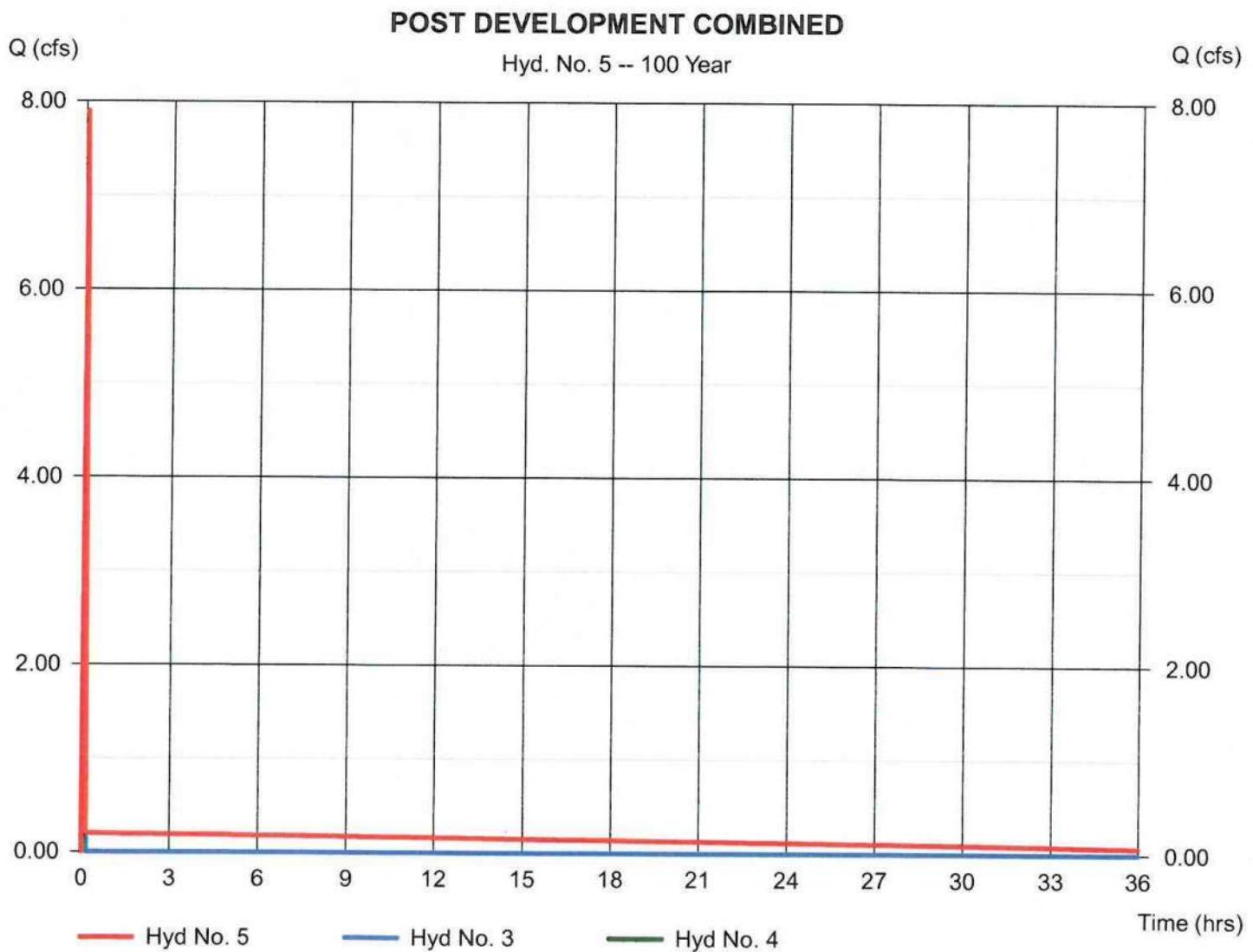
Friday, Feb 5, 2021

## Hyd. No. 5

### POST DEVELOPMENT COMBINED

Hydrograph type = Combine  
Storm frequency = 100 yrs  
Time interval = 1 min  
Inflow hyds. = 3, 4

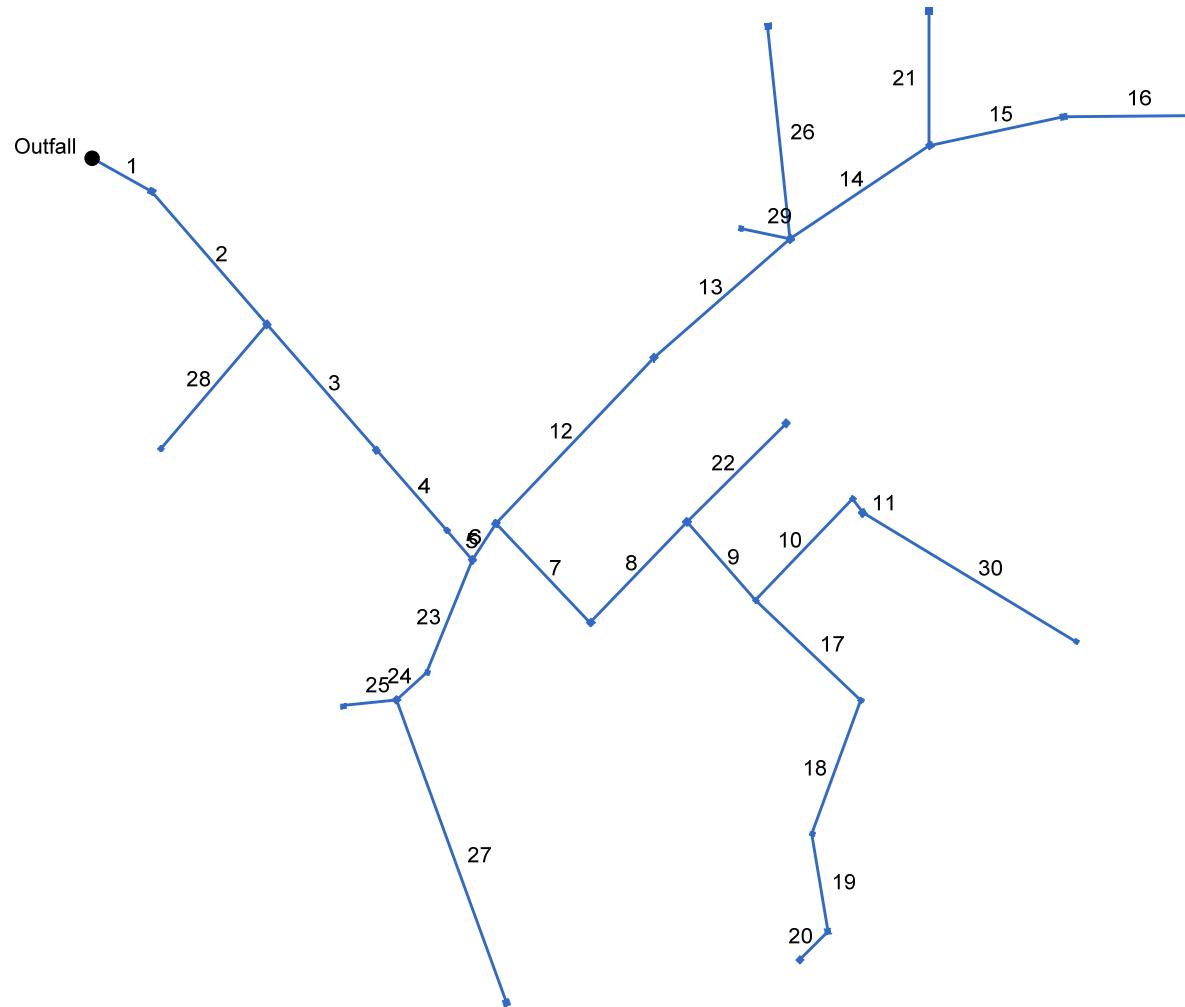
Peak discharge = 7.899 cfs  
Time to peak = 0.08 hrs  
Hyd. volume = 21,933 cuft  
Contrib. drain. area= 1.630 ac



# **STORMWATER RUNOFF**

**10-YEAR PIPE SIZING  
10-YEAR HYDRAULIC GRADE LINES**

# Hydraflow Storm Sewers Extension for Autodesk® Civil 3D® Plan



Project File: 19157 - Pipe Sizing.stm

Number of lines: 30

Date: 4/28/2022

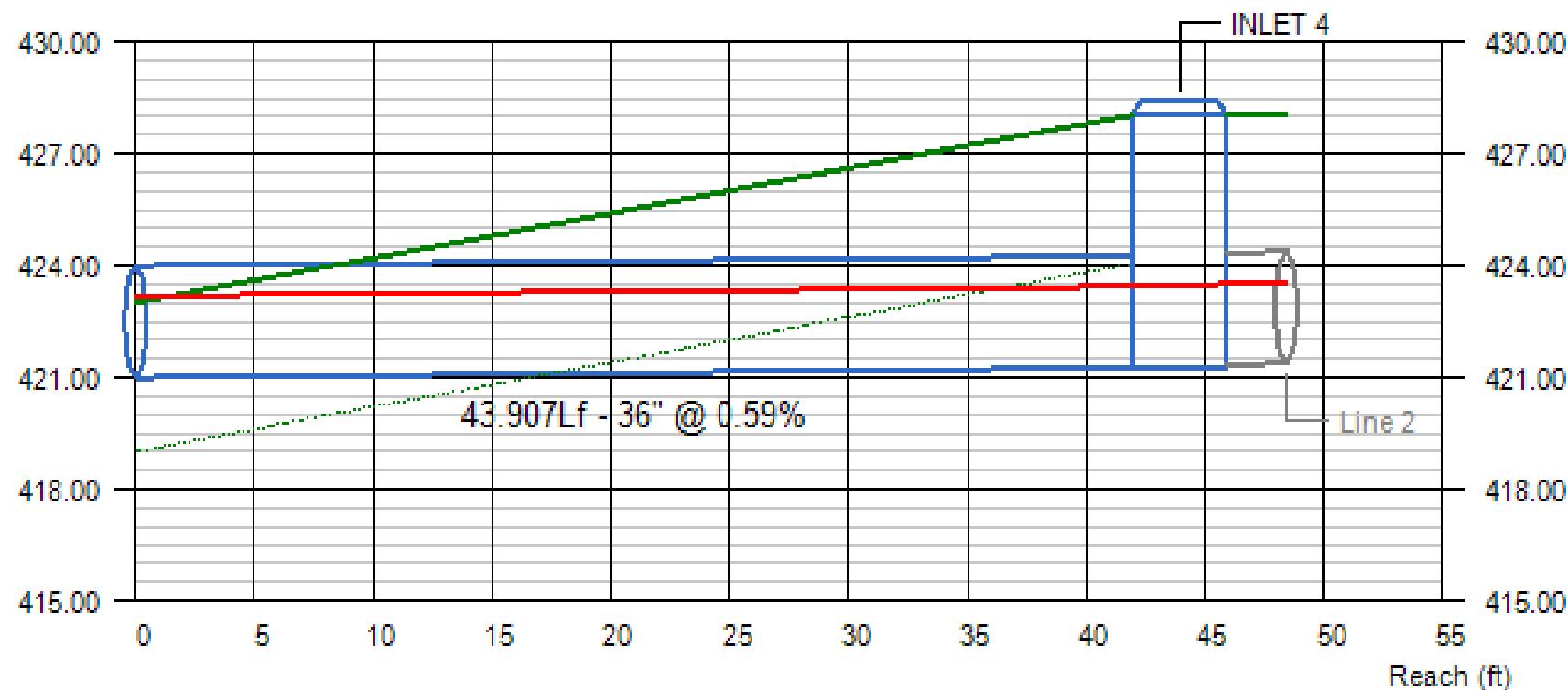
NOTES: Intensity =  $67.84 / (\text{Inlet time} + 12.00)^{0.79}$  – Return period = 10 Yrs. ; \*\* Critical depth

Line No.	Inlet ID	Drg Area	Runoff Coeff	Incr CxA	Inlet Time	i Inlet	Incr Q	Q Capt	Q Byp	Q Carry	Total Area	Total Runoff	Capac Full	Flow Rate	Vel Ave	Line Size	
		(ac)	(C)		(min)	(in/hr)	(cfs)	(cfs)	(cfs)	(cfs)	(ac)	(cfs)	(cfs)	(cfs)	(ft/s)	(in)	
24	INLET 22	0.67	0.83	0.55	5.0	7.19	3.97	4.96	0.00	0.99	1.56	6.97	6.45	6.97	5.68	15	
25	INLET 29	0.21	0.51	0.11	5.0	7.19	0.77	0.77	0.00	0.00	0.21	0.77	6.47	0.77	3.18	15	
26	INLET 30	1.47	0.64	0.94	5.0	7.19	6.76	6.76	0.00	0.00	1.47	6.76	8.15	6.76	3.83	18	
27	INLET 23	0.68	0.56	0.38	5.0	7.19	2.74	1.74	0.99	0.00	0.68	2.74	6.46	2.74	3.18	15	
28	INLET 15	0.14	0.58	0.08	5.0	7.19	0.58	0.58	0.00	0.00	0.14	0.58	6.44	0.58	1.55	15	
29	INLET 34	0.45	0.79	0.36	5.0	7.19	2.55	2.55	0.00	0.00	0.45	2.55	3.55	2.55	4.69	12	
30	INLET 35	0.23	0.90	0.21	5.0	7.19	1.49	1.49	0.00	0.00	0.80	4.85	6.46	4.85	4.56	15	
Project File: 19157 - Pipe Sizing.stm												Number of lines: 30			Date: 4/28/2022		
NOTES: Intensity = $67.84 / (\text{Inlet time} + 12.00)^{0.79}$ – Return period = 10 Yrs. ; ** Critical depth																	

# Line Profile (Line 1) - INLET 4 OUTLET

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Line 1 - INLET 4 OUTLET



Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
1	44.58	421.00	421.26	2.17	2.17	2.17	423.17	423.43	423.43	8.14	8.13	-1.00	3.78

Project File:

No. Lines: 32

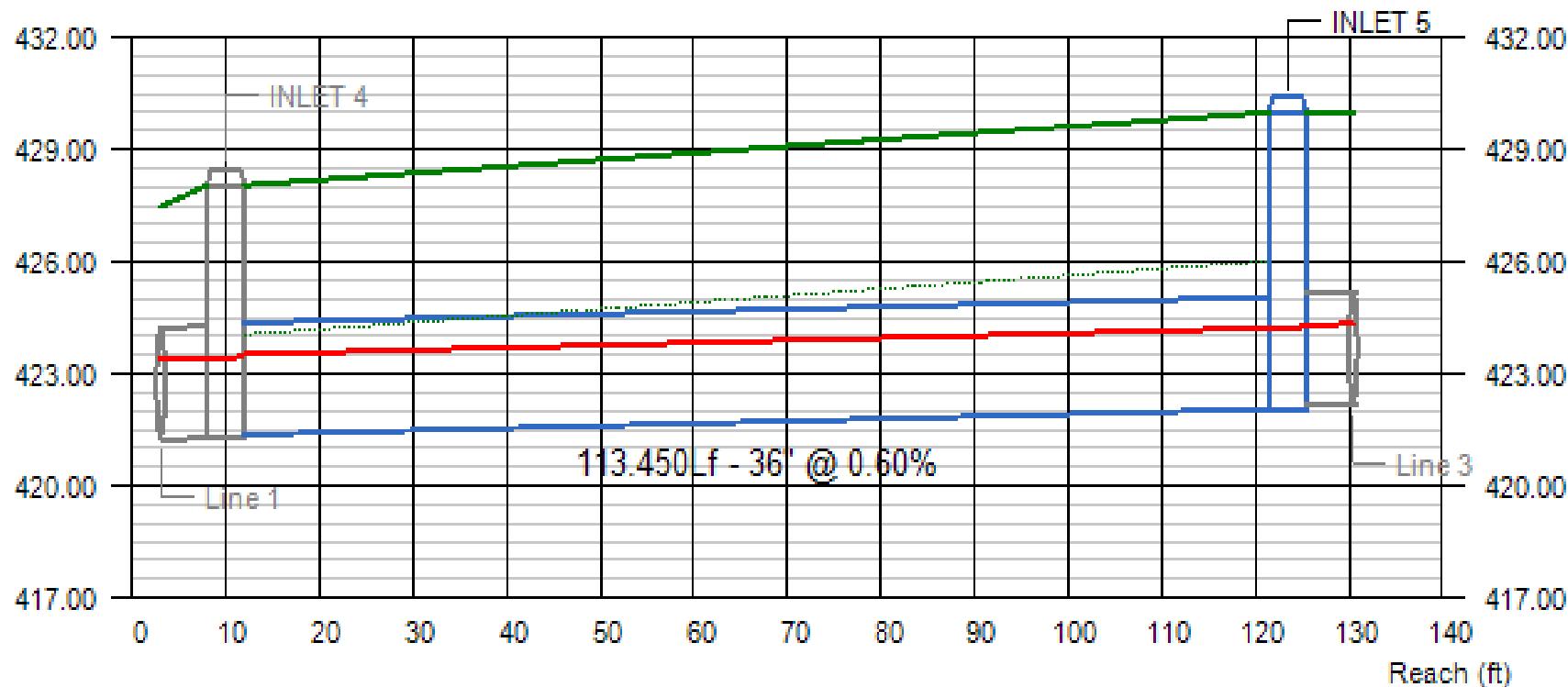
Run Date: 4/28/2022

# Line Profile (Line 2) - INLET 5 OUTLET

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Line 2 - INLET 5 OUTLET

Elev (ft)



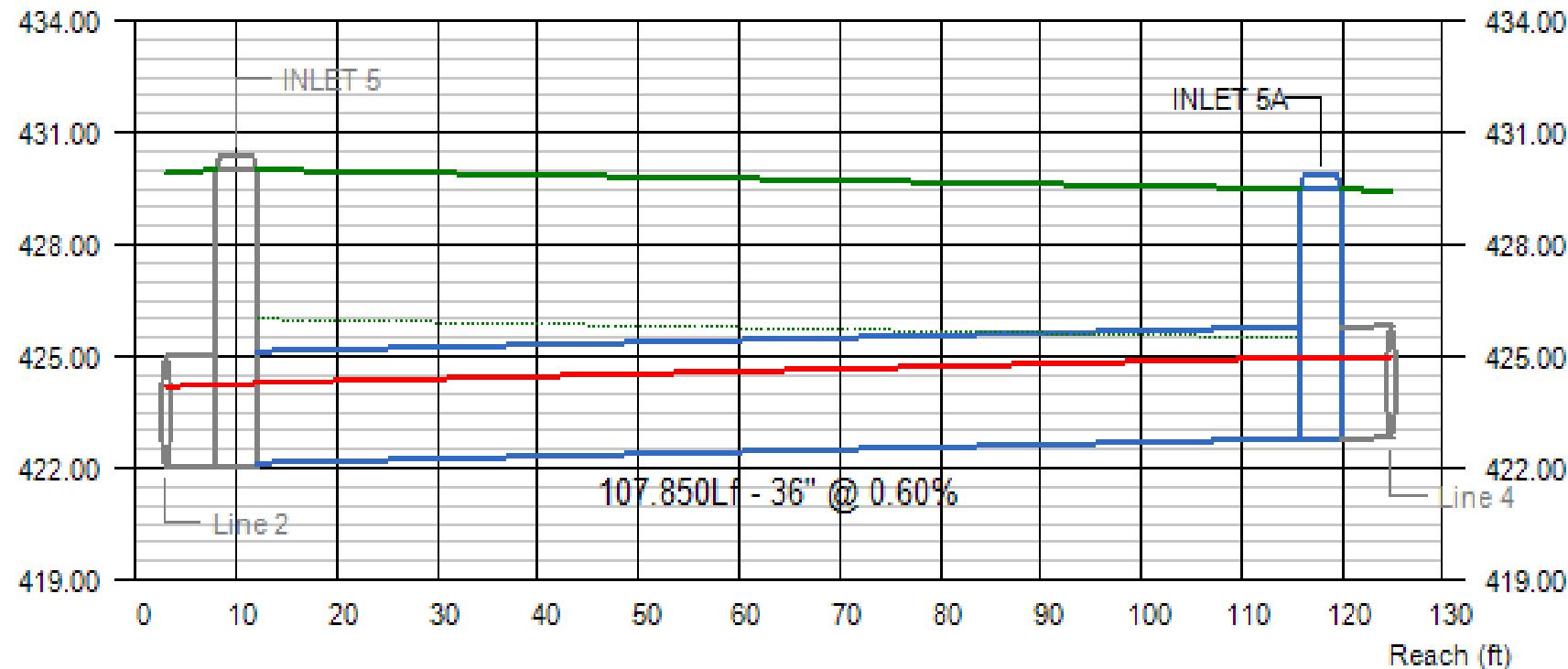
Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
2	44.89	421.36	422.04	2.16	2.18	2.18	423.52	424.22	424.22	8.23	8.15	3.68	4.96
Project File:							No. Lines: 32			Run Date: 4/28/2022			

# Line Profile (Line 3) - INLET 5A OUTLET

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Line 3 - INLET 5A OUTLET

Elev (ft)



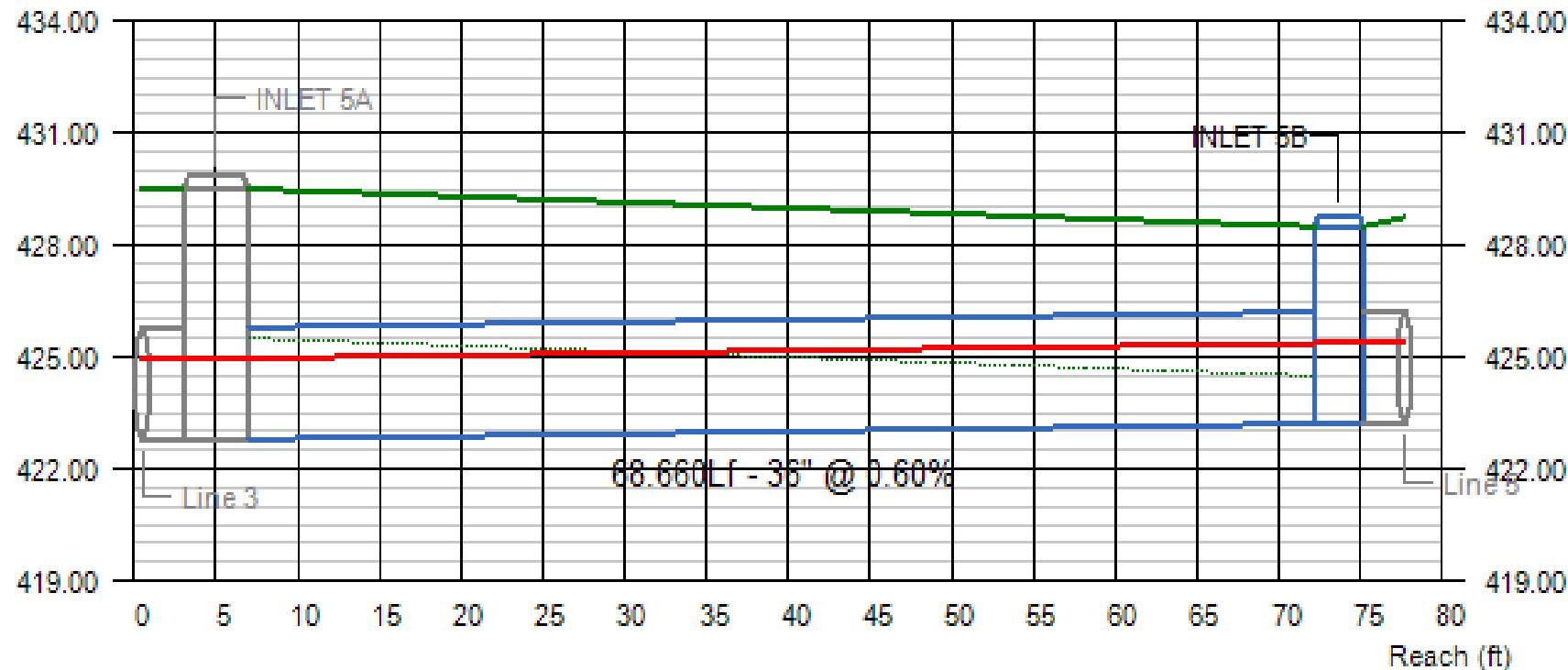
Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
3	44.84	422.14	422.79	2.16	2.18	2.18	424.30	424.97	424.97	8.24	8.15	4.86	3.71
Project File:							No. Lines: 32			Run Date: 4/28/2022			

# Line Profile (Line 4) - INLET 5B OUTLET

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Line 4 - INLET 5B OUTLET

Elev (ft)



Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
4	44.52	422.79	423.20	2.18	2.17	2.17	424.97	425.37	425.37	8.09	8.12	3.71	2.30

Project File:

No. Lines: 32

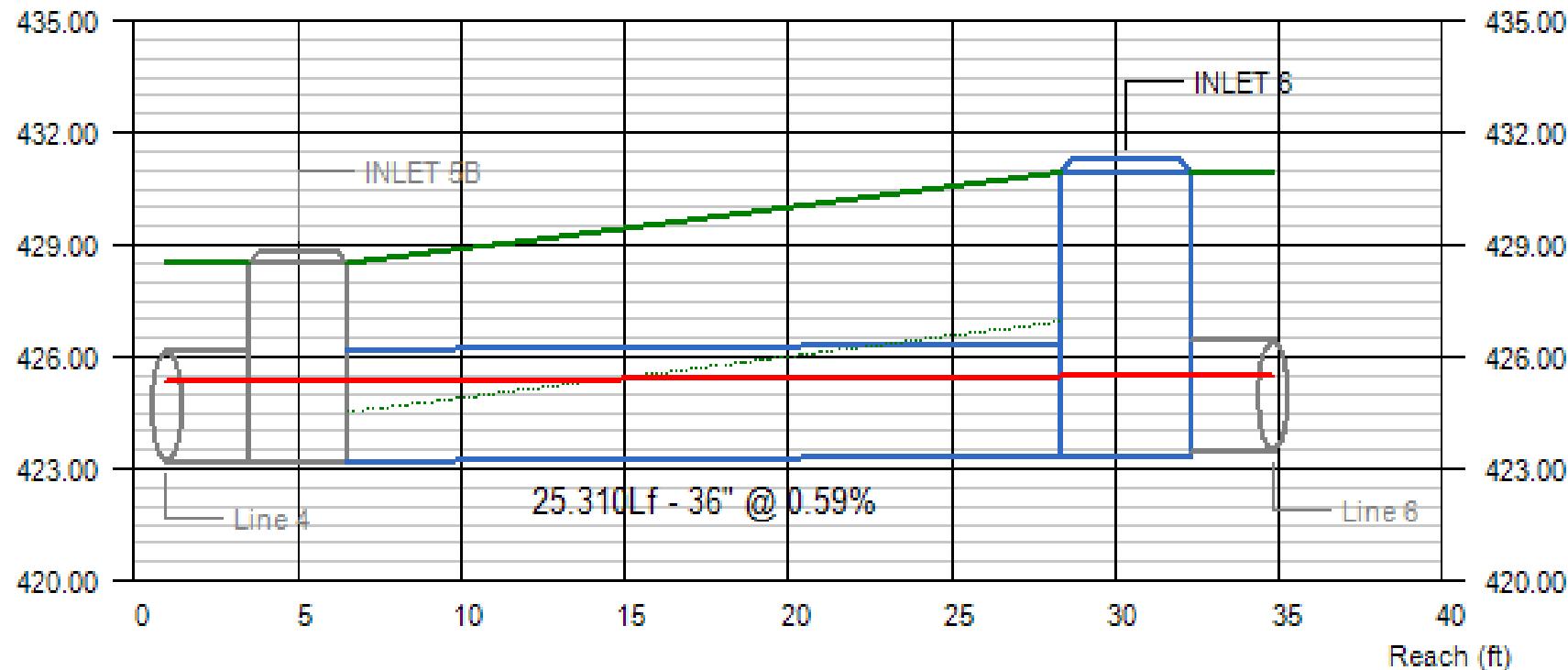
Run Date: 4/28/2022

# Line Profile (Line 5) - INLET 6 OUTLET

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Line 5 - INLET 6 OUTLET

Elev (ft)



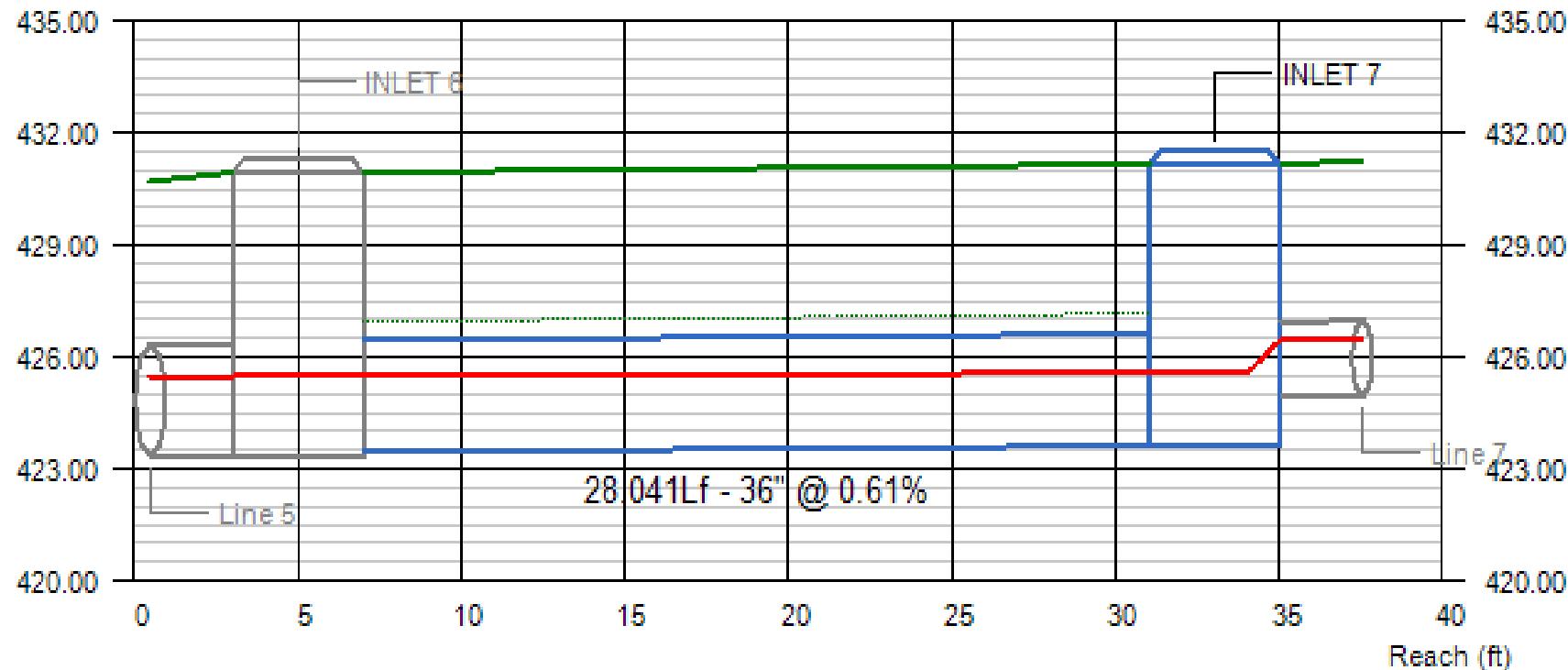
Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
5	43.31	423.20	423.35	2.17	2.14	2.14	425.37	425.49	425.49	7.90	8.02	2.30	4.59
Project File:							No. Lines: 32			Run Date: 4/28/2022			

# Line Profile (Line 6) - INLET 7 OUTLET

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Line 6 - INLET 7 OUTLET

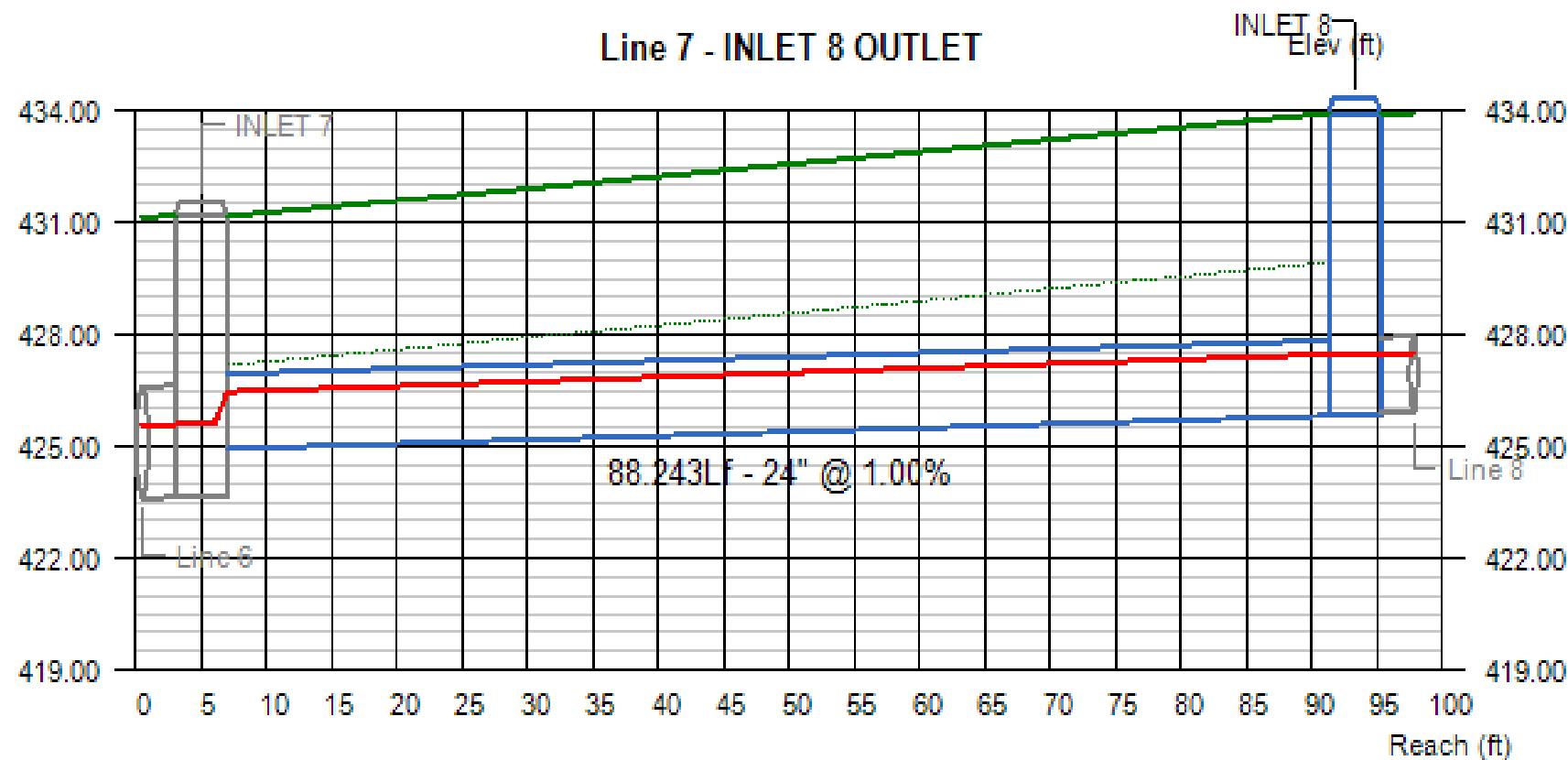
Elev (ft)



Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
6	36.76	423.45	423.62	2.04	1.97	1.97	425.49	425.59	425.59	7.17	7.47	4.49	4.54
Project File:							No. Lines: 32			Run Date: 4/28/2022			

# Line Profile (Line 7) - INLET 8 OUTLET

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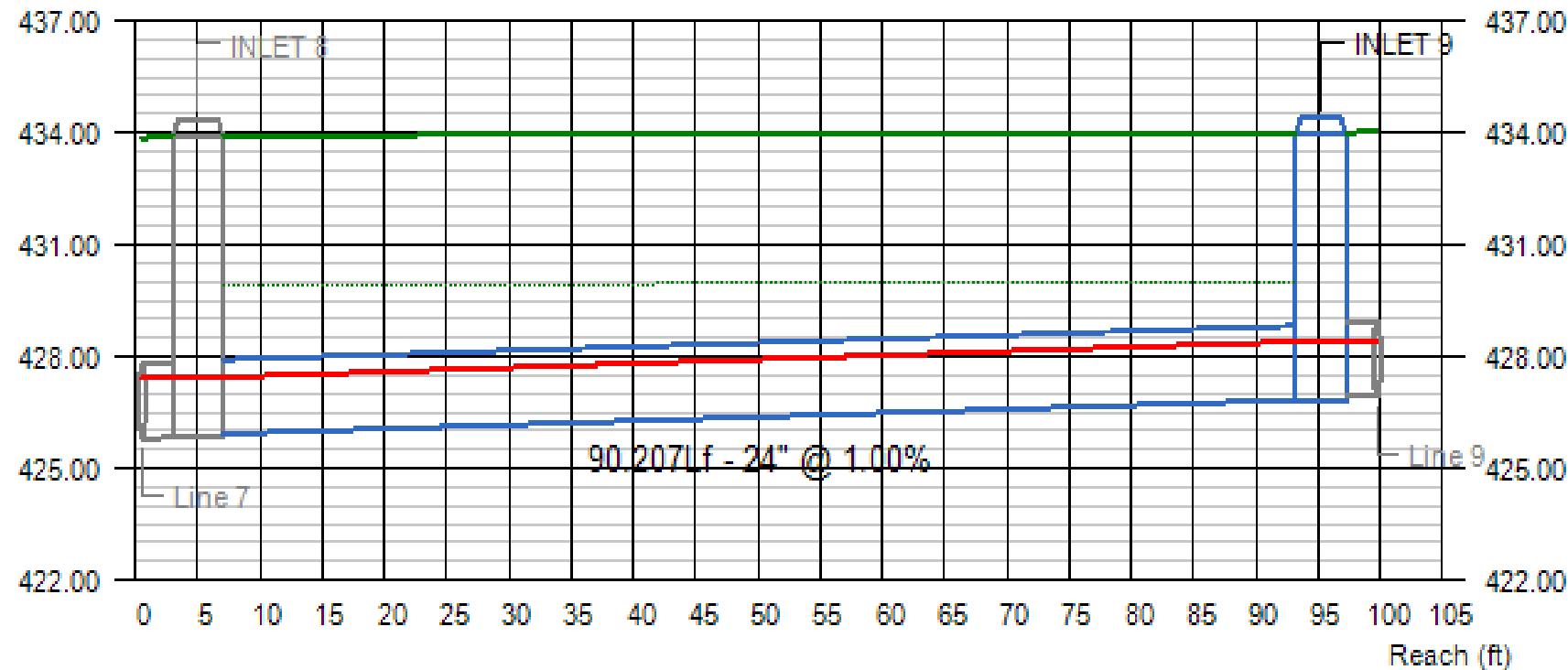
Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
7	20.87	424.94	425.82	1.52	1.64	1.64	426.46	427.46	427.46	8.16	7.59	4.22	6.10
Project File:							No. Lines: 32			Run Date: 4/28/2022			

# Line Profile (Line 8) - INLET 9 OUTLET

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Line 8 - INLET 9 OUTLET

Elev (ft)



Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
8	19.37	425.92	426.82	1.54	1.58	1.58	427.46	428.40	428.40	7.48	7.27	6.00	5.15

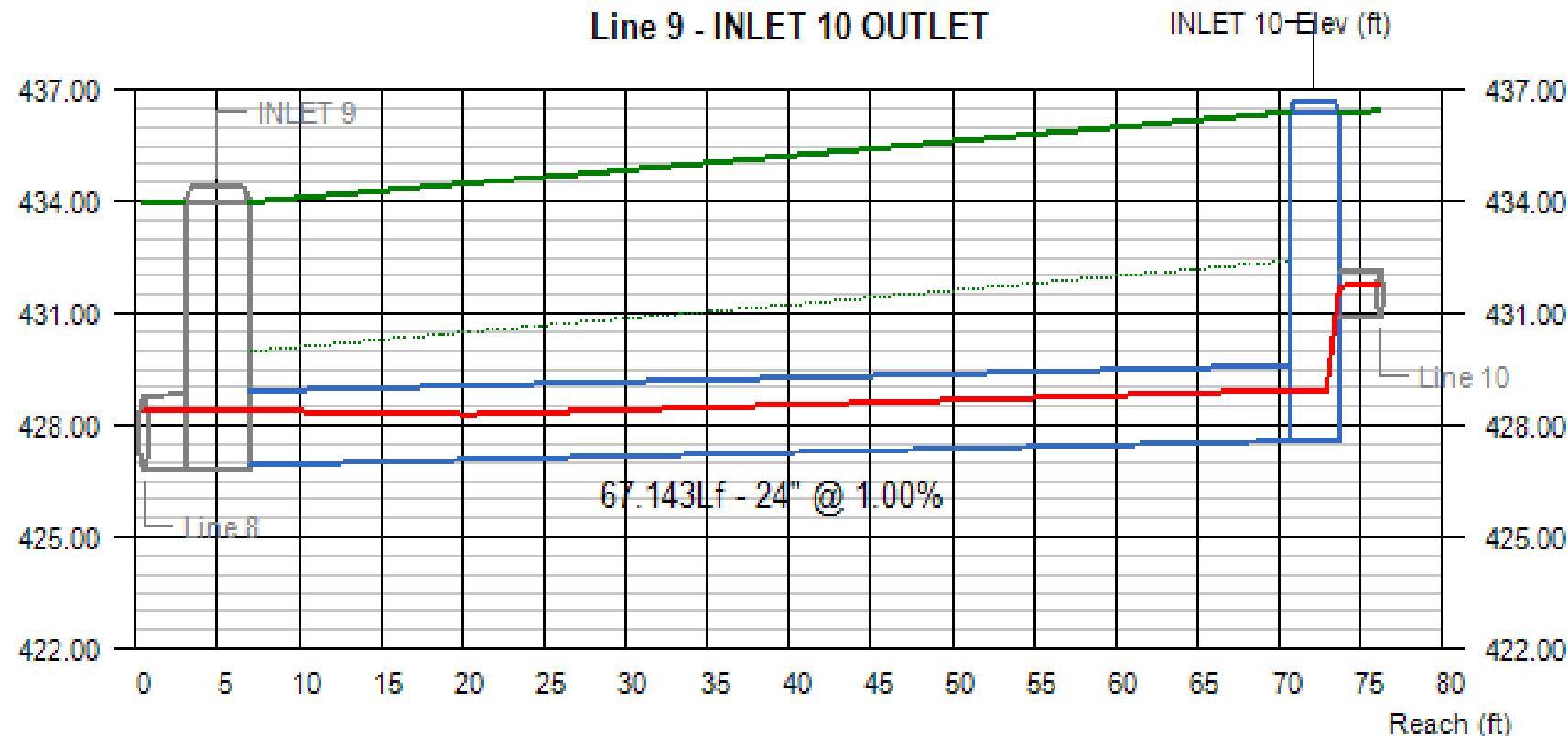
Project File:

No. Lines: 32

Run Date: 4/28/2022

# Line Profile (Line 9) - INLET 10 OUTLET

Page 1 of 1



Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
9	13.99	426.92	427.59	1.48	1.35	1.35	428.40	428.94 j	428.94	5.61	6.22	5.05	6.81

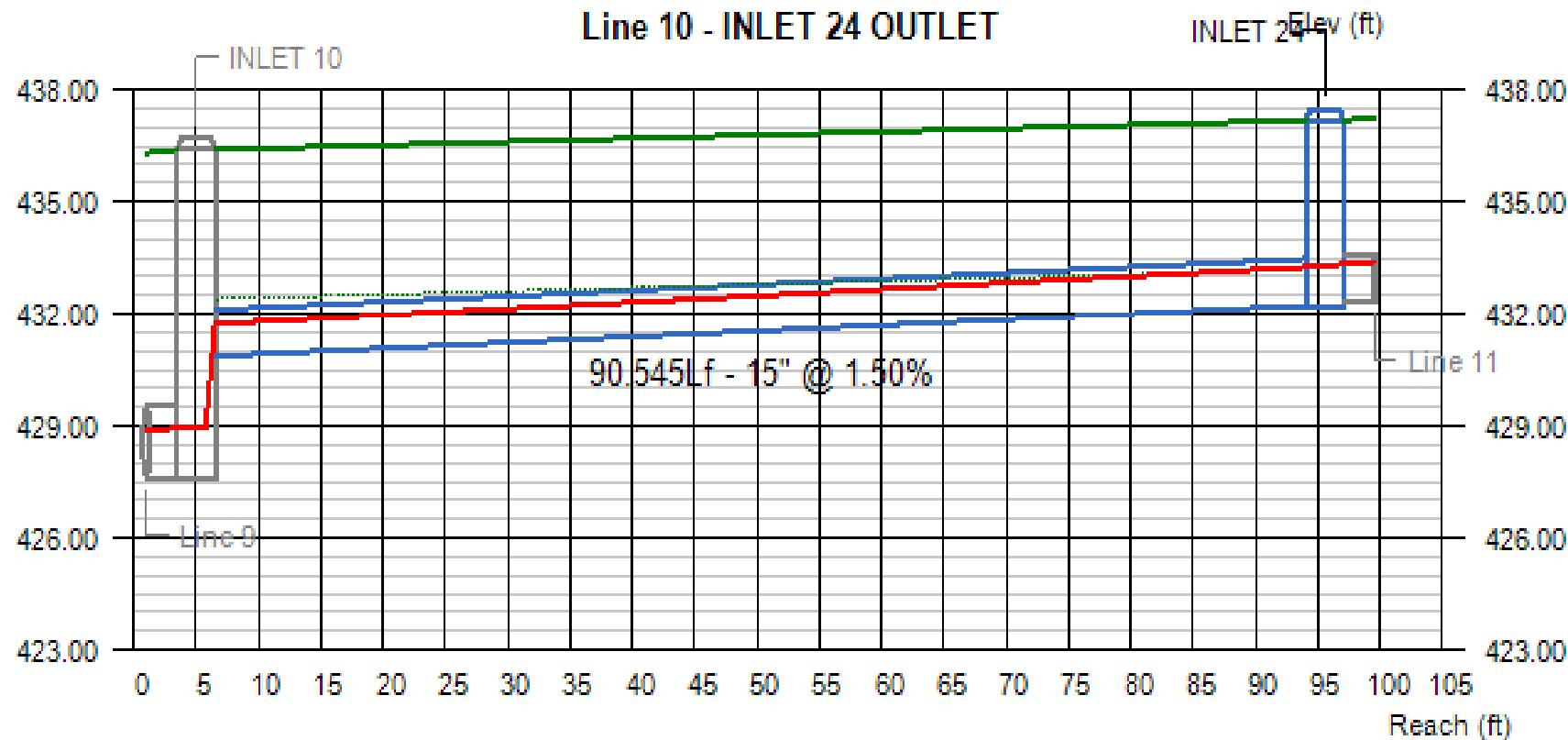
Project File:

No. Lines: 32

Run Date: 4/28/2022

# Line Profile (Line 10) - INLET 24 OUTLET

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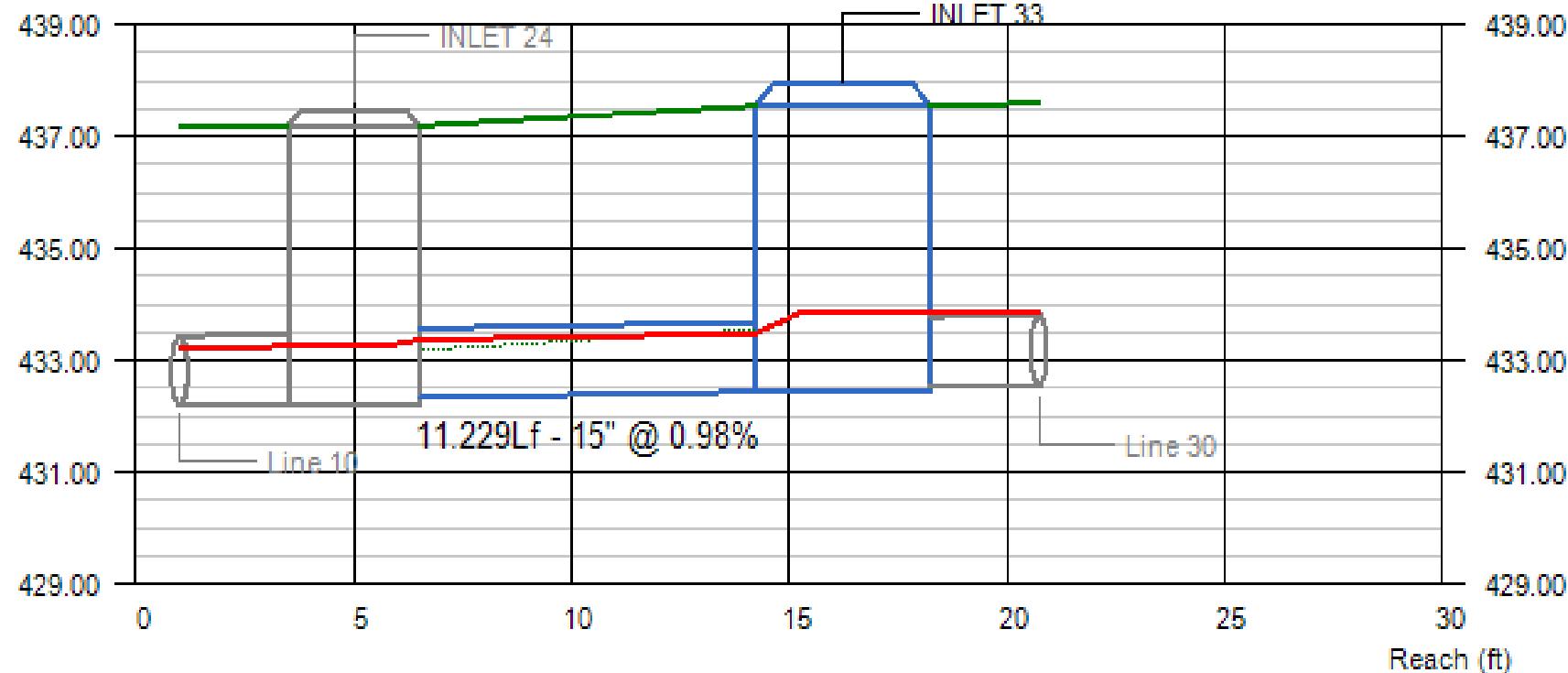
Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
10	6.57	430.86	432.22	0.87	1.03	1.03	431.73	433.25	433.25	7.21	6.07	4.29	3.71
Project File:							No. Lines: 32			Run Date: 4/28/2022			

# Line Profile (Line 11) - INLET 33 OUTLET

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Line 11 - INLET 33 OUTLET

Elev (ft)



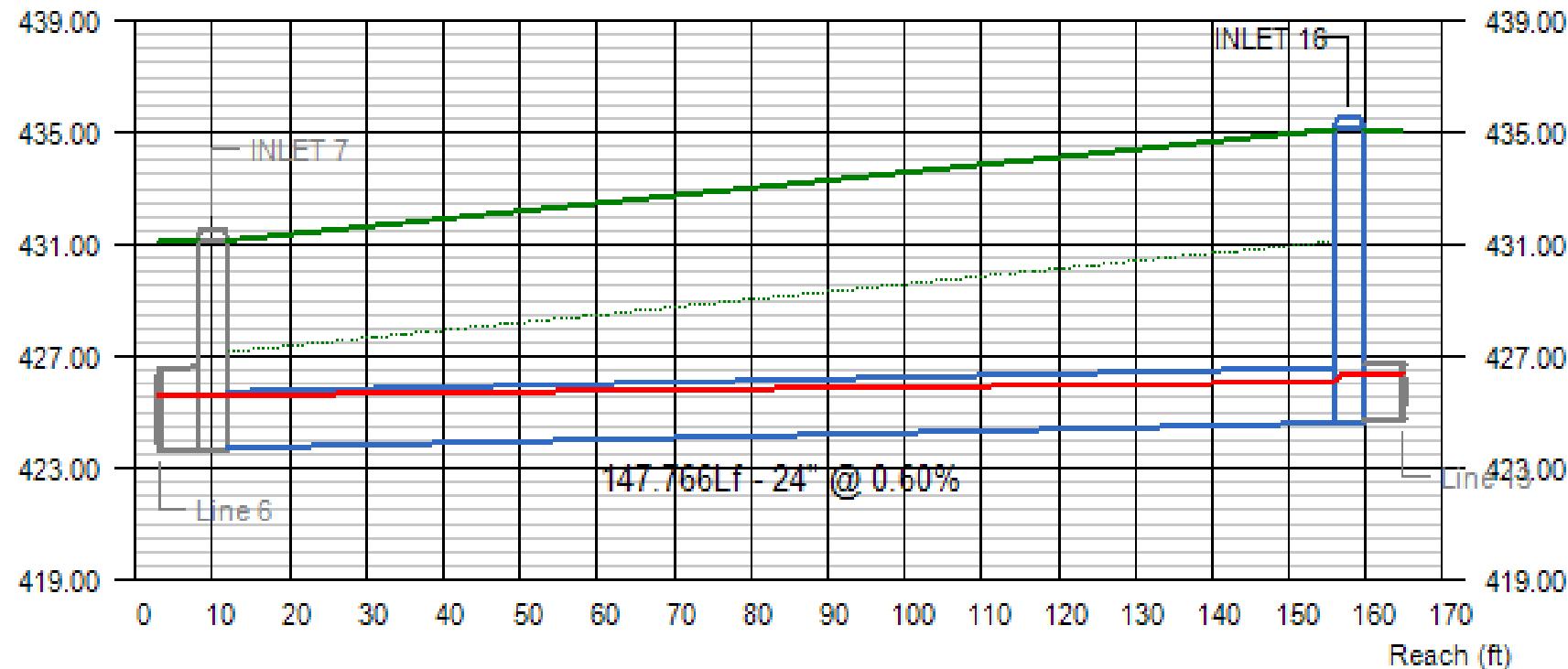
Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
11	6.52	432.32	432.43	1.05	1.05	1.41	433.37	433.48	433.84	5.93	5.93	3.61	3.87
Project File:								No. Lines: 32			Run Date: 4/28/2022		

# Line Profile (Line 12) - INLET 16 OUTLET

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Line 12 - INLET 16 OUTLET

Elev (ft)



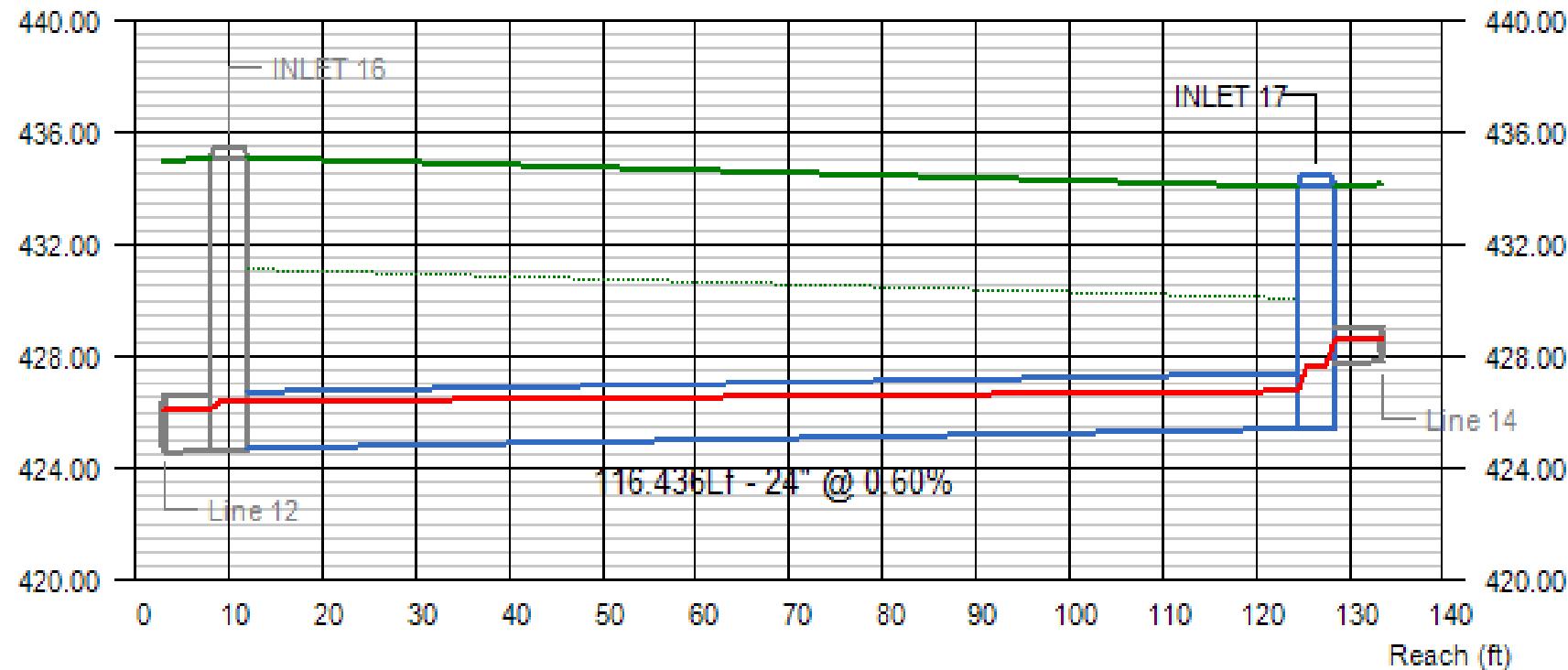
Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
12	15.04	423.72	424.61	1.87	1.48	1.76	425.59	426.09	426.37	4.92	6.04	5.44	8.49
Project File:								No. Lines: 32			Run Date: 4/28/2022		

# Line Profile (Line 13) - INLET 17 OUTLET

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Line 13 - INLET 17 OUTLET

Elev (ft)



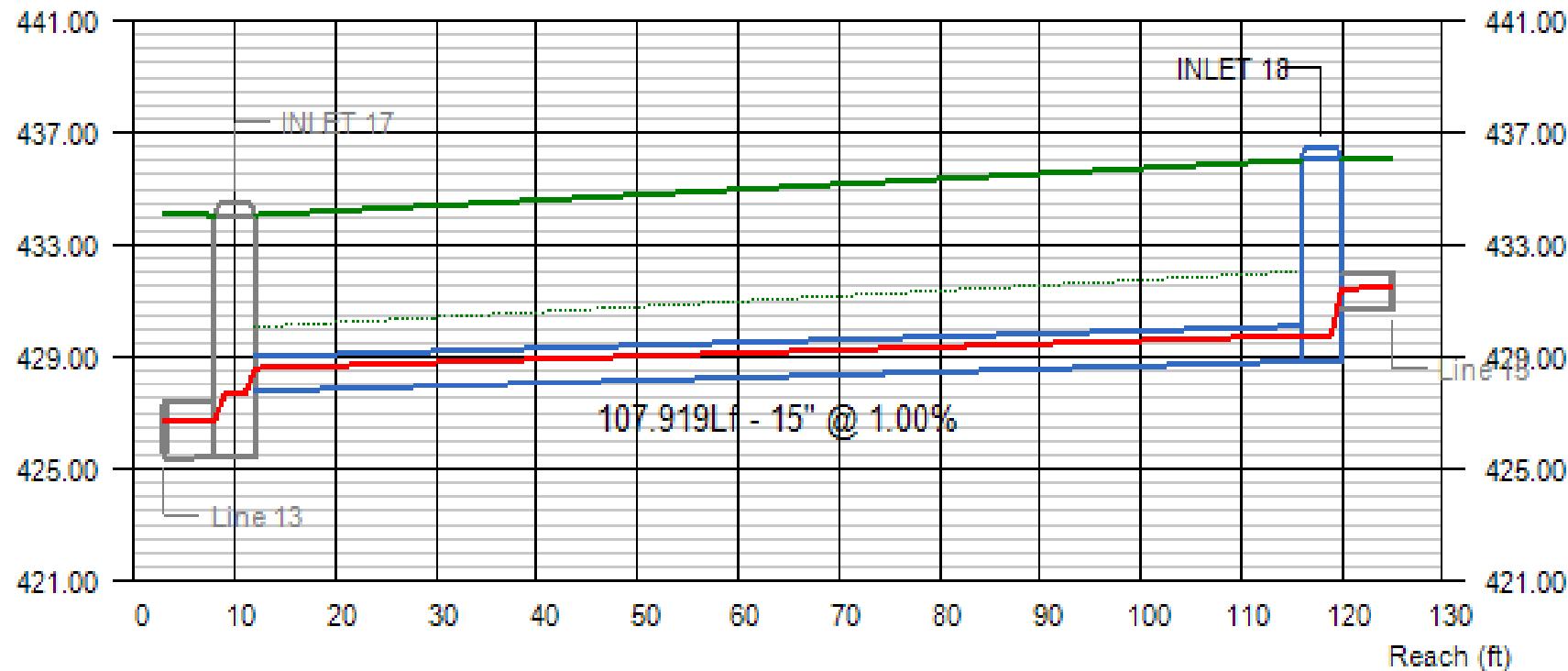
Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
13	13.81	424.71	425.41	1.66	1.34	2.23	426.37	426.75	427.64	4.95	6.16	8.39	6.66
Project File:							No. Lines: 32			Run Date: 4/28/2022			

# Line Profile (Line 14) - INLET 18 OUTLET

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Line 14 - INLET 18 OUTLET

Elev (ft)



Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
14	5.12	427.77	428.85	0.84	0.92	0.92	428.61	429.77	429.77	5.84	5.31	5.05	5.93

Project File:

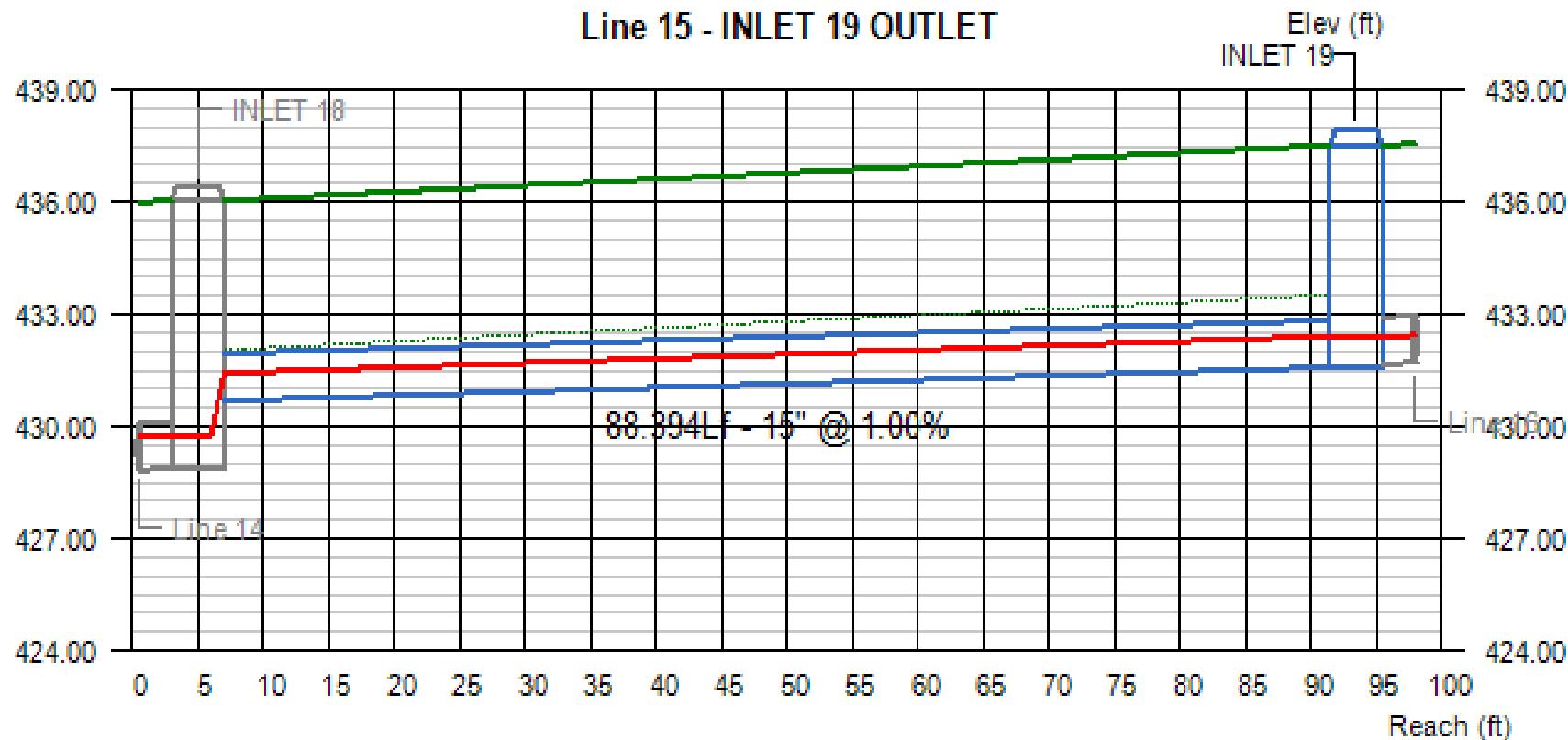
No. Lines: 32

Run Date: 4/28/2022

# Line Profile (Line 15) - INLET 19 OUTLET

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Line 15 - INLET 19 OUTLET



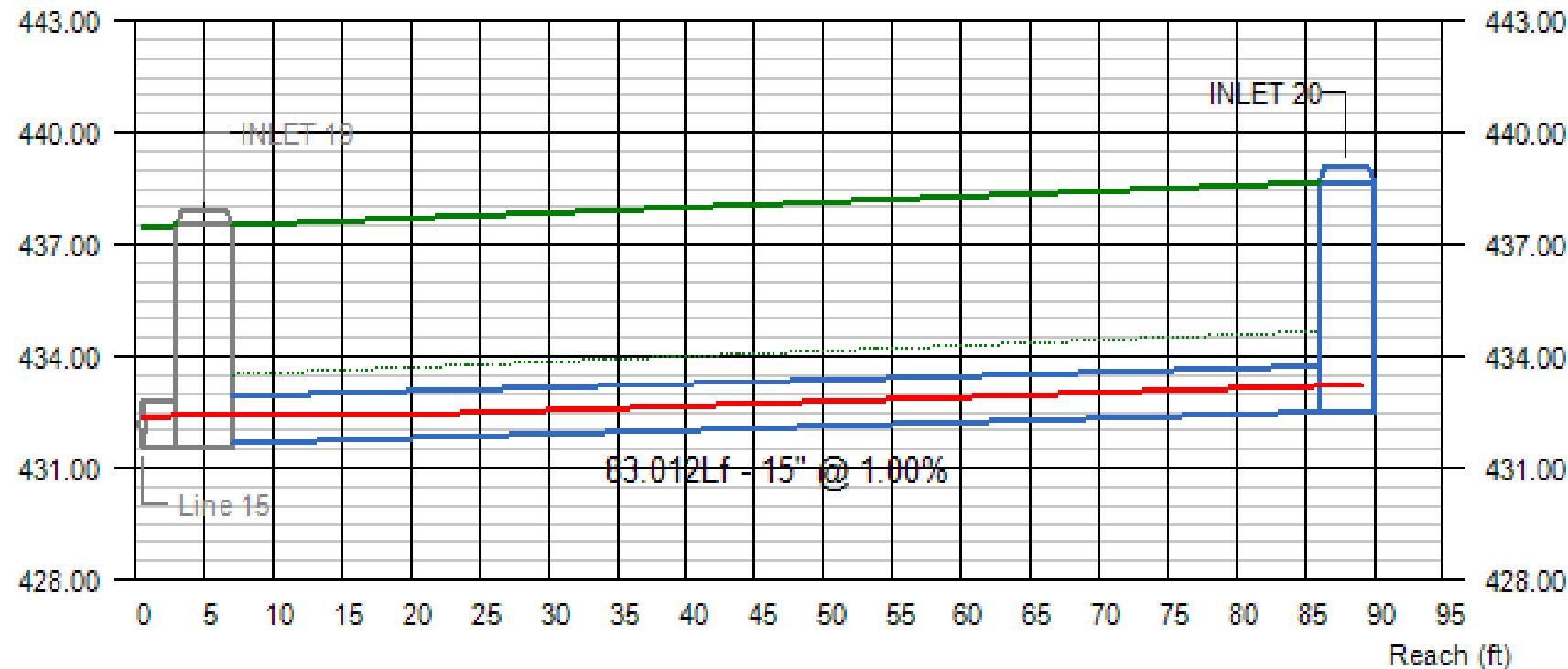
Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
15	4.18	430.69	431.57	0.73	0.83	0.83	431.42	432.40	432.40	5.58	4.85	4.09	4.70
Project File:								No. Lines: 32			Run Date: 4/28/2022		

# Line Profile (Line 16) - INLET 20 OUTLET

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Line 16 - INLET 20 OUTLET

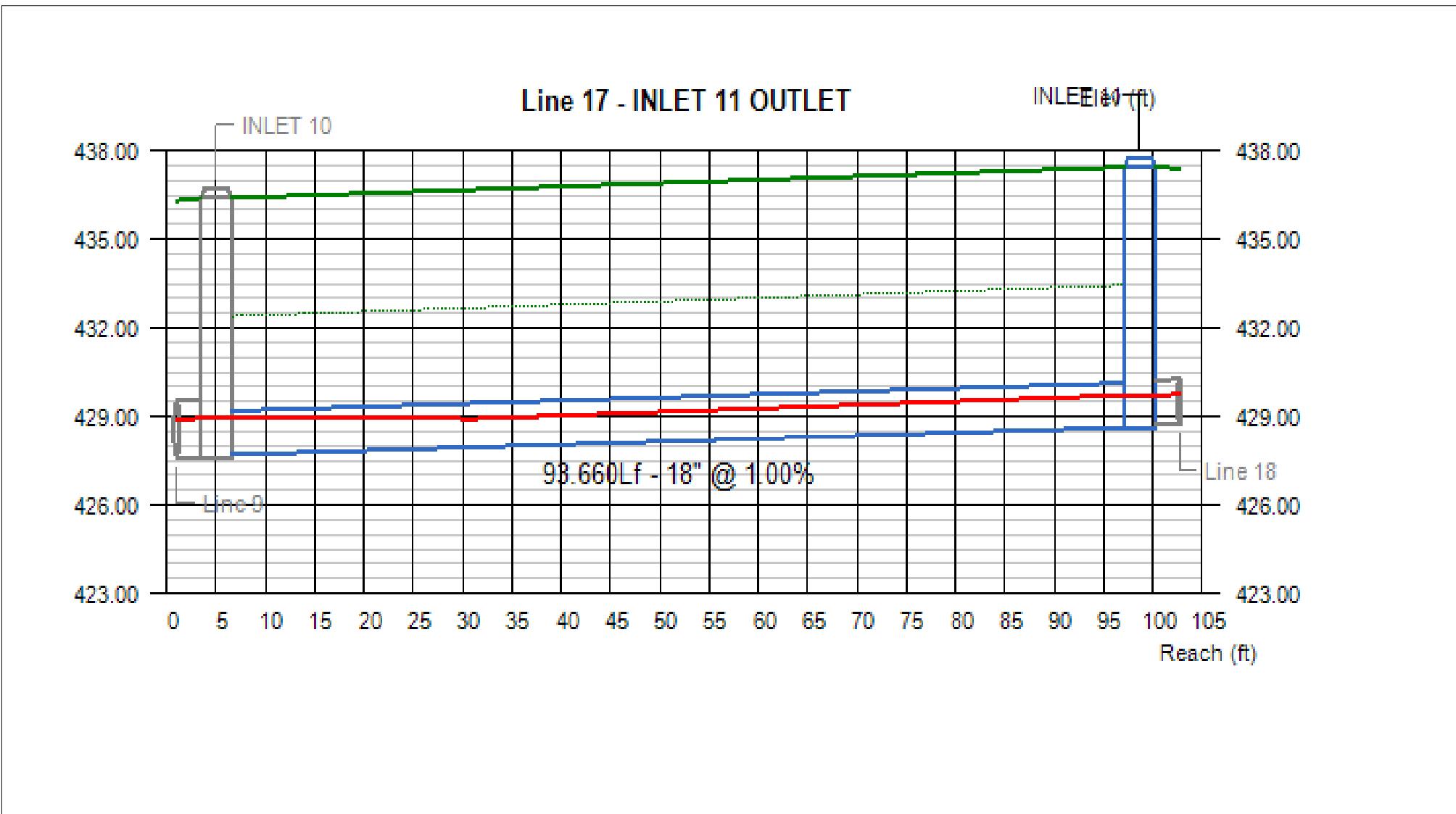
Elev (ft)



Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
16	3.05	431.67	432.50	0.73	0.70	0.70	432.40	433.20 j	433.20	4.12	4.30	4.60	4.92
Project File:							No. Lines: 32			Run Date: 4/28/2022			

# Line Profile (Line 17) - INLET 11 OUTLET

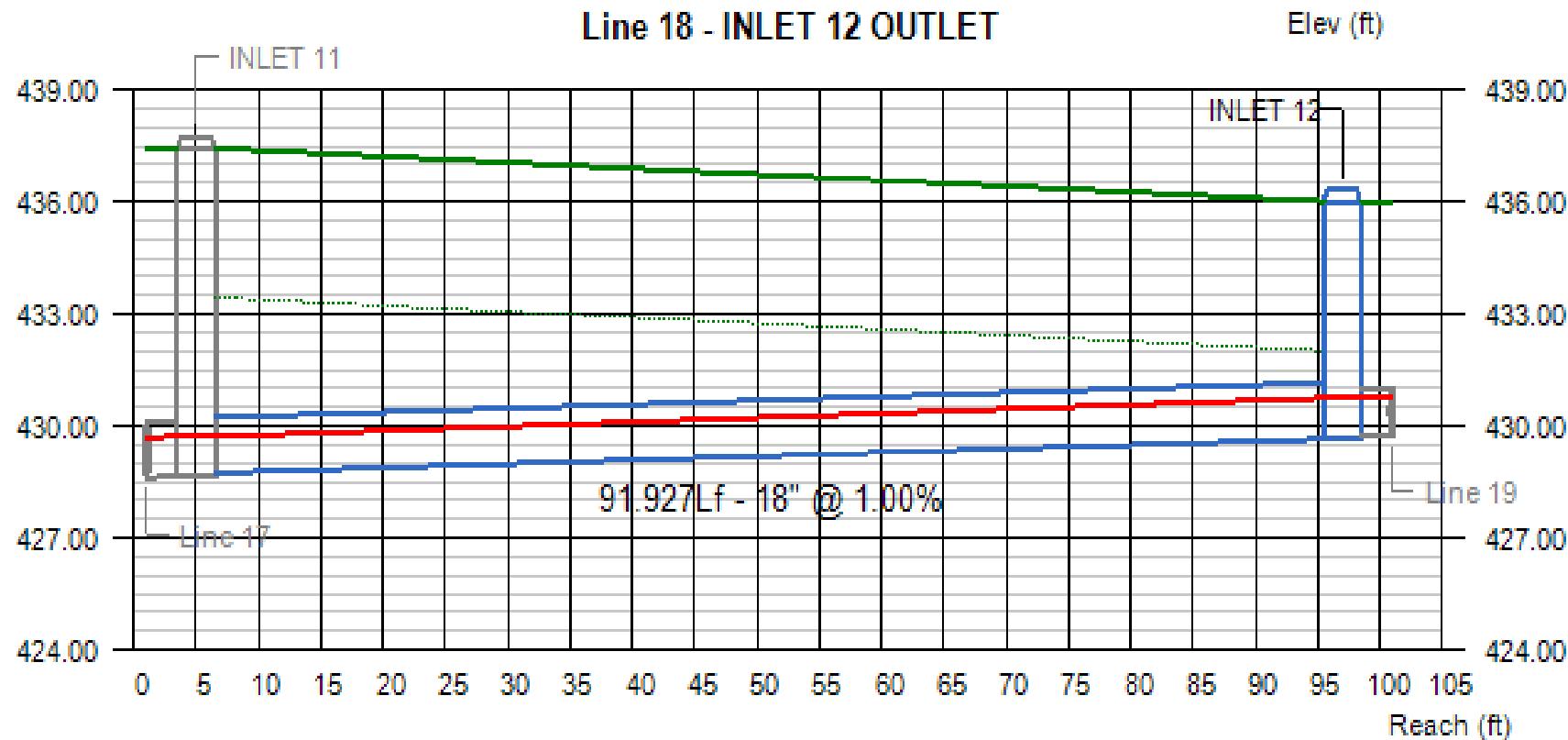
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Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
17	7.91	427.69	428.63	1.25	1.09	1.09	428.94	429.72 j	429.72	5.04	5.76	7.21	7.31
Project File:							No. Lines: 32			Run Date: 4/28/2022			

# Line Profile (Line 18) - INLET 12 OUTLET

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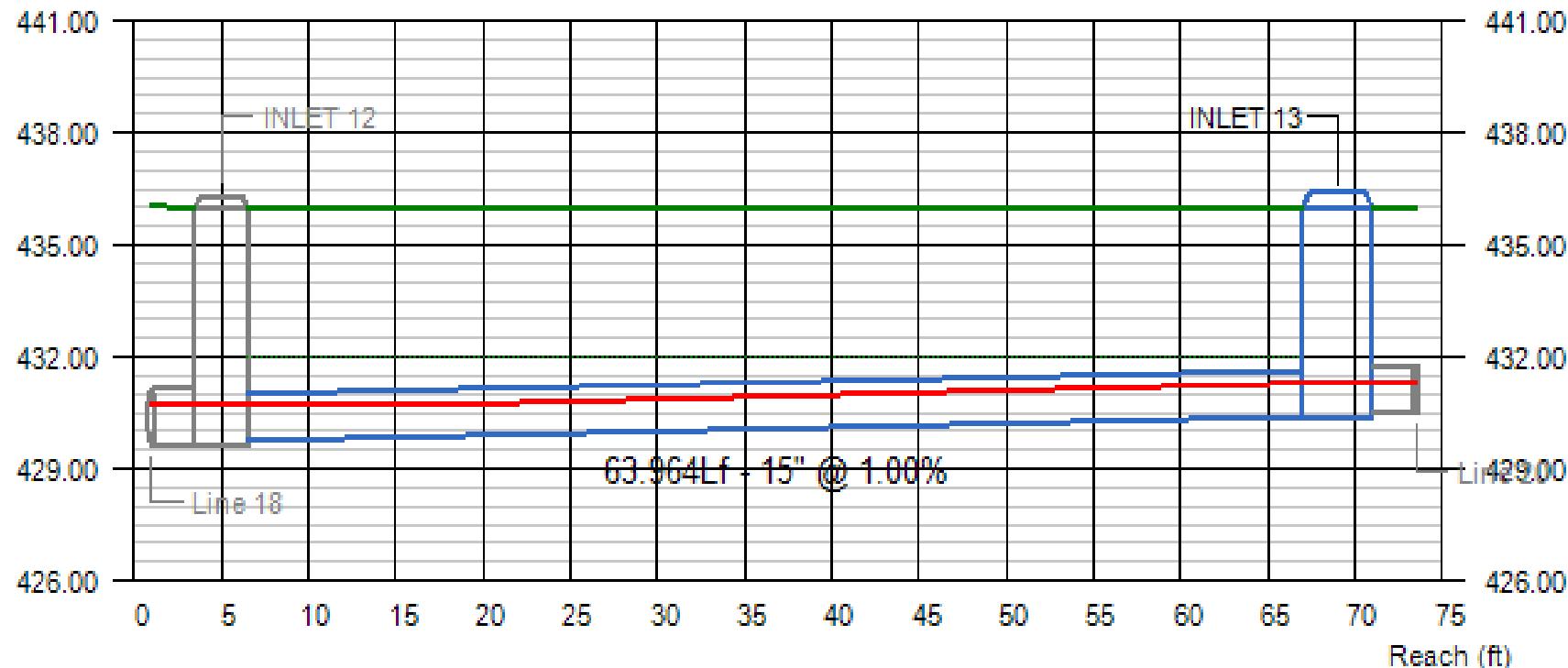
Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
18	7.97	428.73	429.65	0.99	1.09	1.09	429.72	430.74	430.74	6.45	5.78	7.21	4.85
Project File:							No. Lines: 32			Run Date: 4/28/2022			

# Line Profile (Line 19) - INLET 13 OUTLET

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Line 19 - INLET 13 OUTLET

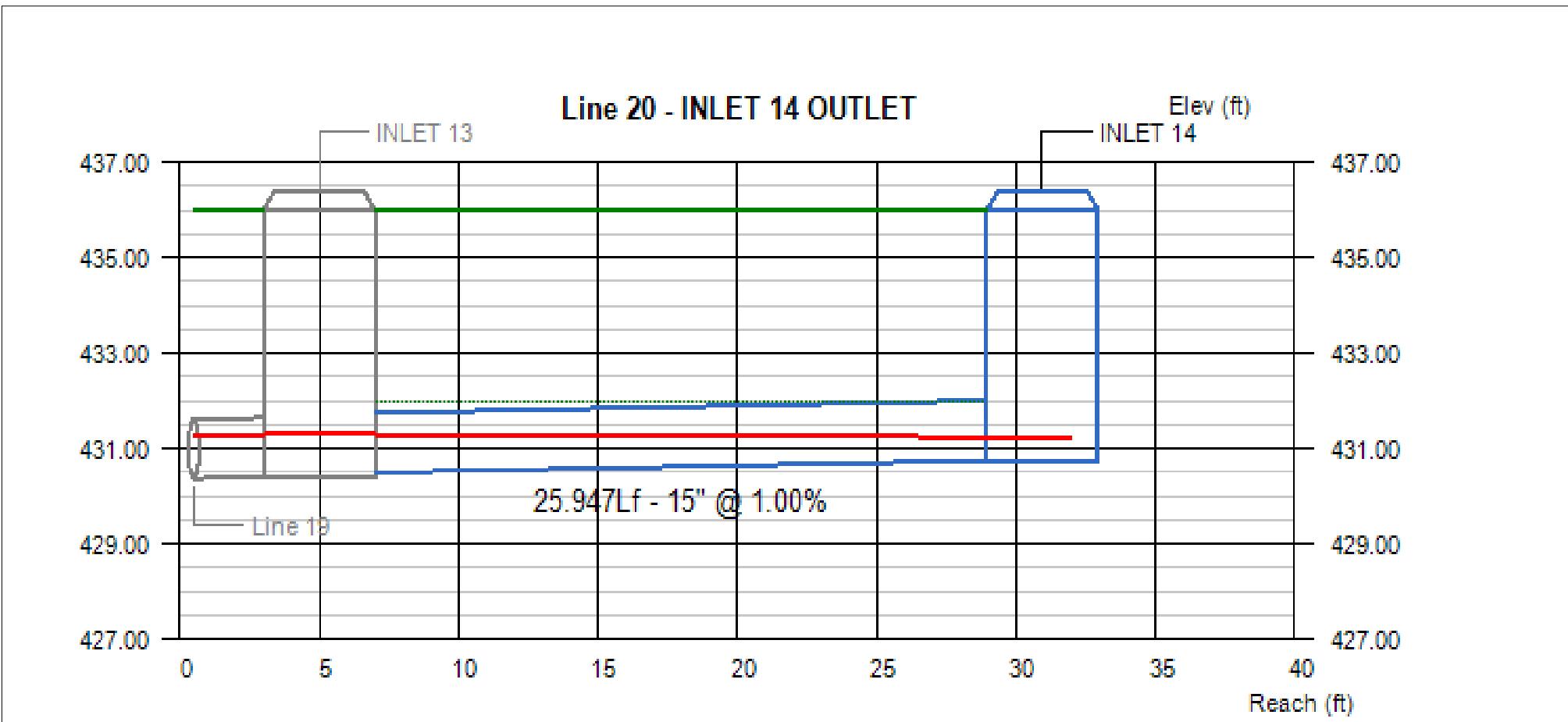
Elev (ft)



Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
19	4.99	429.75	430.39	0.99	0.91	0.91	430.74	431.30 j	431.30	4.78	5.25	5.00	4.36
Project File:							No. Lines: 32			Run Date: 4/28/2022			

# Line Profile (Line 20) - INLET 14 OUTLET

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Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
20	1.53	430.49	430.75	0.81	0.49	0.49	431.30	431.24	431.24	1.83	3.43	4.26	4.00

Project File:

No. Lines: 32

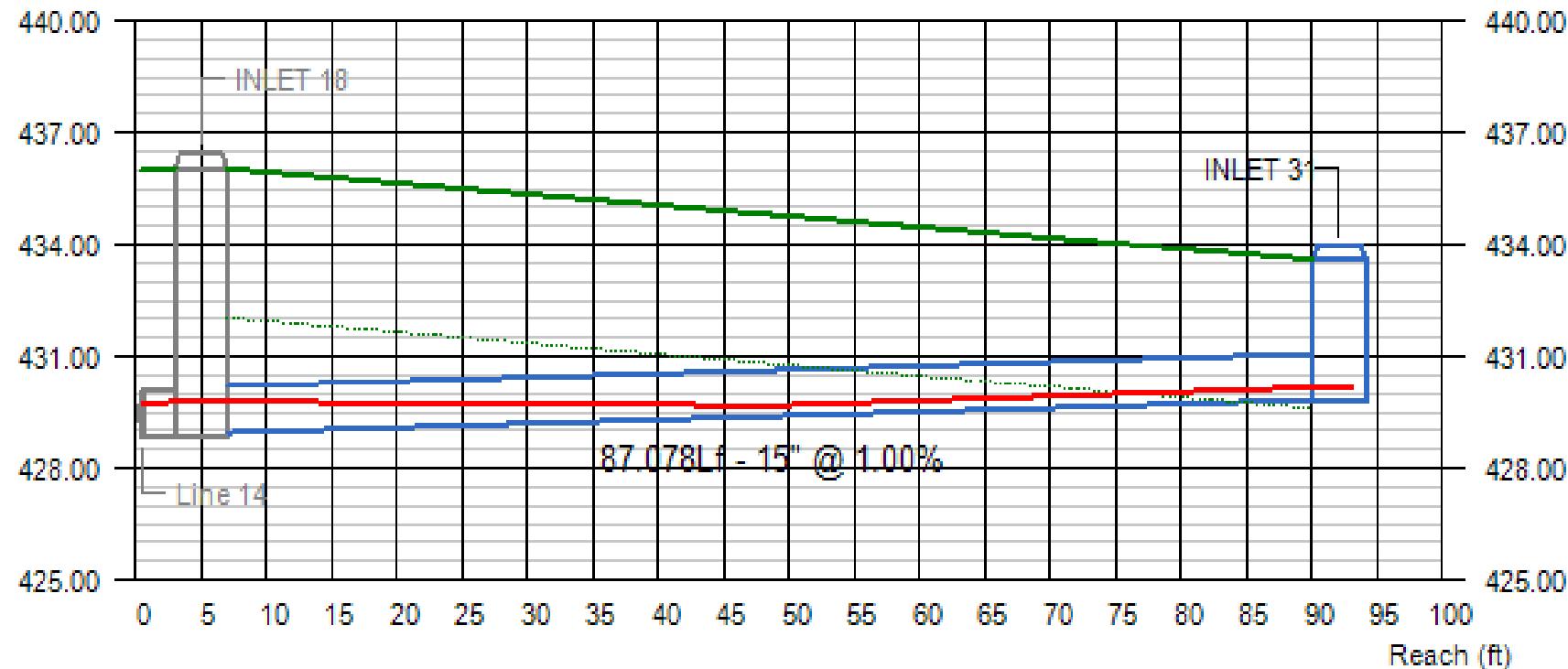
Run Date: 4/28/2022

# Line Profile (Line 21) - INLET 31 OUTLET

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Line 21 - INLET 31 OUTLET

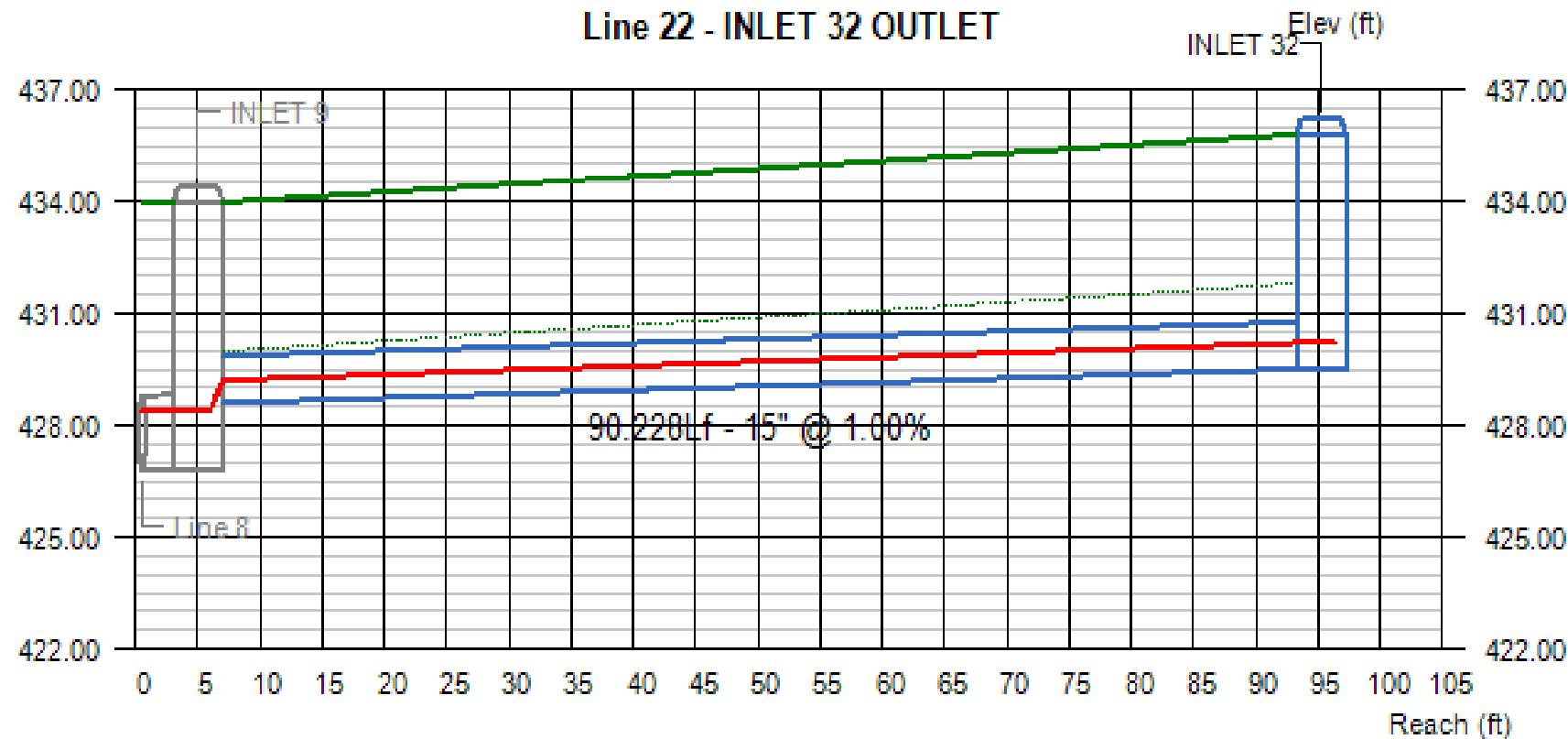
Elev (ft)



Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
21	0.78	428.95	429.82	0.82	0.34	0.34	429.77	430.16 j	430.16	0.91	2.82	5.83	2.52
Project File:							No. Lines: 32			Run Date: 4/28/2022			

# Line Profile (Line 22) - INLET 32 OUTLET

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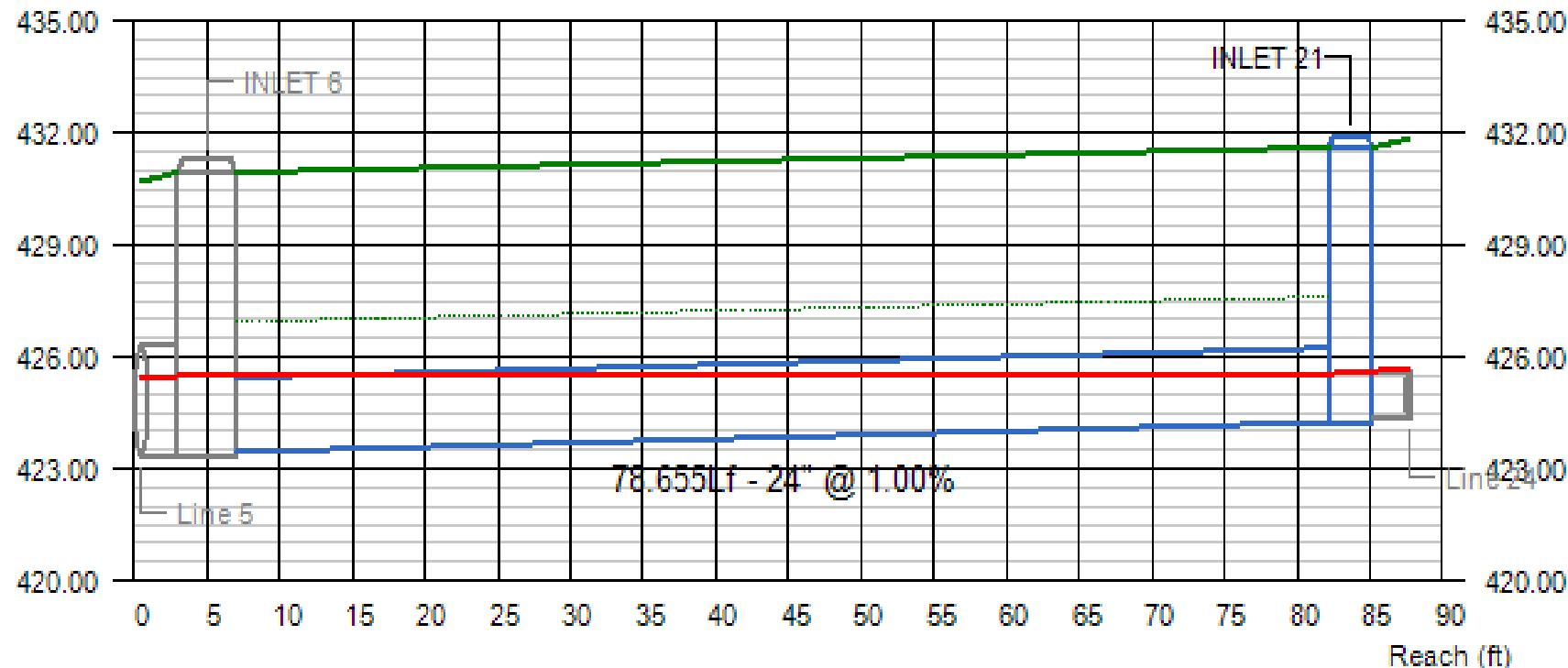
Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
22	3.07	428.60	429.50	0.61	0.70	0.70	429.21	430.20	430.20	5.19	4.31	4.12	5.05
Project File:							No. Lines: 32			Run Date: 4/28/2022			

# Line Profile (Line 23) - INLET 21 OUTLET

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Line 23 - INLET 21 OUTLET

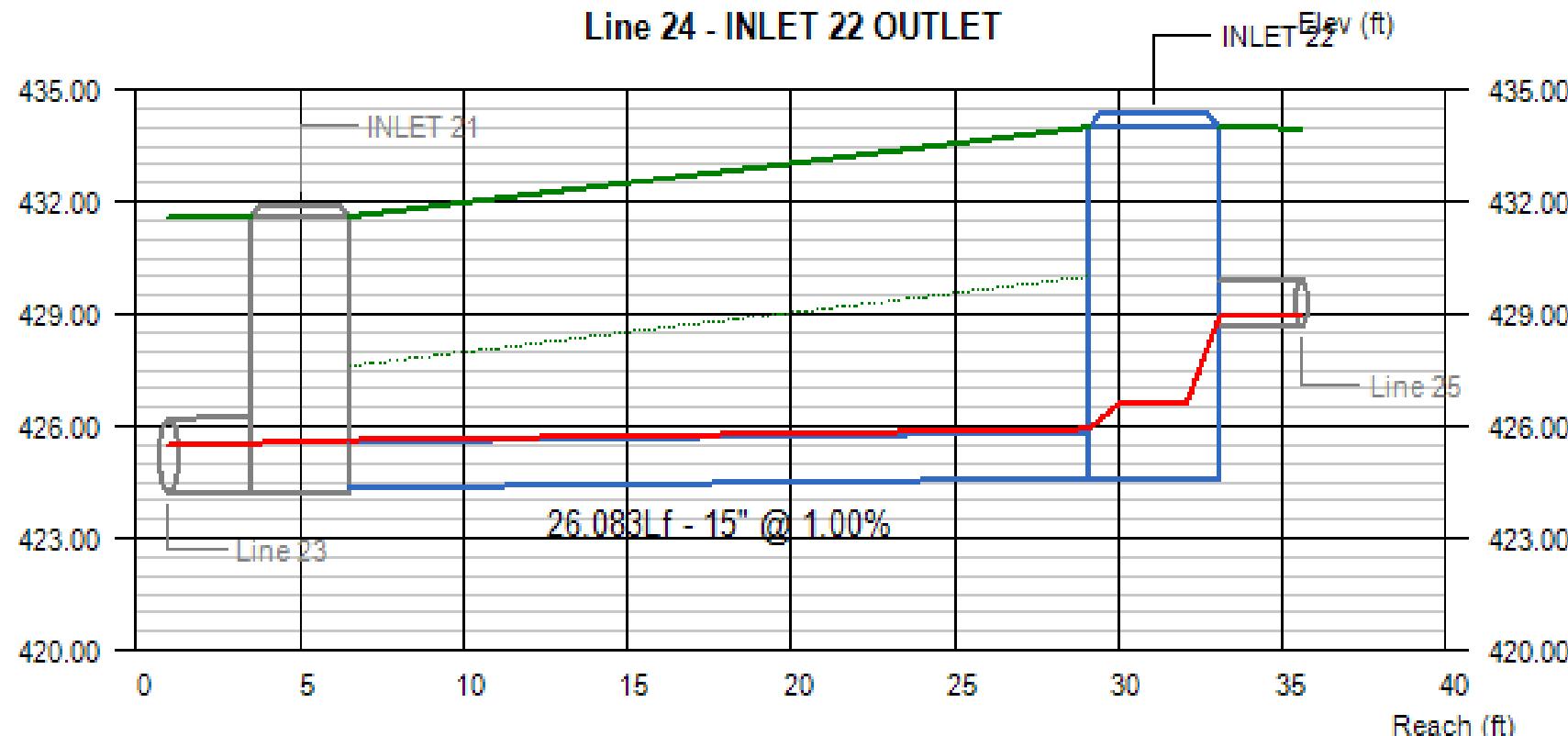
Elev (ft)



Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
23	7.01	423.45	424.24	2.00	1.27	1.39	425.49	425.51	425.63	2.23	3.35	5.49	5.36
Project File:							No. Lines: 32			Run Date: 4/28/2022			

# Line Profile (Line 24) - INLET 22 OUTLET

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Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
24	6.97	424.34	424.60	1.25	1.25	2.05	425.63	425.94	426.65	5.68	5.68	6.01	8.15

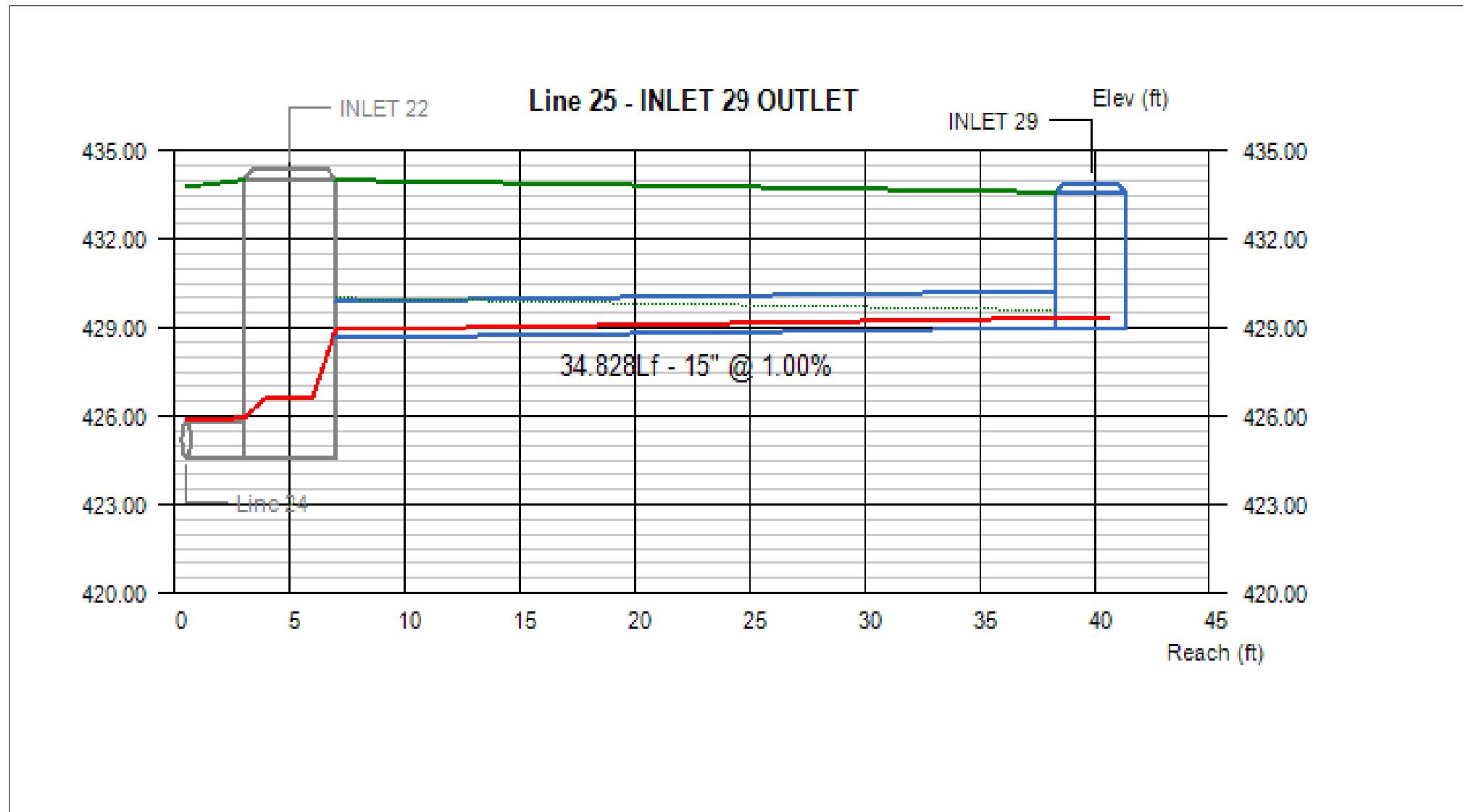
Project File:

No. Lines: 32

Run Date: 4/28/2022

# Line Profile (Line 25) - INLET 29 OUTLET

Page 1 of 1



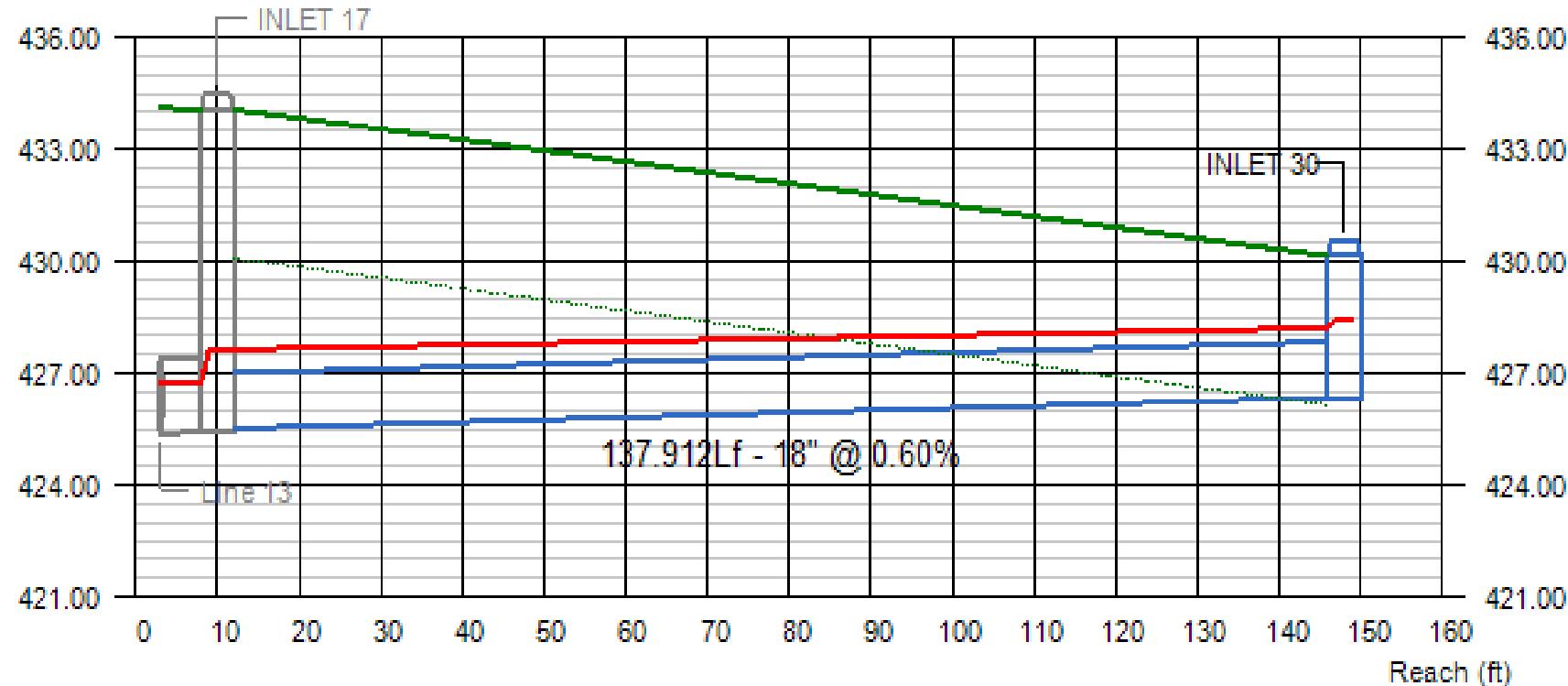
Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
25	0.77	428.64	428.99	0.29	0.34	0.34	428.93	429.33	429.33	3.54	2.81	4.11	3.35
Project File:								No. Lines: 32			Run Date: 4/28/2022		

# Line Profile (Line 26) - INLET 30 OUTLET

Page 1 of 1

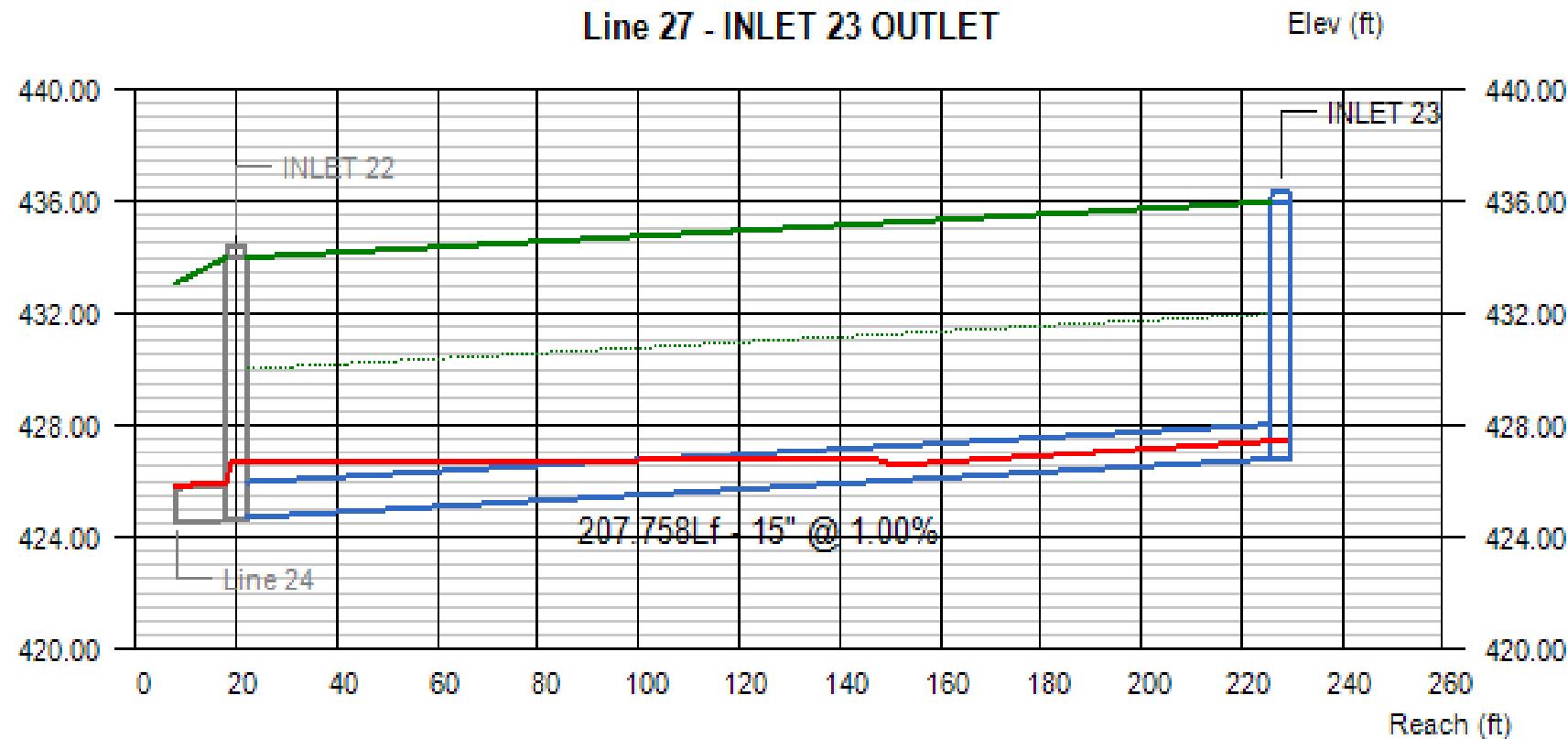
Line 26 - INLET 30 OUTLET

Elev (ft)



Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
26	6.76	425.51	426.34	1.50	1.50	2.10	427.64	428.21	428.44	3.83	3.83	7.06	2.31
Project File:								No. Lines: 32				Run Date: 4/28/2022	

## Line Profile (Line 27) - INLET 23 OUTLET



Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
27	2.74	424.70	426.78	1.25	0.66	0.66	426.65	427.44 j	427.44	2.23	4.14	8.05	7.94

### Project File:

No. Lines: 32

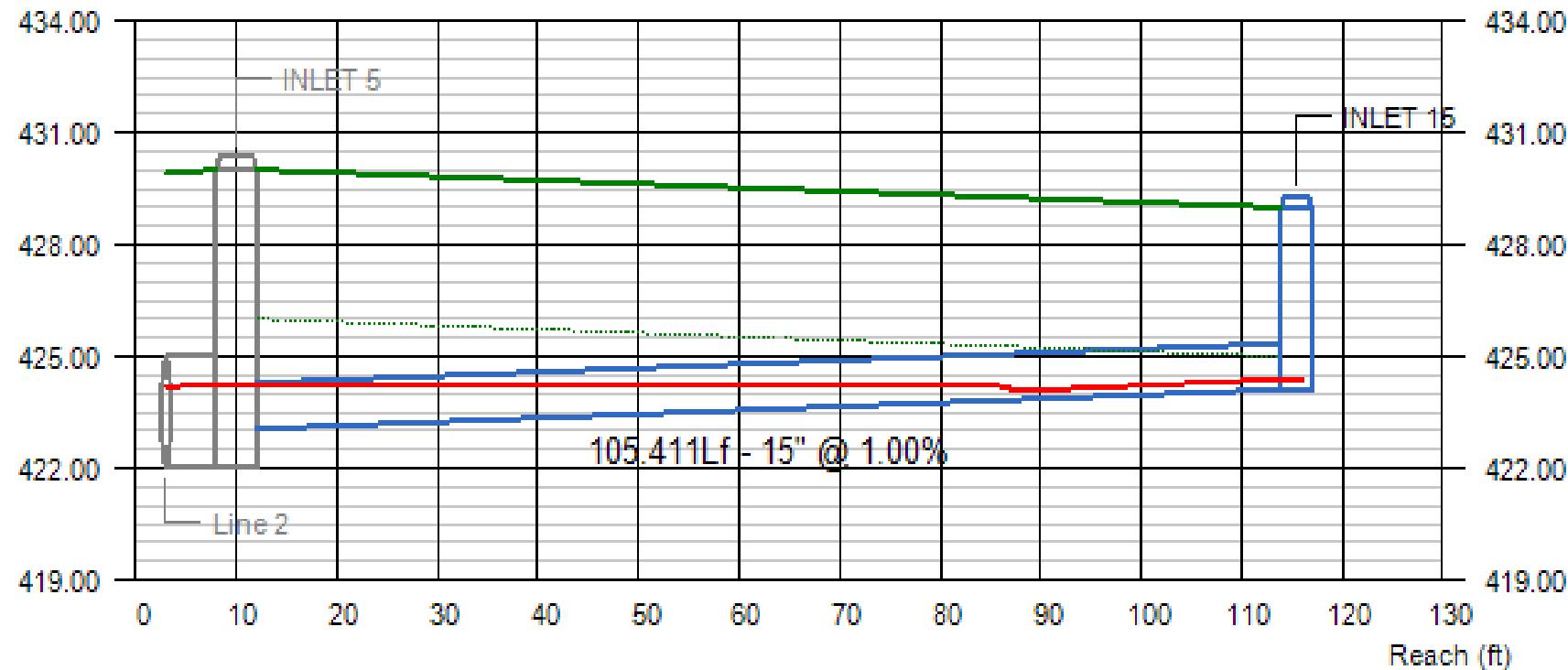
Run Date: 4/28/2022

# Line Profile (Line 28) - INLET 15 OUTLET

Page 1 of 1

Line 28 - INLET 15 OUTLET

Elev (ft)



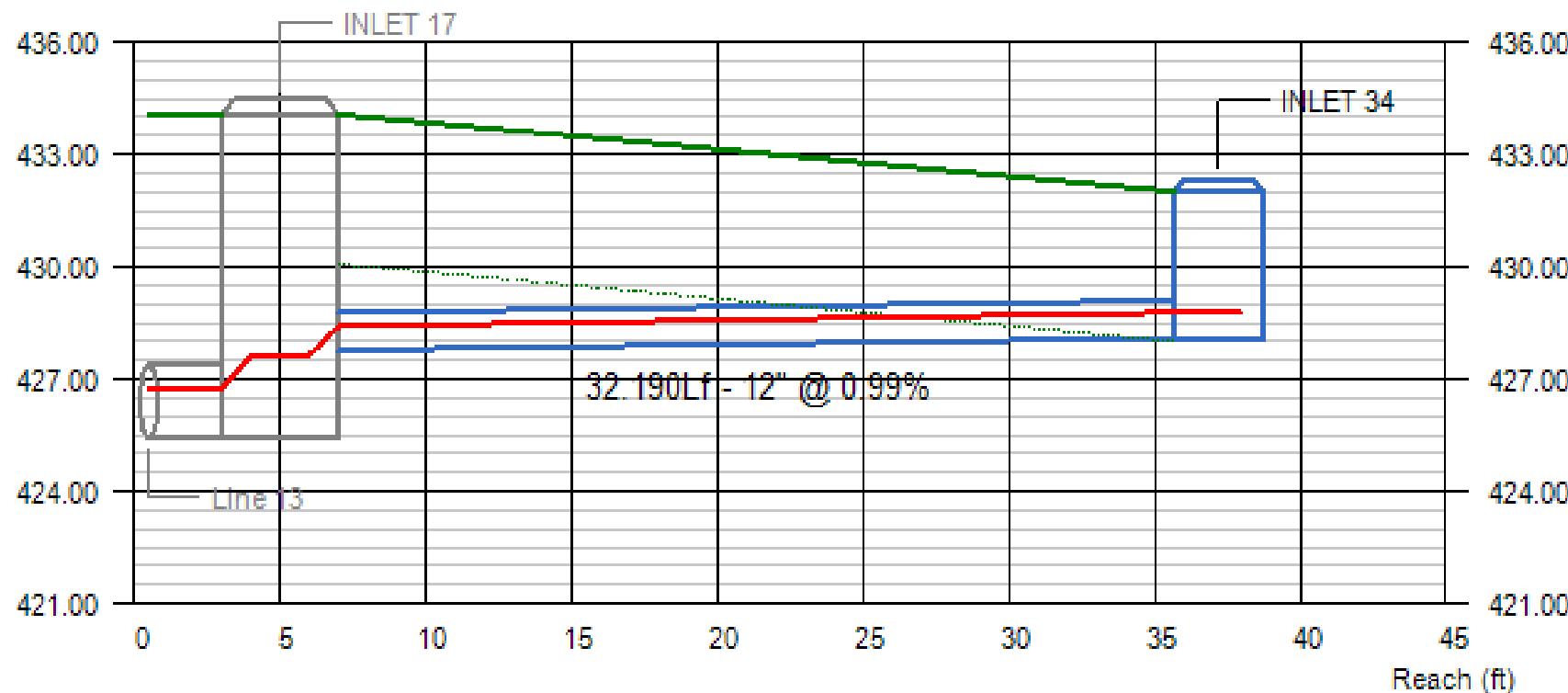
Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
28	0.58	423.05	424.10	1.17	0.30	0.30	424.22	424.40 j	424.40	0.49	2.61	5.70	3.65
Project File:								No. Lines: 32			Run Date: 4/28/2022		

# Line Profile (Line 29) - INLET 34 OUTLET

Page 1 of 1

Line 29 - INLET 34 OUTLET

Elev (ft)



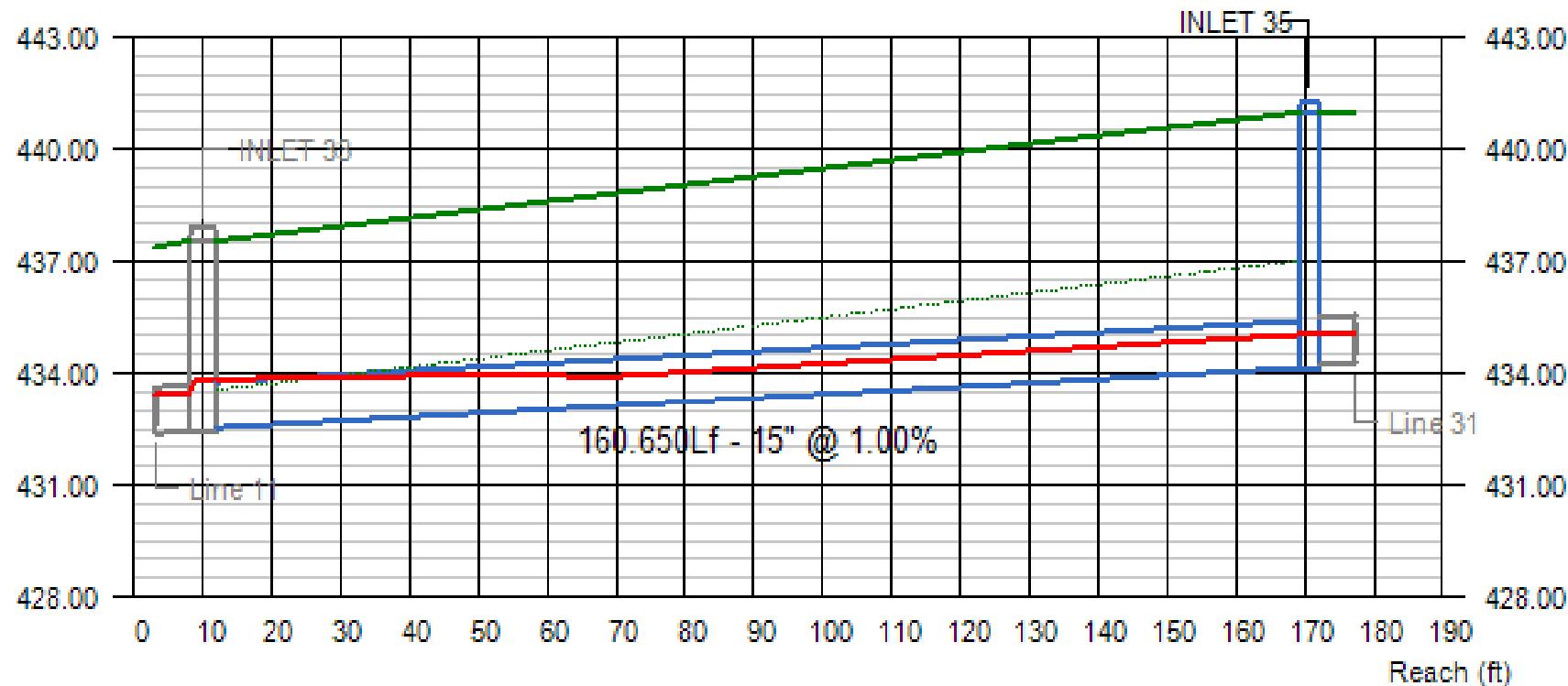
Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
29	2.55	427.77	428.09	0.63	0.68	0.68	428.40	428.77	428.77	4.92	4.46	5.30	2.91
Project File:								No. Lines: 32			Run Date: 4/28/2022		

# Line Profile (Line 30) - INLET 35 OUTLET

Page 1 of 1

Line 30 - INLET 35 OUTLET

Elev (ft)



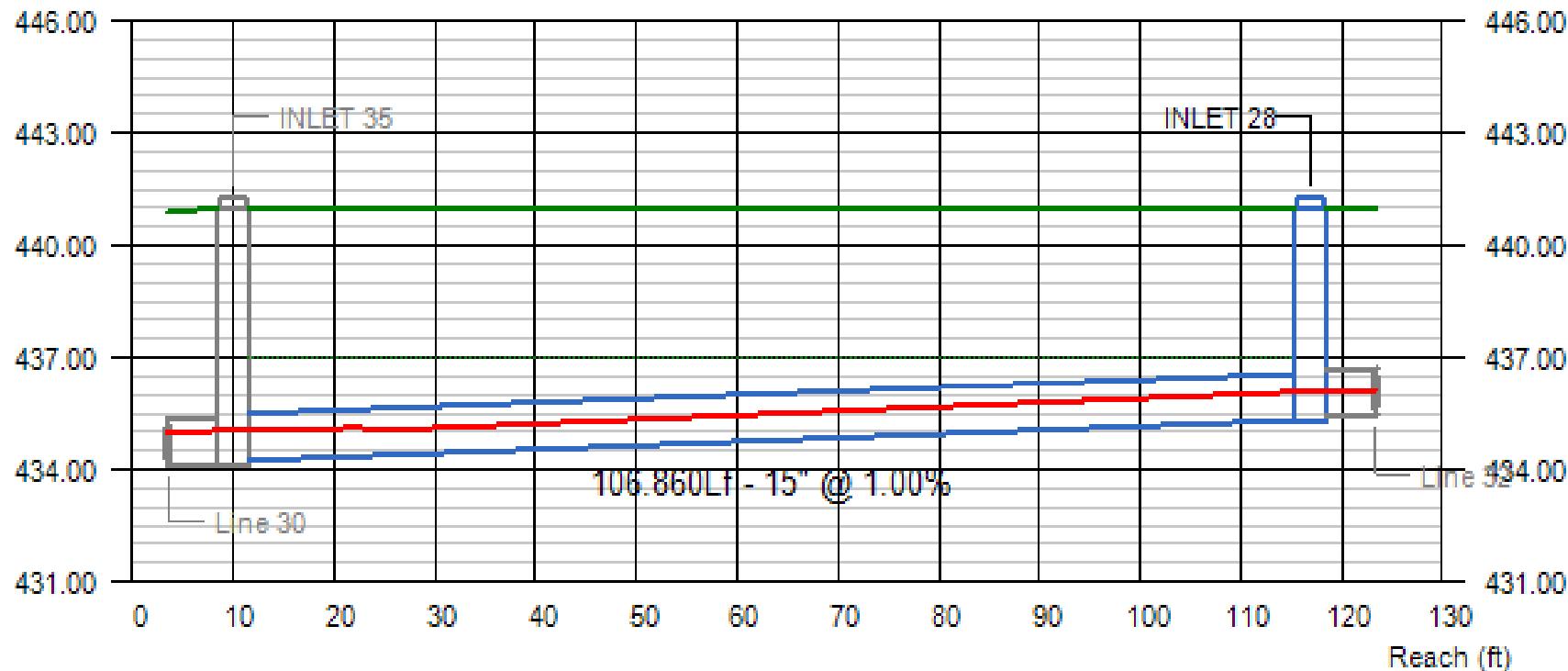
Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
30	4.85	432.53	434.14	1.25	0.89	0.89	433.84	435.03 j	435.03	3.95	5.17	3.77	5.61
Project File:								No. Lines: 32			Run Date: 4/28/2022		

# Line Profile (Line 31) - INLET 28 OUTLET

Page 1 of 1

Line 31 - INLET 28 OUTLET

Elev (ft)



Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
31	3.55	434.24	435.31	0.79	0.76	0.76	435.03	436.07 j	436.07	4.33	4.54	5.51	4.44

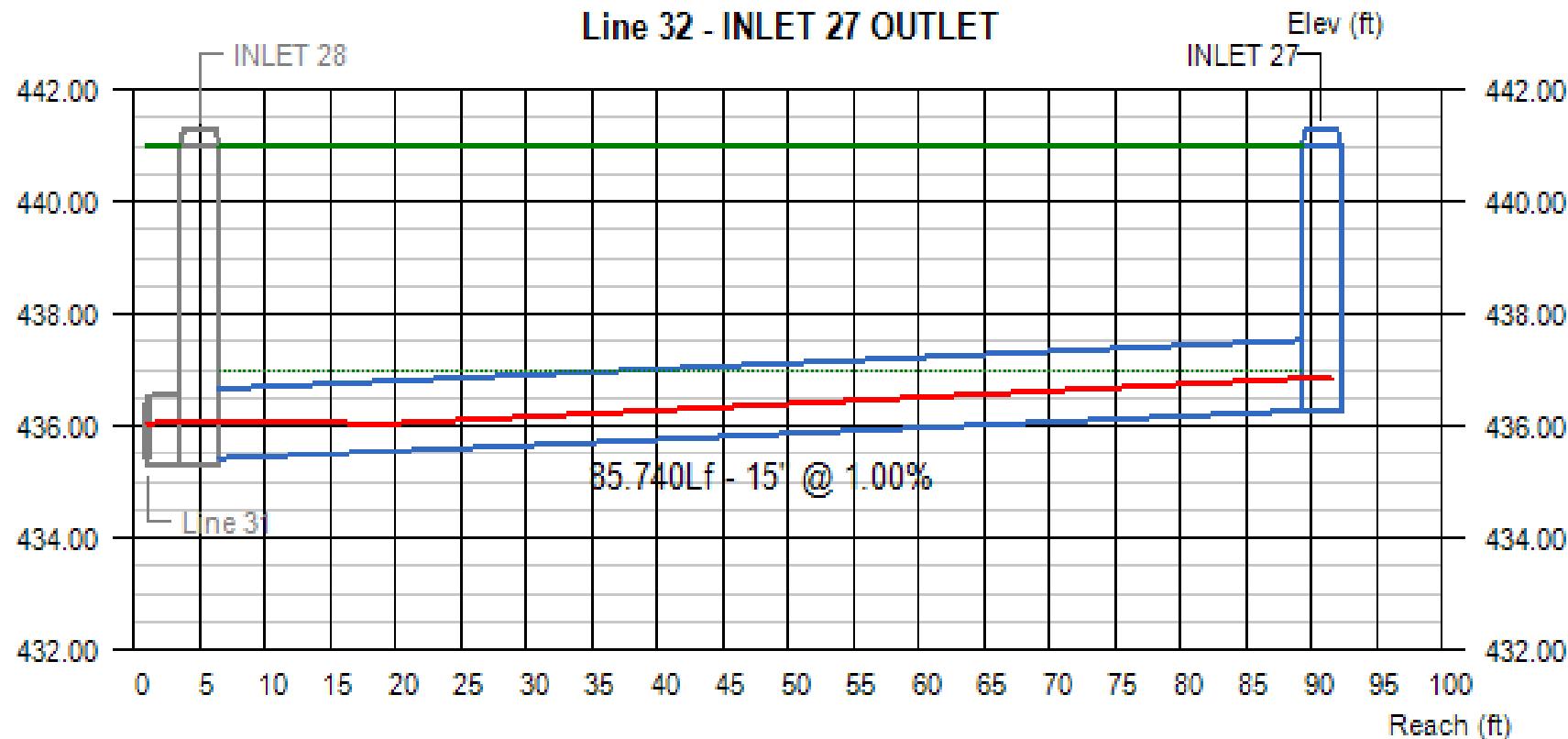
Project File:

No. Lines: 32

Run Date: 4/28/2022

# Line Profile (Line 32) - INLET 27 OUTLET

Page 1 of 1



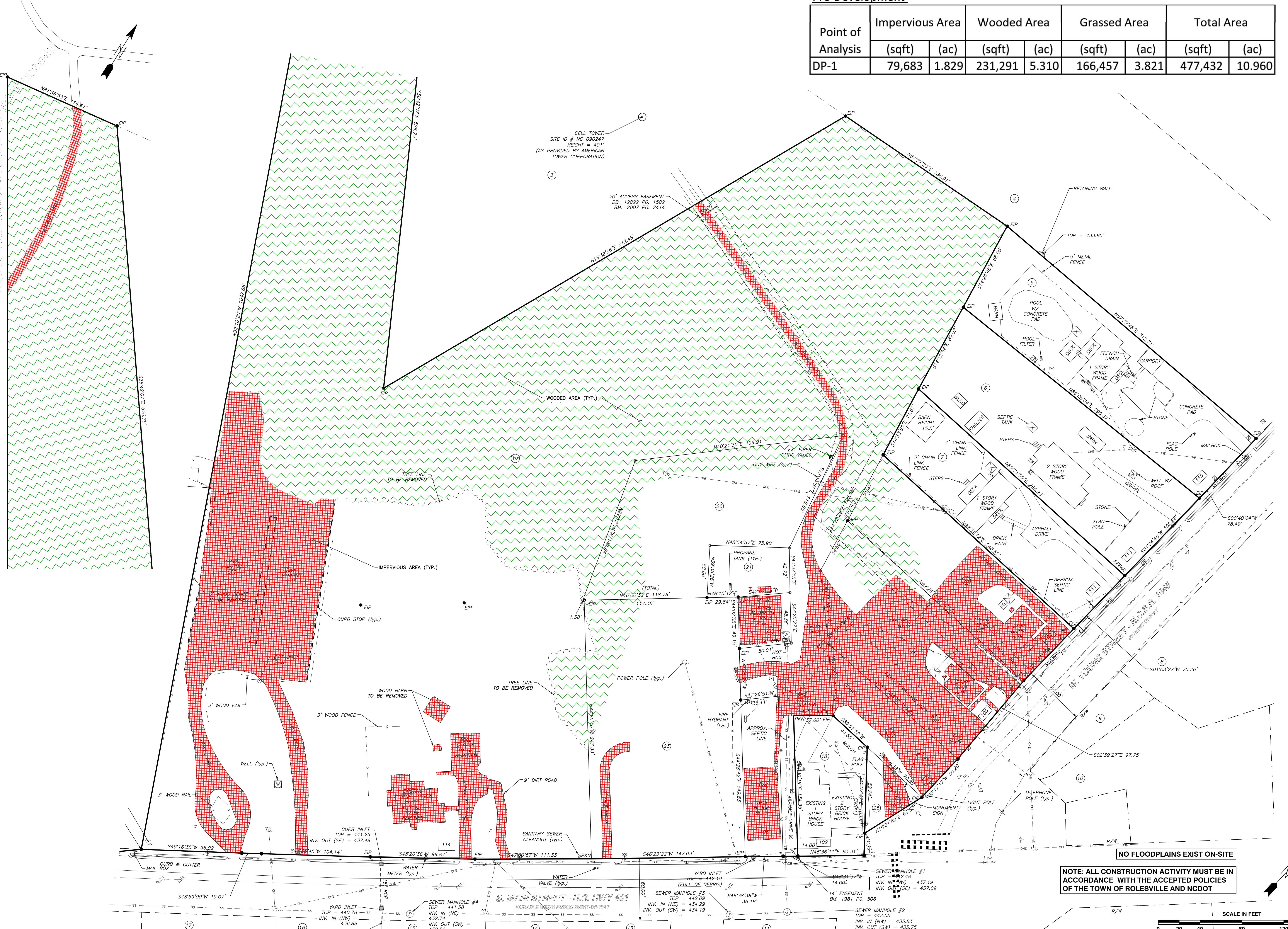
Line #	Q (cfs)	Invert Elevation		Depth of Flow			Hydraulic Grade Line			Velocity		Cover	
		Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Hw (ft)	Dn (ft)	Up (ft)	Jnct (ft)	Dn (ft/s)	Up (ft/s)	Dn (ft)	Up (ft)
32	2.07	435.41	436.27	0.66	0.57	0.57	436.07	436.84 j	436.84	3.15	3.77	4.34	3.48
Project File:								No. Lines: 32			Run Date: 4/28/2022		

# **APPENDIX**

**PRE-DEVELOPMENT DRAINAGE AREA MAP  
POST-DEVELOPMENT DRAINAGE AREA MAP  
USGS MAP  
WAKE COUNTY SOILS MAP  
FIRMETTE MAP  
NOAA RAIN DATA**

Pre-Development

Point of Analysis	Impervious Area		Wooded Area		Grassed Area		Total Area	
	(sqft)	(ac)	(sqft)	(ac)	(sqft)	(ac)	(sqft)	(ac)
DP-1	79,683	1.829	231,291	5.310	166,457	3.821	477,432	10.960

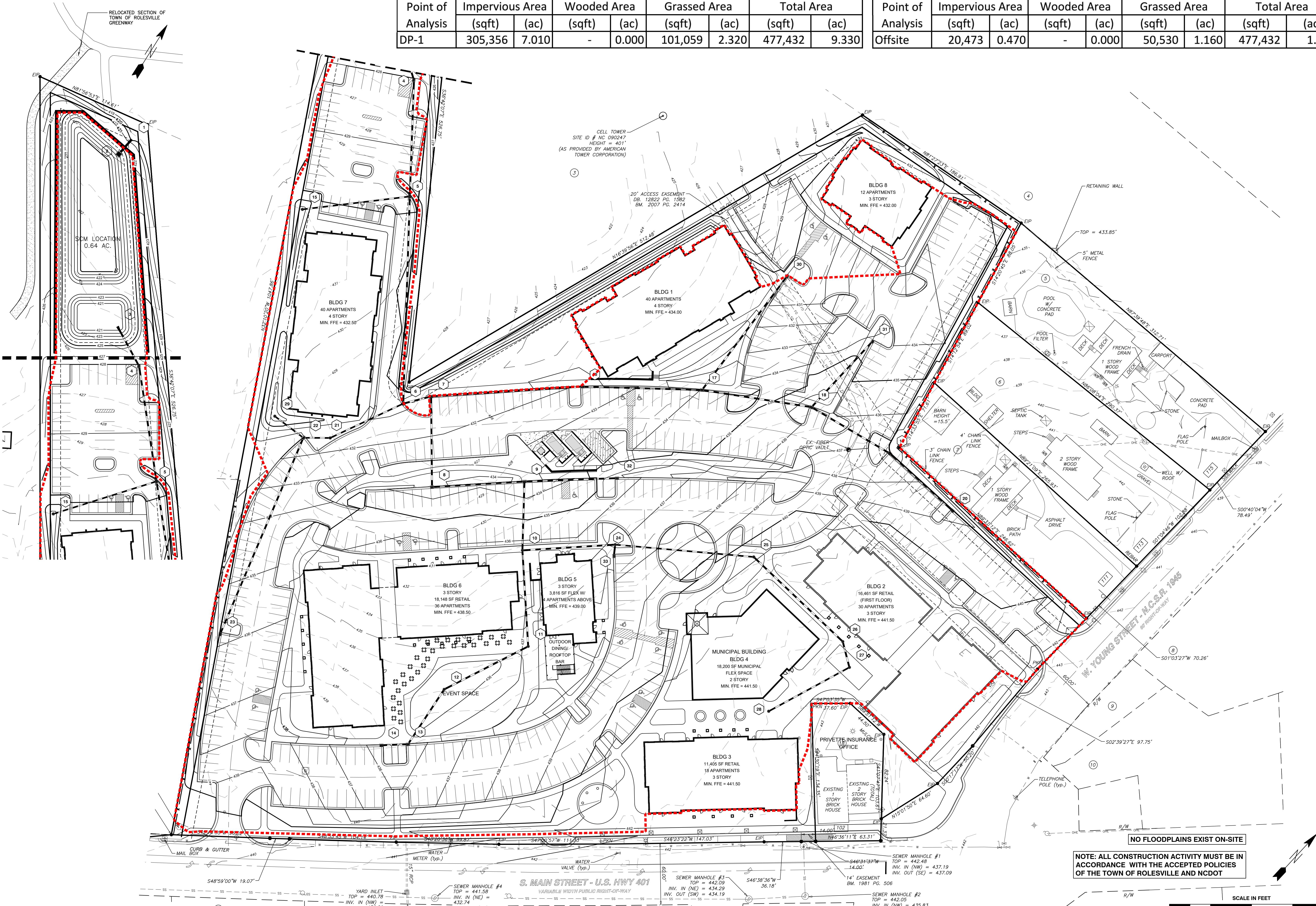


### Post-Development - to SCM

Point of Analysis	Impervious Area		Wooded Area		Grassed Area		Total Area	
	(sqft)	(ac)	(sqft)	(ac)	(sqft)	(ac)	(sqft)	(ac)
DP-1	305,356	7.010	-	0.000	101,059	2.320	477,432	9.330

### Post-Development - Bypass

Point of Analysis	Impervious Area		Wooded Area		Grassed Area		Total Area	
	(sqft)	(ac)	(sqft)	(ac)	(sqft)	(ac)	(sqft)	(ac)
Offsite	20,473	0.470	-	0.000	50,530	1.160	477,432	1.630



BASS, NIXON & KENNEDY, INC.  
CONSULTING ENGINEERS  
6310 CHAPEL HILL ROAD, SUITE 250, RALEIGH, NC 27607  
TELEPHONE: (919)851-4422 FAX: (919)851-3988  
CERTIFICATION NUMBERS: NCBELS (C-0110); NCBELA (C-0267)

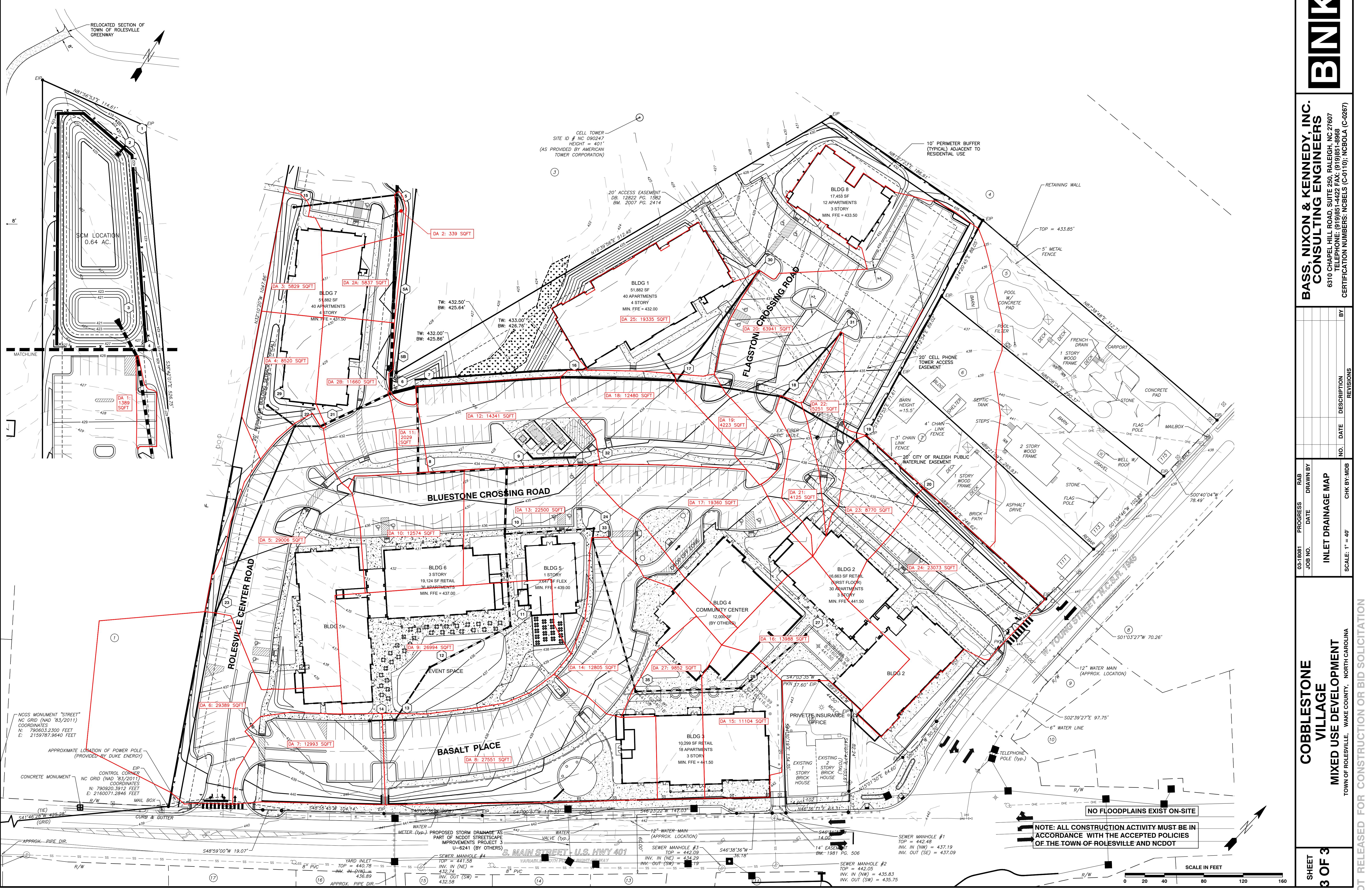
**BNK**

NO.	DATE	DESCRIPTION	REVISIONS
03-18081	03-18081	PROGRESS DRAWN BY POST-DEVELOPMENT DRAINAGE MAP	BY CHK BY: MBD SCALE: 1" = 40'

**COBBLESTONE VILLAGE**  
**MIXED USE DEVELOPMENT**  
TOWN OF ROLESVILLE, WAKE COUNTY, NORTH CAROLINA

NOT RELEASED FOR CONSTRUCTION OR BID SOLICITATION

SHEET  
2 OF 3



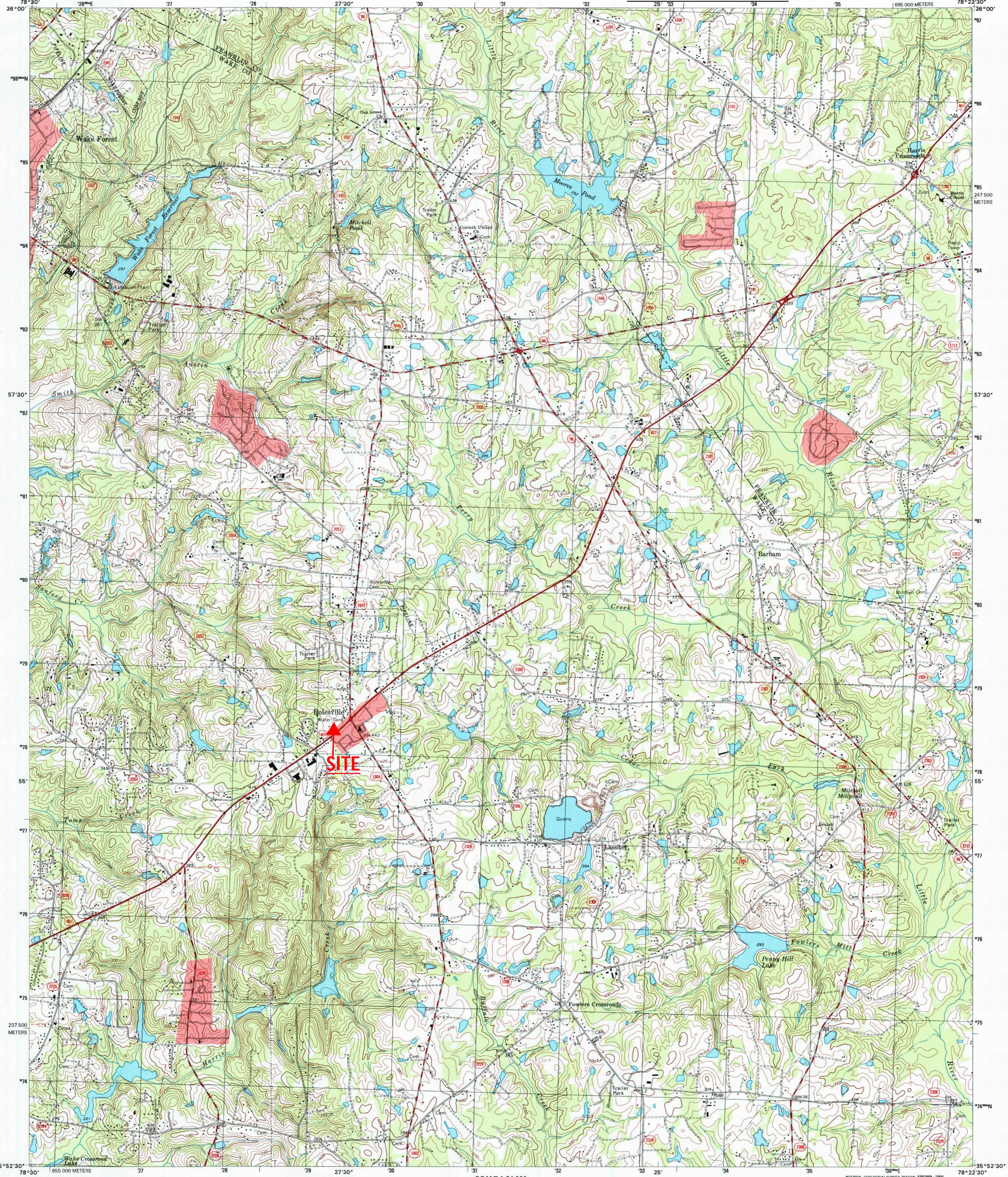


U.S. DEPARTMENT OF THE INTERIOR  
U.S. GEOLOGICAL SURVEY

STATE OF NORTH CAROLINA  
DEPARTMENT OF ENVIRONMENT AND NATURAL RESOURCES  
DIVISION OF LAND RESOURCES  
NORTH CAROLINA GEOLOGICAL SURVEY

# ROLESVILLE, NC COBBLESTONE VILLAGE

ROLESVILLE QUADRANGLE  
NORTH CAROLINA  
7.5-MINUTE SERIES (TOPOGRAPHIC)



Produced by the United States Geological Survey  
in cooperation with the North Carolina Department of Environment and Natural Resources

Topography compiled 1964. Planimetry derived from imagery taken 1993 and other sources. Survey control current as of 1967  
North American Datum of 1983 (NAD 83). Projection and 1:24,000 scale. Contour interval 10 feet. Dashed lines indicate 2500-meter ticks; North Carolina Coordinate System of 1983  
North American Datum of 1927 (NAD 27) is shown by dashed corner ticks. The values of the shift between NAD 83 and NAD 27 for 7.5-minute intersections are obtainable from National Geodetic Survey NADCON software  
Landmark buildings verified 1967

RECEIVED  
JUN 30 1999  
USGS NMD  
HISTORICAL MAP ARCHIVES

SCALE 1:24 000  
KILOMETERS  
METERS  
FEET  
CONTOUR INTERVAL 10 FEET  
NATIONAL GEODETIC VERTICAL DATUM OF 1929  
TO CONVERT FROM FEET TO METERS, MULTIPLY BY 0.3048

THIS MAP COMPLIES WITH NATIONAL MAP ACCURACY STANDARDS  
FOR SALE BY U.S. GEOLOGICAL SURVEY, P.O. BOX 25286, DENVER, COLORADO 80225  
A FOLDER DESCRIBING TOPOGRAPHIC MAPS AND SYMBOLS IS AVAILABLE UPON REQUEST

1	2	3
4	5	6
6	7	8

ADJOINING 7.5' QUADRANGLE NAMES

Primary highway  
Light-duty road, hard or improved surface  
Secondary highway  
Unimproved road  
Interstate Route  
U.S. Route  
State Route



ROLESVILLE, NC  
1993

NIMA 5355 IV NW-SERIES V842

# COBBLESTONE VILLAGE - ROLESVILLE, NC

22

N

1 Mile  
5000 Feet

(Joins sheet 21)

Scale 1:15840

(Joins sheet 23)



(Joins sheet 31)

LwB2 WmB2 Me

ApC2 ApB2

ApB2

Cm

Me

WKE

WKE

WKE

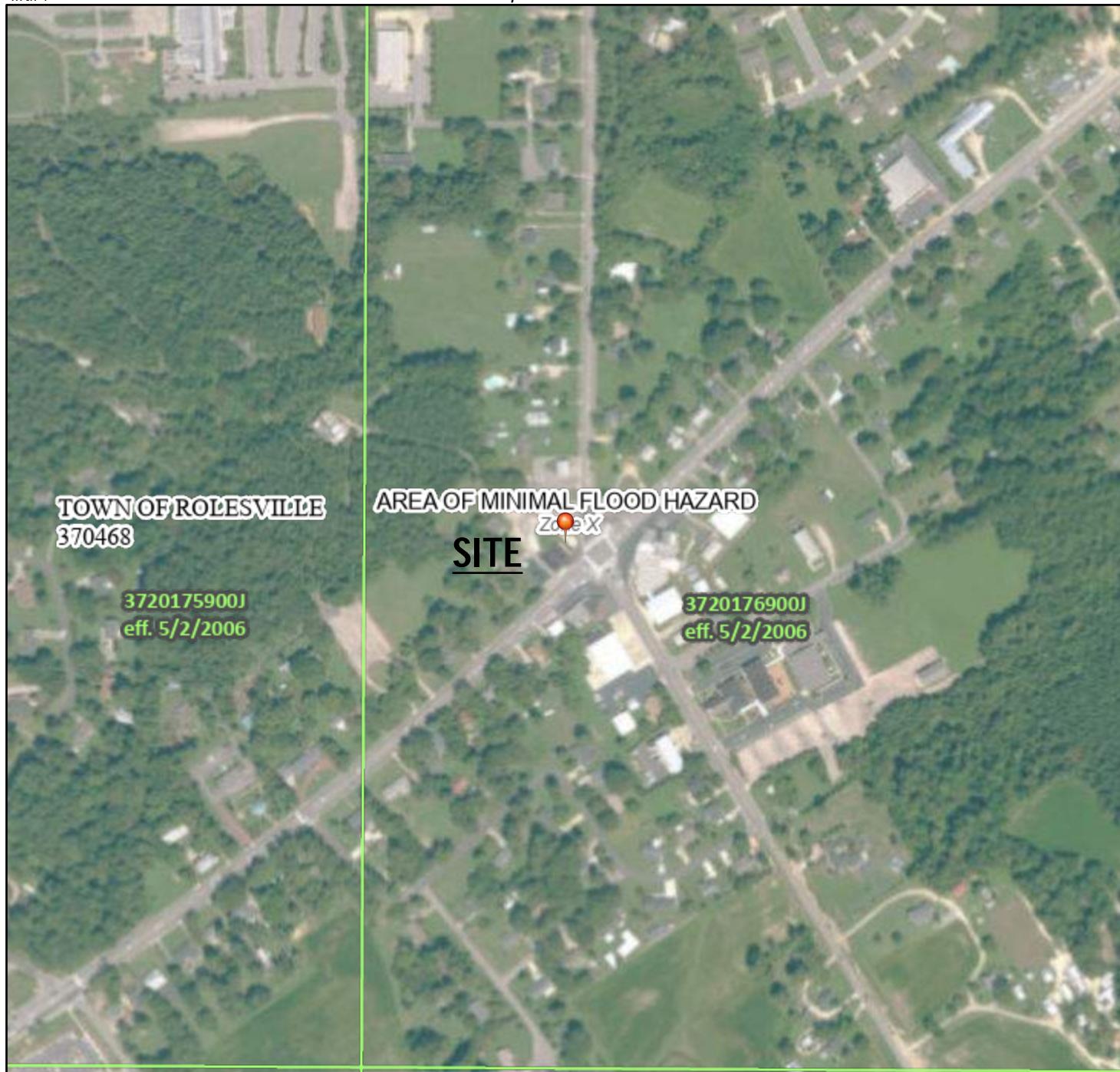
WKE

DWL RQD O RRG-DJUGDHU )5WWH

ROLESVILLE, NC - COBBLESTONE VILLAGE



FEMA



HJOG

6577 6578 6579 6580 6581

6582  
6583

26562  
2655

2656

6525  
6526

26  
2655

6536

6537

00001

%DWLRQD O S 2WKRQH DWDUHUMHG%REHU

LWKW %DWHRG OHDWLRQ %  
=RQH 9 \$  
LWK%RUHWK =RQH \$ 2-9 \$  
SHODWRU)ORRG

\$DOD &OFRHORRG-DJUG \$JHD/  
R DQDOD RAOFHORRG ZWKDHUDH  
GHWKHVWDQFHRRW RU ZWKGDUD  
DUHD/R OHW WKQRQHVXDUHPOHH;  
XWUH&QBLWLQV \$DOD  
&OFRHORRG-DJUG =RQH;  
\$JHDZWK\$GPHC)ORFG\$VNGHWR  
MMH GH RVHV =RQH;  
\$JHDZWK)ORFG\$VNGHWRMMH =RQH'

\$JHD R DQLOD)ORRG-DJUG =RQH;  
II-FWL YH  
\$JHD R &QHWHUPQH)ORRG-DJUG =RQH'  
----- &QHQH &OYHUW RU &WRURH  
MMH LNH RU DQRGZO

----- &JRW &FWLRQ/ZWK\$DOD &OFRH  
D/HU &UDFH OHDWLRQ  
----- &RDWDO 7DQJHW  
-----%DH)ORRG OHDWLRQ %  
LPW R WVG  
XULVGLFWLRQ%RQGDU  
----- &RDWDO 7DQJHW %DQHOLQH  
--- URLOH%DQHOLQH  
----- URLDBLF)DUXH

LLWDO DWD\$DLODEOH  
RLLWDO DWD\$DLODEOH  
SOPSHG

7KHSQGLVSDHGRQWIKBSLVDDQSRULBWH  
SLQWVHOHWGEBWHXHU DDGRWVCRWUHJUH  
DQDWKULWDLWLYHJSURSHUWORFDWLQH

7KVBFRBOLH/ZWKDVWDDQJUG/IRU WKH XHR  
GLWDOIORRGDB/LI LW LV CRW YRLGD/GHWULEGHEORZ  
7KEDHBSVRZFRBOLH/ZWKDVWDDQJUG/IRU WKH XHR  
DFXUDRWDQDQJUG/

7KIORGKODJGLQJRWBLRQLVGHULYHGGLUHWOIURWIKH  
DWKULWDLWLYH%ZEVHULRV SURYLGHGE 7KVB  
DWSRUWHGRQ DW 7KIORGKODJGLQJRWBLRQLVGHULYHGGLUHWOIURWIKH  
UHOHWFDQH/RU DQGDPDWVWVHDXQWWRWKVCDWHDOG  
WLA 7KIDQGHIFWLQHLQRWBVLRQBRQOQH  
EHRPVAUWCHGEQZQDWDRUWLPJ

7KVBFRBOLVYRLGLIWKHFRHJUHRWHRHORZQPS  
HOHQWVCRQVDSHJDUEWBSLPHJUORRGHQDHOHV  
OHQHGVDQHEDUWFSUHDMLRQGDWHRQFLWLGQWLHUV  
)SODQH QAUH DQG )SHIFWLHYGDWHDLSLBH/IRU  
XQBSGCDQGXRQHULQHGDJHD/DOQGRVHXM-GIRU  
UHODWRSUSRMV



**NOAA Atlas 14, Volume 2, Version 3**  
**Location name: Rolesville, North Carolina, USA\***  
**Latitude: 35.9233°, Longitude: -78.4579°**  
**Elevation: 444.08 ft\*\***  
\* source: ESRI Maps  
\*\* source: USGS



## POINT PRECIPITATION FREQUENCY ESTIMATES

G.M. Bonnin, D. Martin, B. Lin, T. Parzybok, M. Yekta, and D. Riley

NOAA, National Weather Service, Silver Spring, Maryland

[PF tabular](#) | [PF graphical](#) | [Maps & aerials](#)

### PF tabular

Duration	Average recurrence interval (years)									
	1	2	5	10	25	50	100	200	500	1000
5-min	<b>4.84</b> (4.43-5.29)	<b>5.62</b> (5.15-6.13)	<b>6.41</b> (5.87-6.98)	<b>7.19</b> (6.58-7.85)	<b>7.98</b> (7.27-8.70)	<b>8.60</b> (7.81-9.38)	<b>9.17</b> (8.26-9.98)	<b>9.66</b> (8.65-10.5)	<b>10.2</b> (9.07-11.1)	<b>10.7</b> (9.43-11.7)
10-min	<b>3.86</b> (3.54-4.22)	<b>4.49</b> (4.12-4.91)	<b>5.13</b> (4.70-5.60)	<b>5.75</b> (5.26-6.27)	<b>6.36</b> (5.79-6.93)	<b>6.85</b> (6.22-7.47)	<b>7.28</b> (6.56-7.93)	<b>7.66</b> (6.86-8.35)	<b>8.08</b> (7.18-8.82)	<b>8.42</b> (7.42-9.22)
15-min	<b>3.22</b> (2.95-3.52)	<b>3.77</b> (3.45-4.11)	<b>4.32</b> (3.96-4.72)	<b>4.85</b> (4.44-5.29)	<b>5.38</b> (4.89-5.86)	<b>5.78</b> (5.25-6.30)	<b>6.14</b> (5.53-6.68)	<b>6.44</b> (5.77-7.03)	<b>6.78</b> (6.02-7.40)	<b>7.05</b> (6.21-7.71)
30-min	<b>2.21</b> (2.02-2.41)	<b>2.60</b> (2.38-2.84)	<b>3.07</b> (2.82-3.35)	<b>3.51</b> (3.21-3.83)	<b>3.98</b> (3.62-4.34)	<b>4.36</b> (3.95-4.75)	<b>4.70</b> (4.24-5.12)	<b>5.01</b> (4.49-5.47)	<b>5.39</b> (4.79-5.89)	<b>5.71</b> (5.03-6.25)
60-min	<b>1.38</b> (1.26-1.51)	<b>1.63</b> (1.50-1.78)	<b>1.97</b> (1.81-2.15)	<b>2.29</b> (2.09-2.50)	<b>2.65</b> (2.41-2.89)	<b>2.95</b> (2.68-3.22)	<b>3.24</b> (2.92-3.53)	<b>3.52</b> (3.15-3.84)	<b>3.87</b> (3.44-4.22)	<b>4.17</b> (3.67-4.56)
2-hr	<b>0.804</b> (0.732-0.887)	<b>0.957</b> (0.874-1.05)	<b>1.17</b> (1.06-1.28)	<b>1.37</b> (1.25-1.50)	<b>1.61</b> (1.45-1.76)	<b>1.83</b> (1.64-1.99)	<b>2.03</b> (1.81-2.22)	<b>2.24</b> (1.98-2.44)	<b>2.51</b> (2.20-2.74)	<b>2.74</b> (2.39-3.01)
3-hr	<b>0.568</b> (0.516-0.629)	<b>0.676</b> (0.617-0.746)	<b>0.828</b> (0.754-0.913)	<b>0.979</b> (0.888-1.08)	<b>1.16</b> (1.05-1.28)	<b>1.33</b> (1.19-1.46)	<b>1.49</b> (1.32-1.63)	<b>1.66</b> (1.46-1.82)	<b>1.89</b> (1.65-2.07)	<b>2.09</b> (1.81-2.30)
6-hr	<b>0.342</b> (0.312-0.378)	<b>0.407</b> (0.372-0.448)	<b>0.499</b> (0.455-0.548)	<b>0.591</b> (0.537-0.648)	<b>0.704</b> (0.637-0.771)	<b>0.807</b> (0.724-0.882)	<b>0.910</b> (0.810-0.993)	<b>1.02</b> (0.897-1.11)	<b>1.17</b> (1.01-1.27)	<b>1.30</b> (1.12-1.42)
12-hr	<b>0.200</b> (0.183-0.221)	<b>0.239</b> (0.219-0.262)	<b>0.294</b> (0.269-0.322)	<b>0.350</b> (0.319-0.383)	<b>0.420</b> (0.381-0.459)	<b>0.485</b> (0.436-0.527)	<b>0.550</b> (0.489-0.597)	<b>0.620</b> (0.546-0.673)	<b>0.716</b> (0.621-0.778)	<b>0.806</b> (0.688-0.876)
24-hr	<b>0.119</b> (0.111-0.128)	<b>0.144</b> (0.134-0.155)	<b>0.181</b> (0.168-0.195)	<b>0.210</b> (0.195-0.226)	<b>0.250</b> (0.231-0.269)	<b>0.282</b> (0.260-0.303)	<b>0.314</b> (0.289-0.338)	<b>0.348</b> (0.319-0.375)	<b>0.395</b> (0.360-0.426)	<b>0.432</b> (0.392-0.466)
2-day	<b>0.069</b> (0.064-0.074)	<b>0.083</b> (0.078-0.090)	<b>0.104</b> (0.097-0.112)	<b>0.120</b> (0.111-0.129)	<b>0.142</b> (0.131-0.153)	<b>0.159</b> (0.147-0.171)	<b>0.177</b> (0.163-0.191)	<b>0.196</b> (0.179-0.211)	<b>0.221</b> (0.201-0.239)	<b>0.241</b> (0.219-0.261)
3-day	<b>0.049</b> (0.046-0.052)	<b>0.059</b> (0.055-0.063)	<b>0.073</b> (0.068-0.078)	<b>0.084</b> (0.078-0.090)	<b>0.099</b> (0.092-0.106)	<b>0.111</b> (0.103-0.119)	<b>0.124</b> (0.114-0.133)	<b>0.136</b> (0.125-0.147)	<b>0.154</b> (0.141-0.166)	<b>0.168</b> (0.153-0.181)
4-day	<b>0.039</b> (0.036-0.041)	<b>0.046</b> (0.043-0.050)	<b>0.057</b> (0.054-0.061)	<b>0.066</b> (0.062-0.071)	<b>0.078</b> (0.072-0.083)	<b>0.087</b> (0.081-0.093)	<b>0.097</b> (0.089-0.104)	<b>0.107</b> (0.098-0.115)	<b>0.121</b> (0.110-0.129)	<b>0.131</b> (0.120-0.141)
7-day	<b>0.026</b> (0.024-0.027)	<b>0.031</b> (0.029-0.033)	<b>0.037</b> (0.035-0.040)	<b>0.043</b> (0.040-0.046)	<b>0.050</b> (0.047-0.053)	<b>0.056</b> (0.052-0.060)	<b>0.062</b> (0.057-0.066)	<b>0.068</b> (0.063-0.073)	<b>0.076</b> (0.070-0.082)	<b>0.083</b> (0.076-0.089)
10-day	<b>0.020</b> (0.019-0.022)	<b>0.024</b> (0.023-0.026)	<b>0.029</b> (0.027-0.031)	<b>0.033</b> (0.031-0.035)	<b>0.038</b> (0.036-0.041)	<b>0.043</b> (0.040-0.045)	<b>0.047</b> (0.043-0.050)	<b>0.051</b> (0.047-0.055)	<b>0.057</b> (0.052-0.061)	<b>0.061</b> (0.056-0.066)
20-day	<b>0.014</b> (0.013-0.015)	<b>0.016</b> (0.015-0.017)	<b>0.019</b> (0.018-0.020)	<b>0.022</b> (0.020-0.023)	<b>0.025</b> (0.023-0.026)	<b>0.027</b> (0.025-0.029)	<b>0.030</b> (0.028-0.032)	<b>0.032</b> (0.030-0.034)	<b>0.036</b> (0.033-0.038)	<b>0.039</b> (0.035-0.041)
30-day	<b>0.011</b> (0.011-0.012)	<b>0.013</b> (0.013-0.014)	<b>0.016</b> (0.015-0.017)	<b>0.017</b> (0.016-0.018)	<b>0.020</b> (0.018-0.021)	<b>0.021</b> (0.020-0.023)	<b>0.023</b> (0.021-0.024)	<b>0.025</b> (0.023-0.026)	<b>0.027</b> (0.025-0.029)	<b>0.029</b> (0.027-0.031)
45-day	<b>0.010</b> (0.009-0.010)	<b>0.011</b> (0.011-0.012)	<b>0.013</b> (0.012-0.014)	<b>0.014</b> (0.013-0.015)	<b>0.016</b> (0.015-0.017)	<b>0.017</b> (0.016-0.018)	<b>0.018</b> (0.017-0.019)	<b>0.020</b> (0.018-0.021)	<b>0.021</b> (0.020-0.022)	<b>0.022</b> (0.021-0.024)
60-day	<b>0.009</b> (0.008-0.009)	<b>0.010</b> (0.010-0.011)	<b>0.011</b> (0.011-0.012)	<b>0.013</b> (0.012-0.013)	<b>0.014</b> (0.013-0.015)	<b>0.015</b> (0.014-0.016)	<b>0.016</b> (0.015-0.017)	<b>0.017</b> (0.016-0.018)	<b>0.018</b> (0.017-0.019)	<b>0.019</b> (0.018-0.020)

<sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

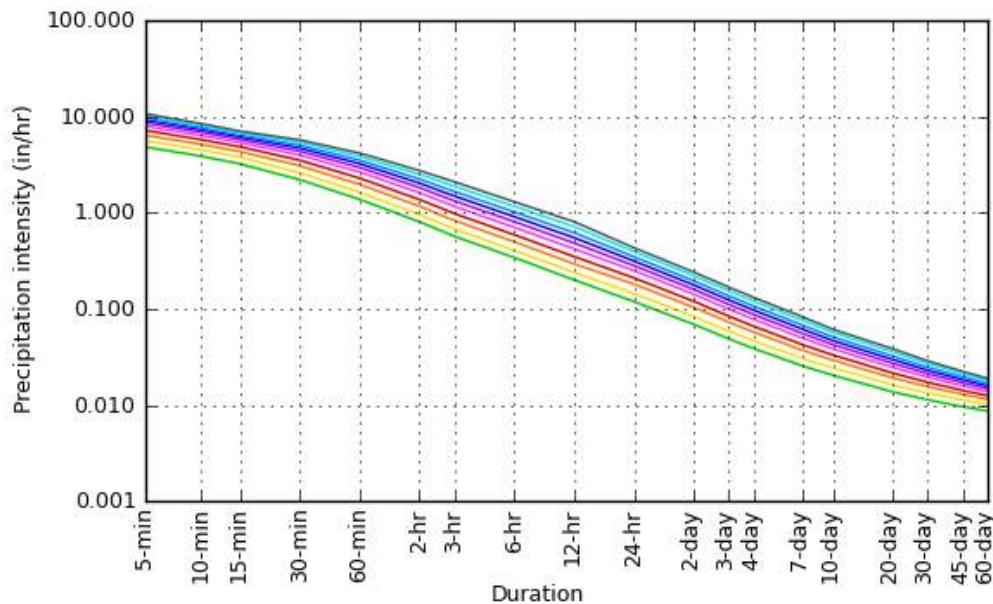
Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

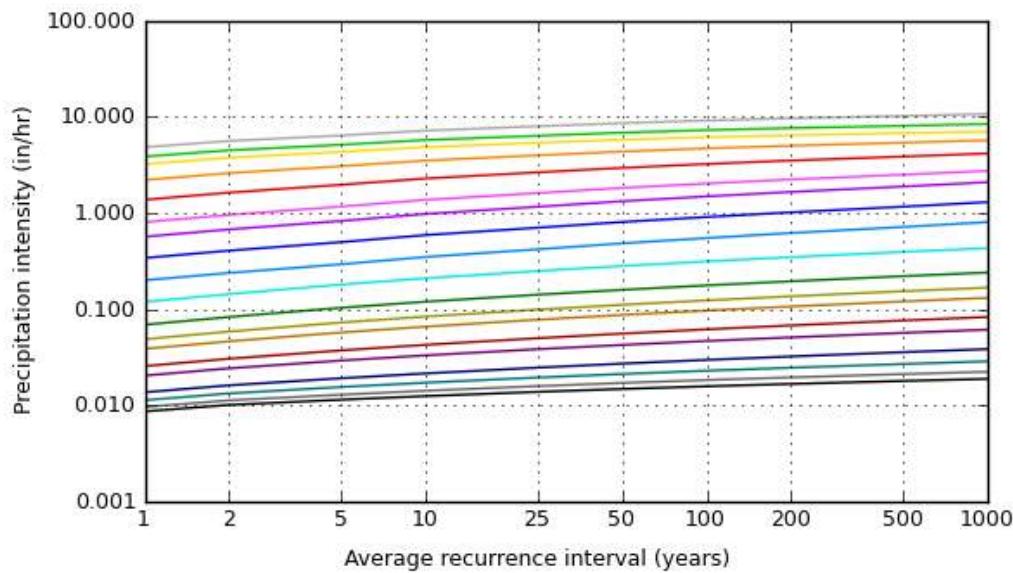
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### PF graphical

PDS-based intensity-duration-frequency (IDF) curves  
Latitude: 35.9233°, Longitude: -78.4579°



Average recurrence interval (years)
1
2
5
10
25
50
100
200
500
1000



Duration
5-min
10-min
15-min
30-min
60-min
2-hr
3-hr
6-hr
12-hr
24-hr
2-day
3-day
4-day
7-day
10-day
20-day
30-day
45-day
60-day

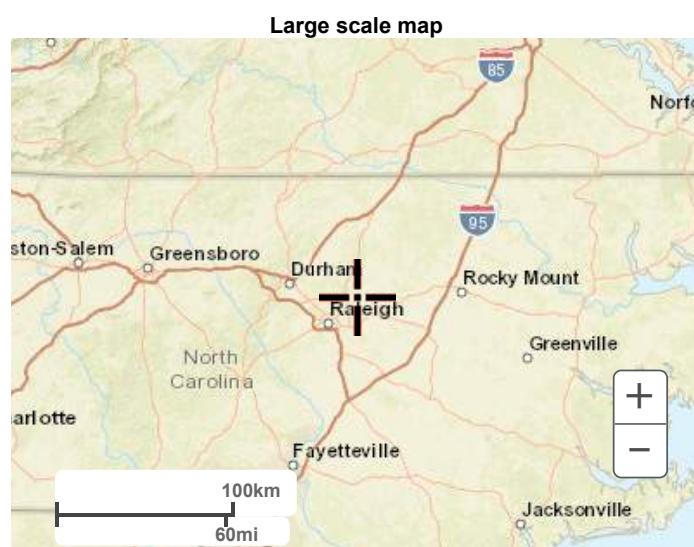
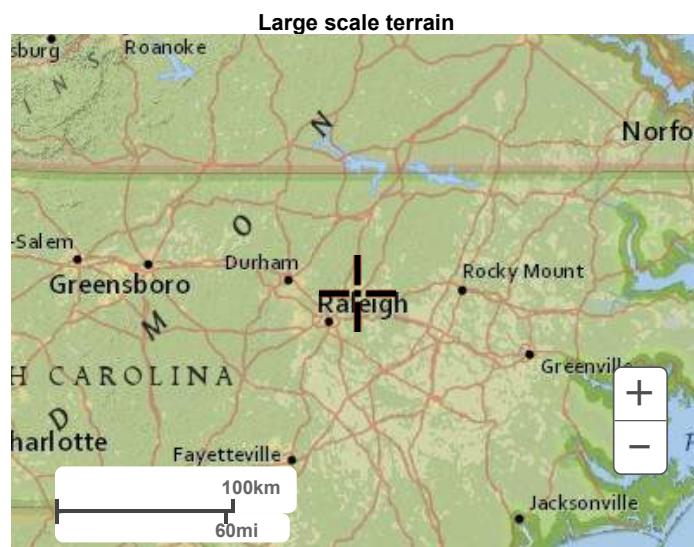
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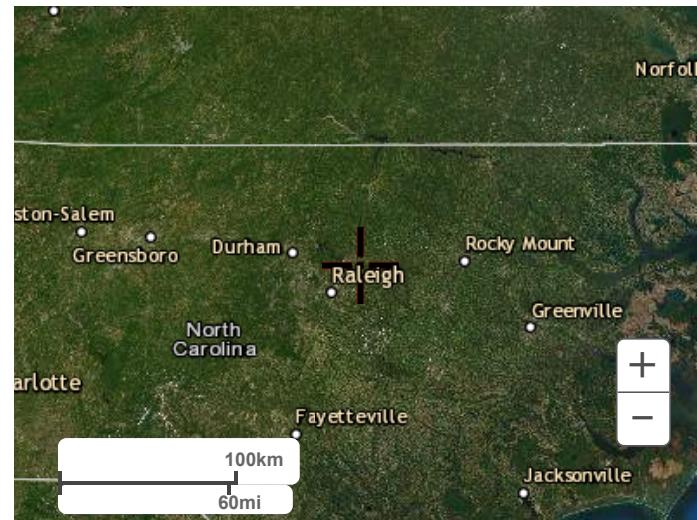
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## Maps & aerials

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Large scale aerial



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